

**REGIONE
PUGLIA**



CUP: E75G19000040005

**PIANO DEGLI INTERVENTI AIP 2020-2023 DI CUI ALLA DELIBERA N.6 DEL 22/02/2021
CON COPERTURA FINANZIARIA " FONDI DERIVANTI DA PROVENTI TARIFFARI"**

**PROGETTO DEFINITIVO
POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E DEL RECAPITO FINALE
A SERVIZIO DELL'AGGLOMERATO DEL COMUNE DI SQUINZANO (LE)**

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Direzione Ingegneria**

**Il Responsabile del Procedimento
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**Il Direttore
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PROGETTAZIONE

**Il Progettista
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Elaborato

R.37.12

**TABULATI DI CALCOLO STRUTTURALE
-EDIFICIO GRIGLIATURA FINE-**

Codice Intervento P1370

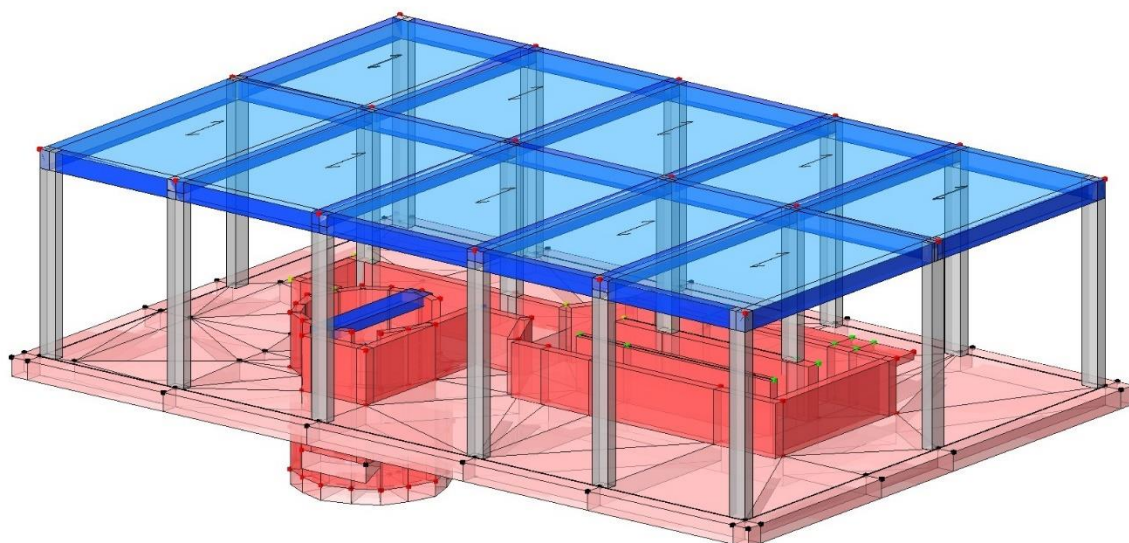
**Codice SAP
210000023391**

**Prot. N. 27346
Data 23/04/2021**

Scala:

00	MAG.2021	Emesso per Progetto DEFINITIVO			
N. Rev.	Data	Descrizione	Disegnato	Controllato	Approvato





Vita nominale, classi d'uso e periodo di riferimento

La costruzione in oggetto è definita dalla seguente tipologia (p.to 2.4 delle NT):

Vita della struttura	
Tipo	Opere infr. imp. normale (50-100)
Vita nominale VN [anni]	50.0
Classe d'uso	III
Coefficiente d'uso CU	1.500
Periodo di riferimento VR [anni]	75.000
Probabilità di superamento PVR allo Stato limite di esercizio - SLD	63.0%
Probabilità di superamento PVR allo Stato limite ultimo - SLV	10.0%
Periodo di ritorno TR SLD [anni]	75.4
Periodo di ritorno TR SLV [anni]	711.8

Per maggiori dettagli riguardo l'azione sismica si veda la definizione degli spettri di risposta

Materiali impiegati e resistenze di calcolo

Per la realizzazione dell'opera in oggetto saranno impiegati i seguenti materiali, di cui si riportano nell'ordine le proprietà meccaniche adottate nel calcolo elastico e le resistenze di calcolo per le verifiche di sicurezza:

Materiali		
C35/45		
Peso specifico	kg/mc	2500
Modulo di Young E	kg/cmq	3E05
Modulo di Poisson v		0.13
Coefficiente di dilatazione termica λ	1/°C	1e-05

Caratteristiche dei materiali delle parti in calcestruzzo armato		
Classe calcestruzzo		Classe C35/45
Resistenza cubica Rck	kg/cmq	450
Resistenza di calcolo fcd	kg/cmq	212
Resistenza a trazione di calcolo fctd	kg/cmq	16
Resistenza cilindrica fck	kg/cmq	374
Resistenza a trazione media fctm	kg/cmq	34

Classe acciaio barre longitudinali		Acciaio barre B450C
Resistenza allo snervamento f_{yk}	kg/cm ²	≥ 4500
Resistenza alla rottura barre f_{tk}	kg/cm ²	≥ 5400
Classe acciaio staffe		Acciaio barre B450C
Resistenza allo snervamento f_{yk}	kg/cm ²	≥ 4500
Resistenza alla rottura barre f_{tk}	kg/cm ²	≥ 5400

Spettri di risposta

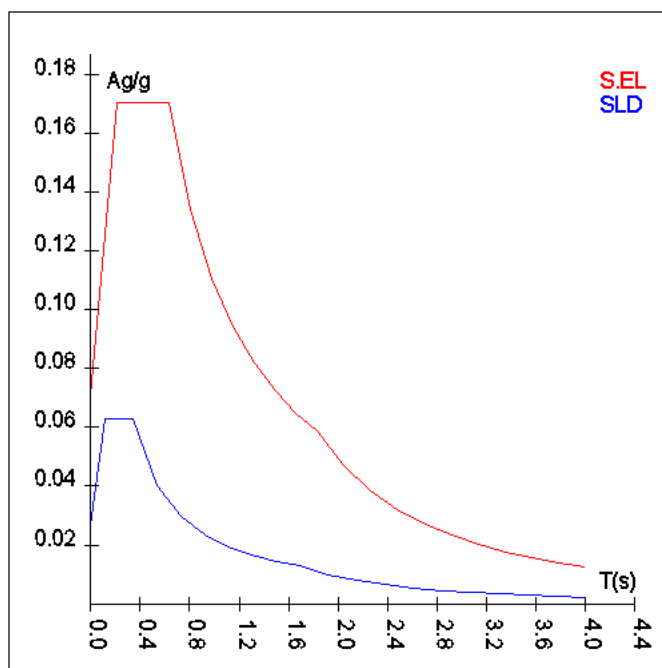
Spettro: **SpettroNT_2018**

Il calcolo degli spettri e del fattore di comportamento sono stati calcolati per la seguente tipologia di terreno e struttura.

Vita della struttura	
Tipo	Opere infr. imp. normale (50-100)
Vita nominale VN [anni]	50.0
Classe d'uso	III
Coefficiente d'uso CU	1.500
Periodo di riferimento VR [anni]	75.000
Probabilità di superamento PVR allo Stato limite di esercizio - SLD	63.0%
Probabilità di superamento PVR allo Stato limite ultimo - SLV	10.0%
Periodo di ritorno TR SLD [anni]	75.4
Periodo di ritorno TR SLV [anni]	711.8
Parametri del sito	
Comune	
Longitudine	18.212
Latitudine	40.289
Id reticolo del sito	35259-35037-35260-35038
Valori di riferimento del sito	
Accelerazione orizzontale massima del sito A_g/g - SLD (TR=75.4)	0.0222
Fattore di amplificazione dello spettro F_0 - SLD (TR=75.4)	2.3607
Periodo di riferimento di inizio del tratto a velocità costante T^*C [s] - SLD (TR=75.4)	0.235
Accelerazione orizzontale massima del sito A_g/g - SLV (TR=711.8)	0.0587
Fattore di amplificazione dello spettro F_0 - SLV (TR=711.8)	2.4204
Periodo di riferimento di inizio del tratto a velocità costante T^*C [s] - SLV (TR=711.8)	0.501
Coefficiente Amplificazione Topografica S_t	1.000
Categoria terreno	B
Stato limite SLV	
Coefficiente di amplificazione stratigrafica S_s	1.20
Periodo di inizio del tratto ad accelerazione costante dello spettro TB [s]	0.21
Periodo di inizio del tratto a velocità costante dello spettro TC [s]	0.63
Periodo di inizio del tratto a spostamento costante dello spettro TD [s]	1.83
Stato limite SLD	
Coefficiente di amplificazione stratigrafica S_s	1.20
Periodo di inizio del tratto ad accelerazione costante dello spettro TB [s]	0.12
Periodo di inizio del tratto a velocità costante dello spettro TC [s]	0.35
Periodo di inizio del tratto a spostamento costante dello spettro TD [s]	1.69
Spettro Elastico	
Smorzamento viscoso %	5.0

T El. [s]	Sd El. [a/g]	T SLD [s]	Sd SLD [a/g]
0.00000	0.07045	0.00000	0.02660
0.21106	0.17051	0.11515	0.06280
0.63318	0.17051	0.34546	0.06280
0.80485	0.13415	0.53735	0.04037
0.97651	0.11056	0.72923	0.02975
1.14817	0.09403	0.92112	0.02355
1.31984	0.08180	1.11301	0.01949
1.49150	0.07239	1.30490	0.01663
1.66317	0.06492	1.49679	0.01449
1.83483	0.05884	1.68867	0.01285
2.05135	0.04708	1.91981	0.00994
2.26786	0.03852	2.15094	0.00792
2.48438	0.03210	2.38207	0.00646
2.70090	0.02716	2.61320	0.00536
2.91741	0.02327	2.84434	0.00453

T El. [s]	Sd El. [a/g]	T SLD [s]	Sd SLD [a/g]
3.13393	0.02017	3.07547	0.00387
3.35045	0.01765	3.30660	0.00335
3.56697	0.01557	3.53773	0.00293
3.78348	0.01384	3.76887	0.00258
4.00000	0.01238	4.00000	0.00229



Azioni sulla struttura

Descrizione	Tipo
Peso Proprio	Automatica
Spinta Terreno accidentali	Utente
QP Solai	Automatica
QV Solai	Automatica
QV SolaiPsi0	Automatica
QV SolaiPsi1	Automatica
QV SolaiPsi2	Automatica
spinta acqua permanenti	Utente
grigliatura	Utente
QFissi Solai	Automatica
Muro esterno	Utente
neve	Utente
muratura	Utente

Scenario di calcolo

Scenario : ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO
Combinazione n° 1: Solo Permanenti
 Tipo: STR+GEO
 Spettro: n.a.
 Fattore sisma: n.a.
 Angolo ingresso sisma [°]: n.a.
 Kmod: 0.60

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Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
Spinta Terreno accidentali	1.5 1	Si No	n.a. n.a.	n.a. n.a.
QP Solai	1.5	Si	n.a.	n.a.
QV Solai	1.5	No	n.a.	n.a.
QV SolaiPsi0	1	No	n.a.	n.a.
QV SolaiPsi1	1.5	No	n.a.	n.a.
QV SolaiPsi2	1.3	No	n.a.	n.a.
spinta acqua permanenti	1 1.5	No Si	n.a. n.a.	n.a. n.a.
grigliatura	1.5	Si	n.a.	n.a.
QFissi Solai	1.5	Si	n.a.	n.a.
Muro esterno	1.5	Si	n.a.	n.a.
neve	1	No	n.a.	n.a.
muratura	1.5	Si	n.a.	n.a.

Combinazione n° 2: SLU1
 Tipo: STR+GEO
 Spettro: n.a.
 Fattore sisma: n.a.
 Angolo ingresso sisma [°]: n.a.
 Kmod: 0.90

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
Spinta Terreno accidentali	1.5 1.5	Si Si	n.a. n.a.	n.a. n.a.
QP Solai	1.5	Si	n.a.	n.a.
QV Solai	1.5	Si	n.a.	n.a.
QV SolaiPsi0	1	No	n.a.	n.a.
QV SolaiPsi1	1.5	No	n.a.	n.a.
QV SolaiPsi2	1.3	No	n.a.	n.a.
spinta acqua permanenti	1.5 1.5	Si Si	n.a. n.a.	n.a. n.a.
grigliatura	1.5	Si	n.a.	n.a.
QFissi Solai	1.5	Si	n.a.	n.a.
Muro esterno	1.5	Si	n.a.	n.a.
neve	1.05	Si	n.a.	n.a.
muratura	1.5	Si	n.a.	n.a.

Combinazione n° 3: SLU2
 Tipo: STR+GEO
 Spettro: n.a.
 Fattore sisma: n.a.
 Angolo ingresso sisma [°]: n.a.
 Kmod: 0.90

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
Spinta Terreno accidentali	1.5 1.5	Si No	n.a. n.a.	n.a. n.a.
QP Solai	1.5	Si	n.a.	n.a.
QV Solai	1.5	Si	n.a.	n.a.
QV SolaiPsi0	1	No	n.a.	n.a.
QV SolaiPsi1	1.5	No	n.a.	n.a.
QV SolaiPsi2	1.3	No	n.a.	n.a.
spinta acqua permanenti	1.5 1.5	Si Si	n.a. n.a.	n.a. n.a.
grigliatura	1.5	Si	n.a.	n.a.
QFissi Solai	1.5	Si	n.a.	n.a.
Muro esterno	1.5	Si	n.a.	n.a.
neve	1.05	Si	n.a.	n.a.
muratura	1.5	Si	n.a.	n.a.

Combinazione n° 4: SISMAX1_SLV
 Tipo: Modale STR+GEO
 Spettro: SpettroNT_2018
 Fattore sisma: 1.00
 Angolo ingresso sisma [°]: 0
 Kmod: 1.00

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Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
Spinta Terreno	1.1	Si	Si	1
accidentali	0.2	Si	Si	1
QP Solai	1	Si	Si	1
QV Solai	1	No	No	1
QV SolaiPsi0	1	Si	No	1
QV SolaiPsi1	1	Si	No	1
QV SolaiPsi2	1	Si	Si	1
spinta acqua	1.1	Si	Si	1
permanenti	1	Si	Si	1
grigliatura	1	Si	Si	1
QFissi Solai	1	Si	Si	1
Muro esterno	1	Si	Si	1
neve	1	No	No	1
muratura	1	Si	Si	1

Combinazione n° 5: **SISMAY1_SLV**
 Tipo: Modale STR+GEO
 Spettro: SpettroNT_2018
 Fattore sisma: 1.00
 Angolo ingresso sisma [°]: 90
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
Spinta Terreno	1.1	Si	Si	1
accidentali	0.2	Si	Si	1
QP Solai	1	Si	Si	1
QV Solai	1	No	No	1
QV SolaiPsi0	1	Si	No	1
QV SolaiPsi1	1	Si	No	1
QV SolaiPsi2	1	Si	Si	1
spinta acqua	1.1	Si	Si	1
permanenti	1	Si	Si	1
grigliatura	1	Si	Si	1
QFissi Solai	1	Si	Si	1
Muro esterno	1	Si	Si	1
neve	1	No	No	1
muratura	1	Si	Si	1

Combinazione n° 6: **AD QVSolai**
 Tipo: SLE Rara
 Spettro: n.a.
 Fattore sisma: n.a.
 Angolo ingresso sisma [°]: n.a.
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
Spinta Terreno	1	Si	n.a.	n.a.
accidentali	1	Si	n.a.	n.a.
QP Solai	1	Si	n.a.	n.a.
QV Solai	1	Si	n.a.	n.a.
QV SolaiPsi0	1	No	n.a.	n.a.
QV SolaiPsi1	1	No	n.a.	n.a.
QV SolaiPsi2	1	No	n.a.	n.a.
spinta acqua	1	Si	n.a.	n.a.
permanenti	1	Si	n.a.	n.a.
grigliatura	1	Si	n.a.	n.a.
QFissi Solai	1	Si	n.a.	n.a.
Muro esterno	1	Si	n.a.	n.a.
neve	0.2	Si	n.a.	n.a.
muratura	1	Si	n.a.	n.a.

Combinazione n° 7: **AD QVSolai**
 Tipo: SLE Freq.
 Spettro: n.a.
 Fattore sisma: n.a.
 Angolo ingresso sisma [°]: n.a.
 Kmod: 1.00

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Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
Spinta Terreno	1	Si	n.a.	n.a.
accidentali	0.5	Si	n.a.	n.a.
QP Solai	1	Si	n.a.	n.a.
QV Solai	1	No	n.a.	n.a.
QV SolaiPsi0	1	No	n.a.	n.a.
QV SolaiPsi1	1	Si	n.a.	n.a.
QV SolaiPsi2	1	No	n.a.	n.a.
spinta acqua	1	Si	n.a.	n.a.
permanenti	1	Si	n.a.	n.a.
grigliatura	1	Si	n.a.	n.a.
QFissi Solai	1	Si	n.a.	n.a.
Muro esterno	1	Si	n.a.	n.a.
neve	1	No	n.a.	n.a.
muratura	1	Si	n.a.	n.a.

Combinazione n° 8: Quasi P1
 Tipo: SLE Q.Perm.
 Spettro: n.a.
 Fattore sisma: n.a.
 Angolo ingresso sisma [°]: n.a.
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
Spinta Terreno	1	Si	n.a.	n.a.
accidentali	0.2	Si	n.a.	n.a.
QP Solai	1	Si	n.a.	n.a.
QV Solai	1	No	n.a.	n.a.
QV SolaiPsi0	1	No	n.a.	n.a.
QV SolaiPsi1	1	No	n.a.	n.a.
QV SolaiPsi2	1	Si	n.a.	n.a.
spinta acqua	1	Si	n.a.	n.a.
permanenti	1	Si	n.a.	n.a.
grigliatura	1	Si	n.a.	n.a.
QFissi Solai	1	Si	n.a.	n.a.
Muro esterno	1	Si	n.a.	n.a.
neve	1	No	n.a.	n.a.
muratura	1	Si	n.a.	n.a.

Combinazione n° 9: SISMAX_SLD
 Tipo: Modale SLE
 Spettro: SpettroNT_ 2018
 Fattore sisma: 1.00
 Angolo ingresso sisma [°]: 0
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
Spinta Terreno	1	Si	Si	1
accidentali	0.2	No	Si	1
QP Solai	1	Si	Si	1
QV Solai	1	No	No	1
QV SolaiPsi0	1	No	No	1
QV SolaiPsi1	1	No	No	1
QV SolaiPsi2	1	Si	Si	1
spinta acqua	1	Si	Si	1
permanenti	1	Si	Si	1
grigliatura	1	Si	Si	1
QFissi Solai	1	Si	Si	1
Muro esterno	1	Si	Si	1
neve	1	No	No	1
muratura	1	Si	Si	1

Combinazione n° 10: SISMAX_SLD
 Tipo: Modale SLE
 Spettro: SpettroNT_ 2018
 Fattore sisma: 1.00
 Angolo ingresso sisma [°]: 90
 Kmod: 1.00

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Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
Spinta Terreno	1	Si	Si	1
accidentali	0.2	Si	Si	1
QP Solai	1	Si	Si	1
QV Solai	1	Si	No	1
QV SolaiPsi0	1	Si	No	1
QV SolaiPsi1	1	Si	No	1
QV SolaiPsi2	1	Si	Si	1
spinta acqua	1	Si	Si	1
permanenti	1	Si	Si	1
grigliatura	1	Si	Si	1
QFissi Solai	1	Si	Si	1
Muro esterno	1	Si	Si	1
neve	1	Si	No	1
muratura	1	Si	Si	1

Criteri di verifica

CLS_Pilastri		
Generici		
Resistenza caratteristica Rck	kg/cm ²	450
Tensione caratteristica snervamento acciaio barre fyk	kg/cm ²	4500
Tensione caratteristica snervamento acciaio staffe fyk	kg/cm ²	4500
Deformazione unitaria ε _{c0}		0.002
Deformazione ultima ε _{cu}		0.0035
ε _{fu} (solo incrudimento)		0.01
Modulo elastico E acciaio	kg/cm ²	2E06
Copriferro di calcolo	cm	6.1
Copriferro di disegno	cm	4.5
Coefficiente di sicurezza γ _{Cl}		1.5
Coefficiente di sicurezza γ _{Acc}		1.15
Riduzione fcd calcestruzzo		0.85
Usa staffe minime di normativa in assenza di sisma		Si
Usa staffe minime di normativa in presenza di sisma		Si
Generici N.T.		
Inclinazione bielle compresse cotg(θ)		1.00
Modello acciaio		Elasto-plastico
Elemento esistente		No
Sforzo normale ammissibile v _{max} (CDA)		0.550
Sforzo normale ammissibile v _{max} (CDB)		0.650
Generici D.M. 96 T.A.		
Tensione ammissibile σ _c	kg/cm ²	135.0
Tensione ammissibile σ _c in trazione	kg/cm ²	28.6
Tensione ammissibile σ _c acciaio	kg/cm ²	2600.0
Tensione tangenziale ammissibile τ _{c0}	kg/cm ²	8.0
Tensione tangenziale massima τ _{c1}	kg/cm ²	22.6
Coefficiente di omogeneizzazione n		15
Coefficiente di omogeneizzazione n in trazione		0.5
Sezione interamente reagente		No
Fessurazioni		
Verifica a decompressione		No
Verifica formazione fessure		No
Verifica aperture fessure		Si
Classe di esposizione		XA2
Tipo armatura		Poco sensibile
Combinazione Rara		No
Combinazione QP		Si
W ammissibile Combinazione QP	mm	0.200
Combinazione Freq.		Si
W ammissibile Combinazione Freq.	mm	0.300
Valore caratteristico apertura fessure w _k (*w _m)		1
Resistenza media a trazione f _{ctm}	kg/cm ²	33.52
Coefficiente di breve o lunga durata k _t		0.40
Coefficiente di aderenza k _l		0.80
Tensioni ammissibili di esercizio		

Verifica Combinazione Rara		Si
Tensione ammissibile σ_{Cl}	kg/cm ²	224
Tensione ammissibile $\sigma_{Acciaio}$	kg/cm ²	3600
Verifica Combinazione QP		Si
Tensione ammissibile σ_{Cl}	kg/cm ²	168
Tensione ammissibile $\sigma_{Acciaio}$	kg/cm ²	3600
Verifica Combinazione Freq.		No
Coefficienti di omogeneizzazione		
Acciaio - Cls compresso		15
Cls teso - Cls compresso		0.5
Armatura pilastri		
Massimo numero di ferri in ogni spigolo		1
Diametro ferri di spigolo	mm	20
Diametro ferri laterali	mm	20
Diametro staffe	mm	8
Numero braccia staffe lato lungo		2
Minima percentuale armatura rispetto al Cls	%	1.00
Massima percentuale armatura rispetto al Cls	%	4.00
Verifica pilastri		
Verifica a carico di punta		No
Verifica a pressoflessione deviata		Si
Verifica come pareti		No
Verifica Duttibilità N.T. 2018		
Verifica di duttilità		NO
Fattore confinamento minimo		1.000
Calcolo Fattore confinamento		NO
Verifica N.T. pilastri		
Verifica pilastri tozzi		SI
Gerarchia Flessione-Taglio		SI
Verifica a taglio pilastri		
Effetto spinotto		Si
Traslazione momento		Si
Considera la resistenza a taglio VRDns		NO
Verifica a taglio pilastri DM 3274/DM96		
Coefficiente di amplificazione γ_{Rd}		1.2
Sforzo normale ammissibile v_{max}		0.8
Effetto della pressoflessione		Si
Verifica a taglio N.T. pilastri		
γ_{Rd} (CDA) Pressoflessione		1.3
γ_{Rd} (CDB) Pressoflessione		1.3
γ_{Rd} (CDA) Taglio		1.3
γ_{Rd} (CDB) Taglio		1.1
Verifica Nodi secondo EC8		SI
Stampa pilastri		
Informazioni sollecitazioni di verifica		No
Verifica per tutte le combinazioni di carico		No
Fattori di amplificazione		No
Gerarchia delle resistenze pilastri		
Direzione Y		Si
Direzione Z		Si

CLS TraviAlte		
Generici		
Resistenza caratteristica R_{ck}	kg/cm ²	450
Tensione caratteristica snervamento acciaio barre f_{yk}	kg/cm ²	4500
Tensione caratteristica snervamento acciaio staffe f_{yk}	kg/cm ²	4500
Deformazione unitaria ϵ_{c0}		0.002
Deformazione ultima ϵ_{cu}		0.0035
ϵ_{fu} (solo incrudimento)		0.01
Modulo elastico E acciaio	kg/cm ²	2E06
Copriferro di calcolo	cm	6.1
Copriferro di disegno	cm	5.0
Coefficiente di sicurezza γ_{Cl}		1.5
Coefficiente di sicurezza γ_{Acc}		1.15
Riduzione f_{cd} calcestruzzo		0.85
Usa staffe minime di normativa in assenza di sisma		Si
Usa staffe minime di normativa in presenza di sisma		Si
Generici N.T.		
Inclinazione bielle compresse $\cotg(\theta)$		1.00

Modello acciaio		Elasto-plastico
Elemento esistente		No
Generici D.M. 96 T.A.		
Tensione ammissibile σ_c	kg/cmq	135.0
Tensione ammissibile σ_c in trazione	kg/cmq	28.6
Tensione ammissibile σ_c acciaio	kg/cmq	2600.0
Tensione tangenziale ammissibile τ_{c0}	kg/cmq	8.0
Tensione tangenziale massima τ_{c1}	kg/cmq	22.6
Coefficiente di omogeneizzazione n		15
Coefficiente di omogeneizzazione n in trazione		0.5
Sezione interamente reagente		No
Fessurazioni		
Verifica a decompressione		No
Verifica formazione fessure		No
Verifica aperture fessure		Si
Classe di esposizione		XA2
Tipo armatura		Poco sensibile
Combinazione Rara		No
Combinazione QP		Si
W ammissibile Combinazione QP	mm	0.200
Combinazione Freq.		Si
W ammissibile Combinazione Freq.	mm	0.300
Valore caratteristico apertura fessure $w_k(*w_m)$		1
Resistenza media a trazione f_{ctm}	kg/cmq	33.52
Coefficiente di breve o lunga durata k_t		0.40
Coefficiente di aderenza k_l		0.80
Tensioni ammissibili di esercizio		
Verifica Combinazione Rara		Si
Tensione ammissibile σ_{ClS}	kg/cmq	224
Tensione ammissibile $\sigma_{Acciaio}$	kg/cmq	3600
Verifica Combinazione QP		Si
Tensione ammissibile σ_{ClS}	kg/cmq	168
Tensione ammissibile $\sigma_{Acciaio}$	kg/cmq	3600
Verifica Combinazione Freq.		No
Coefficienti di omogeneizzazione		
Acciaio - Cls compresso		15
Cls teso - Cls compresso		0.5
Armatura travi		
Numero di bracci delle staffe		2
Numero minimo di ferri superiori		2
Numero minimo di ferri inferiori		2
Numero minimo di ferri di parete		1
Numero reggistaffe superiori		0
Numero reggistaffe intermedi		0
Numero reggistaffe inferiori		0
Diametro ferri superiori	mm	16
Diametro ferri inferiori	mm	16
Diametro staffe	mm	8
Percentuale armatura rispetto alla base per verifica a taglio	%	100.00
Minima percentuale armatura compressa rispetto alla tesa	%	50.00
Minima percentuale armatura rispetto al Cls	%	0.31
Massima percentuale armatura rispetto al Cls	%	1.55
Calcolo travi		
Traslazione momento		Si
Verifica travi		
Verifica a torsione		No
Verifica a pressoflessione retta		No
Trave a spessore		No
Verifica N.T. travi		
Trave tozza		Si
Gerarchia Flessione-Taglio		Si
Escludi dalla gerarchia trave-pilastro		No
Verifica a taglio DM 3274 travi		
Coefficiente di sovra resistenza γ_{Rd}		1.2
Includi effetto della pressoflessione nel taglio		Si
Verifica a taglio N.T. travi		
Includi effetto spinotto nel taglio		Si
Considera la resistenza a taglio VRDns		NO
Coefficiente di sovra resistenza γ_{Rd} (CDA)		1.2
Coefficiente di sovra resistenza γ_{Rd} (CDB)		1.1
Verifica Duttilità N.T. 2018		

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Verifica di duttilità		NO
Fattore confinamento minimo		1.000
Calcolo Fattore confinamento		NO
Verifica a taglio D.M. 96 T.A. travi		
Percentuale taglio alle staffe	%	60
Percentuale taglio ferri parete	%	40
Stampa travi		
Stampa informazioni relative all'asse neutro		Si

CLS Muri ND		
Generici		
Resistenza caratteristica Rck	kg/cmq	450
Tensione caratteristica snervamento acciaio barre fyk	kg/cmq	4500
Tensione caratteristica snervamento acciaio staffe fyk	kg/cmq	4500
Deformazione unitaria ϵ_{c0}		0.002
Deformazione ultima ϵ_{cu}		0.0022
ϵ_{fu} (solo incrudimento)		0.002
Modulo elastico E acciaio	kg/cmq	2E06
Copriferro di calcolo	cm	5.0
Copriferro di disegno	cm	5.0
Coefficiente di sicurezza γ_{ClS}		1.5
Coefficiente di sicurezza γ_{Acc}		1.15
Riduzione fcd calcestruzzo		0.85
Usa staffe minime di normativa in assenza di sisma		Si
Usa staffe minime di normativa in presenza di sisma		No
Generici N.T.		
Inclinazione bielle compresse $\cotg(\theta)$		1.00
Modello acciaio		Incrudente
Incrudimento E_y/E_0		0.000
Elemento esistente		No
Generici D.M. 96 T.A.		
Tensione ammissibile σ_c	kg/cmq	135.0
Tensione ammissibile σ_c in trazione	kg/cmq	40.2
Tensione ammissibile σ_c acciaio	kg/cmq	2600.0
Tensione tangenziale ammissibile τ_{c0}	kg/cmq	8.0
Tensione tangenziale massima τ_{c1}	kg/cmq	22.6
Coefficiente di omogeneizzazione n		15
Coefficiente di omogeneizzazione n in trazione		0.5
Sezione interamente reagente		No
Fessurazioni		
Verifica a decompressione		No
Verifica formazione fessure		No
Verifica aperture fessure		Si
Classe di esposizione		XA2
Tipo armatura		Poco sensibile
Combinazione Rara		No
Combinazione QP		Si
W ammissibile Combinazione QP	mm	0.200
Combinazione Freq.		Si
W ammissibile Combinazione Freq.	mm	0.300
Valore caratteristico apertura fessure $w_k(*w_m)$		1
Resistenza media a trazione f_{ctm}	kg/cmq	33.52
Coefficiente di breve o lunga durata k_t		0.40
Coefficiente di aderenza k_l		0.80
Tensioni ammissibili di esercizio		
Verifica Combinazione Rara		Si
Tensione ammissibile σ_{ClS}	kg/cmq	224
Tensione ammissibile $\sigma_{Acciaio}$	kg/cmq	3600
Verifica Combinazione QP		Si
Tensione ammissibile σ_{ClS}	kg/cmq	168
Tensione ammissibile $\sigma_{Acciaio}$	kg/cmq	3600
Verifica Combinazione Freq.		No
Coefficienti di omogeneizzazione		
Acciaio - Cls compresso		15
ClS teso - Cls compresso		0.5
Armatura muri		
Minima percentuale armatura rispetto al Cls in direzione X	%	0.1
Minima percentuale armatura rispetto al Cls in direzione Y	%	0.1
Massima percentuale armatura rispetto al Cls in direzione X	%	2

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Massima percentuale armatura rispetto al Cls in direzione Y	%	2
Verifica muri		
Step incremento armatura	cmq	0.01
Verifica muri come pareti		No

CLS Platee ND		
Generici		
Resistenza caratteristica Rck	kg/cmq	450
Tensione caratteristica snervamento acciaio barre fyk	kg/cmq	4500
Tensione caratteristica snervamento acciaio staffe fyk	kg/cmq	4500
Deformazione unitaria ϵ_{c0}		0.002
Deformazione ultima ϵ_{cu}		0.0022
ϵ_{fu} (solo incrudimento)		0.002
Modulo elastico E acciaio	kg/cmq	2E06
Copriferro di calcolo	cm	5.0
Copriferro di disegno	cm	5.0
Coefficiente di sicurezza γ_{ClS}		1.5
Coefficiente di sicurezza γ_{Acc}		1.15
Riduzione fcd calcestruzzo		0.85
Usa staffe minime di normativa in assenza di sisma		Si
Usa staffe minime di normativa in presenza di sisma		No
Generici N.T.		
Inclinazione bielle compresse $\cotg(\theta)$		1.00
Modello acciaio		Incrudente
Incrudimento Ey/E0		0.000
Elemento esistente		No
Generici D.M. 96 T.A.		
Tensione ammissibile σ_c	kg/cmq	135.0
Tensione ammissibile σ_c in trazione	kg/cmq	40.2
Tensione ammissibile σ_c acciaio	kg/cmq	2600.0
Tensione tangenziale ammissibile τ_{c0}	kg/cmq	8.0
Tensione tangenziale massima τ_{c1}	kg/cmq	22.6
Coefficiente di omogeneizzazione n		15
Coefficiente di omogeneizzazione n in trazione		0.5
Sezione interamente reagente		No
Fessurazioni		
Verifica a decompressione		No
Verifica formazione fessure		No
Verifica aperture fessure		Si
Classe di esposizione		XA2
Tipo armatura		Poco sensibile
Combinazione Rara		No
Combinazione QP		Si
W ammissibile Combinazione QP	mm	0.200
Combinazione Freq.		Si
W ammissibile Combinazione Freq.	mm	0.300
Valore caratteristico apertura fessure $w_k(*w_m)$		1
Resistenza media a trazione f_{ctm}	kg/cmq	33.52
Coefficiente di breve o lunga durata k_t		0.40
Coefficiente di aderenza k_l		0.80
Tensioni ammissibili di esercizio		
Verifica Combinazione Rara		Si
Tensione ammissibile σ_{ClS}	kg/cmq	224
Tensione ammissibile $\sigma_{Acciaio}$	kg/cmq	3600
Verifica Combinazione QP		Si
Tensione ammissibile σ_{ClS}	kg/cmq	168
Tensione ammissibile $\sigma_{Acciaio}$	kg/cmq	3600
Verifica Combinazione Freq.		No
Coefficienti di omogeneizzazione		
Acciaio - Cls compresso		15
Cls teso - Cls compresso		0.5
Armatura muri		
Minima percentuale armatura rispetto al Cls in direzione X	%	0.1
Minima percentuale armatura rispetto al Cls in direzione Y	%	0.1
Massima percentuale armatura rispetto al Cls in direzione X	%	2
Massima percentuale armatura rispetto al Cls in direzione Y	%	2
Verifica muri		
Step incremento armatura	cmq	0.01
Verifica muri come pareti		No

Risultati Analisi Dinamica - Statistiche matrice di rigidità

Scenario di calcolo: ScenarioNT_2018 A2_SLV_SLD_STR_GEO

Minimo della diagonale	1.852586e+05
Massimo della diagonale	1.738210e+13
Rapporto Max/Min	9.382619e+07
Media della diagonale	2.090394e+10
Densità	2.057265e-01

Dati generali

Nome struttura	
Fattore rigidità assiale pilastri	10
Numero di frequenze	15
% Filtro masse libere	0.1
% Coefficiente di smorzamento viscoso	5
Spostamenti modali con segno	Si
Deformabilità a taglio delle aste	Si
Spostamento ammissibile impalcato	0.0050*h

Impalcato

N°	Quota m	Rigido m	Incr.Soll.Pil	Inc.Soll.Par.
0	-2.75	Si	1.000	1.000
1	-1.45	Si	1.000	1.000
2	0.00	No	1.000	1.000
3	1.45	Si	1.000	1.000
4	5.45	Si	1.000	1.000

Percentuali Spostamento masse impalcato

Posizione	% Spostamento direzione X	% Spostamento direzione Y
1	0	-5
2	5	0
3	0	5
4	-5	0

Combinazioni del Sisma in X e Y e Verticale

Comb.	Pos. SismaX	Pos. SismaY	Fx	Fy	Fz
1	1	2	1	0.3	0
2	1	2	0.3	1	0
3	1	4	1	0.3	0
4	1	4	0.3	1	0
5	3	2	1	0.3	0
6	3	2	0.3	1	0
7	3	4	1	0.3	0
8	3	4	0.3	1	0

Comb. Numero di combinazione dei sismi
 Pos. SismaX Posizione in cui viene scelto il sisma in direzione X
 Pos. SismaY Posizione in cui viene scelto il sisma in direzione Y
 Fx Fattore con cui il sisma X partecipa
 Fy Fattore con cui il sisma Y partecipa
 Fz Fattore con cui il sisma Verticale partecipa (quando richiesto)

Ogni combinazione genera al massimo 8 sotto-combinazioni in base a tutte le combinazioni possibili dei segni di Fx ed Fy ed Fz.

Nodi - Geometria e vincoli

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
		Coordinate [m]				Vincoli				
1	1.78	13.56	-1.55	1	1	0	0	0	1	1
2	4.60	17.66	-1.55	0	0	0	0	0	0	1
3	4.60	17.66	-2.67	0	0	0	0	0	0	0
4	3.82	17.41	-2.67	0	0	0	0	0	0	0
5	3.82	17.41	-1.55	0	0	0	0	0	0	1
6	3.15	17.06	-2.67	0	0	0	0	0	0	0
7	3.15	17.06	-1.55	0	0	0	0	0	0	1
8	2.80	16.39	-2.67	0	0	0	0	0	0	0
9	2.80	16.39	-1.55	0	0	0	0	0	0	1

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Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
10	2.55	15.61	-2.67	0	0	0	0	0	0	0
11	2.55	15.61	-1.55	0	0	0	0	0	0	1
12	2.80	14.83	-2.67	0	0	0	0	0	0	0
13	2.80	14.83	-1.55	0	0	0	0	0	0	1
14	3.15	14.16	-2.67	0	0	0	0	0	0	0
15	3.15	14.16	-1.55	0	0	0	0	0	0	1
16	3.82	13.81	-2.67	0	0	0	0	0	0	0
17	3.82	13.81	-1.55	0	0	0	0	0	0	1
18	4.60	13.56	-2.67	0	0	0	0	0	0	0
19	4.60	13.56	-1.55	0	0	0	0	0	0	1
20	5.38	13.81	-2.67	0	0	0	0	0	0	0
21	5.38	13.81	-1.55	0	0	0	0	0	0	1
22	6.05	14.16	-2.67	0	0	0	0	0	0	0
23	6.05	14.16	-1.55	0	0	0	0	0	0	1
24	6.40	14.83	-2.67	0	0	0	0	0	0	0
25	6.40	14.83	-1.55	0	0	0	0	0	0	1
26	6.65	15.61	-2.67	0	0	0	0	0	0	0
27	6.65	15.61	-1.55	0	0	0	0	0	0	1
28	6.40	16.39	-2.67	0	0	0	0	0	0	0
29	6.40	16.39	-1.55	0	0	0	0	0	0	1
30	6.05	17.06	-2.67	0	0	0	0	0	0	0
31	6.05	17.06	-1.55	0	0	0	0	0	0	1
32	5.38	17.41	-2.67	0	0	0	0	0	0	0
33	5.38	17.41	-1.55	0	0	0	0	0	0	1
34	3.74	15.46	-2.67	1	1	0	0	0	1	0
35	3.74	15.76	-2.67	1	1	0	0	0	1	0
36	3.84	16.05	-2.67	1	1	0	0	0	1	0
37	4.04	16.28	-2.67	1	1	0	0	0	1	0
38	4.90	14.79	-2.67	1	1	0	0	0	1	0
39	4.60	14.73	-2.67	1	1	0	0	0	1	0
40	4.30	16.43	-2.67	1	1	0	0	0	1	0
41	4.60	16.48	-2.67	1	1	0	0	0	1	0
42	3.84	15.17	-2.67	1	1	0	0	0	1	0
43	4.30	14.79	-2.67	1	1	0	0	0	1	0
44	4.04	14.94	-2.67	1	1	0	0	0	1	0
45	4.90	16.43	-2.67	1	1	0	0	0	1	0
46	5.16	16.28	-2.67	1	1	0	0	0	1	0
47	5.16	14.94	-2.67	1	1	0	0	0	1	0
48	5.46	15.46	-2.67	1	1	0	0	0	1	0
49	5.36	15.17	-2.67	1	1	0	0	0	1	0
50	5.46	15.76	-2.67	1	1	0	0	0	1	0
51	5.36	16.05	-2.67	1	1	0	0	0	1	0
52	4.60	15.61	-2.67	1	1	0	0	0	1	0
53	1.78	15.61	-1.55	0	0	0	0	0	0	1
2001	0.00	0.00	0.00	1	1	0	0	0	1	2
2002	7.82	0.00	0.00	1	1	0	0	0	1	2
2003	14.60	0.00	0.00	1	1	0	0	0	1	2
2004	0.00	4.65	0.00	1	1	0	0	0	1	2
2005	7.97	4.65	0.00	1	1	0	0	0	1	2
2006	14.60	4.65	0.00	1	1	0	0	0	1	2
2007	0.00	8.65	0.00	1	1	0	0	0	1	2
2008	7.97	8.65	0.00	0	0	0	0	0	0	2
2009	14.60	8.65	0.00	1	1	0	0	0	1	2
2010	0.00	13.65	0.00	1	1	0	0	0	1	2
2011	7.97	13.65	0.00	0	0	0	0	0	0	2
2012	14.60	13.65	0.00	1	1	0	0	0	1	2
2013	0.00	18.25	0.00	1	1	0	0	0	1	2
2014	7.97	18.25	0.00	1	1	0	0	0	1	2
2015	14.60	18.25	0.00	1	1	0	0	0	1	2
2016	0.00	22.60	0.00	1	1	0	0	0	1	2
2017	7.82	22.60	0.00	1	1	0	0	0	1	2
2018	14.60	22.60	0.00	1	1	0	0	0	1	2
2019	-0.50	-0.50	0.00	1	1	0	0	0	1	2
2020	0.00	-0.50	0.00	1	1	0	0	0	1	2
2021	4.90	-0.50	0.00	1	1	0	0	0	1	2
2022	7.82	-0.50	0.00	1	1	0	0	0	1	2
2023	14.60	-0.50	0.00	1	1	0	0	0	1	2
2024	15.10	-0.50	0.00	1	1	0	0	0	1	2
2025	-0.50	0.00	0.00	1	1	0	0	0	1	2
2026	4.90	0.00	0.00	1	1	0	0	0	1	2
2027	15.10	0.00	0.00	1	1	0	0	0	1	2
2028	4.90	2.67	0.00	0	0	0	0	0	0	2
2029	9.52	2.67	0.00	0	0	0	0	0	0	2
2031	6.17	3.95	0.00	1	1	0	0	0	1	2
2032	7.97	3.95	0.00	1	1	0	0	0	1	2
2033	9.52	3.95	0.00	1	1	0	0	0	1	2

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2035	-0.50	4.65	0.00	1	1	0	0	0	1	2
2036	4.90	4.65	0.00	0	0	0	0	0	0	2
2037	6.17	4.65	0.00	0	0	0	0	0	0	2
2038	9.52	4.65	0.00	1	1	0	0	0	1	2
2040	15.10	4.65	0.00	1	1	0	0	0	1	2
2041	-0.50	8.65	0.00	1	1	0	0	0	1	2
2042	4.90	8.65	0.00	0	0	0	0	0	0	2
2043	6.17	8.65	0.00	1	1	0	0	0	1	2
2044	9.52	8.65	0.00	1	1	0	0	0	1	2
2046	15.10	8.65	0.00	1	1	0	0	0	1	2
2047	4.90	10.17	0.00	0	0	0	0	0	0	2
2048	6.17	10.17	0.00	1	1	0	0	0	1	2
2049	7.97	10.17	0.00	0	0	0	0	0	0	2
2050	9.52	10.17	0.00	0	0	0	0	0	0	2
2052	12.46	11.00	0.00	1	1	0	0	0	1	2
2053	4.90	11.12	0.00	0	0	0	0	0	0	2
2054	9.52	11.12	0.00	0	0	0	0	0	0	2
2056	6.55	12.02	0.00	0	0	0	0	0	0	2
2057	7.97	12.02	0.00	0	0	0	0	0	0	2
2058	1.78	13.56	0.00	0	0	0	0	0	0	2
2059	4.60	13.56	0.00	0	0	0	0	0	0	2
2060	6.55	13.56	0.00	0	0	0	0	0	0	2
2061	-0.50	13.65	0.00	1	1	0	0	0	1	2
2062	11.30	13.65	0.00	1	1	0	0	0	1	2
2063	15.10	13.65	0.00	1	1	0	0	0	1	2
2064	3.82	13.81	0.00	0	0	0	0	0	0	2
2065	5.38	13.81	0.00	0	0	0	0	0	0	2
2066	3.15	14.16	0.00	0	0	0	0	0	0	2
2067	6.05	14.16	0.00	0	0	0	0	0	0	2
2068	2.80	14.83	0.00	0	0	0	0	0	0	2
2069	6.40	14.83	0.00	0	0	0	0	0	0	2
2070	1.78	15.61	0.00	0	0	0	0	0	0	2
2071	2.55	15.61	0.00	0	0	0	0	0	0	2
2072	6.65	15.61	0.00	0	0	0	0	0	0	2
2073	2.80	16.39	0.00	0	0	0	0	0	0	2
2074	6.40	16.39	0.00	0	0	0	0	0	0	2
2075	3.15	17.06	0.00	0	0	0	0	0	0	2
2076	6.05	17.06	0.00	0	0	0	0	0	0	2
2077	3.82	17.41	0.00	0	0	0	0	0	0	2
2078	5.38	17.41	0.00	1	1	0	0	0	1	2
2079	4.60	17.66	0.00	0	0	0	0	0	0	2
2080	-0.50	18.25	0.00	1	1	0	0	0	1	2
2081	15.10	18.25	0.00	1	1	0	0	0	1	2
2082	2.80	18.41	0.00	1	1	0	0	0	1	2
2083	3.82	18.41	0.00	1	1	0	0	0	1	2
2084	5.38	18.80	0.00	1	1	0	0	0	1	2
2085	7.97	18.80	0.00	1	1	0	0	0	1	2
2086	10.97	19.00	0.00	1	1	0	0	0	1	2
2087	0.20	21.65	0.00	1	1	0	0	0	1	2
2088	4.90	21.65	0.00	1	1	0	0	0	1	2
2089	8.67	21.75	0.00	1	1	0	0	0	1	2
2090	12.30	21.75	0.00	1	1	0	0	0	1	2
2091	-0.50	22.60	0.00	1	1	0	0	0	1	2
2092	4.90	22.60	0.00	1	1	0	0	0	1	2
2093	15.10	22.60	0.00	1	1	0	0	0	1	2
2094	-0.50	23.10	0.00	1	1	0	0	0	1	2
2095	0.00	23.10	0.00	1	1	0	0	0	1	2
2096	4.90	23.10	0.00	1	1	0	0	0	1	2
2097	7.82	23.10	0.00	1	1	0	0	0	1	2
2098	14.60	23.10	0.00	1	1	0	0	0	1	2
2099	15.10	23.10	0.00	1	1	0	0	0	1	2
3005	7.97	4.65	1.45	0	0	0	0	0	0	3
3008	7.97	8.65	1.45	0	0	0	0	0	0	3
3011	7.97	13.65	1.45	0	0	0	0	0	0	3
3014	7.97	18.25	1.45	0	0	0	0	0	0	3
3028	4.90	2.67	1.45	0	0	0	0	0	0	3
3029	9.52	2.67	1.45	0	0	0	0	0	0	3
3030	10.22	2.67	1.45	0	0	0	0	0	0	3
3031	6.17	3.95	1.45	0	0	0	0	0	0	3
3032	7.97	3.95	1.45	0	0	0	0	0	0	3
3033	9.52	3.95	1.45	0	0	0	0	0	0	3
3034	10.22	3.95	1.45	0	0	0	0	0	0	3
3036	4.90	4.65	1.45	0	0	0	0	0	0	3
3037	6.17	4.65	1.45	0	0	0	0	0	0	3
3038	9.52	4.65	1.45	0	0	0	0	0	0	3
3039	10.22	4.65	1.45	0	0	0	0	0	0	3

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
3042	4.90	8.65	1.45	0	0	0	0	0	0	3
3043	6.17	8.65	1.45	0	0	0	0	0	0	3
3044	9.52	8.65	1.45	0	0	0	0	0	0	3
3045	10.22	8.65	1.45	0	0	0	0	0	0	3
3047	4.90	10.17	1.45	0	0	0	0	0	0	3
3048	6.17	10.17	1.45	0	0	0	0	0	0	3
3049	7.97	10.17	1.45	0	0	0	0	0	0	3
3050	9.52	10.17	1.45	0	0	0	0	0	0	3
3051	10.22	10.17	1.45	0	0	0	0	0	0	3
3053	4.90	11.12	1.45	0	0	0	0	0	0	3
3054	9.52	11.12	1.45	0	0	0	0	0	0	3
3055	10.22	11.12	1.45	0	0	0	0	0	0	3
3056	6.55	12.02	1.45	0	0	0	0	0	0	3
3057	7.97	12.02	1.45	0	0	0	0	0	0	3
3058	1.78	13.56	1.45	0	0	0	0	0	0	3
3059	4.60	13.56	1.45	0	0	0	0	0	0	3
3060	6.55	13.56	1.45	0	0	0	0	0	0	3
3064	3.82	13.81	1.45	0	0	0	0	0	0	3
3066	3.15	14.16	1.45	0	0	0	0	0	0	3
3068	2.80	14.83	1.45	0	0	0	0	0	0	3
3069	6.40	14.83	1.45	0	0	0	0	0	0	3
3070	1.78	15.61	1.45	0	0	0	0	0	0	3
3071	2.55	15.61	1.45	0	0	0	0	0	0	3
3072	6.65	15.61	1.45	0	0	0	0	0	0	3
3073	2.80	16.39	1.45	0	0	0	0	0	0	3
3074	6.40	16.39	1.45	0	0	0	0	0	0	3
3075	3.15	17.06	1.45	0	0	0	0	0	0	3
3076	6.05	17.06	1.45	0	0	0	0	0	0	3
3077	3.82	17.41	1.45	0	0	0	0	0	0	3
3078	5.38	17.41	1.45	0	0	0	0	0	0	3
3079	4.60	17.66	1.45	0	0	0	0	0	0	3
3084	5.38	18.80	1.45	0	0	0	0	0	0	3
3085	7.97	18.80	1.45	0	0	0	0	0	0	3
4001	0.00	0.00	5.45	0	0	0	0	0	0	4
4002	7.82	0.00	5.45	0	0	0	0	0	0	4
4003	14.60	0.00	5.45	0	0	0	0	0	0	4
4004	0.00	4.65	5.45	0	0	0	0	0	0	4
4005	7.97	4.65	5.45	0	0	0	0	0	0	4
4006	14.60	4.65	5.45	0	0	0	0	0	0	4
4007	0.00	8.65	5.45	0	0	0	0	0	0	4
4008	7.97	8.65	5.45	0	0	0	0	0	0	4
4009	14.60	8.65	5.45	0	0	0	0	0	0	4
4010	0.00	13.65	5.45	0	0	0	0	0	0	4
4011	7.97	13.65	5.45	0	0	0	0	0	0	4
4012	14.60	13.65	5.45	0	0	0	0	0	0	4
4013	0.00	18.25	5.45	0	0	0	0	0	0	4
4014	7.97	18.25	5.45	0	0	0	0	0	0	4
4015	14.60	18.25	5.45	0	0	0	0	0	0	4
4016	0.00	22.60	5.45	0	0	0	0	0	0	4
4017	7.82	22.60	5.45	0	0	0	0	0	0	4
4018	14.60	22.60	5.45	0	0	0	0	0	0	4

Input - Aste - Tabella sezioni tipo

Tipo	Nome	Base	Altezza	Larg.mag.
R		m	m	m
	30x50	0.30	0.50	0.00
	50x30	0.50	0.30	0.00
	70x25	0.70	0.25	0.00

Aste - Geometria e vincoli

	Ni	Nf	Vin c.	Sez.	Mat.	Crit.pr .	Rot °	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
									m							m	
2001	2001	4001	I-I	30x50	C35/45	CLS_Pil astri	0	1010	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	5.45	5.45
2002	2002	4002	I-I	50x30	C35/45	CLS_Pil astri	0	2020	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	5.45	5.45
2003	2003	4003	I-I	30x50	C35/45	CLS_Pil astri	0	3030	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	5.45	5.45
2004	2004	4004	I-I	30x50	C35/45	CLS_Pil astri	0	4040	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	5.45	5.45
2005	2005	3005	I-I	30x50	C35/45	CLS_Pil astri	0	6060	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	1.45	1.45

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	Ni	Nf	Vin C.	Sez.	Mat.	Crit.pr .	Rot .	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
2005	3005	4005	I-I	30x50	C35/45	CLS_Pil astri	0	6060	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	4.00	4.00
2006	2006	4006	I-I	30x50	C35/45	CLS_Pil astri	0	6060	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	5.45	5.45
2007	2007	4007	I-I	30x50	C35/45	CLS_Pil astri	0	4040	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	5.45	5.45
2008	2008	3008	I-I	30x50	C35/45	CLS_Pil astri	0	6060	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	1.45	1.45
2008	3008	4008	I-I	30x50	C35/45	CLS_Pil astri	0	6060	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	4.00	4.00
2009	2009	4009	I-I	30x50	C35/45	CLS_Pil astri	0	6060	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	5.45	5.45
2010	2010	4010	I-I	30x50	C35/45	CLS_Pil astri	0	4040	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	5.45	5.45
2011	2011	3011	I-I	30x50	C35/45	CLS_Pil astri	0	6060	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	1.45	1.45
2011	3011	4011	I-I	30x50	C35/45	CLS_Pil astri	0	6060	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	4.00	4.00
2012	2012	4012	I-I	30x50	C35/45	CLS_Pil astri	0	6060	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	5.45	5.45
2013	2013	4013	I-I	30x50	C35/45	CLS_Pil astri	0	4040	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	5.45	5.45
2014	2014	3014	I-I	30x50	C35/45	CLS_Pil astri	0	6060	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	1.45	1.45
2014	3014	4014	I-I	30x50	C35/45	CLS_Pil astri	0	6060	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	4.00	4.00
2015	2015	4015	I-I	30x50	C35/45	CLS_Pil astri	0	6060	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	5.45	5.45
2016	2016	4016	I-I	30x50	C35/45	CLS_Pil astri	0	7070	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	5.45	5.45
2017	2017	4017	I-I	50x30	C35/45	CLS_Pil astri	0	8080	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	5.45	5.45
2018	2018	4018	I-I	30x50	C35/45	CLS_Pil astri	0	9090	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	5.45	5.45
301	3071	3072	I-I	70x25	C35/45	CLS_Tra viAlte	0	8080	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	4.10	4.10
401	4001	4002	I-I	30x50	C35/45	CLS_Tra viAlte	0	7172	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	7.82	7.82
401	4002	4003	I-I	30x50	C35/45	CLS_Tra viAlte	0	7273	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	6.78	6.78
402	4003	4006	I-I	30x50	C35/45	CLS_Tra viAlte	0	7376	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	4.65	4.65
402	4006	4009	I-I	30x50	C35/45	CLS_Tra viAlte	0	7676	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	4.00	4.00
402	4009	4012	I-I	30x50	C35/45	CLS_Tra viAlte	0	7679	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	5.00	5.00
402	4012	4015	I-I	30x50	C35/45	CLS_Tra viAlte	0	7679	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	4.60	4.60
402	4015	4018	I-I	30x50	C35/45	CLS_Tra viAlte	0	7679	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	4.35	4.35
403	4011	4010	I-I	50x30	C35/45	CLS_Tra viAlte	0	8484	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	7.97	7.97
403	4012	4011	I-I	50x30	C35/45	CLS_Tra viAlte	0	7978	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	6.63	6.63
404	4004	4001	I-I	30x50	C35/45	CLS_Tra viAlte	0	7471	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	4.65	4.65
404	4007	4004	I-I	30x50	C35/45	CLS_Tra viAlte	0	7474	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	4.00	4.00
404	4010	4007	I-I	30x50	C35/45	CLS_Tra viAlte	0	7774	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	5.00	5.00
404	4013	4010	I-I	30x50	C35/45	CLS_Tra viAlte	0	7774	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	4.60	4.60
404	4016	4013	I-I	30x50	C35/45	CLS_Tra viAlte	0	7774	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	4.35	4.35
405	4005	4004	I-I	50x30	C35/45	CLS_Tra viAlte	0	8484	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	7.97	7.97
405	4005	4006	I-I	50x30	C35/45	CLS_Tra viAlte	0	8586	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	6.63	6.63
406	4008	4007	I-I	50x30	C35/45	CLS_Tra viAlte	0	7784	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	7.97	7.97
406	4008	4009	I-I	50x30	C35/45	CLS_Tra viAlte	0	8586	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	6.63	6.63
407	4002	4005	I-I	30x50	C35/45	CLS_Tra viAlte	0	8285	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	4.65	4.65
407	4005	4008	I-I	30x50	C35/45	CLS_Tra viAlte	0	8585	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	4.00	4.00

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	Ni	Nf	Vin c.	Sez.	Mat.	Crit.pr c.	Rot .	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
407	4008	4011	I-I	30x50	C35/45	CLS_Tra viAlte	0	8588	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	5.00	5.00
407	4011	4014	I-I	30x50	C35/45	CLS_Tra viAlte	0	8588	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	4.60	4.60
407	4014	4017	I-I	30x50	C35/45	CLS_Tra viAlte	0	8588	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	4.35	4.35
408	4014	4013	I-I	50x30	C35/45	CLS_Tra viAlte	0	8484	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	7.97	7.97
408	4015	4014	I-I	50x30	C35/45	CLS_Tra viAlte	0	7978	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	6.63	6.63
409	4017	4016	I-I	30x50	C35/45	CLS_Tra viAlte	0	7877	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	7.82	7.82
409	4018	4017	I-I	30x50	C35/45	CLS_Tra viAlte	0	7978	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	6.78	6.78

Aste - Carichi

Descrizione carichi aste

UnifG Uniforme globale
UnifL Uniforme locale
VarG Variabile lineare globale
VarL Variabile lineare locale
PolG Poligonale globale
Termico Distorsione termica
Torcente Carico torcente
Precomp. Carico da precompressione
PolL Poligonale locale

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					m	car. dist. kg/m			m	car. dist. kg/m		
						coppie torc. kg*m/m				coppie torc. kg*m/m		
Pilastro 2001												
30x50	2001	4001	Peso Proprio	UnifG	0.00	0	0	375	5.45	0	0	375
Pilastro 2002												
50x30	2002	4002	Peso Proprio	UnifG	0.00	0	0	375	5.45	0	0	375
Pilastro 2003												
30x50	2003	4003	Peso Proprio	UnifG	0.00	0	0	375	5.45	0	0	375
Pilastro 2004												
30x50	2004	4004	Peso Proprio	UnifG	0.00	0	0	375	5.45	0	0	375
Pilastro 2005												
30x50	2005	3005	Peso Proprio	UnifG	0.00	0	0	375	1.45	0	0	375
30x50	3005	4005	Peso Proprio	UnifG	0.00	0	0	375	4.00	0	0	375
Pilastro 2006												
30x50	2006	4006	Peso Proprio	UnifG	0.00	0	0	375	5.45	0	0	375
Pilastro 2007												
30x50	2007	4007	Peso Proprio	UnifG	0.00	0	0	375	5.45	0	0	375
Pilastro 2008												
30x50	2008	3008	Peso Proprio	UnifG	0.00	0	0	375	1.45	0	0	375
30x50	3008	4008	Peso Proprio	UnifG	0.00	0	0	375	4.00	0	0	375
Pilastro 2009												
30x50	2009	4009	Peso Proprio	UnifG	0.00	0	0	375	5.45	0	0	375
Pilastro 2010												
30x50	2010	4010	Peso Proprio	UnifG	0.00	0	0	375	5.45	0	0	375
Pilastro 2011												
30x50	2011	3011	Peso Proprio	UnifG	0.00	0	0	375	1.45	0	0	375
30x50	3011	4011	Peso Proprio	UnifG	0.00	0	0	375	4.00	0	0	375
Pilastro 2012												
30x50	2012	4012	Peso Proprio	UnifG	0.00	0	0	375	5.45	0	0	375
Pilastro 2013												
30x50	2013	4013	Peso Proprio	UnifG	0.00	0	0	375	5.45	0	0	375
Pilastro 2014												
30x50	2014	3014	Peso Proprio	UnifG	0.00	0	0	375	1.45	0	0	375
30x50	3014	4014	Peso Proprio	UnifG	0.00	0	0	375	4.00	0	0	375
Pilastro 2015												
30x50	2015	4015	Peso Proprio	UnifG	0.00	0	0	375	5.45	0	0	375
Pilastro 2016												
30x50	2016	4016	Peso Proprio	UnifG	0.00	0	0	375	5.45	0	0	375
Pilastro 2017												
50x30	2017	4017	Peso Proprio	UnifG	0.00	0	0	375	5.45	0	0	375
Pilastro 2018												
30x50	2018	4018	Peso Proprio	UnifG	0.00	0	0	375	5.45	0	0	375
Trave 0												
Sezione Nulla	2001	2026	muratura	UnifG	0.00	0	0	2000	4.90	0	0	2000
Sezione Nulla	2001	2026	muratura	UnifG	0.00	0	0	2000	4.90	0	0	2000

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Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Sezione Nulla	2002	2003	muratura	UnifG	0.00	0	0	2000	7.03	0	0	2000
Sezione Nulla	2002	2003	muratura	UnifG	0.00	0	0	2000	7.03	0	0	2000
Sezione Nulla	2003	2006	muratura	UnifG	0.00	0	0	2000	4.65	0	0	2000
Sezione Nulla	2003	2006	muratura	UnifG	0.00	0	0	2000	4.65	0	0	2000
Sezione Nulla	2004	2001	muratura	UnifG	0.00	0	0	2000	4.65	0	0	2000
Sezione Nulla	2004	2001	muratura	UnifG	0.00	0	0	2000	4.65	0	0	2000
Sezione Nulla	2006	2009	muratura	UnifG	0.00	0	0	2000	4.25	0	0	2000
Sezione Nulla	2006	2009	muratura	UnifG	0.00	0	0	2000	4.25	0	0	2000
Sezione Nulla	2007	2004	muratura	UnifG	0.00	0	0	2000	4.25	0	0	2000
Sezione Nulla	2007	2004	muratura	UnifG	0.00	0	0	2000	4.25	0	0	2000
Sezione Nulla	2009	2012	muratura	UnifG	0.00	0	0	2000	4.75	0	0	2000
Sezione Nulla	2009	2012	muratura	UnifG	0.00	0	0	2000	4.75	0	0	2000
Sezione Nulla	2010	2007	muratura	UnifG	0.00	0	0	2000	4.75	0	0	2000
Sezione Nulla	2010	2007	muratura	UnifG	0.00	0	0	2000	4.75	0	0	2000
Sezione Nulla	2012	2015	muratura	UnifG	0.00	0	0	2000	4.85	0	0	2000
Sezione Nulla	2012	2015	muratura	UnifG	0.00	0	0	2000	4.85	0	0	2000
Sezione Nulla	2013	2010	muratura	UnifG	0.00	0	0	2000	4.85	0	0	2000
Sezione Nulla	2013	2010	muratura	UnifG	0.00	0	0	2000	4.85	0	0	2000
Sezione Nulla	2015	2018	muratura	UnifG	0.00	0	0	2000	4.10	0	0	2000
Sezione Nulla	2015	2018	muratura	UnifG	0.00	0	0	2000	4.10	0	0	2000
Sezione Nulla	2016	2013	muratura	UnifG	0.00	0	0	2000	4.10	0	0	2000
Sezione Nulla	2016	2013	muratura	UnifG	0.00	0	0	2000	4.10	0	0	2000
Sezione Nulla	2017	2092	muratura	UnifG	0.00	0	0	2000	2.67	0	0	2000
Sezione Nulla	2017	2092	muratura	UnifG	0.00	0	0	2000	2.67	0	0	2000
Sezione Nulla	2018	2017	muratura	UnifG	0.00	0	0	2000	7.03	0	0	2000
Sezione Nulla	2018	2017	muratura	UnifG	0.00	0	0	2000	7.03	0	0	2000
Sezione Nulla	2026	2002	muratura	UnifG	0.00	0	0	2000	2.67	0	0	2000
Sezione Nulla	2026	2002	muratura	UnifG	0.00	0	0	2000	2.67	0	0	2000
Sezione Nulla	2092	2016	muratura	UnifG	0.00	0	0	2000	4.90	0	0	2000
Sezione Nulla	2092	2016	muratura	UnifG	0.00	0	0	2000	4.90	0	0	2000
Sezione Nulla	3005	3008	grigliatura	UnifG	0.00	0	0	2000	4.00	0	0	2000
Sezione Nulla	3037	3043	grigliatura	UnifG	0.00	0	0	2000	4.00	0	0	2000
Trave 301												
70x25	3071	3072	Peso Proprio	UnifG	0.00	0	0	438	4.10	0	0	438
70x25	3071	3072	permanenti	UnifG	0.00	0	0	1000	4.10	0	0	1000
Trave 401												
30x50	4001	4002	Peso Proprio	UnifG	0.00	0	0	375	7.82	0	0	375
30x50	4001	4002	Muro esterno	UnifG	0.00	0	0	1000	7.82	0	0	1000
30x50	4001	4002	Muro esterno	Torcente	0.00	-1000	0	0	7.82	-1000	0	0
30x50	4002	4003	Peso Proprio	UnifG	0.00	0	0	375	6.78	0	0	375
30x50	4002	4003	Muro esterno	Torcente	0.00	-1000	0	0	6.78	-1000	0	0
30x50	4002	4003	Muro esterno	UnifG	0.00	0	0	1000	6.78	0	0	1000
Trave 402												
30x50	4003	4006	Peso Proprio	UnifG	0.00	0	0	375	4.65	0	0	375
30x50	4003	4006	QP Solai	PolG	0.15	0	0	1193	4.65	0	0	1193
30x50	4003	4006	QV Solai	PolG	0.15	0	0	166	4.65	0	0	166

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30x50	4003	4006	QFissi Solai	PolG	0.15	0	0	663	4.65	0	0	663
30x50	4003	4006	Muro esterno	Torcente	0.00	-1000	0	0	4.65	-1000	0	0
30x50	4003	4006	Muro esterno	UnifG	0.00	0	0	1000	4.65	0	0	1000
30x50	4003	4006	neve	PolG	0.15	0	0	199	4.65	0	0	199
30x50	4006	4009	Peso Proprio	UnifG	0.00	0	0	375	4.00	0	0	375
30x50	4006	4009	QP Solai	PolG	0.00	0	0	1193	4.00	0	0	1193
30x50	4006	4009	QV Solai	PolG	0.00	0	0	166	4.00	0	0	166
30x50	4006	4009	QFissi Solai	PolG	0.00	0	0	663	4.00	0	0	663
30x50	4006	4009	Muro esterno	UnifG	0.00	0	0	1000	4.00	0	0	1000
30x50	4006	4009	Muro esterno	Torcente	0.00	-1000	0	0	4.00	-1000	0	0
30x50	4006	4009	neve	PolG	0.00	0	0	199	4.00	0	0	199
30x50	4009	4012	Peso Proprio	UnifG	0.00	0	0	375	5.25	0	0	375
30x50	4009	4012	QP Solai	PolG	0.00	0	0	1193	5.00	0	0	1193
30x50	4009	4012	QV Solai	PolG	0.00	0	0	166	5.00	0	0	166
30x50	4009	4012	QFissi Solai	PolG	0.00	0	0	663	5.00	0	0	663
30x50	4009	4012	Muro esterno	Torcente	0.00	-1000	0	0	5.25	-1000	0	0
30x50	4009	4012	Muro esterno	UnifG	0.00	0	0	1000	5.25	0	0	1000
30x50	4009	4012	neve	PolG	0.00	0	0	199	5.00	0	0	199
30x50	4012	4015	Peso Proprio	UnifG	0.00	0	0	375	4.85	0	0	375
30x50	4012	4015	QP Solai	PolG	0.00	0	0	1193	4.60	0	0	1193
30x50	4012	4015	QV Solai	PolG	0.00	0	0	166	4.60	0	0	166
30x50	4012	4015	QFissi Solai	PolG	0.00	0	0	663	4.60	0	0	663
30x50	4012	4015	Muro esterno	Torcente	0.00	-1000	0	0	4.85	-1000	0	0
30x50	4012	4015	Muro esterno	UnifG	0.00	0	0	1000	4.85	0	0	1000
30x50	4015	4018	Peso Proprio	UnifG	0.00	0	0	375	4.35	0	0	375
30x50	4015	4018	QP Solai	PolG	0.00	0	0	1193	4.20	0	0	1193
30x50	4015	4018	QV Solai	PolG	0.00	0	0	166	4.20	0	0	166
30x50	4015	4018	QFissi Solai	PolG	0.00	0	0	663	4.20	0	0	663
30x50	4015	4018	Muro esterno	Torcente	0.00	-1000	0	0	4.35	-1000	0	0
30x50	4015	4018	Muro esterno	UnifG	0.00	0	0	1000	4.35	0	0	1000
Trave 403												
50x30	4011	4010	Peso Proprio	UnifG	0.00	0	0	375	7.67	0	0	375
50x30	4012	4011	Peso Proprio	UnifG	0.00	0	0	375	6.78	0	0	375
Trave 404												
30x50	4004	4001	Peso Proprio	UnifG	0.00	0	0	375	4.65	0	0	375
30x50	4004	4001	QP Solai	PolG	0.00	0	0	1381	4.50	0	0	1381
30x50	4004	4001	QV Solai	PolG	0.00	0	0	192	4.50	0	0	192
30x50	4004	4001	QFissi Solai	PolG	0.00	0	0	767	4.50	0	0	767
30x50	4004	4001	Muro esterno	Torcente	0.00	-1000	0	0	4.65	-1000	0	0
30x50	4004	4001	Muro esterno	UnifG	0.00	0	0	1000	4.65	0	0	1000
30x50	4007	4004	Peso Proprio	UnifG	0.00	0	0	375	4.00	0	0	375
30x50	4007	4004	QP Solai	PolG	0.00	0	0	1381	4.00	0	0	1381
30x50	4007	4004	QV Solai	PolG	0.00	0	0	192	4.00	0	0	192
30x50	4007	4004	QFissi Solai	PolG	0.00	0	0	767	4.00	0	0	767
30x50	4007	4004	Muro esterno	Torcente	0.00	-1000	0	0	4.00	-1000	0	0
30x50	4007	4004	Muro esterno	UnifG	0.00	0	0	1000	4.00	0	0	1000
30x50	4010	4007	Peso Proprio	UnifG	0.00	0	0	375	5.25	0	0	375
30x50	4010	4007	QP Solai	PolG	0.25	0	0	1381	5.25	0	0	1381
30x50	4010	4007	QV Solai	PolG	0.25	0	0	192	5.25	0	0	192
30x50	4010	4007	QFissi Solai	PolG	0.25	0	0	767	5.25	0	0	767
30x50	4010	4007	Muro esterno	Torcente	0.00	-1000	0	0	5.25	-1000	0	0
30x50	4010	4007	Muro esterno	UnifG	0.00	0	0	1000	5.25	0	0	1000
30x50	4013	4010	Peso Proprio	UnifG	0.00	0	0	375	4.85	0	0	375
30x50	4013	4010	QP Solai	PolG	0.25	0	0	1381	4.85	0	0	1381
30x50	4013	4010	QV Solai	PolG	0.25	0	0	192	4.85	0	0	192
30x50	4013	4010	QFissi Solai	PolG	0.25	0	0	767	4.85	0	0	767
30x50	4013	4010	Muro esterno	UnifG	0.00	0	0	1000	4.85	0	0	1000
30x50	4013	4010	Muro esterno	Torcente	0.00	-1000	0	0	4.85	-1000	0	0
30x50	4016	4013	Peso Proprio	UnifG	0.00	0	0	375	4.35	0	0	375
30x50	4016	4013	QP Solai	PolG	0.15	0	0	1381	4.35	0	0	1381
30x50	4016	4013	QV Solai	PolG	0.15	0	0	192	4.35	0	0	192
30x50	4016	4013	QFissi Solai	PolG	0.15	0	0	767	4.35	0	0	767
30x50	4016	4013	Muro esterno	Torcente	0.00	-1000	0	0	4.35	-1000	0	0
30x50	4016	4013	Muro esterno	UnifG	0.00	0	0	1000	4.35	0	0	1000
Trave 405												
50x30	4005	4006	Peso Proprio	UnifG	0.00	0	0	375	6.78	0	0	375
50x30	4005	4004	Peso Proprio	UnifG	0.00	0	0	375	7.67	0	0	375
Trave 406												
50x30	4008	4007	Peso Proprio	UnifG	0.00	0	0	375	7.67	0	0	375
50x30	4008	4009	Peso Proprio	UnifG	0.00	0	0	375	6.78	0	0	375
Trave 407												
30x50	4002	4005	Peso Proprio	UnifG	0.00	0	0	375	4.65	0	0	375
30x50	4002	4005	QP Solai	PolG	0.15	0	0	2574	4.65	0	0	2574
30x50	4002	4005	QV Solai	PolG	0.15	0	0	357	4.65	0	0	357
30x50	4002	4005	QFissi Solai	PolG	0.15	0	0	1430	4.65	0	0	1430
30x50	4002	4005	neve	PolG	0.15	0	0	199	4.65	0	0	199

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30x50	4005	4008	Peso Proprio	UnifG	0.00	0	0	375	4.00	0	0	375
30x50	4005	4008	QP Solai	PolG	0.00	0	0	2574	4.00	0	0	2574
30x50	4005	4008	QV Solai	PolG	0.00	0	0	357	4.00	0	0	357
30x50	4005	4008	QFissi Solai	PolG	0.00	0	0	1430	4.00	0	0	1430
30x50	4005	4008	neve	PolG	0.00	0	0	199	4.00	0	0	199
30x50	4008	4011	Peso Proprio	UnifG	0.00	0	0	375	5.25	0	0	375
30x50	4008	4011	QP Solai	PolG	0.00	0	0	2574	5.00	0	0	2574
30x50	4008	4011	QV Solai	PolG	0.00	0	0	357	5.00	0	0	358
30x50	4008	4011	QFissi Solai	PolG	0.00	0	0	1430	5.00	0	0	1430
30x50	4008	4011	neve	PolG	0.00	0	0	199	5.00	0	0	199
30x50	4011	4014	Peso Proprio	UnifG	0.00	0	0	375	4.85	0	0	375
30x50	4011	4014	QP Solai	PolG	0.00	0	0	2574	4.60	0	0	2574
30x50	4011	4014	QV Solai	PolG	0.00	0	0	357	4.60	0	0	358
30x50	4011	4014	QFissi Solai	PolG	0.00	0	0	1430	4.60	0	0	1430
30x50	4014	4017	Peso Proprio	UnifG	0.00	0	0	375	4.35	0	0	375
30x50	4014	4017	QP Solai	PolG	0.00	0	0	2574	4.20	0	0	2574
30x50	4014	4017	QV Solai	PolG	0.00	0	0	357	4.20	0	0	358
30x50	4014	4017	QFissi Solai	PolG	0.00	0	0	1430	4.20	0	0	1430
Trave 408												
50x30	4014	4013	Peso Proprio	UnifG	0.00	0	0	375	7.67	0	0	375
50x30	4015	4014	Peso Proprio	UnifG	0.00	0	0	375	6.78	0	0	375
Trave 409												
30x50	4017	4016	Peso Proprio	UnifG	0.00	0	0	375	7.82	0	0	375
30x50	4017	4016	Muro esterno	Torcente	0.00	-1000	0	0	7.82	-1000	0	0
30x50	4017	4016	Muro esterno	UnifG	0.00	0	0	1000	7.82	0	0	1000
30x50	4018	4017	Peso Proprio	UnifG	0.00	0	0	375	6.78	0	0	375
30x50	4018	4017	Muro esterno	UnifG	0.00	0	0	1000	6.78	0	0	1000
30x50	4018	4017	Muro esterno	Torcente	0.00	-1000	0	0	6.78	-1000	0	0

Pareti - geometria e vincoli

Parete	Nodi	Tipo	Materiale	Criterio	N.P.	N.P.X	N.P.Y	Spess.
								m
1	2024-2027-2003-2023	Platea	C35/45	CLS Platee ND	4			0.50
2	2023-2003-2002-2022	Platea	C35/45	CLS Platee ND	28			0.50
3	2022-2002-2026-2021	Platea	C35/45	CLS Platee ND	12			0.50
4	2021-2026-2001-2020	Platea	C35/45	CLS Platee ND	20			0.50
5	2020-2001-2025-2019	Platea	C35/45	CLS Platee ND	4			0.50
6	2001-2004-2035-2025	Platea	C35/45	CLS Platee ND	20			0.50
7	2004-2007-2041-2035	Platea	C35/45	CLS Platee ND	16			0.50
8	2007-2010-2061-2041	Platea	C35/45	CLS Platee ND	20			0.50
9	2010-2013-2080-2061	Platea	C35/45	CLS Platee ND	20			0.50
10	2013-2016-2091-2080	Platea	C35/45	CLS Platee ND	16			0.50
11	2016-2095-2094-2091	Platea	C35/45	CLS Platee ND	4			0.50
12	2092-2096-2095-2016	Platea	C35/45	CLS Platee ND	20			0.50
13	2017-2097-2096-2092	Platea	C35/45	CLS Platee ND	12			0.50
14	2093-2099-2098-2018	Platea	C35/45	CLS Platee ND	4			0.50
15	2018-2098-2097-2017	Platea	C35/45	CLS Platee ND	28			0.50
16	2027-2040-2006-2003	Platea	C35/45	CLS Platee ND	20			0.50
17	2040-2046-2009-2006	Platea	C35/45	CLS Platee ND	16			0.50
18	2046-2063-2012-2009	Platea	C35/45	CLS Platee ND	20			0.50
19	2063-2081-2015-2012	Platea	C35/45	CLS Platee ND	20			0.50
20	2081-2093-2018-2015	Platea	C35/45	CLS Platee ND	16			0.50
21	2018-2017-2089-2090	Platea	C35/45	CLS Platee ND	28			0.50
22	2090-2015-2018	Platea	C35/45	CLS Platee ND	13			0.50
23	2012-2062-2054	Platea	C35/45	CLS Platee ND	31			0.50
24	2062-2014-2011	Platea	C35/45	CLS Platee ND	15			0.50
25	2015-2062-2012	Platea	C35/45	CLS Platee ND	35			0.50
26	2013-2087-2016	Platea	C35/45	CLS Platee ND	14			0.50
27	2004-2036-2007	Platea	C35/45	CLS Platee ND	51			0.50
28	2001-2026-2028	Platea	C35/45	CLS Platee ND	44			0.50
29	2009-2044-2006	Platea	C35/45	CLS Platee ND	56			0.50
30	2003-2029-2002	Platea	C35/45	CLS Platee ND	56			0.50
31	2084-2085-2088	Platea	C35/45	CLS Platee ND	21			0.50
32	2002-2028-2026	Platea	C35/45	CLS Platee ND	25			0.50
33	2037-2043-2042-2036	Platea	C35/45	CLS Platee ND	8			0.80
34	2032-2031-2028-2029	Platea	C35/45	CLS Platee ND	16			0.80
35	2033-2038-2005-2032	Platea	C35/45	CLS Platee ND	16			0.80
36	2033-2032-2029	Platea	C35/45	CLS Platee ND	9			0.80
37	2032-2005-2037-2031	Platea	C35/45	CLS Platee ND	16			0.80
38	2038-2044-2008-2005	Platea	C35/45	CLS Platee ND	16			0.80
39	2044-2050-2049-2008	Platea	C35/45	CLS Platee ND	16			0.80
40	2005-2008-2043-2037	Platea	C35/45	CLS Platee ND	16			0.80
41	2029-2028-2002	Platea	C35/45	CLS Platee ND	25			0.50
42	2001-2028-2036-2004	Platea	C35/45	CLS Platee ND	100			0.50

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Parete	Nodi	Tipo	Materiale	Criterio	N.P.	N.P.X	N.P.Y	Spess.
43	2003-2006-2029	Platea	C35/45	CLS Platee ND	69			0.50
44	2006-2033-2029	Platea	C35/45	CLS Platee ND	23			0.50
45	2006-2038-2033	Platea	C35/45	CLS Platee ND	22			0.50
46	2006-2044-2038	Platea	C35/45	CLS Platee ND	42			0.50
47	2009-2050-2044	Platea	C35/45	CLS Platee ND	27			0.50
48	4-3-2-5	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
49	6-4-5-7	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
50	8-6-7-9	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
51	10-8-9-11	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
52	12-10-11-13	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
53	14-12-13-15	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
54	16-14-15-17	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
55	18-16-17-19	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
56	20-18-19-21	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
57	22-20-21-23	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
58	24-22-23-25	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
59	26-24-25-27	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
60	28-26-27-29	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
61	30-28-29-31	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
62	32-30-31-33	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
63	3-32-33-2	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
64	5-2-2079-2077	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
65	7-5-2077-2075	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
66	9-7-2075-2073	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
67	11-9-2073-2071	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
68	13-11-2071-2068	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
69	15-13-2068-2066	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
70	17-15-2066-2064	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
71	19-17-2064-2059	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
72	21-19-2059-2065	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
73	23-21-2065-2067	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
74	25-23-2067-2069	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
75	27-25-2069-2072	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
76	29-27-2072-2074	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
77	31-29-2074-2076	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
78	33-31-2076-2078	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
79	2-33-2078-2079	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
80	53-1-2058-2070	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
81	10-12-34-35	Platea	C35/45	CLS Platee ND	8			0.40
82	6-8-36-37	Platea	C35/45	CLS Platee ND	8			0.40
83	18-20-38-39	Platea	C35/45	CLS Platee ND	9			0.40
84	4-6-37-40	Platea	C35/45	CLS Platee ND	8			0.40
85	3-4-40-41	Platea	C35/45	CLS Platee ND	8			0.40
86	12-42-34	Platea	C35/45	CLS Platee ND	3			0.40
87	14-16-43-44	Platea	C35/45	CLS Platee ND	8			0.40
88	8-10-35-36	Platea	C35/45	CLS Platee ND	8			0.40
89	16-18-39-43	Platea	C35/45	CLS Platee ND	8			0.40
90	12-14-44-42	Platea	C35/45	CLS Platee ND	8			0.40
91	30-32-45-46	Platea	C35/45	CLS Platee ND	8			0.40
92	20-22-47-38	Platea	C35/45	CLS Platee ND	8			0.40
93	22-24-48-49	Platea	C35/45	CLS Platee ND	8			0.40
94	22-49-47	Platea	C35/45	CLS Platee ND	3			0.40
95	24-26-50-48	Platea	C35/45	CLS Platee ND	8			0.40
96	26-28-51-50	Platea	C35/45	CLS Platee ND	8			0.40
97	28-30-46-51	Platea	C35/45	CLS Platee ND	8			0.40
98	52-41-40	Platea	C35/45	CLS Platee ND	8			0.40
99	32-3-41-45	Platea	C35/45	CLS Platee ND	8			0.40
100	52-40-37	Platea	C35/45	CLS Platee ND	8			0.40
101	52-43-39	Platea	C35/45	CLS Platee ND	8			0.40
102	52-44-43	Platea	C35/45	CLS Platee ND	8			0.40
103	52-39-38	Platea	C35/45	CLS Platee ND	3			0.40
104	52-42-44	Platea	C35/45	CLS Platee ND	8			0.40
105	52-37-36	Platea	C35/45	CLS Platee ND	3			0.40
106	52-36-35	Platea	C35/45	CLS Platee ND	8			0.40
107	52-35-34	Platea	C35/45	CLS Platee ND	3			0.40
108	52-34-42	Platea	C35/45	CLS Platee ND	3			0.40
109	52-38-47	Platea	C35/45	CLS Platee ND	8			0.40
110	52-47-49	Platea	C35/45	CLS Platee ND	3			0.40
111	52-51-46	Platea	C35/45	CLS Platee ND	8			0.40
112	52-50-51	Platea	C35/45	CLS Platee ND	8			0.40
113	52-48-50	Platea	C35/45	CLS Platee ND	8			0.40
114	52-46-45	Platea	C35/45	CLS Platee ND	8			0.40
115	52-49-48	Platea	C35/45	CLS Platee ND	8			0.40
116	52-45-41	Platea	C35/45	CLS Platee ND	8			0.40
117	1-19-2059-2058	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
118	2062-2011-2057	Platea	C35/45	CLS Platee ND	19			0.50

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Parete	Nodi	Tipo	Materiale	Criterio	N.P.	N.P.X	N.P.Y	Spess.
119	2062-2057-2054	Platea	C35/45	CLS Platee ND	17			0.50
120	2086-2014-2062	Platea	C35/45	CLS Platee ND	16			0.50
121	53-2070-2071-11	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
122	2007-2036-2042	Platea	C35/45	CLS Platee ND	42			0.50
123	2043-2008-2049-2048	Platea	C35/45	CLS Platee ND	16			0.80
124	2042-2043-2048-2047	Platea	C35/45	CLS Platee ND	8			0.80
125	2015-2086-2062	Platea	C35/45	CLS Platee ND	15			0.50
126	2015-2090-2086	Platea	C35/45	CLS Platee ND	9			0.50
127	2090-2089-2086	Platea	C35/45	CLS Platee ND	42			0.50
128	2089-2085-2086	Platea	C35/45	CLS Platee ND	12			0.50
129	2050-2054-2049	Platea	C35/45	CLS Platee ND	10			0.80
130	2049-2054-2057	Platea	C35/45	CLS Platee ND	12			0.80
131	2048-2049-2057	Platea	C35/45	CLS Platee ND	12			0.80
132	2048-2057-2056	Platea	C35/45	CLS Platee ND	10			0.80
133	2048-2056-2053	Platea	C35/45	CLS Platee ND	9			0.80
134	2047-2048-2053	Platea	C35/45	CLS Platee ND	7			0.80
135	2056-2057-2011-2060	Platea	C35/45	CLS Platee ND	8			0.80
136	2088-2085-2089	Platea	C35/45	CLS Platee ND	27			0.50
137	2009-2052-2050	Platea	C35/45	CLS Platee ND	28			0.50
138	2052-2054-2050	Platea	C35/45	CLS Platee ND	14			0.50
139	2012-2054-2052	Platea	C35/45	CLS Platee ND	31			0.50
140	2009-2012-2052	Platea	C35/45	CLS Platee ND	29			0.50
141	2079-2078-2084	Platea	C35/45	CLS Platee ND	8			0.50
142	2083-2079-2084	Platea	C35/45	CLS Platee ND	8			0.50
143	2083-2077-2079	Platea	C35/45	CLS Platee ND	8			0.50
144	2088-2083-2084	Platea	C35/45	CLS Platee ND	13			0.50
145	2082-2075-2077	Platea	C35/45	CLS Platee ND	8			0.50
146	2082-2077-2083	Platea	C35/45	CLS Platee ND	3			0.50
147	2013-2082-2087	Platea	C35/45	CLS Platee ND	31			0.50
148	2082-2083-2088	Platea	C35/45	CLS Platee ND	14			0.50
149	2082-2088-2087	Platea	C35/45	CLS Platee ND	43			0.50
150	2014-2085-2078	Platea	C35/45	CLS Platee ND	14			0.80
151	2085-2084-2078	Platea	C35/45	CLS Platee ND	11			0.80
152	2078-2076-2014	Platea	C35/45	CLS Platee ND	13			0.80
153	2014-2076-2074	Platea	C35/45	CLS Platee ND	10			0.80
154	2014-2074-2072-2069-2067-2011	Platea	C35/45	CLS Platee ND	68			0.80
155	1-15-13-11-53	Platea	C35/45	CLS Platee ND	27			0.50
156	2010-2058-2070-2013	Platea	C35/45	CLS Platee ND	43			0.50
157	2070-2071-2073	Platea	C35/45	CLS Platee ND	8			0.50
158	2013-2070-2073	Platea	C35/45	CLS Platee ND	11			0.50
159	2073-2075-2082	Platea	C35/45	CLS Platee ND	9			0.50
160	2013-2073-2082	Platea	C35/45	CLS Platee ND	15			0.50
161	2007-2058-2010	Platea	C35/45	CLS Platee ND	29			0.50
162	2007-2042-2047	Platea	C35/45	CLS Platee ND	28			0.50
163	2056-2060-2059	Platea	C35/45	CLS Platee ND	9			0.50
164	2053-2056-2059	Platea	C35/45	CLS Platee ND	10			0.50
165	2058-2053-2059	Platea	C35/45	CLS Platee ND	15			0.50
166	2007-2047-2053	Platea	C35/45	CLS Platee ND	24			0.50
167	2007-2053-2058	Platea	C35/45	CLS Platee ND	51			0.50
168	2067-2065-2060	Platea	C35/45	CLS Platee ND	8			0.80
169	2011-2067-2060	Platea	C35/45	CLS Platee ND	6			0.80
170	2031-2037-2036	Platea	C35/45	CLS Platee ND	8			0.80
171	2028-2031-2036	Platea	C35/45	CLS Platee ND	7			0.80
172	2087-2088-2092	Platea	C35/45	CLS Platee ND	19			0.50
173	2087-2092-2016	Platea	C35/45	CLS Platee ND	19			0.50
174	2089-2017-2088	Platea	C35/45	CLS Platee ND	14			0.50
175	2017-2092-2088	Platea	C35/45	CLS Platee ND	11			0.50
176	17-1-15	Platea	C35/45	CLS Platee ND	7			0.50
177	2086-2085-2014	Platea	C35/45	CLS Platee ND	10			0.50
178	2029-3029-3028-2028	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
179	2036-3036-3028-2028	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
180	2037-2043-3043-3037	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
181	2029-2033-3033-3029	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
182	2036-2042-3042-3036	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
183	2032-2005-3005-3032	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
184	2031-2037-3037-3031	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
185	2033-2038-3038-3033	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
186	2005-2008-3008-3005	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
187	2008-2049-3049-3008	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
188	2038-2044-3044-3038	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
189	2044-2050-3050-3044	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
190	2050-2054-3054-3050	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
191	2054-2057-3057-3054	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
192	2011-2014-3014-3011	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
193	2057-3057-3011-2011	Discreto	C35/45	CLS Muri ND	16	4	4	0.30

Parete	Nodi	Tipo	Materiale	Criterio	N.P.	N.P.X	N.P.Y	Spess.
194	2014-3014-3085-2085	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
195	2084-2085-3085-3084	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
196	2078-3078-3084-2084	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
197	3030-3034-3033-3029	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
198	3034-3039-3038-3033	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
199	3039-3045-3044-3038	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
200	3045-3051-3050-3044	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
201	3051-3055-3054-3050	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
202	2073-2075-3075-3073	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
203	2068-2071-3071-3068	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
204	2071-2073-3073-3071	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
205	2075-2077-3077-3075	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
206	2077-2079-3079-3077	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
207	2074-2072-3072-3074	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
208	2059-2064-3064-3059	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
209	2079-2078-3078-3079	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
210	2072-2069-3069-3072	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
211	2064-2066-3066-3064	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
212	2076-2074-3074-3076	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
213	2078-2076-3076-3078	Discreto	C35/45	CLS Muri ND	16	4	4	0.25
214	2060-3060-3059-2059	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
215	2058-2059-3059-3058	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
216	2070-2058-3058-3070	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
217	2070-3070-3071-2071	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
218	2042-2047-3047-3042	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
219	2043-2048-3048-3043	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
220	2053-3053-3047-2047	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
221	2053-2056-3056-3053	Discreto	C35/45	CLS Muri ND	16	4	4	0.30
222	2056-2060-3060-3056	Discreto	C35/45	CLS Muri ND	16	4	4	0.30

Muri - Carichi

Shell Indice dello shell
Cond. Condizione di carico
Tipo Tipologia di spinta
 γ Peso specifico: terreno o acqua
Ht Quota del piano di campagna
 \emptyset Angolo di attrito interno
c Coesione
 δ Angolo di attrito terreno paramento shell
 β Angolo di inclinazione del piano di campagna
 k_0 Coefficiente di spinta a riposo (quando richiesto)
 β_m Coefficiente di riduzione dell'accelerazione massima attesa al sito (quando richiesto)
Ag Accelerazione del sito a meno di 'g': quando richiesto, rappresenta il valore della accelerazione dello spettro per $T=0$, quindi comprensiva dei coefficienti di amplificazione topografica (S_T) e stratigrafica (S_S)
Q Valore del carico uniforme
Vert.1 Valore del carico nel primo vertice⁽¹⁾
Vert.2 Valore del carico nel secondo vertice⁽¹⁾
Vert.3 Valore del carico nel terzo vertice⁽¹⁾
Vert.4 Valore del carico nel quarto vertice⁽¹⁾
Hw Altezza del pelo libero dell'acqua
⁽¹⁾: Per shell con numero di vertici maggiori 4, per carichi trapezoidali, il valore del carico nei vertici e' stampato a gruppi di 4 secondo l'ordine con cui i vertici sono stati definiti

Shell 1	Cond.	Tipo	Ht	γ	\emptyset	c	δ	β	k_0	β_m	Ag
			m	kg/m ³	°	daN/cm ²	°	°			
48	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
49	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
50	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
51	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
52	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
53	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
54	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
55	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
56	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
57	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
58	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
59	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
60	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
61	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
62	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
63	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
64	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
65	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--

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Shel 1	Cond.	Tipo	Ht	γ	\emptyset	c	δ	β	k0	β_m	Ag
66	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
67	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
68	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
69	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
70	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
71	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
72	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
73	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
74	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
75	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
76	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
77	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
78	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
79	Spinta Terreno	Terreno - Riposo - Dir.Neg.	0.00	1900	--	--	--	--	0.50	--	--
80	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
117	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
178	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
179	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
181	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
182	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
183	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
184	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
185	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
186	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
188	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
192	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
202	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
203	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
204	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
205	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
206	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
207	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
208	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
209	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
210	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
211	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
212	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
213	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--
216	Spinta Terreno	Terreno - Riposo - Dir.Pos.	0.00	1900	--	--	--	--	0.50	--	--

She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
			t/mq	t/mq	t/mq	t/mq	t/mq	m	kg/mc
1	Peso Proprio	Peso Proprio kg	313						
1	accidentali	Uniforme GLOBZ	0.60						
1	permanenti	Uniforme GLOBZ	0.60						
2	Peso Proprio	Peso Proprio kg	4237						
2	accidentali	Uniforme GLOBZ	0.60						
2	permanenti	Uniforme GLOBZ	0.60						
3	Peso Proprio	Peso Proprio kg	1825						
3	accidentali	Uniforme GLOBZ	0.60						
3	permanenti	Uniforme GLOBZ	0.60						
4	Peso Proprio	Peso Proprio kg	3063						
4	accidentali	Uniforme GLOBZ	0.60						
4	permanenti	Uniforme GLOBZ	0.60						
5	Peso Proprio	Peso Proprio kg	313						
5	accidentali	Uniforme GLOBZ	0.60						
5	permanenti	Uniforme GLOBZ	0.60						
6	Peso Proprio	Peso Proprio kg	2906						
6	accidentali	Uniforme GLOBZ	0.60						
6	permanenti	Uniforme GLOBZ	0.60						
7	Peso Proprio	Peso Proprio kg	2500						
7	accidentali	Uniforme GLOBZ	0.60						
7	permanenti	Uniforme GLOBZ	0.60						
8	Peso Proprio	Peso Proprio kg	3125						
8	accidentali	Uniforme GLOBZ	0.60						
8	permanenti	Uniforme GLOBZ	0.60						
9	Peso Proprio	Peso Proprio kg	2875						
9	accidentali	Uniforme GLOBZ	0.60						
9	permanenti	Uniforme GLOBZ	0.60						
10	Peso Proprio	Peso Proprio kg	2719						
10	accidentali	Uniforme GLOBZ	0.60						
10	permanenti	Uniforme GLOBZ	0.60						
11	Peso Proprio	Peso Proprio kg	313						
11	accidentali	Uniforme GLOBZ	0.60						

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She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
11	permanenti	Uniforme GLOBZ	0.60						
12	Peso Proprio	Peso Proprio kg	3063						
12	accidentali	Uniforme GLOBZ	0.60						
12	permanenti	Uniforme GLOBZ	0.60						
13	Peso Proprio	Peso Proprio kg	1825						
13	accidentali	Uniforme GLOBZ	0.60						
13	permanenti	Uniforme GLOBZ	0.60						
14	Peso Proprio	Peso Proprio kg	313						
14	accidentali	Uniforme GLOBZ	0.60						
14	permanenti	Uniforme GLOBZ	0.60						
15	Peso Proprio	Peso Proprio kg	4237						
15	accidentali	Uniforme GLOBZ	0.60						
15	permanenti	Uniforme GLOBZ	0.60						
16	Peso Proprio	Peso Proprio kg	2906						
16	accidentali	Uniforme GLOBZ	0.60						
16	permanenti	Uniforme GLOBZ	0.60						
17	Peso Proprio	Peso Proprio kg	2500						
17	accidentali	Uniforme GLOBZ	0.60						
17	permanenti	Uniforme GLOBZ	0.60						
18	Peso Proprio	Peso Proprio kg	3125						
18	accidentali	Uniforme GLOBZ	0.60						
18	permanenti	Uniforme GLOBZ	0.60						
19	Peso Proprio	Peso Proprio kg	2875						
19	accidentali	Uniforme GLOBZ	0.60						
19	permanenti	Uniforme GLOBZ	0.60						
20	Peso Proprio	Peso Proprio kg	2719						
20	accidentali	Uniforme GLOBZ	0.60						
20	permanenti	Uniforme GLOBZ	0.60						
21	Peso Proprio	Peso Proprio kg	5530						
21	accidentali	Uniforme GLOBZ	0.60						
21	spinta acqua	Idrostatico - Negativo						0.00	1100
21	permanenti	Uniforme GLOBZ	0.60						
22	Peso Proprio	Peso Proprio kg	6253						
22	accidentali	Uniforme GLOBZ	0.60						
22	permanenti	Uniforme GLOBZ	0.60						
23	Peso Proprio	Peso Proprio kg	5218						
23	accidentali	Uniforme GLOBZ	0.60						
23	permanenti	Uniforme GLOBZ	0.60						
24	Peso Proprio	Peso Proprio kg	9574						
24	accidentali	Uniforme GLOBZ	0.60						
24	permanenti	Uniforme GLOBZ	0.60						
25	Peso Proprio	Peso Proprio kg	9488						
25	accidentali	Uniforme GLOBZ	0.60						
25	permanenti	Uniforme GLOBZ	0.60						
26	Peso Proprio	Peso Proprio kg	544						
26	accidentali	Uniforme GLOBZ	0.60						
26	permanenti	Uniforme GLOBZ	0.60						
27	Peso Proprio	Peso Proprio kg	12250						
27	accidentali	Uniforme GLOBZ	0.60						
27	permanenti	Uniforme GLOBZ	0.60						
28	Peso Proprio	Peso Proprio kg	8177						
28	accidentali	Uniforme GLOBZ	0.60						
28	permanenti	Uniforme GLOBZ	0.60						
29	Peso Proprio	Peso Proprio kg	12700						
29	accidentali	Uniforme GLOBZ	0.60						
29	permanenti	Uniforme GLOBZ	0.60						
30	Peso Proprio	Peso Proprio kg	11314						
30	accidentali	Uniforme GLOBZ	0.60						
30	permanenti	Uniforme GLOBZ	0.60						
31	Peso Proprio	Peso Proprio kg	4613						
31	accidentali	Uniforme GLOBZ	0.60						
31	permanenti	Uniforme GLOBZ	0.60						
32	Peso Proprio	Peso Proprio kg	4873						
32	accidentali	Uniforme GLOBZ	0.60						
32	permanenti	Uniforme GLOBZ	0.60						
33	Peso Proprio	Peso Proprio kg	10160						
33	accidentali	Uniforme GLOBZ	0.60						
33	spinta acqua	Idrostatico - Negativo						0.00	1100
33	permanenti	Uniforme GLOBZ	0.60						
34	Peso Proprio	Peso Proprio kg	8218						
34	accidentali	Uniforme GLOBZ	0.60						
34	spinta acqua	Idrostatico - Negativo						0.00	1100
34	permanenti	Uniforme GLOBZ	0.60						
35	Peso Proprio	Peso Proprio kg	2170						
35	accidentali	Uniforme GLOBZ	0.60						

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She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
35	spinta acqua	Idrostatico - Negativo						0.00	1100
35	permanent	Uniforme GLOBZ	0.60						
36	Peso Proprio	Peso Proprio kg	1984						
36	accidentali	Uniforme GLOBZ	0.60						
36	spinta acqua	Idrostatico - Negativo						0.00	1100
36	permanent	Uniforme GLOBZ	0.60						
37	Peso Proprio	Peso Proprio kg	2520						
37	accidentali	Uniforme GLOBZ	0.60						
37	spinta acqua	Idrostatico - Negativo						0.00	1100
37	permanent	Uniforme GLOBZ	0.60						
38	Peso Proprio	Peso Proprio kg	12400						
38	accidentali	Uniforme GLOBZ	0.60						
38	spinta acqua	Idrostatico - Negativo						0.00	1100
38	permanent	Uniforme GLOBZ	0.60						
39	Peso Proprio	Peso Proprio kg	4712						
39	accidentali	Uniforme GLOBZ	0.60						
39	permanent	Uniforme GLOBZ	0.60						
40	Peso Proprio	Peso Proprio kg	14400						
40	accidentali	Uniforme GLOBZ	0.60						
40	permanent	Uniforme GLOBZ	0.60						
41	Peso Proprio	Peso Proprio kg	7710						
41	accidentali	Uniforme GLOBZ	0.60						
41	permanent	Uniforme GLOBZ	0.60						
42	Peso Proprio	Peso Proprio kg	20304						
42	accidentali	Uniforme GLOBZ	0.60						
42	permanent	Uniforme GLOBZ	0.60						
43	Peso Proprio	Peso Proprio kg	14764						
43	accidentali	Uniforme GLOBZ	0.60						
43	permanent	Uniforme GLOBZ	0.60						
44	Peso Proprio	Peso Proprio kg	4064						
44	accidentali	Uniforme GLOBZ	0.60						
44	permanent	Uniforme GLOBZ	0.60						
45	Peso Proprio	Peso Proprio kg	2222						
45	accidentali	Uniforme GLOBZ	0.60						
45	permanent	Uniforme GLOBZ	0.60						
46	Peso Proprio	Peso Proprio kg	12700						
46	accidentali	Uniforme GLOBZ	0.60						
46	permanent	Uniforme GLOBZ	0.60						
47	Peso Proprio	Peso Proprio kg	4826						
47	accidentali	Uniforme GLOBZ	0.60						
47	permanent	Uniforme GLOBZ	0.60						
48	Peso Proprio	Peso Proprio kg	573						
48	spinta acqua	Idrostatico - Negativo						0.00	1100
49	Peso Proprio	Peso Proprio kg	529						
49	spinta acqua	Idrostatico - Negativo						0.00	1100
50	Peso Proprio	Peso Proprio kg	529						
50	spinta acqua	Idrostatico - Negativo						0.00	1100
51	Peso Proprio	Peso Proprio kg	573						
51	spinta acqua	Idrostatico - Negativo						0.00	1100
52	Peso Proprio	Peso Proprio kg	573						
52	spinta acqua	Idrostatico - Negativo						0.00	1100
53	Peso Proprio	Peso Proprio kg	529						
53	spinta acqua	Idrostatico - Negativo						0.00	1100
54	Peso Proprio	Peso Proprio kg	529						
54	spinta acqua	Idrostatico - Negativo						0.00	1100
55	Peso Proprio	Peso Proprio kg	573						
55	spinta acqua	Idrostatico - Negativo						0.00	1100
56	Peso Proprio	Peso Proprio kg	573						
56	spinta acqua	Idrostatico - Negativo						0.00	1100
57	Peso Proprio	Peso Proprio kg	529						
57	spinta acqua	Idrostatico - Negativo						0.00	1100
58	Peso Proprio	Peso Proprio kg	529						
58	spinta acqua	Idrostatico - Negativo						0.00	1100
59	Peso Proprio	Peso Proprio kg	573						
59	spinta acqua	Idrostatico - Negativo						0.00	1100
60	Peso Proprio	Peso Proprio kg	573						
60	spinta acqua	Idrostatico - Negativo						0.00	1100
61	Peso Proprio	Peso Proprio kg	529						
61	spinta acqua	Idrostatico - Negativo						0.00	1100
62	Peso Proprio	Peso Proprio kg	529						
62	spinta acqua	Idrostatico - Negativo						0.00	1100
63	Peso Proprio	Peso Proprio kg	573						
63	spinta acqua	Idrostatico - Negativo						0.00	1100
64	Peso Proprio	Peso Proprio kg	793						
64	spinta acqua	Idrostatico - Negativo						0.00	1100

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She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
65	Peso Proprio	Peso Proprio kg	732						
65	spinta acqua	Idrostatico - Negativo						0.00	1100
66	Peso Proprio	Peso Proprio kg	732						
66	spinta acqua	Idrostatico - Negativo						0.00	1100
67	Peso Proprio	Peso Proprio kg	793						
67	spinta acqua	Idrostatico - Negativo						0.00	1100
68	Peso Proprio	Peso Proprio kg	793						
68	spinta acqua	Idrostatico - Negativo						0.00	1100
69	Peso Proprio	Peso Proprio kg	732						
69	spinta acqua	Idrostatico - Negativo						0.00	1100
70	Peso Proprio	Peso Proprio kg	732						
70	spinta acqua	Idrostatico - Negativo						0.00	1100
71	Peso Proprio	Peso Proprio kg	793						
71	spinta acqua	Idrostatico - Negativo						0.00	1100
72	Peso Proprio	Peso Proprio kg	793						
72	spinta acqua	Idrostatico - Negativo						0.00	1100
73	Peso Proprio	Peso Proprio kg	732						
73	spinta acqua	Idrostatico - Negativo						0.00	1100
74	Peso Proprio	Peso Proprio kg	732						
74	spinta acqua	Idrostatico - Negativo						0.00	1100
75	Peso Proprio	Peso Proprio kg	793						
75	spinta acqua	Idrostatico - Negativo						0.00	1100
76	Peso Proprio	Peso Proprio kg	793						
76	spinta acqua	Idrostatico - Negativo						0.00	1100
77	Peso Proprio	Peso Proprio kg	732						
77	spinta acqua	Idrostatico - Negativo						0.00	1100
78	Peso Proprio	Peso Proprio kg	732						
78	spinta acqua	Idrostatico - Negativo						0.00	1100
79	Peso Proprio	Peso Proprio kg	793						
79	spinta acqua	Idrostatico - Negativo						0.00	1100
80	Peso Proprio	Peso Proprio kg	2383						
80	spinta acqua	Idrostatico - Negativo						0.00	1100
81	Peso Proprio	Peso Proprio kg	625						
81	spinta acqua	Idrostatico - Positivo						0.00	1100
81	permanenti	Uniforme GLOBZ	2.00						
82	Peso Proprio	Peso Proprio kg	589						
82	spinta acqua	Idrostatico - Positivo						0.00	1100
82	permanenti	Uniforme GLOBZ	2.00						
83	Peso Proprio	Peso Proprio kg	617						
83	spinta acqua	Idrostatico - Positivo						0.00	1100
83	permanenti	Uniforme GLOBZ	2.00						
84	Peso Proprio	Peso Proprio kg	582						
84	spinta acqua	Idrostatico - Positivo						0.00	1100
84	permanenti	Uniforme GLOBZ	2.00						
85	Peso Proprio	Peso Proprio kg	617						
85	spinta acqua	Idrostatico - Positivo						0.00	1100
85	permanenti	Uniforme GLOBZ	2.00						
86	Peso Proprio	Peso Proprio kg	167						
86	spinta acqua	Idrostatico - Positivo						0.00	1100
86	permanenti	Uniforme GLOBZ	2.00						
87	Peso Proprio	Peso Proprio kg	582						
87	spinta acqua	Idrostatico - Positivo						0.00	1100
87	permanenti	Uniforme GLOBZ	2.00						
88	Peso Proprio	Peso Proprio kg	611						
88	spinta acqua	Idrostatico - Positivo						0.00	1100
88	permanenti	Uniforme GLOBZ	2.00						
89	Peso Proprio	Peso Proprio kg	617						
89	spinta acqua	Idrostatico - Positivo						0.00	1100
89	permanenti	Uniforme GLOBZ	2.00						
90	Peso Proprio	Peso Proprio kg	589						
90	spinta acqua	Idrostatico - Positivo						0.00	1100
90	permanenti	Uniforme GLOBZ	2.00						
91	Peso Proprio	Peso Proprio kg	582						
91	spinta acqua	Idrostatico - Positivo						0.00	1100
91	permanenti	Uniforme GLOBZ	2.00						
92	Peso Proprio	Peso Proprio kg	582						
92	spinta acqua	Idrostatico - Positivo						0.00	1100
92	permanenti	Uniforme GLOBZ	2.00						
93	Peso Proprio	Peso Proprio kg	576						
93	spinta acqua	Idrostatico - Positivo						0.00	1100
93	permanenti	Uniforme GLOBZ	2.00						
94	Peso Proprio	Peso Proprio kg	179						
94	spinta acqua	Idrostatico - Positivo						0.00	1100
94	permanenti	Uniforme GLOBZ	2.00						
95	Peso Proprio	Peso Proprio kg	625						

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She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
95	spinta acqua	Idrostatico - Positivo						0.00	1100
95	permanentil	Uniforme GLOBZ	2.00						
96	Peso Proprio	Peso Proprio kg	611						
96	spinta acqua	Idrostatico - Positivo						0.00	1100
96	permanentil	Uniforme GLOBZ	2.00						
97	Peso Proprio	Peso Proprio kg	589						
97	spinta acqua	Idrostatico - Positivo						0.00	1100
97	permanentil	Uniforme GLOBZ	2.00						
98	Peso Proprio	Peso Proprio kg	131						
98	spinta acqua	Idrostatico - Positivo						0.00	1100
98	permanentil	Uniforme GLOBZ	2.00						
99	Peso Proprio	Peso Proprio kg	617						
99	spinta acqua	Idrostatico - Positivo						0.00	1100
99	permanentil	Uniforme GLOBZ	2.00						
100	Peso Proprio	Peso Proprio kg	131						
100	spinta acqua	Idrostatico - Positivo						0.00	1100
100	permanentil	Uniforme GLOBZ	2.00						
101	Peso Proprio	Peso Proprio kg	131						
101	spinta acqua	Idrostatico - Positivo						0.00	1100
101	permanentil	Uniforme GLOBZ	2.00						
102	Peso Proprio	Peso Proprio kg	131						
102	spinta acqua	Idrostatico - Positivo						0.00	1100
102	permanentil	Uniforme GLOBZ	2.00						
103	Peso Proprio	Peso Proprio kg	131						
103	spinta acqua	Idrostatico - Positivo						0.00	1100
103	permanentil	Uniforme GLOBZ	2.00						
104	Peso Proprio	Peso Proprio kg	131						
104	spinta acqua	Idrostatico - Positivo						0.00	1100
104	permanentil	Uniforme GLOBZ	2.00						
105	Peso Proprio	Peso Proprio kg	131						
105	spinta acqua	Idrostatico - Positivo						0.00	1100
105	permanentil	Uniforme GLOBZ	2.00						
106	Peso Proprio	Peso Proprio kg	131						
106	spinta acqua	Idrostatico - Positivo						0.00	1100
106	permanentil	Uniforme GLOBZ	2.00						
107	Peso Proprio	Peso Proprio kg	131						
107	spinta acqua	Idrostatico - Positivo						0.00	1100
107	permanentil	Uniforme GLOBZ	2.00						
108	Peso Proprio	Peso Proprio kg	131						
108	spinta acqua	Idrostatico - Positivo						0.00	1100
108	permanentil	Uniforme GLOBZ	2.00						
109	Peso Proprio	Peso Proprio kg	131						
109	spinta acqua	Idrostatico - Positivo						0.00	1100
109	permanentil	Uniforme GLOBZ	2.00						
110	Peso Proprio	Peso Proprio kg	131						
110	spinta acqua	Idrostatico - Positivo						0.00	1100
110	permanentil	Uniforme GLOBZ	2.00						
111	Peso Proprio	Peso Proprio kg	131						
111	spinta acqua	Idrostatico - Positivo						0.00	1100
111	permanentil	Uniforme GLOBZ	2.00						
112	Peso Proprio	Peso Proprio kg	131						
112	spinta acqua	Idrostatico - Positivo						0.00	1100
112	permanentil	Uniforme GLOBZ	2.00						
113	Peso Proprio	Peso Proprio kg	131						
113	spinta acqua	Idrostatico - Positivo						0.00	1100
113	permanentil	Uniforme GLOBZ	2.00						
114	Peso Proprio	Peso Proprio kg	131						
114	spinta acqua	Idrostatico - Positivo						0.00	1100
114	permanentil	Uniforme GLOBZ	2.00						
115	Peso Proprio	Peso Proprio kg	131						
115	spinta acqua	Idrostatico - Positivo						0.00	1100
115	permanentil	Uniforme GLOBZ	2.00						
116	Peso Proprio	Peso Proprio kg	131						
116	spinta acqua	Idrostatico - Positivo						0.00	1100
116	permanentil	Uniforme GLOBZ	2.00						
117	Peso Proprio	Peso Proprio kg	3278						
118	Peso Proprio	Peso Proprio kg	3392						
118	accidentali	Uniforme GLOBZ	0.60						
118	permanentil	Uniforme GLOBZ	0.60						
119	Peso Proprio	Peso Proprio kg	3452						
119	accidentali	Uniforme GLOBZ	0.60						
119	permanentil	Uniforme GLOBZ	0.60						
120	Peso Proprio	Peso Proprio kg	10186						
120	accidentali	Uniforme GLOBZ	0.60						
120	permanentil	Uniforme GLOBZ	0.60						

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She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
121	Peso Proprio	Peso Proprio kg	895						
122	Peso Proprio	Peso Proprio kg	12250						
122	accidentali	Uniforme GLOBZ	0.60						
122	permanenti	Uniforme GLOBZ	0.60						
123	Peso Proprio	Peso Proprio kg	5472						
123	accidentali	Uniforme GLOBZ	0.60						
123	permanenti	Uniforme GLOBZ	0.60						
124	Peso Proprio	Peso Proprio kg	3861						
124	accidentali	Uniforme GLOBZ	0.60						
124	permanenti	Uniforme GLOBZ	0.60						
125	Peso Proprio	Peso Proprio kg	11983						
125	accidentali	Uniforme GLOBZ	0.60						
125	permanenti	Uniforme GLOBZ	0.60						
126	Peso Proprio	Peso Proprio kg	6863						
126	accidentali	Uniforme GLOBZ	0.60						
126	accidentali	Uniforme GLOBZ	0.60						
126	permanenti	Uniforme GLOBZ	0.60						
127	Peso Proprio	Peso Proprio kg	6239						
127	accidentali	Uniforme GLOBZ	0.60						
127	permanenti	Uniforme GLOBZ	0.60						
128	Peso Proprio	Peso Proprio kg	5444						
128	accidentali	Uniforme GLOBZ	0.60						
128	permanenti	Uniforme GLOBZ	0.60						
129	Peso Proprio	Peso Proprio kg	1472						
129	accidentali	Uniforme GLOBZ	0.60						
129	permanenti	Uniforme GLOBZ	0.60						
130	Peso Proprio	Peso Proprio kg	2867						
130	accidentali	Uniforme GLOBZ	0.60						
130	permanenti	Uniforme GLOBZ	0.60						
131	Peso Proprio	Peso Proprio kg	3330						
131	accidentali	Uniforme GLOBZ	0.60						
131	permanenti	Uniforme GLOBZ	0.60						
132	Peso Proprio	Peso Proprio kg	2627						
132	accidentali	Uniforme GLOBZ	0.60						
132	permanenti	Uniforme GLOBZ	0.60						
133	Peso Proprio	Peso Proprio kg	2711						
133	accidentali	Uniforme GLOBZ	0.60						
133	permanenti	Uniforme GLOBZ	0.60						
134	Peso Proprio	Peso Proprio kg	1206						
134	accidentali	Uniforme GLOBZ	0.60						
134	permanenti	Uniforme GLOBZ	0.60						
135	Peso Proprio	Peso Proprio kg	4501						
135	accidentali	Uniforme GLOBZ	0.60						
135	permanenti	Uniforme GLOBZ	0.60						
136	Peso Proprio	Peso Proprio kg	6907						
136	accidentali	Uniforme GLOBZ	0.60						
136	permanenti	Uniforme GLOBZ	0.60						
137	Peso Proprio	Peso Proprio kg	5428						
137	accidentali	Uniforme GLOBZ	0.60						
137	permanenti	Uniforme GLOBZ	0.60						
138	Peso Proprio	Peso Proprio kg	1746						
138	accidentali	Uniforme GLOBZ	0.60						
138	permanenti	Uniforme GLOBZ	0.60						
139	Peso Proprio	Peso Proprio kg	5030						
139	accidentali	Uniforme GLOBZ	0.60						
139	permanenti	Uniforme GLOBZ	0.60						
140	Peso Proprio	Peso Proprio kg	6688						
140	accidentali	Uniforme GLOBZ	0.60						
140	permanenti	Uniforme GLOBZ	0.60						
141	Peso Proprio	Peso Proprio kg	678						
141	accidentali	Uniforme GLOBZ	0.60						
141	permanenti	Uniforme GLOBZ	0.60						
142	Peso Proprio	Peso Proprio kg	921						
142	accidentali	Uniforme GLOBZ	0.60						
142	permanenti	Uniforme GLOBZ	0.60						
143	Peso Proprio	Peso Proprio kg	488						
143	accidentali	Uniforme GLOBZ	0.60						
143	permanenti	Uniforme GLOBZ	0.60						
144	Peso Proprio	Peso Proprio kg	2896						
144	accidentali	Uniforme GLOBZ	0.60						
144	permanenti	Uniforme GLOBZ	0.60						
145	Peso Proprio	Peso Proprio kg	642						
145	accidentali	Uniforme GLOBZ	0.60						
145	permanenti	Uniforme GLOBZ	0.60						
146	Peso Proprio	Peso Proprio kg	638						

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146	accidentali	Uniforme GLOBZ	0.60						
146	permanenti	Uniforme GLOBZ	0.60						
147	Peso Proprio	Peso Proprio kg	5930						
147	accidentali	Uniforme GLOBZ	0.60						
147	permanenti	Uniforme GLOBZ	0.60						
148	Peso Proprio	Peso Proprio kg	2065						
148	accidentali	Uniforme GLOBZ	0.60						
148	permanenti	Uniforme GLOBZ	0.60						
149	Peso Proprio	Peso Proprio kg	9517						
149	accidentali	Uniforme GLOBZ	0.60						
149	permanenti	Uniforme GLOBZ	0.60						
150	Peso Proprio	Peso Proprio kg	1425						
150	accidentali	Uniforme GLOBZ	0.60						
150	permanenti	Uniforme GLOBZ	0.60						
151	Peso Proprio	Peso Proprio kg	3600						
151	accidentali	Uniforme GLOBZ	0.60						
151	permanenti	Uniforme GLOBZ	0.60						
152	Peso Proprio	Peso Proprio kg	1469						
152	accidentali	Uniforme GLOBZ	0.60						
152	permanenti	Uniforme GLOBZ	0.60						
153	Peso Proprio	Peso Proprio kg	1703						
153	accidentali	Uniforme GLOBZ	0.60						
153	permanenti	Uniforme GLOBZ	0.60						
154	Peso Proprio	Peso Proprio kg	10746						
154	accidentali	Uniforme GLOBZ	0.60						
154	permanenti	Uniforme GLOBZ	0.60						
155	Peso Proprio	Peso Proprio kg	2387						
156	Peso Proprio	Peso Proprio kg	7398						
156	accidentali	Uniforme GLOBZ	0.60						
156	permanenti	Uniforme GLOBZ	0.60						
157	Peso Proprio	Peso Proprio kg	375						
157	accidentali	Uniforme GLOBZ	0.60						
157	permanenti	Uniforme GLOBZ	0.60						
158	Peso Proprio	Peso Proprio kg	2551						
158	accidentali	Uniforme GLOBZ	0.60						
158	permanenti	Uniforme GLOBZ	0.60						
159	Peso Proprio	Peso Proprio kg	442						
159	accidentali	Uniforme GLOBZ	0.60						
159	permanenti	Uniforme GLOBZ	0.60						
160	Peso Proprio	Peso Proprio kg	3535						
160	accidentali	Uniforme GLOBZ	0.60						
160	permanenti	Uniforme GLOBZ	0.60						
161	Peso Proprio	Peso Proprio kg	5563						
161	accidentali	Uniforme GLOBZ	0.60						
161	permanenti	Uniforme GLOBZ	0.60						
162	Peso Proprio	Peso Proprio kg	4655						
162	accidentali	Uniforme GLOBZ	0.60						
162	permanenti	Uniforme GLOBZ	0.60						
163	Peso Proprio	Peso Proprio kg	1877						
163	accidentali	Uniforme GLOBZ	0.60						
163	permanenti	Uniforme GLOBZ	0.60						
164	Peso Proprio	Peso Proprio kg	2685						
164	accidentali	Uniforme GLOBZ	0.60						
164	permanenti	Uniforme GLOBZ	0.60						
165	Peso Proprio	Peso Proprio kg	4301						
165	accidentali	Uniforme GLOBZ	0.60						
165	permanenti	Uniforme GLOBZ	0.60						
166	Peso Proprio	Peso Proprio kg	2909						
166	accidentali	Uniforme GLOBZ	0.60						
166	permanenti	Uniforme GLOBZ	0.60						
167	Peso Proprio	Peso Proprio kg	12289						
167	accidentali	Uniforme GLOBZ	0.60						
167	permanenti	Uniforme GLOBZ	0.60						
168	Peso Proprio	Peso Proprio kg	577						
168	accidentali	Uniforme GLOBZ	0.60						
168	permanenti	Uniforme GLOBZ	0.60						
169	Peso Proprio	Peso Proprio kg	897						
169	accidentali	Uniforme GLOBZ	0.60						
169	permanenti	Uniforme GLOBZ	0.60						
170	Peso Proprio	Peso Proprio kg	889						
170	accidentali	Uniforme GLOBZ	0.60						
170	permanenti	Uniforme GLOBZ	0.60						
171	Peso Proprio	Peso Proprio kg	2515						
171	accidentali	Uniforme GLOBZ	0.60						
171	permanenti	Uniforme GLOBZ	0.60						

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She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
172	Peso Proprio	Peso Proprio kg	2791						
172	accidentali	Uniforme GLOBZ	0.60						
172	permanenti	Uniforme GLOBZ	0.60						
173	Peso Proprio	Peso Proprio kg	2909						
173	accidentali	Uniforme GLOBZ	0.60						
173	permanenti	Uniforme GLOBZ	0.60						
174	Peso Proprio	Peso Proprio kg	2056						
174	accidentali	Uniforme GLOBZ	0.60						
174	permanenti	Uniforme GLOBZ	0.60						
175	Peso Proprio	Peso Proprio kg	1734						
175	accidentali	Uniforme GLOBZ	0.60						
175	permanenti	Uniforme GLOBZ	0.60						
176	Peso Proprio	Peso Proprio kg	551						
177	Peso Proprio	Peso Proprio kg	1031						
177	accidentali	Uniforme GLOBZ	0.60						
177	permanenti	Uniforme GLOBZ	0.60						
178	Peso Proprio	Peso Proprio kg	5024						
178	spinta acqua	Idrostatico - Negativo						0.40	1100
178	spinta acqua	Idrostatico - Negativo						0.00	1100
179	Peso Proprio	Peso Proprio kg	2153						
179	spinta acqua	Idrostatico - Negativo						0.00	1100
179	spinta acqua	Idrostatico - Positivo						0.40	1100
180	Peso Proprio	Peso Proprio kg	4350						
180	spinta acqua	Idrostatico - Negativo						0.00	1100
180	spinta acqua	Idrostatico - Positivo						0.40	1100
181	Peso Proprio	Peso Proprio kg	1392						
181	spinta acqua	Idrostatico - Negativo						0.00	1100
181	spinta acqua	Idrostatico - Negativo						0.40	1100
182	Peso Proprio	Peso Proprio kg	4350						
182	spinta acqua	Idrostatico - Negativo						0.00	1100
182	spinta acqua	Idrostatico - Positivo						0.40	1100
183	Peso Proprio	Peso Proprio kg	1015						
183	spinta acqua	Idrostatico - Positivo						0.40	1100
183	spinta acqua	Idrostatico - Negativo						0.00	1100
184	Peso Proprio	Peso Proprio kg	761						
184	spinta acqua	Idrostatico - Positivo						0.40	1100
184	spinta acqua	Idrostatico - Negativo						0.00	1100
185	Peso Proprio	Peso Proprio kg	761						
185	spinta acqua	Idrostatico - Negativo						0.00	1100
185	spinta acqua	Idrostatico - Negativo						0.40	1100
186	Peso Proprio	Peso Proprio kg	5800						
186	spinta acqua	Idrostatico - Negativo						0.00	1100
186	spinta acqua	Idrostatico - Positivo						0.40	1100
187	Peso Proprio	Peso Proprio kg	2204						
187	spinta acqua	Idrostatico - Positivo						0.40	1100
188	Peso Proprio	Peso Proprio kg	4350						
188	spinta acqua	Idrostatico - Negativo						0.40	1100
188	spinta acqua	Idrostatico - Negativo						0.00	1100
189	Peso Proprio	Peso Proprio kg	1653						
189	spinta acqua	Idrostatico - Negativo						0.40	1100
190	Peso Proprio	Peso Proprio kg	1033						
190	spinta acqua	Idrostatico - Negativo						0.40	1100
191	Peso Proprio	Peso Proprio kg	1949						
191	spinta acqua	Idrostatico - Negativo						0.40	1100
192	Peso Proprio	Peso Proprio kg	5002						
192	spinta acqua	Idrostatico - Negativo						0.00	1100
192	spinta acqua	Idrostatico - Negativo						0.40	1100
193	Peso Proprio	Peso Proprio kg	1773						
193	spinta acqua	Idrostatico - Positivo						0.40	1100
194	Peso Proprio	Peso Proprio kg	598						
194	spinta acqua	Idrostatico - Positivo						0.40	1100
195	Peso Proprio	Peso Proprio kg	2817						
195	spinta acqua	Idrostatico - Positivo						0.40	1100
196	Peso Proprio	Peso Proprio kg	1512						
196	spinta acqua	Idrostatico - Positivo						0.40	1100
197	Peso Proprio	Peso Proprio kg	448						
197	accidentali	Uniforme GLOBZ	0.60						
198	Peso Proprio	Peso Proprio kg	245						
198	accidentali	Uniforme GLOBZ	0.60						
199	Peso Proprio	Peso Proprio kg	1400						
199	accidentali	Uniforme GLOBZ	0.60						
200	Peso Proprio	Peso Proprio kg	532						
200	accidentali	Uniforme GLOBZ	0.60						
201	Peso Proprio	Peso Proprio kg	332						
201	accidentali	Uniforme GLOBZ	0.60						

She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
202	Peso Proprio	Peso Proprio kg	685						
202	spinta acqua	Idrostatico - Negativo						0.00	1100
202	spinta acqua	Idrostatico - Positivo						0.40	1100
203	Peso Proprio	Peso Proprio kg	742						
203	spinta acqua	Idrostatico - Positivo						0.40	1100
203	spinta acqua	Idrostatico - Negativo						0.00	1100
204	Peso Proprio	Peso Proprio kg	742						
204	spinta acqua	Idrostatico - Negativo						0.00	1100
204	spinta acqua	Idrostatico - Positivo						0.40	1100
205	Peso Proprio	Peso Proprio kg	685						
205	spinta acqua	Idrostatico - Positivo						0.40	1100
205	spinta acqua	Idrostatico - Negativo						0.00	1100
206	Peso Proprio	Peso Proprio kg	742						
206	spinta acqua	Idrostatico - Negativo						0.00	1100
206	spinta acqua	Idrostatico - Positivo						0.40	1100
207	Peso Proprio	Peso Proprio kg	742						
207	spinta acqua	Idrostatico - Positivo						0.40	1100
207	spinta acqua	Idrostatico - Negativo						0.00	1100
208	Peso Proprio	Peso Proprio kg	742						
208	spinta acqua	Idrostatico - Positivo						0.40	1100
208	spinta acqua	Idrostatico - Negativo						0.00	1100
209	Peso Proprio	Peso Proprio kg	742						
209	spinta acqua	Idrostatico - Negativo						0.00	1100
209	spinta acqua	Idrostatico - Positivo						0.40	1100
210	Peso Proprio	Peso Proprio kg	742						
210	spinta acqua	Idrostatico - Positivo						0.40	1100
210	spinta acqua	Idrostatico - Negativo						0.00	1100
211	Peso Proprio	Peso Proprio kg	685						
211	spinta acqua	Idrostatico - Negativo						0.00	1100
211	spinta acqua	Idrostatico - Positivo						0.40	1100
212	Peso Proprio	Peso Proprio kg	685						
212	spinta acqua	Idrostatico - Negativo						0.00	1100
212	spinta acqua	Idrostatico - Positivo						0.40	1100
213	Peso Proprio	Peso Proprio kg	685						
213	spinta acqua	Idrostatico - Negativo						0.00	1100
213	spinta acqua	Idrostatico - Positivo						0.40	1100
214	Peso Proprio	Peso Proprio kg	2121						
214	spinta acqua	Idrostatico - Negativo						0.40	1100
215	Peso Proprio	Peso Proprio kg	3067						
215	spinta acqua	Idrostatico - Negativo						0.40	1100
216	Peso Proprio	Peso Proprio kg	2229						
216	spinta acqua	Idrostatico - Negativo						0.40	1100
216	spinta acqua	Idrostatico - Negativo						0.00	1100
217	Peso Proprio	Peso Proprio kg	837						
217	spinta acqua	Idrostatico - Negativo						0.40	1100
218	Peso Proprio	Peso Proprio kg	1653						
218	spinta acqua	Idrostatico - Positivo						0.40	1100
219	Peso Proprio	Peso Proprio kg	1653						
219	spinta acqua	Idrostatico - Positivo						0.40	1100
220	Peso Proprio	Peso Proprio kg	1033						
220	spinta acqua	Idrostatico - Positivo						0.40	1100
221	Peso Proprio	Peso Proprio kg	2044						
221	spinta acqua	Idrostatico - Positivo						0.40	1100
222	Peso Proprio	Peso Proprio kg	1675						
222	spinta acqua	Idrostatico - Positivo						0.40	1100

Tabella solai tipo

Sol.N°	Descrizione	Spessore	QP	QF	QVar.	ψ_0	ψ_1	ψ_2	Luce netta	Def	%QX	%QY
		m	t/mq	t/mq	t/mq							
1	Copertura	0.30	0.36	0.20	0.05	0.00	0.00	0.00	No	No	100	0

Dati solai

Solaio n°	Nodi	Tipo
1	4004-4001-4002-4005	Copertura
1	4005-4002-4003-4006	Copertura
2	4007-4004-4005-4008	Copertura
2	4008-4005-4006-4009	Copertura
3	4011-4008-4009-4012	Copertura
3	4010-4007-4008-4011	Copertura
4	4014-4011-4012-4015	Copertura
4	4013-4010-4011-4014	Copertura

Solaio n°	Nodi	Tipo
5	4016-4013-4014-4017	Copertura
5	4017-4014-4015-4018	Copertura

Tabulati di verifica

L'esito di ogni elaborazione viene sintetizzato nei disegni e schemi grafici allegati, che evidenziano i valori numerici nei punti e/o nelle sezioni significative, ai fini della valutazione del comportamento complessivo della struttura, e quelli necessari ai fini delle verifiche di misura della sicurezza.

Di seguito si riportano le tabelle relative a:

- Forze sismiche e masse
- Massime tensioni terreno platee per combinazione
- Massimi spostamenti dei nodi
- Massime reazioni vincolari
- Massimi spostamenti degli impalcati
- Massimi spostamenti degli impalcati (SLD)
- Massime sollecitazioni travi
- Massime sollecitazioni pilastri
- Massime sollecitazioni muri Discretizzati
- Massime tensioni terreno platee per combinazione (SLE)
- Massimi spostamenti dei nodi (SLE)
- Massime reazioni vincolari (SLE)
- Massime sollecitazioni travi (SLE)
- Massime sollecitazioni pilastri (SLE)
- Massime sollecitazioni muri Discretizzati (SLE)

Risultati Analisi Dinamica - Baricentri masse e masse

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Piano	Rigido	Massa kg	X m	Y m	Z m
0	Si	0	0.00	0.00	0.00
1	Si	19917	3.86	14.98	-1.38
2	No	1262006	7.36	9.94	0.01
3	Si	61551	6.86	8.82	1.32
4	Si	327036	7.38	10.14	5.45

Piano	Rigido	Massa kg	X m	Y m	Z m
0	Si	0	0.00	0.00	0.00
1	Si	19917	4.10	15.17	-1.38
2	No	1262006	8.11	11.10	0.01
3	Si	61551	7.23	9.63	1.32
4	Si	327036	8.11	11.27	5.45

Piano	Rigido	Massa kg	X m	Y m	Z m
0	Si	0	0.00	0.00	0.00
1	Si	19917	3.86	15.36	-1.38
2	No	1262006	7.36	12.25	0.01
3	Si	61551	6.86	10.44	1.32
4	Si	327036	7.38	12.40	5.45

Piano	Rigido	Massa kg	X m	Y m	Z m
0	Si	0	0.00	0.00	0.00
1	Si	19917	3.63	15.17	-1.38
2	No	1262006	6.60	11.10	0.01
3	Si	61551	6.50	9.63	1.32
4	Si	327036	6.65	11.27	5.45

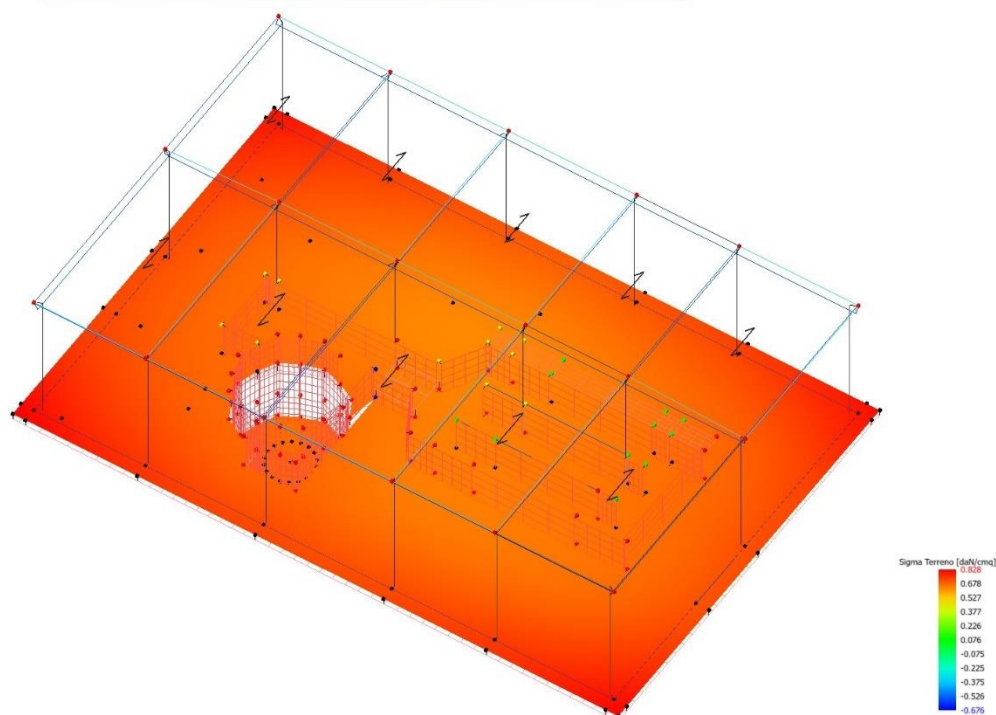
Risultati Analisi Dinamica - Sollecitazioni massime per combinazione - Sigma terreno platea

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Combinazione	Muro	Nodi	SigmaMax daN/cm ²	SigmaMin daN/cm ²
1	5	2020-2001-2025-2019	0.73	0.51
2	11	2016-2095-2094-2091	0.83	0.63

Combinazione	Muro	Nodi	SigmaMax	SigmaMin
3	11	2016-2095-2094-2091	0.74	0.54
4-I-1	1	2024-2027-2003-2023	0.55	0.39
4-II-1	11	2016-2095-2094-2091	0.57	0.38
4-I-2	1	2024-2027-2003-2023	0.55	0.39
4-II-2	11	2016-2095-2094-2091	0.57	0.38
4-I-3	1	2024-2027-2003-2023	0.55	0.39
4-II-3	11	2016-2095-2094-2091	0.56	0.38
4-I-4	1	2024-2027-2003-2023	0.55	0.39
4-II-4	11	2016-2095-2094-2091	0.57	0.38
5-I-1	11	2016-2095-2094-2091	0.57	0.39
5-II-1	5	2020-2001-2025-2019	0.56	0.39
5-I-2	11	2016-2095-2094-2091	0.57	0.39
5-II-2	5	2020-2001-2025-2019	0.56	0.39
5-I-3	11	2016-2095-2094-2091	0.57	0.39
5-II-3	5	2020-2001-2025-2019	0.56	0.39
5-I-4	11	2016-2095-2094-2091	0.57	0.39
5-II-4	5	2020-2001-2025-2019	0.56	0.39
Assoluti				
2	11	2016-2095-2094-2091	0.83	
4-II-2	11	2016-2095-2094-2091		0.38

Tipo diagramma: Tensioni medie terreno
Combinazione corrente : Scenario ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO - C 2
Tensioni medie terreno aste
Tensioni medie terreno platee



Risultati Analisi Dinamica - Spostamenti massimi - Nodi
Scenario di calcolo: ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Nodo	Trasl. X mm	Trasl. Y mm	Trasl. Z mm	Rotaz. X mrad	Rotaz. Y mrad	Rotaz. Z mrad
1	0.00 (1)	0.00 (1)	-13.57 (2)	0.03 (1)	-0.03 (1)	0.00 (1)
2	0.04 (3)	-0.02 (5-I-3)	-13.43 (2)	-0.02 (3)	0.10 (3)	0.01 (3)
3	0.05 (3)	-0.01 (3)	-13.42 (2)	0.05 (3)	-0.02 (3)	0.02 (3)
4	0.04 (3)	-0.01 (5-I-3)	-13.45 (2)	0.07 (3)	0.01 (3)	0.02 (3)
5	0.05 (3)	-0.04 (3)	-13.45 (2)	-0.03 (5-II-3)	0.05 (3)	0.01 (2)
6	0.04 (3)	-0.01 (5-I-3)	-13.47 (2)	0.06 (3)	0.04 (3)	0.01 (1)
7	0.06 (3)	-0.04 (3)	-13.47 (2)	-0.04 (5-II-3)	0.05 (3)	0.03 (1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
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Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
8	0.04(3)	-0.01(5-I-3)	-13.48(2)	0.04(3)	0.08(3)	0.02(1)
9	0.09(3)	-0.04(2)	-13.49(2)	-0.02(5-II-3)	0.03(1)	0.04(1)
10	0.04(3)	-0.02(5-I-3)	-13.49(2)	0.01(1)	0.09(3)	-0.01(3)
11	0.10(1)	-0.03(1)	-13.52(2)	0.03(1)	-0.07(1)	-0.02(2)
12	0.04(3)	-0.02(1)	-13.49(2)	-0.02(3)	0.06(3)	-0.03(3)
13	0.06(1)	-0.03(1)	-13.51(2)	-0.01(3)	-0.08(1)	-0.04(1)
14	0.05(3)	-0.02(1)	-13.48(2)	-0.03(3)	0.01(3)	-0.02(1)
15	0.03(3)	-0.04(1)	-13.49(2)	-0.01(4-I-1)	-0.08(1)	0.01(3)
16	0.05(3)	-0.02(1)	-13.44(2)	-0.05(3)	-0.02(1)	-0.03(1)
17	0.03(3)	-0.03(1)	-13.45(2)	0.02(3)	-0.07(3)	0.04(3)
18	0.05(3)	0.01(5-II-3)	-13.40(2)	-0.04(3)	-0.03(3)	-0.01(3)
19	0.03(4-II-4)	0.02(5-II-3)	-13.40(2)	0.01(5-I-1)	0.03(3)	0.02(3)
20	0.03(1)	0.01(5-II-3)	-13.37(2)	-0.04(3)	-0.05(3)	-0.02(4-II-4)
21	0.02(1)	0.02(5-II-3)	-13.37(2)	0.01(5-I-2)	0.03(3)	-0.00(4-II-1)
22	0.03(1)	0.01(5-II-3)	-13.35(2)	-0.02(4-I-4)	-0.04(3)	-0.01(4-II-4)
23	0.02(1)	0.01(5-II-3)	-13.35(2)	-0.03(4-II-4)	0.05(4-II-4)	0.01(1)
24	0.02(1)	0.01(5-II-3)	-13.33(2)	-0.02(3)	-0.06(3)	-0.01(5-II-3)
25	-0.02(4-I-2)	0.01(5-II-3)	-13.33(2)	-0.02(5-II-3)	0.03(4-II-2)	0.01(1)
26	0.02(1)	-0.01(5-I-3)	-13.33(2)	-0.00(5-I-4)	-0.05(3)	0.01(5-I-3)
27	0.02(4-II-2)	-0.01(5-I-3)	-13.33(2)	0.03(5-I-3)	0.01(4-II-2)	-0.00(4-I-1)
28	0.02(1)	-0.02(3)	-13.34(2)	0.01(3)	-0.06(3)	0.01(5-I-3)
29	-0.02(4-I-3)	-0.02(5-I-3)	-13.35(2)	0.02(1)	0.03(4-II-3)	-0.01(2)
30	0.03(3)	-0.02(3)	-13.37(2)	0.02(3)	-0.05(3)	0.01(4-II-3)
31	0.03(4-II-3)	-0.02(5-I-3)	-13.37(2)	0.05(1)	0.07(3)	-0.01(1)
32	0.04(3)	-0.02(3)	-13.39(2)	0.05(3)	-0.04(3)	0.03(4-II-3)
33	0.03(4-II-3)	-0.03(5-I-3)	-13.40(2)	0.02(1)	0.07(3)	-0.01(1)
34	0.00(1)	0.00(1)	-13.52(2)	-0.02(5-I-3)	-0.07(1)	0.00(1)
35	0.00(1)	0.00(1)	-13.52(2)	-0.01(5-I-3)	-0.07(1)	0.00(1)
36	0.00(1)	0.00(1)	-13.51(2)	0.01(5-II-3)	-0.07(1)	0.00(1)
37	0.00(1)	0.00(1)	-13.50(2)	0.02(5-II-3)	-0.07(3)	0.00(1)
38	0.00(1)	0.00(1)	-13.43(2)	-0.02(5-I-3)	-0.09(3)	0.00(1)
39	0.00(1)	0.00(1)	-13.45(2)	-0.03(3)	-0.09(3)	0.00(1)
40	0.00(1)	0.00(1)	-13.49(2)	0.02(5-II-3)	-0.08(3)	0.00(1)
41	0.00(1)	0.00(1)	-13.47(2)	0.01(5-II-3)	-0.08(3)	0.00(1)
42	0.00(1)	0.00(1)	-13.51(2)	-0.03(3)	-0.07(1)	0.00(1)
43	0.00(1)	0.00(1)	-13.47(2)	-0.03(3)	-0.08(3)	0.00(1)
44	0.00(1)	0.00(1)	-13.49(2)	-0.03(3)	-0.08(1)	0.00(1)
45	0.00(1)	0.00(1)	-13.45(2)	-0.02(1)	-0.09(3)	0.00(1)
46	0.00(1)	0.00(1)	-13.43(2)	-0.02(1)	-0.09(3)	0.00(1)
47	0.00(1)	0.00(1)	-13.41(2)	-0.02(5-I-3)	-0.09(3)	0.00(1)
48	0.00(1)	0.00(1)	-13.40(2)	-0.02(5-I-3)	-0.08(3)	0.00(1)
49	0.00(1)	0.00(1)	-13.41(2)	-0.02(5-I-3)	-0.08(3)	0.00(1)
50	0.00(1)	0.00(1)	-13.41(2)	-0.02(5-I-3)	-0.08(3)	0.00(1)
51	0.00(1)	0.00(1)	-13.42(2)	-0.02(1)	-0.09(3)	0.00(1)
52	0.00(1)	0.00(1)	-13.47(2)	-0.01(5-I-3)	-0.07(3)	0.00(1)
53	0.11(1)	0.01(5-II-3)	-13.57(2)	0.02(1)	-0.05(1)	-0.03(1)
2001	0.00(1)	0.00(1)	-16.03(2)	0.32(5-II-2)	-0.50(4-II-1)	0.00(1)
2002	0.00(1)	0.00(1)	-14.21(2)	0.29(1)	0.22(4-I-1)	0.00(1)
2003	0.00(1)	0.00(1)	-15.85(2)	0.33(5-II-1)	0.44(4-I-1)	0.00(1)
2004	0.00(1)	0.00(1)	-14.83(2)	0.22(5-II-1)	-0.44(4-II-1)	0.00(1)
2005	0.00(1)	0.00(1)	-13.18(2)	0.14(1)	-0.12(4-II-1)	0.00(1)
2006	0.00(1)	0.00(1)	-14.56(2)	0.24(5-II-1)	0.41(4-I-1)	0.00(1)
2007	0.00(1)	0.00(1)	-14.37(2)	0.12(1)	-0.38(4-II-1)	0.00(1)
2008	-0.02(4-II-1)	0.00(5-I-1)	-12.86(2)	0.11(1)	-0.15(4-II-1)	0.01(3)
2009	0.00(1)	0.00(1)	-13.98(2)	0.15(5-II-1)	0.38(1)	0.00(1)
2010	0.00(1)	0.00(1)	-14.35(2)	-0.09(5-I-2)	-0.34(1)	0.00(1)
2011	-0.04(3)	0.03(3)	-12.88(2)	-0.11(3)	-0.21(4-II-2)	0.01(4-II-3)
2012	0.00(1)	0.00(1)	-13.84(2)	-0.12(5-I-3)	0.40(1)	0.00(1)
2013	0.00(1)	0.00(1)	-14.94(2)	-0.26(1)	-0.44(1)	0.00(1)
2014	0.00(1)	0.00(1)	-13.24(2)	-0.12(1)	-0.16(4-II-3)	0.00(1)
2015	0.00(1)	0.00(1)	-14.49(2)	-0.24(5-I-3)	0.42(1)	0.00(1)
2016	0.00(1)	0.00(1)	-16.19(2)	-0.34(1)	-0.48(1)	0.00(1)
2017	0.00(1)	0.00(1)	-14.26(2)	-0.34(1)	-0.21(4-II-3)	0.00(1)
2018	0.00(1)	0.00(1)	-15.77(2)	-0.34(5-I-3)	0.42(1)	0.00(1)
2019	0.00(1)	0.00(1)	-16.40(2)	0.32(5-II-1)	-0.49(3)	0.00(1)
2020	0.00(1)	0.00(1)	-16.16(2)	0.32(5-II-2)	-0.50(3)	0.00(1)
2021	0.00(1)	0.00(1)	-14.29(2)	0.34(1)	-0.17(4-II-3)	0.00(1)
2022	0.00(1)	0.00(1)	-14.33(2)	0.29(1)	0.17(4-I-1)	0.00(1)
2023	0.00(1)	0.00(1)	-15.99(2)	0.32(5-II-1)	0.43(4-I-1)	0.00(1)
2024	0.00(1)	0.00(1)	-16.18(2)	0.32(5-II-1)	0.42(4-I-1)	0.00(1)
2025	0.00(1)	0.00(1)	-16.26(2)	0.32(5-II-1)	-0.49(4-II-1)	0.00(1)
2026	0.00(1)	0.00(1)	-14.13(2)	0.34(1)	-0.18(4-II-3)	0.00(1)
2027	0.00(1)	0.00(1)	-16.04(2)	0.33(5-II-1)	0.43(4-I-1)	0.00(1)
2028	0.03(2)	0.02(3)	-13.31(2)	0.18(1)	-0.09(4-II-4)	-0.01(3)
2029	-0.01(4-I-2)	0.00(5-II-3)	-13.44(2)	0.19(1)	0.11(4-I-1)	-0.01(3)
2031	0.00(1)	0.00(1)	-13.19(2)	0.16(1)	-0.11(4-II-1)	0.00(1)

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Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
2032	0.00(1)	0.00(1)	-13.24(2)	0.15(1)	-0.11(4-II-1)	0.00(1)
2033	0.00(1)	0.00(1)	-13.26(2)	0.16(1)	0.10(4-I-1)	0.00(1)
2035	0.00(1)	0.00(1)	-15.03(2)	0.21(1)	-0.43(3)	0.00(1)
2036	0.04(2)	0.02(3)	-13.08(2)	0.14(1)	0.09(4-I-1)	-0.01(3)
2037	0.02(2)	0.01(3)	-13.12(2)	0.13(1)	0.09(4-I-1)	-0.01(2)
2038	0.00(1)	0.00(1)	-13.18(2)	0.15(1)	-0.10(4-II-1)	0.00(1)
2040	0.00(1)	0.00(1)	-14.75(2)	0.22(5-II-1)	0.40(2)	0.00(1)
2041	0.00(1)	0.00(1)	-14.54(2)	0.12(1)	-0.38(3)	0.00(1)
2042	0.03(3)	0.02(3)	-12.85(2)	0.07(1)	0.06(4-I-1)	0.01(3)
2043	0.00(1)	0.00(1)	-12.87(2)	0.09(1)	-0.11(4-II-2)	0.00(1)
2044	0.00(1)	0.00(1)	-12.77(2)	0.12(1)	-0.12(4-II-2)	0.00(1)
2046	0.00(1)	0.00(1)	-14.16(2)	0.14(5-II-2)	0.38(1)	0.00(1)
2047	0.03(4-II-2)	0.02(3)	-12.83(2)	-0.08(5-I-1)	-0.06(4-II-2)	0.02(3)
2048	0.00(1)	0.00(1)	-12.82(2)	0.07(1)	-0.11(4-II-2)	0.00(1)
2049	-0.03(3)	0.00(4-II-3)	-12.75(2)	0.09(1)	-0.15(4-II-2)	0.02(5-II-1)
2050	-0.06(3)	-0.01(1)	-12.63(2)	0.11(1)	-0.17(4-II-2)	0.02(3)
2052	0.00(1)	0.00(1)	-12.90(2)	0.07(5-II-2)	0.33(1)	0.00(1)
2053	0.02(4-II-2)	0.03(3)	-12.86(2)	-0.09(5-I-1)	-0.07(4-II-2)	0.05(3)
2054	-0.07(3)	-0.01(1)	-12.57(2)	0.09(1)	-0.18(4-II-2)	-0.00(5-I-3)
2056	-0.04(3)	0.04(3)	-12.88(2)	-0.11(5-I-1)	-0.16(4-II-2)	0.02(1)
2057	-0.06(3)	0.04(3)	-12.75(2)	-0.09(5-I-1)	-0.17(4-II-2)	-0.02(1)
2058	-0.02(4-I-2)	-0.02(1)	-13.61(2)	0.04(1)	-0.29(1)	0.03(3)
2059	-0.03(4-I-2)	0.09(3)	-13.33(2)	-0.25(3)	-0.13(3)	0.03(3)
2060	-0.03(3)	0.03(3)	-13.10(2)	-0.14(3)	-0.20(4-II-2)	-0.03(3)
2061	0.00(1)	0.00(1)	-14.50(2)	-0.07(5-I-4)	-0.35(1)	0.00(1)
2062	0.00(1)	0.00(1)	-12.65(2)	-0.09(5-I-2)	0.23(1)	0.00(1)
2063	0.00(1)	0.00(1)	-14.02(2)	-0.10(5-I-2)	0.40(1)	0.00(1)
2064	-0.04(3)	0.02(3)	-13.43(2)	-0.12(3)	-0.13(3)	0.12(3)
2065	-0.04(2)	0.03(3)	-13.35(2)	-0.12(3)	-0.19(3)	-0.05(1)
2066	-0.09(3)	-0.07(1)	-13.50(2)	-0.12(3)	-0.20(3)	0.08(3)
2067	-0.06(3)	0.03(3)	-13.28(2)	-0.14(3)	-0.23(3)	0.02(4-II-3)
2068	-0.06(3)	-0.04(1)	-13.50(2)	-0.04(1)	-0.10(3)	-0.10(3)
2069	-0.07(3)	0.01(5-II-2)	-13.29(2)	-0.09(3)	-0.26(4-II-3)	0.02(4-II-3)
2070	0.01(4-II-4)	-0.01(5-I-3)	-13.65(2)	-0.13(1)	-0.32(1)	-0.01(1)
2071	0.02(1)	-0.03(1)	-13.53(2)	-0.08(1)	-0.18(1)	-0.04(1)
2072	-0.06(3)	-0.01(5-I-2)	-13.27(2)	-0.05(5-I-3)	-0.25(4-II-3)	-0.02(1)
2073	0.04(1)	-0.04(1)	-13.52(2)	-0.09(1)	-0.21(1)	-0.01(5-II-3)
2074	-0.04(3)	-0.01(5-I-2)	-13.31(2)	-0.04(1)	-0.21(4-II-3)	-0.03(3)
2075	0.03(1)	-0.03(1)	-13.51(2)	-0.13(1)	-0.21(1)	-0.01(5-II-3)
2076	-0.01(3)	-0.01(4-II-2)	-13.34(2)	-0.06(1)	-0.16(4-II-3)	-0.03(3)
2077	0.03(1)	-0.03(1)	-13.47(2)	-0.12(1)	-0.13(1)	-0.02(5-II-3)
2078	0.00(1)	0.00(1)	-13.39(2)	-0.09(1)	-0.13(4-II-3)	0.00(1)
2079	0.01(4-II-4)	-0.01(1)	-13.43(2)	-0.11(1)	-0.09(4-II-4)	-0.02(4-II-3)
2080	0.00(1)	0.00(1)	-15.14(2)	-0.26(1)	-0.44(1)	0.00(1)
2081	0.00(1)	0.00(1)	-14.68(2)	0.23(1)	0.42(1)	0.00(1)
2082	0.00(1)	0.00(1)	-13.80(2)	-0.25(1)	-0.30(1)	0.00(1)
2083	0.00(1)	0.00(1)	-13.58(2)	-0.21(1)	-0.19(1)	0.00(1)
2084	0.00(1)	0.00(1)	-13.46(2)	-0.13(1)	-0.13(4-II-3)	0.00(1)
2085	0.00(1)	0.00(1)	-13.29(2)	-0.14(1)	-0.16(4-II-3)	0.00(1)
2086	0.00(1)	0.00(1)	-13.40(2)	-0.25(1)	0.21(1)	0.00(1)
2087	0.00(1)	0.00(1)	-15.75(2)	-0.38(1)	-0.49(1)	0.00(1)
2088	0.00(1)	0.00(1)	-14.07(2)	-0.33(1)	-0.18(4-II-1)	0.00(1)
2089	0.00(1)	0.00(1)	-13.96(2)	-0.36(1)	-0.12(4-II-2)	0.00(1)
2090	0.00(1)	0.00(1)	-14.56(2)	-0.36(1)	0.34(1)	0.00(1)
2091	0.00(1)	0.00(1)	-16.41(2)	-0.36(1)	-0.48(1)	0.00(1)
2092	0.00(1)	0.00(1)	-14.35(2)	-0.34(1)	-0.19(4-II-1)	0.00(1)
2093	0.00(1)	0.00(1)	-15.96(2)	-0.34(1)	0.43(1)	0.00(1)
2094	0.00(1)	0.00(1)	-16.57(2)	-0.36(1)	-0.48(1)	0.00(1)
2095	0.00(1)	0.00(1)	-16.33(2)	-0.35(1)	-0.49(1)	0.00(1)
2096	0.00(1)	0.00(1)	-14.50(2)	-0.33(1)	-0.19(4-II-1)	0.00(1)
2097	0.00(1)	0.00(1)	-14.41(2)	-0.34(1)	-0.15(4-II-3)	0.00(1)
2098	0.00(1)	0.00(1)	-15.92(2)	-0.34(5-I-3)	0.43(1)	0.00(1)
2099	0.00(1)	0.00(1)	-16.12(2)	-0.34(5-I-3)	0.42(1)	0.00(1)
3005	-0.57(4-II-1)	-0.20(5-II-1)	-13.19(2)	0.28(5-II-1)	0.81(4-I-1)	0.07(4-I-1)
3008	-0.53(4-II-1)	-0.17(5-II-1)	-12.87(2)	0.26(5-II-1)	-0.70(4-I-1)	0.04(5-I-4)
3011	-0.80(4-II-3)	0.19(5-I-3)	-12.91(2)	-0.26(5-I-3)	-1.06(4-II-3)	0.06(4-II-3)
3014	-0.51(4-II-3)	0.18(5-I-3)	-13.25(2)	-0.29(5-I-3)	-0.92(4-II-3)	-0.15(4-II-3)
3028	0.14(4-I-1)	-0.20(1)	-13.30(2)	0.15(1)	0.10(4-I-1)	-0.02(3)
3029	0.15(4-I-1)	-0.22(1)	-13.44(2)	0.15(1)	0.11(4-I-1)	0.03(3)
3030	0.15(4-I-1)	-0.21(1)	-13.51(2)	0.16(1)	0.13(4-I-1)	0.01(3)
3031	0.13(4-I-1)	-0.16(1)	-13.18(2)	0.14(1)	0.08(4-I-1)	-0.02(2)
3032	-0.54(4-II-1)	-0.18(5-II-1)	-13.24(2)	0.16(5-II-1)	0.52(4-I-1)	0.01(5-I-4)
3033	0.14(4-I-1)	-0.22(1)	-13.28(2)	0.17(1)	0.11(4-I-1)	0.02(3)
3034	0.14(4-I-1)	-0.21(1)	-13.35(2)	0.17(1)	0.12(4-I-1)	0.01(3)
3036	0.15(4-I-1)	-0.18(1)	-13.08(2)	0.15(1)	0.09(4-I-1)	-0.02(4-II-2)
3037	0.13(4-I-1)	-0.16(1)	-13.13(2)	0.12(1)	0.08(4-I-1)	-0.02(2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

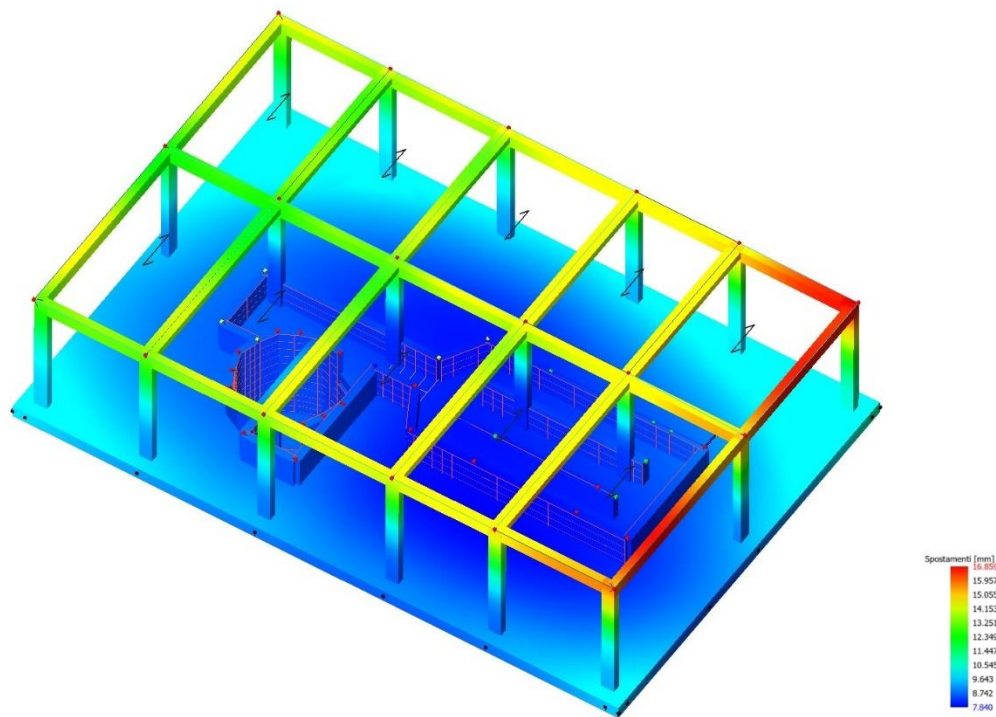
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Maggio 2021

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Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
3038	-0.14(4-II-1)	-0.21(1)	-13.19(2)	0.16(1)	0.10(4-I-1)	0.02(3)
3039	-0.14(4-II-1)	-0.20(1)	-13.26(2)	0.16(1)	0.12(4-I-1)	0.01(3)
3042	0.11(4-I-1)	0.10(5-I-1)	-12.85(2)	0.07(1)	0.07(4-I-1)	0.02(4-I-1)
3043	-0.13(4-II-2)	-0.13(1)	-12.88(2)	0.09(1)	-0.09(4-II-2)	0.03(3)
3044	-0.24(4-II-2)	-0.18(1)	-12.77(2)	0.12(1)	-0.16(4-II-2)	0.06(2)
3045	-0.24(4-II-2)	-0.14(1)	-12.77(2)	0.14(1)	-0.14(4-II-2)	0.06(2)
3047	0.09(4-I-2)	0.12(5-I-1)	-12.85(2)	-0.09(5-I-1)	0.06(4-I-2)	0.02(5-I-4)
3048	-0.15(4-II-2)	-0.13(1)	-12.81(2)	0.08(1)	-0.10(4-II-2)	0.01(3)
3049	-0.41(4-II-1)	-0.16(1)	-12.75(2)	0.10(1)	-0.33(4-II-1)	0.07(4-I-1)
3050	-0.32(4-II-2)	-0.16(1)	-12.64(2)	0.10(1)	-0.19(4-II-2)	0.06(2)
3051	-0.32(4-II-2)	-0.13(1)	-12.61(2)	0.12(1)	-0.17(4-II-2)	0.08(2)
3053	-0.06(4-II-2)	0.13(5-I-1)	-12.86(2)	-0.10(5-I-1)	0.06(4-I-2)	0.10(3)
3054	-0.36(4-II-2)	-0.16(1)	-12.56(2)	0.12(1)	-0.20(4-II-2)	-0.02(1)
3055	-0.36(4-II-2)	-0.13(1)	-12.52(2)	0.11(1)	-0.18(4-II-2)	0.06(2)
3056	-0.15(4-II-2)	0.29(3)	-12.88(2)	-0.16(3)	-0.10(4-II-2)	0.10(3)
3057	-0.32(4-II-2)	0.15(5-I-3)	-12.75(2)	-0.10(5-I-1)	-0.22(4-II-2)	-0.18(4-I-3)
3058	-0.15(3)	-0.01(1)	-13.58(2)	-0.02(3)	-0.10(3)	0.10(3)
3059	-0.17(3)	0.27(3)	-13.34(2)	-0.10(3)	-0.12(3)	0.05(3)
3060	-0.20(3)	0.29(3)	-13.10(2)	-0.18(3)	-0.11(3)	-0.03(4-II-2)
3064	-0.17(3)	0.18(3)	-13.43(2)	-0.13(3)	-0.14(3)	0.14(3)
3066	-0.22(3)	0.09(3)	-13.51(2)	-0.15(3)	-0.16(3)	0.15(3)
3068	-0.20(3)	0.01(4-II-3)	-13.48(2)	-0.05(3)	-0.11(3)	-0.05(3)
3069	-0.26(3)	-0.03(5-II-3)	-13.32(2)	-0.04(5-I-3)	-0.11(1)	-0.07(3)
3070	-0.17(3)	0.03(3)	-13.61(2)	-0.02(3)	-0.11(3)	-0.04(3)
3071	-0.16(3)	0.02(4-II-3)	-13.52(2)	0.06(1)	0.09(2)	-0.02(3)
3072	-0.23(3)	-0.03(5-II-3)	-13.25(2)	0.02(5-II-3)	-0.42(1)	-0.02(4-II-3)
3073	-0.11(3)	0.01(4-II-3)	-13.51(2)	0.01(1)	-0.08(3)	-0.10(1)
3074	-0.14(3)	-0.03(5-II-3)	-13.32(2)	-0.05(1)	-0.10(1)	-0.11(1)
3075	-0.07(5-II-2)	-0.04(1)	-13.49(2)	0.04(1)	-0.06(3)	-0.03(1)
3076	-0.09(4-II-3)	0.05(1)	-13.35(2)	-0.07(1)	-0.06(3)	-0.12(1)
3077	-0.08(4-II-3)	-0.03(1)	-13.45(2)	0.04(1)	-0.08(4-II-3)	0.05(1)
3078	-0.10(4-II-3)	0.11(1)	-13.38(2)	-0.08(1)	-0.07(4-II-3)	0.05(1)
3079	-0.09(3)	0.04(5-I-3)	-13.42(2)	-0.02(5-I-3)	-0.08(4-II-3)	0.09(1)
3084	-0.22(4-II-3)	0.12(1)	-13.46(2)	-0.08(1)	-0.15(4-II-3)	0.06(4-II-3)
3085	-0.25(4-II-3)	0.17(5-I-3)	-13.29(2)	-0.14(5-I-3)	-0.29(4-II-3)	-0.12(4-II-3)
4001	-13.36(4-II-1)	5.03(5-I-2)	-15.85(2)	0.66(5-II-2)	1.35(4-I-1)	0.23(4-I-1)
4002	-13.36(4-II-1)	4.63(5-I-3)	-14.23(2)	0.40(5-II-1)	-1.38(4-II-1)	0.23(4-I-1)
4003	-13.36(4-II-1)	5.12(5-I-4)	-15.74(2)	0.65(5-II-4)	-0.98(4-II-1)	0.23(4-I-1)
4004	-12.45(4-II-1)	5.03(5-I-2)	-14.91(2)	0.48(5-II-2)	-2.05(4-II-1)	0.23(4-I-1)
4005	-12.45(4-II-1)	4.63(5-I-3)	-13.19(2)	0.61(5-II-1)	-1.63(4-II-1)	0.23(4-I-1)
4006	-12.45(4-II-1)	5.12(5-I-4)	-14.66(2)	0.49(5-II-4)	2.06(4-I-1)	0.23(4-I-1)
4007	-11.67(4-II-1)	5.03(5-I-2)	-14.49(2)	-0.47(5-I-2)	-2.20(4-II-1)	0.23(4-I-1)
4008	-11.67(4-II-1)	4.63(5-I-3)	-12.88(2)	-0.63(5-I-1)	-1.55(4-II-1)	0.23(4-I-1)
4009	-11.67(4-II-1)	5.12(5-I-4)	-14.11(2)	-0.44(5-I-4)	2.16(4-I-1)	0.23(4-I-1)
4010	-11.63(4-II-3)	5.03(5-I-2)	-14.50(2)	-0.43(5-I-2)	-2.28(4-II-3)	0.23(4-I-1)
4011	-11.63(4-II-3)	4.63(5-I-3)	-12.93(2)	-0.55(5-I-3)	-1.44(4-II-3)	0.23(4-I-1)
4012	-11.63(4-II-3)	5.12(5-I-4)	-13.98(2)	-0.43(5-I-4)	2.21(4-I-3)	0.23(4-I-1)
4013	-12.50(4-II-3)	5.03(5-I-2)	-15.03(2)	-0.44(5-I-2)	-2.10(4-II-3)	0.23(4-I-1)
4014	-12.50(4-II-3)	4.63(5-I-3)	-13.26(2)	-0.59(5-I-3)	-1.61(4-II-3)	0.23(4-I-1)
4015	-12.50(4-II-3)	5.12(5-I-4)	-14.60(2)	-0.47(5-I-4)	2.07(4-I-3)	0.23(4-I-1)
4016	-13.34(4-II-3)	5.03(5-I-2)	-16.04(2)	-0.73(5-I-2)	1.33(4-I-3)	0.23(4-I-1)
4017	-13.34(4-II-3)	4.63(5-I-3)	-14.31(2)	-0.48(5-I-3)	-1.38(4-II-3)	0.23(4-I-1)
4018	-13.34(4-II-3)	5.12(5-I-4)	-15.68(2)	-0.72(5-I-4)	-1.02(4-II-3)	0.23(4-I-1)

Tipo diagramma: Deformata
Combinazione corrente : Scenario ScenarioNT_2018 A2_SLV_SLD_STR_GEO - C 4-I
Posizione masse N° 1



Risultati Analisi Dinamica - Reazioni massime - Nodi
Scenario di calcolo: ScenarioNT_2018 A2_SLV_SLD_STR_GEO

Nodo	Rx kg	Ry kg	Rz kg	Mx kg*m	My kg*m	Mz kg*m
1	-29943 (3)	-5493 (5-II-3)	0	0	0	4496 (3)
34	-3402 (3)	1019 (1)	0	0	0	114 (1)
35	-2875 (3)	850 (5-I-3)	0	0	0	-8 (3)
36	-2740 (3)	1115 (3)	0	0	0	-34 (1)
37	-2734 (3)	1166 (3)	0	0	0	-39 (3)
38	-1990 (1)	-1057 (5-II-3)	0	0	0	30 (1)
39	-2386 (3)	-900 (5-II-3)	0	0	0	8 (1)
40	-1899 (3)	985 (3)	0	0	0	-25 (3)
41	-1784 (3)	1200 (3)	0	0	0	-14 (4-II-3)
42	-2893 (3)	1213 (1)	0	0	0	-23 (1)
43	-2064 (3)	614 (1)	0	0	0	35 (3)
44	-2251 (3)	919 (1)	0	0	0	31 (3)
45	-1408 (1)	1262 (3)	0	0	0	-23 (4-II-3)
46	-1356 (1)	1292 (3)	0	0	0	-10 (4-II-2)
47	-1928 (1)	-1205 (3)	0	0	0	-60 (3)
48	-982 (1)	-325 (5-II-3)	0	0	0	28 (4-II-2)
49	-1357 (1)	-769 (5-II-3)	0	0	0	67 (3)
50	-1044 (1)	676 (5-I-3)	0	0	0	11 (5-II-3)
51	-1098 (1)	986 (3)	0	0	0	-9 (1)
52	647 (3)	-235 (5-I-3)	0	0	0	-16 (4-II-4)
2001	-28238 (4-I-1)	-31688 (5-I-2)	0	0	0	-1812 (4-II-1)
2002	-65353 (4-I-1)	9619 (5-II-3)	0	0	0	2555 (4-I-1)
2003	29430 (4-II-1)	-31844 (5-I-4)	0	0	0	1717 (4-I-1)
2004	20718 (4-II-1)	-30060 (5-I-2)	0	0	0	-1144 (5-I-2)
2005	-11169 (4-I-1)	-11964 (3)	0	0	0	2942 (4-I-1)
2006	26554 (4-II-1)	-31221 (5-I-4)	0	0	0	1333 (5-I-4)
2007	18521 (4-II-1)	-24874 (5-I-2)	0	0	0	-1219 (5-I-2)
2009	25268 (4-II-1)	-27217 (5-I-4)	0	0	0	-1196 (5-II-4)
2010	-18466 (4-I-3)	25640 (5-II-2)	0	0	0	855 (5-II-2)
2012	25297 (4-II-3)	25671 (5-II-4)	0	0	0	1278 (5-I-4)
2013	-26198 (4-I-3)	28224 (5-II-2)	0	0	0	1250 (5-II-2)
2014	21365 (2)	11088 (1)	0	0	0	4569 (3)

Nodo	Rx	Ry	Rz	Mx	My	Mz
2015	-21247 (4-I-3)	27919 (5-II-4)	0	0	0	-2631 (5-II-4)
2016	-29150 (4-I-3)	32343 (5-II-2)	0	0	0	1850 (4-II-3)
2017	-65474 (4-I-3)	12893 (5-II-1)	0	0	0	2816 (4-II-3)
2018	26368 (4-II-3)	29863 (5-II-4)	0	0	0	-3733 (4-I-3)
2019	-127 (5-II-2)	-158 (4-II-1)	0	0	0	0
2020	1284 (5-II-2)	213 (5-I-2)	0	0	0	27 (5-I-2)
2021	-676 (4-II-1)	-138 (2)	0	0	0	12 (1)
2022	-691 (4-I-4)	205 (5-I-3)	0	0	0	-42 (4-I-1)
2023	-1254 (5-II-4)	200 (5-I-4)	0	0	0	-25 (5-I-4)
2024	117 (5-II-4)	-156 (4-I-1)	0	0	0	0
2025	-258 (4-II-1)	1426 (4-II-1)	0	0	0	-20 (4-I-3)
2026	-4482 (4-II-1)	7712 (3)	0	0	0	580 (4-II-1)
2027	250 (4-I-1)	1312 (4-I-1)	0	0	0	24 (4-I-3)
2031	-28352 (2)	-24560 (3)	0	0	0	833 (3)
2032	-2271 (4-I-1)	-7059 (3)	0	0	0	181 (4-I-1)
2033	9606 (1)	-5500 (2)	0	0	0	630 (3)
2035	328 (4-I-1)	547 (4-II-4)	0	0	0	-17 (5-I-2)
2038	14430 (3)	-2145 (3)	0	0	0	-1889 (3)
2040	242 (4-I-1)	422 (5-II-2)	0	0	0	-12 (5-II-4)
2041	302 (4-I-1)	1132 (4-II-1)	0	0	0	15 (5-II-2)
2043	-24466 (2)	-11234 (3)	0	0	0	-1459 (2)
2044	44135 (3)	9862 (1)	0	0	0	1502 (3)
2046	-268 (4-II-1)	402 (4-I-1)	0	0	0	-18 (5-II-4)
2048	5801 (4-I-2)	-16124 (3)	0	0	0	-413 (3)
2052	-3193 (1)	2759 (5-I-3)	0	0	0	70 (5-I-3)
2061	395 (4-I-3)	-634 (4-I-1)	0	0	0	28 (5-II-2)
2062	13495 (3)	-3099 (5-II-1)	0	0	0	-1038 (3)
2063	-264 (4-II-3)	438 (3)	0	0	0	19 (5-I-4)
2078	-9709 (4-II-2)	4824 (1)	0	0	0	652 (3)
2080	256 (4-I-3)	-624 (3)	0	0	0	-19 (5-I-2)
2081	209 (4-I-3)	-450 (5-I-3)	0	0	0	13 (5-I-4)
2082	-4301 (4-II-2)	4633 (2)	0	0	0	181 (3)
2083	-10258 (4-II-2)	6680 (2)	0	0	0	-143 (1)
2084	-7489 (1)	14095 (3)	0	0	0	741 (1)
2085	5855 (3)	14155 (1)	0	0	0	-219 (1)
2086	-1555 (2)	-1295 (2)	0	0	0	46 (5-I-1)
2087	4953 (1)	-4909 (1)	0	0	0	-160 (1)
2088	-1676 (4-II-3)	-3802 (1)	0	0	0	-29 (3)
2089	4758 (3)	-9541 (1)	0	0	0	420 (3)
2090	-8631 (2)	-8903 (1)	0	0	0	-1828 (1)
2091	-287 (4-II-3)	-1396 (4-II-3)	0	0	0	-27 (4-II-3)
2092	-1359 (4-II-3)	-2133 (1)	0	0	0	-79 (4-II-1)
2093	265 (4-I-3)	-1145 (4-I-3)	0	0	0	26 (4-I-3)
2094	-110 (5-I-2)	160 (4-II-3)	0	0	0	2 (4-II-3)
2095	1298 (5-I-2)	-178 (5-II-2)	0	0	0	19 (5-I-2)
2096	-716 (4-II-3)	75 (1)	0	0	0	-15 (4-II-3)
2097	-1429 (4-I-3)	-112 (5-II-1)	0	0	0	31 (4-II-3)
2098	-872 (5-I-3)	-152 (5-II-4)	0	0	0	18 (5-II-4)
2099	97 (5-I-4)	141 (4-I-3)	0	0	0	-2 (4-I-3)

Risultati Analisi Dinamica - Spostamenti massimi - Impalcati
Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Piano	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	mrاد	mrاد	mrاد
0	0.02 (3-1)	-0.01 (5-I-3)	-13.44 (2-1)	0.00 (1-1)	0.00 (1-1)	0.00 (1-1)
1	0.04 (4-II-4)	-0.02 (1-1)	-13.43 (2-1)	0.00 (1-1)	0.00 (1-1)	0.00 (4-II-1)
3	-0.17 (4-I-2)	-0.06 (5-II-1)	-13.15 (2-1)	0.00 (1-1)	0.00 (1-1)	0.01 (4-I-1)
4	-11.44 (4-I-2)	4.63 (5-I-3)	-9.30 (2-1)	0.00 (1-1)	0.00 (1-1)	0.20 (4-I-1)

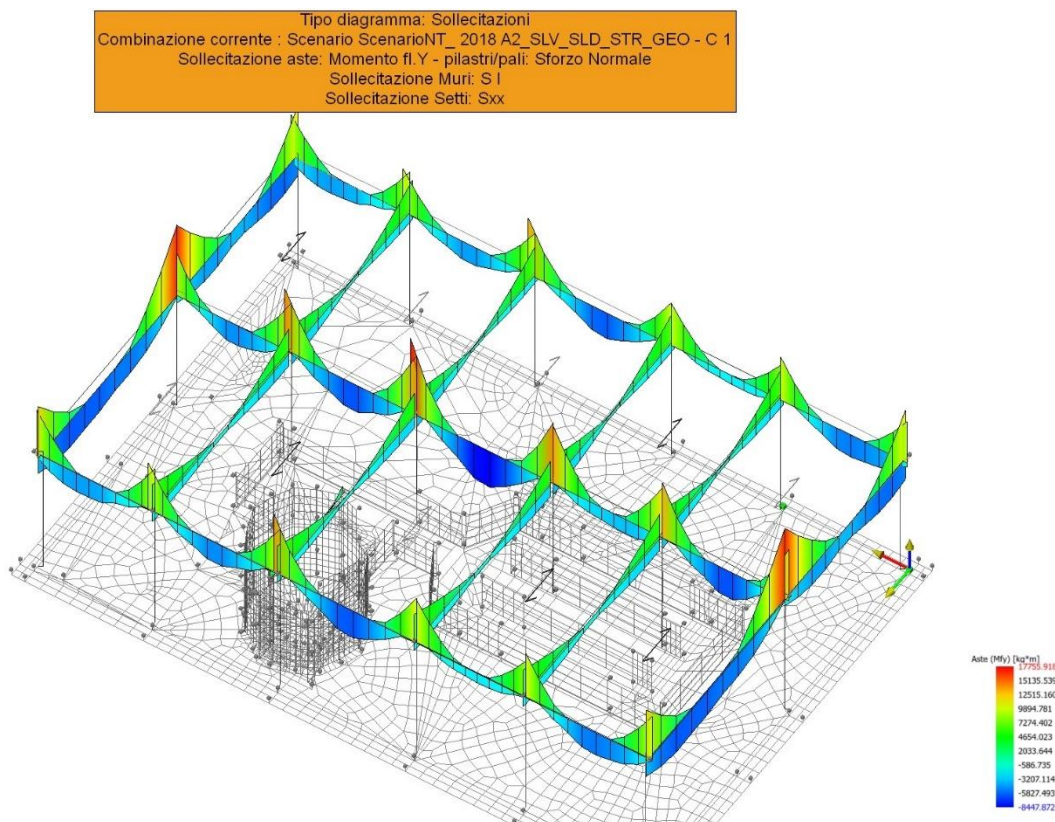
Risultati Analisi Dinamica - Spostamenti massimi - Impalcati (SLD)
Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Piano	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	mrاد	mrاد	mrاد
0	0.01 (9-II-4)	-0.00 (10-I-3)	-9.51 (6-1)	0.00 (6-1)	0.00 (6-1)	0.00 (9-II-4)
1	0.03 (9-II-4)	-0.01 (10-I-3)	-9.51 (6-1)	0.00 (6-1)	0.00 (6-1)	0.00 (10-II-3)
3	-0.09 (9-I-2)	-0.03 (10-II-1)	-9.29 (6-1)	0.00 (6-1)	0.00 (6-1)	0.00 (9-I-1)
4	-3.01 (9-I-2)	1.76 (10-I-3)	-6.51 (6-1)	0.00 (6-1)	0.00 (6-1)	0.06 (10-I-4)

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Travi
Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Asta	N.in. N.fin.	N kg	Ty kg	Tz kg	Mt kg*m	My kg*m	Mz kg*m
301	3071	-1967 (4-II-2)	197 (2)	-4475 (1)	-51 (1)	3000 (1)	444 (2)
	3072	-1967 (4-II-2)	197 (2)	4033 (3)	-51 (1)	2097 (3)	-373 (3)
401	4001	0	12 (5-I-2)	-7051 (3)	5972 (1)	12308 (4-II-1)	47 (5-I-2)
	4002	0	12 (5-I-2)	8503 (1)	-5806 (3)	16792 (4-I-1)	-47 (5-I-2)
401	4002	0	-19 (5-I-4)	-7881 (4-II-1)	5000 (3)	16809 (4-II-1)	-65 (5-I-4)
	4003	0	-19 (5-I-4)	6586 (4-I-1)	-5215 (1)	11435 (4-I-1)	65 (5-I-4)
402	4003	0	135 (4-I-1)	-11001 (2)	4340 (1)	9845 (5-II-4)	314 (4-I-1)
	4006	0	135 (4-I-1)	12831 (3)	-2646 (3)	10304 (3)	-314 (4-I-1)
402	4006	0	48 (4-I-3)	-9804 (3)	3196 (1)	8157 (5-II-4)	97 (4-I-3)
	4009	0	48 (4-I-3)	11117 (2)	-2813 (3)	9993 (5-I-4)	-97 (4-I-3)
402	4009	0	15 (4-I-3)	-13084 (2)	4009 (1)	10080 (2)	40 (4-I-3)
	4012	0	15 (4-I-3)	13564 (3)	-3880 (3)	13356 (2)	-40 (4-I-3)
402	4012	0	-34 (4-I-1)	-12235 (2)	3444 (1)	10429 (5-II-4)	-83 (4-I-1)
	4015	0	-34 (4-I-1)	11402 (3)	-3835 (3)	10199 (5-I-4)	83 (4-I-1)
402	4015	0	-172 (4-I-3)	-11590 (2)	2290 (2)	10160 (5-II-4)	-374 (4-I-3)
	4018	0	-172 (4-I-3)	9838 (3)	-4240 (3)	9753 (5-I-4)	374 (4-I-3)
403	4011	0	10 (5-II-4)	-2331 (4-I-3)	138 (5-II-4)	5451 (4-I-3)	40 (5-II-4)
	4010	0	10 (5-II-4)	2740 (4-II-3)	138 (5-II-4)	7252 (4-II-3)	-40 (5-II-4)
403	4012	0	-12 (5-II-2)	-2799 (4-I-3)	-125 (5-II-2)	7167 (4-I-3)	-41 (5-II-2)
	4011	0	-12 (5-II-2)	2324 (4-II-3)	-125 (5-II-2)	5361 (4-II-3)	41 (5-II-2)
404	4004	0	-155 (4-II-4)	-13298 (2)	2384 (1)	10529 (2)	-360 (4-II-4)
	4001	0	-155 (4-II-4)	11750 (3)	-4596 (3)	10544 (5-II-2)	360 (4-II-4)
404	4007	0	-58 (4-II-3)	-11572 (2)	2736 (1)	10203 (5-I-2)	-116 (4-II-3)
	4004	0	-58 (4-II-3)	10439 (3)	-3269 (3)	8662 (5-II-2)	116 (4-II-3)
404	4010	0	-18 (4-I-1)	-14185 (2)	3852 (1)	13937 (2)	-48 (4-I-1)
	4007	0	-18 (4-I-1)	13826 (3)	-4034 (3)	10790 (3)	48 (4-I-1)
404	4013	0	39 (4-II-1)	-12504 (3)	3899 (3)	11016 (2)	95 (4-II-1)
	4010	0	39 (4-II-1)	13285 (2)	-3379 (1)	10949 (5-II-2)	-95 (4-II-1)
404	4016	0	195 (4-II-3)	-10862 (3)	4508 (3)	10399 (5-I-2)	424 (4-II-3)
	4013	0	195 (4-II-3)	12565 (2)	-2030 (1)	10439 (5-II-2)	-424 (4-II-3)
405	4005	0	-11 (5-I-4)	-2461 (4-I-1)	-142 (5-I-4)	5879 (4-I-1)	-41 (5-I-4)
	4004	0	-11 (5-I-4)	2688 (4-II-1)	-142 (5-I-4)	6846 (4-II-1)	41 (5-I-4)
405	4005	0	15 (5-I-2)	-2551 (4-II-1)	157 (5-I-2)	6146 (4-II-1)	51 (5-I-2)
	4006	0	15 (5-I-2)	2721 (4-I-1)	157 (5-I-2)	6741 (4-I-1)	-51 (5-I-2)
406	4008	0	-10 (5-I-4)	-2371 (4-I-1)	-128 (5-I-4)	5596 (4-I-1)	-37 (5-I-4)
	4007	0	-10 (5-I-4)	2734 (4-II-1)	-128 (5-I-4)	7135 (4-II-1)	37 (5-I-4)
406	4008	0	14 (5-I-2)	-2427 (4-II-1)	147 (5-I-2)	5750 (4-II-1)	48 (5-I-2)
	4009	0	14 (5-I-2)	2781 (4-I-1)	147 (5-I-2)	7039 (4-I-1)	-48 (5-I-2)
407	4002	0	40 (4-I-3)	-15642 (3)	321 (4-I-3)	12317 (3)	92 (4-I-3)
	4005	0	40 (4-I-3)	17014 (2)	321 (4-I-3)	13232 (2)	-92 (4-I-3)
407	4005	0	22 (4-I-3)	-13757 (3)	134 (4-I-3)	11830 (5-II-3)	45 (4-I-3)
	4008	0	22 (4-I-3)	15241 (2)	134 (4-I-3)	13530 (5-I-3)	-45 (4-I-3)
407	4008	0	18 (4-II-1)	-18349 (3)	185 (4-II-1)	14416 (3)	47 (4-II-1)
	4011	0	18 (4-II-1)	18009 (2)	185 (4-II-1)	17756 (2)	-47 (4-II-1)
407	4011	0	-19 (4-II-3)	-16992 (2)	-163 (4-II-3)	14241 (5-II-1)	-45 (4-II-3)
	4014	0	-19 (4-II-3)	15476 (3)	-163 (4-II-3)	14407 (5-I-1)	45 (4-II-3)
407	4014	0	-51 (4-I-1)	-15263 (2)	-360 (4-I-1)	11943 (5-II-1)	-110 (4-I-1)
	4017	0	-51 (4-I-1)	14385 (3)	-360 (4-I-1)	11690 (3)	110 (4-I-1)
408	4014	0	12 (5-II-4)	-2469 (4-I-3)	165 (5-II-4)	5948 (4-I-3)	48 (5-II-4)
	4013	0	12 (5-II-4)	2713 (4-II-3)	165 (5-II-4)	6969 (4-II-3)	-48 (5-II-4)
408	4015	0	-17 (5-II-2)	-2766 (4-I-3)	-174 (5-II-2)	6891 (4-I-3)	-57 (5-II-2)
	4014	0	-17 (5-II-2)	2503 (4-II-3)	-174 (5-II-2)	5983 (4-II-3)	57 (5-II-2)
409	4017	0	-13 (5-II-2)	-8533 (1)	5773 (3)	16882 (4-I-3)	-50 (5-II-2)
	4016	0	-13 (5-II-2)	7040 (3)	-5993 (1)	12347 (4-II-3)	50 (5-II-2)
409	4018	0	20 (5-II-4)	-6602 (4-I-3)	5257 (1)	11457 (4-I-3)	69 (5-II-4)
	4017	0	20 (5-II-4)	7856 (4-II-3)	-4966 (3)	16660 (4-II-3)	-69 (5-II-4)

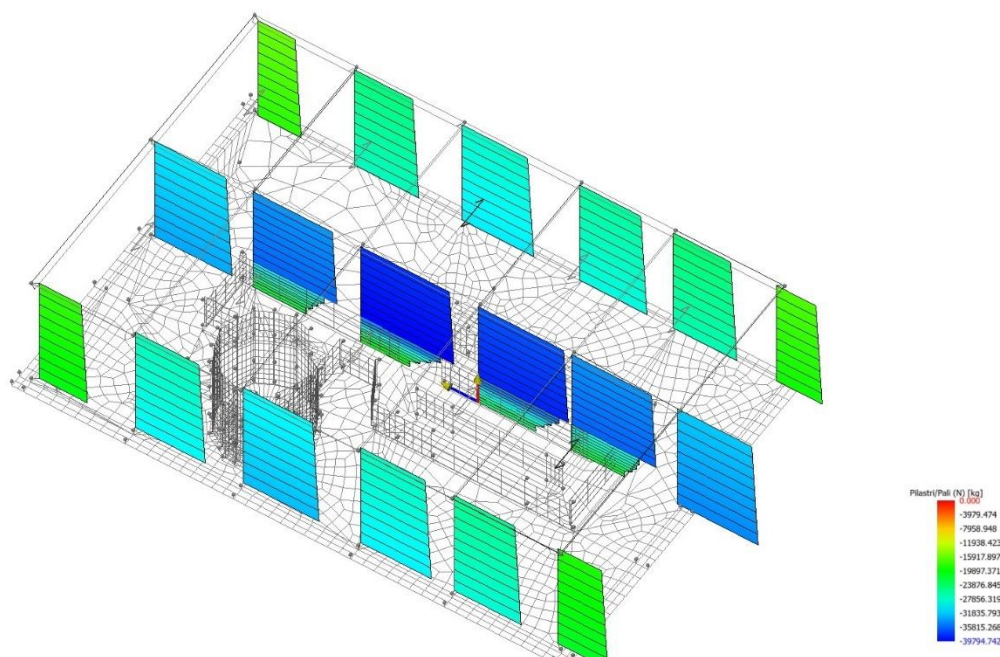


Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Pilastri
Scenario di calcolo: ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO

Asta	N.in. N.fin.	N kg	Ty kg	Tz kg	Mt kg*m	My kg*m	Mz kg*m
2001	2001	-21457 (3)	-2843 (4-II-1)	2644 (5-I-2)	178 (4-I-1)	-8417 (5-I-2)	8517 (4-I-1)
	4001	-18801 (3)	-2843 (4-II-1)	2644 (5-I-2)	178 (4-I-1)	5994 (5-I-2)	7614 (4-II-1)
2002	2002	-34464 (3)	7283 (4-I-1)	1273 (5-I-3)	178 (4-I-1)	-3590 (5-I-3)	21542 (4-I-1)
	4002	-31807 (3)	7283 (4-I-1)	1273 (5-I-3)	178 (4-I-1)	3348 (5-I-3)	-18148 (4-I-1)
2003	2003	-19472 (2)	-3031 (4-II-1)	2717 (5-I-4)	178 (4-I-1)	-8654 (5-I-4)	-8979 (4-II-1)
	4003	-16816 (2)	-3031 (4-II-1)	2717 (5-I-4)	178 (4-I-1)	6153 (5-I-4)	7541 (4-II-1)
2004	2004	-28429 (3)	2646 (4-I-1)	3558 (5-I-2)	178 (4-I-1)	-9936 (5-I-2)	8101 (4-I-1)
	4004	-25772 (3)	2646 (4-I-1)	3558 (5-I-2)	178 (4-I-1)	9454 (5-I-2)	-6318 (4-I-1)
2005	2005	-22533 (3)	504 (4-I-1)	2144 (3)	77 (4-I-1)	-917 (3)	1655 (4-I-1)
	3005	-28720 (3)	-3344 (4-I-1)	-6750 (5-I-3)	184 (4-I-1)	-5090 (5-I-3)	3428 (4-I-1)
2005	3005	-35908 (3)	5092 (4-I-1)	6562 (5-I-3)	-264 (4-I-3)	-13425 (5-I-3)	-10794 (4-II-1)
	4005	-33958 (3)	5092 (4-I-1)	6562 (5-I-3)	-264 (4-I-3)	12824 (5-I-3)	-9650 (4-I-1)
2006	2006	-27092 (2)	-2821 (4-II-1)	3713 (5-I-4)	178 (4-I-1)	-10396 (5-I-4)	-8425 (4-II-1)
	4006	-24435 (2)	-2821 (4-II-1)	3713 (5-I-4)	178 (4-I-1)	9841 (5-I-4)	6948 (4-II-1)
2007	2007	-30181 (3)	2551 (4-I-1)	-3084 (5-II-2)	178 (4-I-1)	8562 (5-II-2)	7703 (4-I-1)
	4007	-27524 (3)	2551 (4-I-1)	-3084 (5-II-2)	178 (4-I-1)	-8247 (5-II-2)	-6202 (4-I-1)
2008	2008	-24634 (3)	199 (4-II-1)	-234 (5-I-3)	92 (3)	-97 (5-I-1)	1171 (4-I-1)
	3008	-34514 (2)	-3240 (4-I-1)	-5985 (5-I-3)	143 (5-I-4)	-4393 (5-I-3)	3171 (4-I-1)
2008	3008	-38455 (2)	4913 (4-I-1)	-6095 (5-II-3)	-259 (4-II-1)	-12272 (5-I-3)	10433 (4-I-1)
	4008	-36505 (2)	4913 (4-I-1)	-6095 (5-II-3)	-259 (4-II-1)	-12144 (5-II-3)	-9217 (4-I-1)
2009	2009	-28796 (2)	-2692 (4-II-1)	2989 (5-I-4)	178 (4-I-1)	-8990 (5-I-4)	-7980 (4-II-1)
	4009	-26139 (2)	-2692 (4-II-1)	2989 (5-I-4)	178 (4-I-1)	-7921 (5-II-4)	6689 (4-II-1)
2010	2010	-32311 (2)	2574 (4-I-3)	-3030 (5-II-2)	178 (4-I-1)	8821 (5-II-2)	7678 (4-I-3)
	4010	-29654 (2)	2574 (4-I-3)	-3030 (5-II-2)	178 (4-I-1)	-7691 (5-II-2)	-6349 (4-I-3)
2011	2011	-20951 (2)	-744 (4-I-3)	-2644 (3)	310 (4-II-3)	1140 (3)	1605 (4-I-3)
	3011	-33914 (2)	-4699 (4-I-3)	6295 (5-II-1)	187 (4-I-1)	4604 (5-II-3)	4825 (4-I-3)
2011	3011	-39795 (2)	4604 (4-I-3)	-5994 (5-II-3)	-277 (4-II-1)	12801 (5-II-3)	9517 (4-I-3)
	4011	-37845 (2)	4604 (4-I-3)	-5994 (5-II-3)	-277 (4-II-1)	-11174 (5-II-3)	-8900 (4-I-3)
2012	2012	-30469 (2)	-2707 (4-II-3)	-2994 (5-II-4)	178 (4-I-1)	8757 (5-II-4)	-7992 (4-II-3)

Asta	N.in.	N	Ty	Tz	Mt	My	Mz
	4012	-27812 (2)	-2707 (4-II-3)	-2994 (5-II-4)	178 (4-I-1)	-7560 (5-II-4)	6763 (4-II-3)
2013	2013	-29775 (2)	2709 (4-I-3)	-3369 (5-II-2)	178 (4-I-1)	9670 (5-II-2)	8246 (4-I-3)
	4013	-27119 (2)	2709 (4-I-3)	-3369 (5-II-2)	178 (4-I-1)	-8693 (5-II-2)	-6516 (4-I-3)
2014	2014	-22786 (3)	-2130 (4-I-3)	-1648 (1)	-506 (4-II-3)	764 (1)	-160 (1)
	3014	-30251 (5-I-3)	-5832 (4-I-3)	-6296 (5-I-1)	-207 (4-II-1)	4646 (5-II-1)	5737 (4-I-3)
2014	3014	-35811 (2)	5276 (4-I-3)	-5896 (5-II-1)	377 (4-II-3)	12446 (5-II-1)	11108 (4-I-3)
	4014	-33861 (2)	5276 (4-I-3)	-5896 (5-II-1)	377 (4-II-3)	-11138 (5-II-1)	-9996 (4-I-3)
2015	2015	-27477 (3)	-2838 (4-II-3)	-3398 (5-II-4)	178 (4-I-1)	9754 (5-II-4)	-8455 (4-II-3)
	4015	-24820 (3)	-2838 (4-II-3)	-3398 (5-II-4)	178 (4-I-1)	-8766 (5-II-4)	7015 (4-II-3)
2016	2016	-20559 (3)	-2871 (4-II-3)	-2774 (5-II-2)	178 (4-I-1)	8583 (5-II-2)	8510 (4-I-3)
	4016	-17902 (3)	-2871 (4-II-3)	-2774 (5-II-2)	178 (4-I-1)	-6537 (5-II-2)	7664 (4-II-3)
2017	2017	-33181 (3)	7354 (4-I-3)	-1337 (5-II-1)	178 (4-I-1)	3685 (5-II-1)	21814 (4-I-3)
	4017	-30524 (3)	7354 (4-I-3)	-1337 (5-II-1)	178 (4-I-1)	-3601 (5-II-1)	-18266 (4-I-3)
2018	2018	-18334 (3)	-3001 (4-II-3)	-2813 (5-II-4)	178 (4-I-1)	8768 (5-II-4)	-8926 (4-II-3)
	4018	-15677 (3)	-3001 (4-II-3)	-2813 (5-II-4)	178 (4-I-1)	-6561 (5-II-4)	7427 (4-II-3)

Tipo diagramma: Sollecitazioni
Combinazione corrente : Scenario ScenarioNT_2018 A2_SLV_SLD_STR_GEO - C 1
Sollecitazione aste: Momento fl.Y - pilastri/pali: Sforzo Normale
Sollecitazione Muri: S I
Sollecitazione Setti: Sxx



Risultati Analisi Dinamica - Sollecitazioni Massime - Muri discretizzati
Scenario di calcolo: ScenarioNT_2018 A2_SLV_SLD_STR_GEO

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
		daN/cm ²	daN/cm ²	daN/cm ²	kg*m/m	kg*m/m	kg*m/m
1	1	0.65 (5-I-4)	0.62 (4-II-1)	-0.55 (4-II-3)	-166 (5-I-4)	-167 (4-II-4)	328 (3)
1	2	-0.38 (5-I-4)	1.98 (3)	-1.08 (3)	119 (5-I-4)	-918 (3)	463 (3)
1	3	2.10 (3)	0.54 (4-I-1)	-1.00 (3)	-1012 (3)	113 (4-II-1)	441 (3)
1	4	-1.19 (5-I-4)	1.59 (4-I-1)	-3.00 (3)	-680 (5-II-4)	-914 (4-I-1)	1158 (4-II-3)
2	1	-0.70 (5-I-4)	3.41 (4-II-1)	-1.07 (5-II-4)	131 (5-I-4)	-1951 (4-II-1)	-519 (5-I-4)
2	2	0.68 (5-I-4)	-2.89 (4-I-1)	-1.38 (5-II-4)	137 (4-II-1)	1175 (4-I-1)	-835 (3)
2	3	0.16 (5-I-4)	-3.89 (4-I-1)	-1.17 (5-II-4)	99 (5-I-4)	1647 (4-I-1)	-731 (3)
2	4	0.09 (5-I-4)	-4.76 (4-I-1)	-1.03 (5-II-4)	52 (5-I-4)	2043 (4-I-1)	-642 (3)
2	5	0.06 (5-I-4)	-6.16 (2)	-0.90 (5-II-4)	38 (5-I-4)	2677 (2)	-522 (3)
2	6	0.05 (5-I-4)	-7.31 (3)	-0.76 (5-II-4)	32 (1)	3163 (3)	-388 (3)
2	7	0.04 (5-I-4)	-8.00 (3)	-0.63 (5-II-4)	29 (1)	3455 (3)	-263 (4-II-1)
2	8	0.03 (5-I-1)	-8.23 (3)	-0.50 (5-II-4)	27 (1)	3556 (3)	-185 (4-II-1)

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
2	9	0.03(5-I-1)	-8.02(3)	-0.37(4-II-1)	23(1)	3472(3)	173(4-I-1)
2	10	-0.03(5-II-1)	-7.36(3)	-0.28(4-II-1)	24(4-II-1)	3200(3)	292(4-I-1)
2	11	-0.04(5-II-1)	-6.22(3)	-0.18(4-II-1)	44(4-II-1)	2727(3)	430(4-I-1)
2	12	0.06(5-I-3)	-4.90(4-II-1)	0.30(4-I-1)	24(5-I-2)	2101(4-II-1)	593(4-I-1)
2	13	0.32(5-I-3)	-4.32(4-II-1)	0.65(4-I-1)	164(4-I-1)	1850(4-II-1)	789(3)
2	14	-0.19(5-I-3)	3.09(4-I-1)	-1.14(4-II-1)	92(4-I-1)	-1870(4-I-1)	715(3)
2	15	-0.89(5-I-4)	5.68(4-II-1)	2.05(5-I-4)	-665(5-II-4)	-2965(4-II-1)	1300(5-II-4)
2	16	0.54(4-I-1)	-2.78(4-I-1)	0.87(5-I-4)	-568(5-I-4)	-1161(4-II-1)	1225(5-II-4)
2	17	0.19(5-I-4)	-3.75(4-I-1)	0.56(5-I-4)	-250(5-I-4)	1564(4-I-1)	1153(5-II-4)
2	18	0.15(5-I-4)	-4.70(4-I-1)	0.36(5-I-4)	-150(5-I-4)	1994(4-I-1)	1031(5-II-4)
2	19	0.11(5-I-4)	-6.09(2)	-0.37(5-II-4)	-96(5-I-4)	2637(2)	903(5-II-4)
2	20	0.08(5-I-4)	-7.21(3)	-0.41(5-II-4)	-73(5-I-4)	3114(3)	771(5-II-4)
2	21	0.07(5-I-4)	-7.88(3)	-0.46(5-II-4)	-59(5-I-1)	3397(3)	642(5-II-4)
2	22	0.05(5-I-1)	-8.10(3)	-0.49(5-II-4)	-46(5-I-1)	3497(3)	504(5-II-4)
2	23	-0.05(5-II-1)	-7.91(3)	-0.53(4-I-3)	48(5-II-1)	3419(3)	381(4-II-1)
2	24	-0.06(5-II-1)	-7.28(3)	-0.60(4-I-3)	60(5-II-1)	3159(3)	290(4-II-1)
2	25	0.07(5-I-1)	-6.16(3)	-0.73(4-I-3)	61(5-II-1)	2694(3)	204(4-II-1)
2	26	0.22(4-I-1)	-4.81(4-II-1)	-0.99(4-I-1)	-100(4-II-1)	2021(4-II-1)	-273(4-I-1)
2	27	0.70(4-II-1)	-4.65(4-II-1)	-1.41(3)	-297(1)	2030(4-II-1)	-295(4-I-1)
2	28	0.47(4-I-1)	7.34(4-I-1)	-3.81(4-II-1)	-440(4-I-1)	-3750(4-I-1)	1549(4-II-1)
3	1	-0.28(5-I-3)	3.81(4-II-1)	0.85(4-I-1)	60(4-II-1)	-2379(4-II-1)	-758(2)
3	2	0.33(5-I-3)	-5.15(4-I-1)	-1.06(4-II-1)	149(4-II-1)	2185(4-I-1)	-976(2)
3	3	-0.05(5-II-1)	-5.70(4-I-1)	-0.67(4-II-1)	25(5-I-1)	2434(4-I-1)	-754(4-II-1)
3	4	-0.07(5-II-2)	-6.55(3)	-0.49(4-II-1)	43(4-I-1)	2864(3)	-610(4-II-1)
3	5	-0.06(5-II-2)	-8.11(3)	-0.34(4-II-1)	25(4-I-1)	3517(3)	-480(4-II-1)
3	6	0.12(4-II-3)	-9.22(3)	0.12(4-I-1)	43(2)	4088(3)	-245(4-II-4)
3	7	0.52(4-II-1)	7.91(4-II-1)	3.32(4-I-1)	-453(4-II-1)	-4196(4-II-1)	1543(4-II-1)
3	8	0.62(4-I-1)	-5.41(4-I-1)	0.86(2)	-252(5-I-3)	2344(4-I-1)	751(4-II-1)
3	9	-0.16(4-II-1)	-5.58(4-I-1)	0.66(4-II-4)	119(4-II-1)	2345(4-I-1)	699(4-II-1)
3	10	-0.09(5-II-1)	-6.47(3)	0.55(4-II-3)	95(5-II-1)	2814(3)	546(4-II-1)
3	11	-0.04(5-II-1)	-8.04(3)	0.54(4-II-3)	66(5-II-1)	3478(3)	370(4-II-1)
3	12	-0.15(5-II-2)	-8.98(3)	0.42(1)	47(5-II-1)	4000(3)	180(4-II-1)
4	1	-0.12(4-II-3)	-10.10(3)	0.24(5-II-2)	23(4-I-1)	4202(3)	-151(4-II-3)
4	2	0.07(1)	-10.50(3)	0.35(5-II-2)	28(1)	4502(3)	-163(4-II-1)
4	3	0.06(1)	-10.50(3)	0.47(5-II-2)	36(1)	4499(3)	202(4-I-1)
4	4	0.07(1)	-10.00(3)	0.57(5-II-2)	36(1)	4287(3)	307(4-I-1)
4	5	0.06(5-I-2)	-8.98(3)	0.66(5-II-2)	37(1)	3862(3)	471(2)
4	6	0.06(5-I-2)	-7.45(3)	0.78(5-II-2)	38(1)	3218(3)	623(2)
4	7	0.08(5-I-2)	-5.50(4-II-1)	0.92(5-II-2)	50(4-II-1)	2365(3)	750(2)
4	8	0.14(5-I-2)	-4.39(4-II-1)	1.07(5-II-2)	94(5-I-2)	1858(4-II-1)	830(2)
4	9	0.67(5-I-2)	-3.17(4-II-1)	1.31(5-II-2)	133(4-I-1)	1298(4-II-1)	924(2)
4	10	-0.72(5-I-2)	3.52(4-I-1)	1.02(5-II-2)	131(5-I-2)	-2038(4-I-1)	554(5-I-2)
4	11	0.06(1)	-9.96(3)	0.46(5-II-2)	-33(5-I-2)	4133(3)	-235(4-I-1)
4	12	0.06(4-I-3)	-10.30(3)	0.47(4-II-3)	-51(5-I-2)	4417(3)	-336(5-II-2)
4	13	0.07(5-I-2)	-10.29(3)	0.39(4-II-3)	-64(5-I-2)	4408(3)	-457(5-II-2)
4	14	0.09(5-I-2)	-9.80(3)	0.30(5-II-2)	-76(5-I-2)	4199(3)	-570(5-II-2)
4	15	0.09(5-I-2)	-8.83(3)	-0.31(5-I-2)	-81(5-I-2)	3789(3)	-679(5-II-2)
4	16	0.10(5-I-2)	-7.35(3)	-0.45(5-I-2)	-92(5-I-2)	3167(3)	-800(5-II-2)
4	17	0.13(5-I-2)	-5.43(4-II-1)	-0.58(5-I-2)	-131(5-I-2)	2331(3)	-933(5-II-2)
4	18	0.14(5-I-2)	-4.25(4-II-1)	-0.76(5-I-2)	-210(5-I-2)	1776(4-II-1)	-1074(5-II-2)
4	19	0.51(4-II-1)	-3.03(4-II-1)	-0.98(5-I-2)	-537(5-I-2)	1245(4-II-1)	-1180(5-II-2)
4	20	-0.89(5-I-2)	5.72(4-I-1)	-2.08(5-I-2)	-618(5-II-2)	-3022(4-I-1)	-1235(5-II-2)
5	1	-0.37(5-I-2)	2.10(2)	1.12(2)	115(5-I-2)	-998(2)	-499(2)
5	2	0.66(5-I-2)	0.67(4-I-1)	0.57(4-I-3)	-171(5-I-2)	-157(4-I-2)	-348(2)
5	3	-1.18(5-I-2)	1.66(4-II-1)	3.12(2)	-669(5-II-2)	-956(4-II-1)	-1204(4-I-3)
5	4	2.14(2)	0.56(4-II-1)	1.05(2)	-1024(2)	127(4-I-1)	-453(2)
6	1	6.13(5-I-2)	1.13(4-II-1)	3.01(4-II-1)	-3189(5-I-2)	-975(4-II-1)	-2009(4-II-1)
6	2	3.52(5-I-2)	0.71(4-II-1)	1.63(4-II-1)	-2038(5-I-2)	125(4-I-1)	458(4-I-1)
6	3	3.08(5-I-2)	0.52(4-I-1)	-0.57(4-I-1)	-1278(5-I-2)	-526(4-I-1)	-1430(4-II-1)
6	4	2.86(5-I-2)	0.62(4-I-1)	1.75(4-II-1)	-1127(5-I-2)	149(1)	738(3)
6	5	-2.26(5-II-2)	-0.26(4-II-1)	-0.40(4-I-3)	1028(5-II-2)	269(4-II-1)	-1179(4-II-1)
6	6	-2.31(5-II-2)	-0.14(4-II-1)	1.23(4-II-1)	1060(5-II-2)	80(4-I-1)	608(3)
6	7	-3.15(5-II-2)	-0.21(4-II-1)	-0.26(4-I-3)	1425(5-II-2)	206(4-II-1)	-882(4-II-1)
6	8	-3.19(5-II-2)	-0.10(4-II-1)	0.91(4-II-1)	1446(5-II-2)	39(4-I-1)	474(3)
6	9	-4.07(3)	-0.16(4-II-1)	0.25(5-II-1)	1877(3)	169(4-II-1)	-613(4-II-1)
6	10	-4.15(3)	-0.08(4-II-1)	0.62(4-II-1)	1904(3)	-26(4-II-1)	309(3)
6	11	-4.75(3)	-0.13(4-II-1)	0.31(5-II-2)	2163(3)	142(4-II-1)	-399(1)
6	12	-4.88(3)	-0.07(4-II-1)	0.41(1)	2210(3)	23(4-I-1)	176(5-I-2)
6	13	-4.84(3)	0.12(4-I-1)	0.42(5-II-2)	2194(3)	126(4-II-1)	-214(1)
6	14	-4.99(3)	-0.07(4-II-1)	0.22(1)	2256(3)	29(4-I-3)	-153(5-II-2)
6	15	-4.23(3)	0.18(4-I-3)	0.64(5-II-2)	1953(3)	-145(4-I-1)	-134(4-I-2)
6	16	-4.45(3)	0.11(4-I-1)	0.13(4-I-2)	2029(3)	49(4-I-1)	-317(5-II-2)
6	17	-2.81(3)	0.56(4-I-3)	1.08(2)	1363(3)	-411(4-I-1)	-242(4-I-1)
6	18	-3.01(3)	0.57(4-I-1)	0.42(4-I-3)	1430(3)	58(5-II-2)	-649(3)
6	19	-2.88(5-I-2)	0.83(4-II-1)	2.46(4-I-3)	1028(5-I-2)	-557(4-II-1)	-883(4-I-3)
6	20	-0.85(4-II-1)	-0.56(4-I-1)	1.01(4-I-3)	-377(5-II-2)	61(4-I-1)	-707(2)

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
7	1	3.48(5-I-2)	0.78(4-II-1)	-2.22(4-I-1)	-1997(5-I-2)	-661(4-II-1)	-1048(4-II-1)
7	2	1.66(5-I-2)	-0.51(4-I-1)	-0.95(4-I-1)	-1180(5-I-2)	63(4-I-3)	573(4-I-1)
7	3	-3.51(5-II-2)	0.55(4-I-1)	-0.75(4-I-1)	1576(5-II-2)	-429(4-I-1)	-906(4-II-1)
7	4	-3.56(5-II-2)	0.56(4-I-1)	1.08(4-II-1)	1583(5-II-2)	82(5-I-2)	588(2)
7	5	-3.88(5-II-2)	0.18(4-I-1)	0.35(4-II-3)	1711(5-II-2)	-153(4-I-1)	-757(4-II-1)
7	6	-4.00(5-II-2)	0.09(4-I-1)	0.79(4-II-1)	1773(5-II-2)	57(4-I-1)	309(5-I-2)
7	7	-4.32(3)	0.15(4-I-1)	0.44(4-II-4)	1946(3)	-106(4-I-1)	-552(4-II-1)
7	8	-4.41(3)	-0.06(4-II-4)	0.59(4-II-1)	1991(3)	35(4-I-1)	159(5-I-2)
7	9	-4.18(3)	0.15(4-I-1)	0.58(1)	1884(3)	-106(4-I-1)	-359(4-II-1)
7	10	-4.28(3)	0.06(4-I-1)	0.38(4-II-1)	1932(3)	34(4-I-4)	-225(5-II-2)
7	11	-3.28(3)	0.19(4-I-3)	0.87(1)	1520(3)	-164(4-I-4)	-288(5-I-2)
7	12	-3.45(3)	0.13(4-I-1)	0.30(5-I-2)	1577(3)	52(4-I-4)	-370(5-II-2)
7	13	-1.77(5-I-2)	0.47(4-I-3)	1.47(3)	857(5-I-2)	-385(4-I-2)	-347(4-I-3)
7	14	-1.75(5-I-2)	0.52(4-I-2)	0.49(5-I-2)	847(3)	78(5-II-2)	-685(3)
7	15	2.47(5-II-2)	0.80(4-II-4)	2.44(5-I-2)	-1455(5-II-2)	-524(4-II-3)	-922(5-I-2)
7	16	1.45(1)	-0.50(4-I-1)	1.04(4-I-3)	-906(2)	60(4-I-1)	-721(3)
8	1	3.59(5-I-2)	0.68(4-II-1)	-2.12(4-I-1)	-2125(5-I-2)	-623(4-II-1)	-1122(4-II-1)
8	2	2.21(5-I-2)	0.45(4-I-1)	0.95(4-II-1)	-1506(5-I-2)	48(4-I-3)	542(2)
8	3	-3.14(5-II-2)	0.54(4-I-1)	-0.66(4-I-1)	1409(5-II-2)	-394(4-I-1)	-1181(4-II-1)
8	4	-3.14(5-II-2)	0.49(4-I-1)	1.31(4-II-1)	1394(5-II-2)	76(5-I-2)	668(1)
8	5	-3.50(5-II-2)	0.19(4-I-1)	0.58(4-II-1)	1534(5-II-2)	-162(4-I-1)	-1068(4-II-1)
8	6	-3.64(5-II-2)	0.10(4-I-4)	1.11(4-II-1)	1612(5-II-2)	53(4-I-1)	381(1)
8	7	-3.86(3)	0.12(4-I-1)	0.61(4-II-1)	1750(3)	101(4-II-1)	-855(4-II-1)
8	8	-4.00(3)	-0.05(4-II-3)	0.90(4-II-1)	1813(3)	35(4-I-1)	218(1)
8	9	-4.15(1)	-0.12(4-II-4)	0.62(3)	1868(1)	116(4-II-4)	-651(4-II-1)
8	10	-4.21(1)	-0.06(4-II-4)	0.69(4-II-1)	1893(2)	23(4-I-1)	-153(5-II-2)
8	11	-4.11(1)	-0.16(4-II-4)	0.63(3)	1853(1)	146(4-II-4)	-470(5-I-2)
8	12	-4.14(1)	-0.07(4-II-4)	0.50(5-I-2)	1863(1)	19(4-I-3)	-251(5-II-2)
8	13	-3.70(1)	-0.21(4-II-3)	0.58(3)	1689(1)	190(4-II-3)	-300(5-I-2)
8	14	-3.69(1)	-0.11(4-II-4)	0.32(5-I-2)	1684(1)	23(4-I-3)	-348(5-II-2)
8	15	-2.84(1)	-0.24(4-II-3)	0.58(4-I-3)	1363(1)	271(4-I-3)	447(5-II-2)
8	16	-2.89(1)	-0.17(4-II-4)	-0.44(5-II-2)	1372(1)	-58(4-II-3)	-447(5-II-2)
8	17	1.80(4-I-1)	0.40(4-I-3)	0.80(4-I-3)	810(1)	-325(4-I-3)	680(4-II-3)
8	18	-1.58(1)	0.50(4-I-3)	-0.79(4-II-3)	854(1)	51(5-II-2)	-672(3)
8	19	4.28(5-II-2)	-0.73(4-I-3)	2.06(4-I-3)	-2405(5-II-2)	-500(4-II-3)	846(4-II-3)
8	20	3.65(4-I-1)	-0.55(4-I-3)	0.80(4-I-3)	-1898(4-I-1)	52(4-I-1)	-606(4-I-3)
9	1	4.17(5-I-2)	0.76(4-II-2)	-3.22(4-I-1)	-2374(5-I-2)	-516(4-II-2)	1199(4-I-1)
9	2	3.36(4-I-3)	-0.61(4-I-3)	-1.38(4-I-1)	-1748(5-I-2)	64(4-I-3)	980(1)
9	3	-3.31(1)	0.57(4-I-1)	-1.95(1)	1595(1)	-425(4-I-1)	577(4-I-1)
9	4	-3.56(1)	0.59(4-I-2)	-0.80(4-I-1)	1666(1)	61(5-I-2)	1005(2)
9	5	-5.76(1)	0.23(4-I-1)	-1.27(3)	2606(1)	-176(4-I-1)	429(4-I-1)
9	6	-5.98(1)	0.13(4-I-3)	-0.46(4-I-1)	2659(1)	-51(4-II-4)	619(5-I-2)
9	7	-7.07(1)	0.18(4-I-2)	-0.75(3)	3122(1)	-125(4-I-4)	360(4-I-1)
9	8	-7.23(1)	0.08(4-I-3)	-0.41(4-I-1)	3181(1)	35(4-I-1)	438(5-I-2)
9	9	-7.43(1)	0.13(4-I-4)	-0.44(5-I-2)	3265(1)	98(4-II-4)	360(5-II-2)
9	10	-7.58(1)	0.06(4-I-4)	-0.38(4-I-1)	3324(1)	31(4-I-4)	271(5-I-2)
9	11	-7.05(1)	0.10(4-I-3)	-0.29(5-I-4)	3086(1)	120(4-II-3)	448(5-II-2)
9	12	-7.16(1)	-0.06(4-II-3)	-0.47(5-II-2)	3136(1)	37(4-I-3)	-221(5-II-2)
9	13	-6.07(1)	0.13(4-I-3)	-0.23(5-I-3)	2655(1)	129(4-II-3)	569(3)
9	14	-6.18(1)	-0.07(4-II-3)	-0.63(3)	2710(1)	51(4-I-3)	-321(5-II-2)
9	15	-4.63(1)	0.23(4-I-3)	0.21(1)	2050(1)	-205(4-I-3)	776(4-II-3)
9	16	-4.75(1)	0.12(4-I-3)	-0.83(4-II-3)	2107(1)	69(4-I-3)	-424(5-II-2)
9	17	-3.87(5-I-2)	0.58(4-I-3)	0.48(4-I-3)	1692(5-I-2)	-444(4-I-3)	945(4-II-3)
9	18	-3.84(5-I-2)	0.49(4-I-3)	-1.14(4-II-3)	1679(5-I-2)	119(5-II-2)	-622(1)
9	19	4.38(5-II-2)	0.84(4-II-3)	1.68(4-I-3)	-2430(5-II-2)	-722(4-II-3)	1092(4-II-3)
9	20	2.56(5-II-2)	0.49(4-II-3)	-0.89(4-II-3)	-1612(5-II-2)	57(4-I-1)	-450(1)
10	1	-2.12(1)	0.84(4-II-3)	-2.10(4-I-1)	613(5-II-2)	-532(4-II-3)	749(4-I-1)
10	2	-1.16(1)	-0.52(4-I-3)	-0.88(4-I-1)	-311(5-II-4)	50(4-I-3)	598(3)
10	3	-2.90(1)	0.41(4-I-1)	-0.70(4-I-3)	1389(1)	-388(4-I-3)	-231(4-II-3)
10	4	-3.15(1)	0.56(4-I-3)	-0.25(4-I-1)	1484(1)	64(5-I-2)	464(3)
10	5	-3.61(1)	-0.16(4-II-4)	-0.49(5-I-2)	1646(1)	197(4-II-3)	92(5-I-2)
10	6	-3.76(1)	-0.14(4-II-3)	-0.10(5-I-4)	1704(1)	67(4-I-3)	211(5-I-2)
10	7	-3.78(1)	-0.15(4-II-3)	-0.47(4-II-1)	1699(1)	149(4-II-3)	394(4-II-3)
10	8	-3.78(1)	-0.10(4-II-3)	-0.42(4-II-3)	1707(1)	39(4-I-3)	91(5-I-2)
10	9	-3.34(5-I-2)	-0.14(4-II-3)	-0.48(4-II-1)	1496(2)	142(4-II-3)	660(4-I-3)
10	10	-3.34(5-I-2)	-0.08(4-II-3)	-0.72(4-II-3)	1501(2)	44(4-I-3)	-137(1)
10	11	-2.91(5-I-2)	0.14(4-I-3)	-0.48(4-II-1)	1295(5-I-2)	-185(4-I-3)	945(4-II-3)
10	12	-2.97(5-I-2)	0.11(4-I-3)	-0.99(4-II-3)	1333(5-I-2)	85(4-I-3)	-290(1)
10	13	-1.97(5-I-2)	0.51(4-I-3)	0.75(4-I-1)	919(5-I-2)	-506(4-I-3)	1157(4-II-3)
10	14	-2.15(5-I-2)	0.65(4-I-3)	-1.42(4-II-3)	1007(5-I-2)	102(3)	-551(1)
10	15	5.60(5-II-2)	0.92(4-II-3)	-2.32(4-II-3)	-2794(5-II-2)	-840(4-II-3)	1638(4-I-3)
10	16	3.14(5-II-2)	0.73(4-II-3)	-1.39(4-II-3)	-1729(5-II-2)	99(4-I-3)	-524(4-I-3)
11	1	-1.28(5-II-2)	1.32(4-II-3)	-2.41(1)	-651(5-I-2)	-780(4-II-3)	971(4-I-1)
11	2	1.81(1)	0.44(4-II-3)	-0.83(4-I-3)	-901(1)	106(4-I-3)	352(2)
11	3	-0.41(5-II-2)	1.72(4-I-2)	-0.87(1)	137(1)	-794(4-I-3)	364(2)
11	4	0.61(5-II-2)	0.57(4-I-3)	-0.50(4-I-1)	-145(5-II-2)	-146(4-I-2)	289(3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
12	1	-0.14(3)	-8.59(1)	0.28(4-I-1)	75(5-I-2)	3607(1)	-127(4-I-1)
12	2	-0.11(5-I-2)	-8.62(1)	-0.40(4-II-1)	64(5-I-2)	3660(1)	238(4-II-1)
12	3	-0.08(5-I-2)	-8.48(1)	-0.46(4-II-1)	42(5-I-2)	3602(1)	384(5-I-2)
12	4	-0.06(5-I-2)	-8.08(1)	-0.49(4-II-1)	-53(5-II-2)	3437(1)	525(5-I-2)
12	5	-0.06(5-I-2)	-7.41(1)	-0.49(4-II-1)	-71(5-II-2)	3153(1)	666(5-I-2)
12	6	0.09(5-II-2)	-6.44(1)	-0.48(4-II-1)	-98(5-II-2)	2749(1)	812(5-I-2)
12	7	0.15(5-II-2)	-5.19(1)	-0.48(4-II-1)	-151(5-II-2)	2220(1)	958(5-I-2)
12	8	0.23(5-II-2)	-4.22(4-II-3)	0.41(4-I-1)	-267(5-II-2)	1764(4-II-3)	1092(5-I-2)
12	9	0.67(4-II-3)	-3.47(4-II-3)	0.85(5-II-2)	-615(5-II-2)	1460(4-II-3)	1139(5-I-2)
12	10	-0.78(5-II-2)	4.90(4-I-3)	2.33(5-II-2)	-658(5-I-2)	-2612(4-I-3)	1090(5-I-2)
12	11	-0.04(5-I-2)	-8.58(1)	0.13(4-I-1)	14(4-I-3)	3610(1)	-60(4-I-1)
12	12	-0.03(5-I-3)	-8.60(1)	-0.24(4-II-1)	30(1)	3656(1)	73(4-II-3)
12	13	0.02(5-II-3)	-8.46(1)	-0.41(5-I-2)	35(3)	3600(1)	-86(4-I-3)
12	14	0.03(5-II-2)	-8.07(1)	-0.56(5-I-2)	36(3)	3440(1)	-126(1)
12	15	0.04(5-II-2)	-7.40(1)	-0.71(5-I-2)	41(3)	3165(1)	-194(1)
12	16	0.05(5-II-2)	-6.46(1)	-0.86(5-I-2)	46(5-II-2)	2774(1)	-264(1)
12	17	0.08(5-II-2)	-5.24(1)	-1.02(5-I-2)	59(5-II-2)	2265(1)	-346(1)
12	18	0.17(5-II-2)	-4.41(4-II-3)	-1.16(5-I-2)	102(5-II-2)	1874(4-II-3)	-453(1)
12	19	0.74(5-II-2)	-3.72(4-II-3)	-1.30(5-I-2)	121(4-I-3)	1560(4-II-3)	-692(2)
12	20	-0.65(5-II-2)	2.72(4-I-3)	0.96(5-II-2)	123(5-II-2)	-1643(4-I-3)	-549(1)
13	1	0.63(4-II-3)	-7.59(4-I-3)	-2.32(4-I-3)	-540(4-II-3)	-3834(4-II-3)	-1390(4-II-3)
13	2	0.64(4-I-3)	-5.66(4-I-3)	0.52(4-I-3)	-303(2)	2444(4-I-3)	-1010(3)
13	3	0.10(4-I-3)	-5.38(4-I-3)	0.74(4-I-4)	82(5-I-3)	2318(1)	-985(3)
13	4	-0.12(5-I-3)	-6.51(1)	0.60(4-I-1)	91(5-I-3)	2804(1)	-795(3)
13	5	-0.17(3)	-7.42(1)	0.42(4-I-1)	113(5-I-3)	3203(1)	-543(3)
13	6	-0.12(5-I-2)	-8.15(1)	0.33(4-I-1)	111(3)	3595(1)	-273(4-I-1)
13	7	0.26(5-I-1)	-3.10(4-I-3)	0.68(4-II-3)	70(4-II-3)	-1958(4-II-3)	579(1)
13	8	0.33(5-II-1)	-5.48(4-I-3)	1.09(4-I-3)	156(4-II-3)	2328(4-I-3)	672(4-II-3)
13	9	-0.06(4-I-3)	-5.46(4-I-3)	1.06(3)	33(5-II-3)	2372(1)	466(4-II-3)
13	10	-0.07(4-I-3)	-6.52(1)	0.85(3)	43(4-I-3)	2818(1)	340(4-II-3)
13	11	-0.05(5-I-2)	-7.43(1)	0.58(3)	22(5-II-3)	3207(1)	256(4-II-3)
13	12	-0.08(5-I-4)	-8.12(1)	0.27(4-I-1)	25(3)	3587(1)	118(4-II-1)
14	1	1.20(5-II-4)	0.38(4-I-3)	0.54(4-II-3)	-600(5-II-4)	69(4-II-3)	-220(4-II-3)
14	2	0.83(5-I-4)	1.23(4-I-3)	1.52(4-II-1)	-494(5-I-4)	-702(4-I-3)	-614(4-II-1)
14	3	0.45(5-II-4)	0.38(4-II-3)	0.32(4-II-1)	-84(5-II-1)	-96(4-II-4)	-190(2)
14	4	-0.24(5-II-4)	1.13(4-II-3)	0.56(5-II-4)	90(5-II-4)	-532(4-II-3)	-234(2)
15	1	-0.85(5-II-4)	3.14(4-II-3)	-1.58(5-II-4)	-591(5-I-4)	-1687(4-II-3)	-775(5-I-4)
15	2	0.35(4-I-3)	-3.72(4-I-3)	-1.34(5-II-4)	-338(2)	1600(4-I-3)	-871(5-I-4)
15	3	0.31(5-II-4)	-4.60(4-I-3)	-0.84(5-II-4)	-322(5-II-4)	1924(4-I-3)	-875(5-I-4)
15	4	0.23(5-II-4)	-5.25(4-I-3)	-0.49(5-II-4)	-230(5-II-4)	2206(3)	-784(5-I-4)
15	5	0.16(5-II-4)	-6.41(3)	0.34(5-I-4)	-155(5-II-4)	2715(3)	-714(5-I-4)
15	6	0.11(5-II-4)	-7.22(3)	0.40(5-I-4)	-111(5-II-4)	3064(3)	-631(5-I-4)
15	7	0.08(5-II-3)	-7.66(3)	0.43(5-I-4)	-84(5-II-4)	3259(3)	-530(5-I-4)
15	8	0.06(5-II-3)	-7.79(2)	0.43(5-I-4)	-65(5-II-3)	3321(2)	-415(5-I-4)
15	9	-0.06(5-I-3)	-7.67(1)	0.46(4-I-1)	-54(5-II-3)	3274(1)	-291(5-I-4)
15	10	-0.06(5-I-3)	-7.27(1)	0.51(4-I-1)	-52(5-II-3)	3110(1)	-164(5-I-4)
15	11	0.08(5-II-3)	-6.56(1)	0.62(4-I-1)	-72(5-II-3)	2814(1)	217(1)
15	12	0.17(4-I-3)	-5.40(1)	0.90(4-I-3)	-115(5-II-3)	2341(1)	289(1)
15	13	0.68(4-II-3)	-4.81(4-II-3)	1.19(4-I-2)	-398(2)	2111(4-II-3)	237(1)
15	14	0.77(4-I-3)	-6.03(4-II-3)	3.41(4-II-3)	-557(4-I-3)	-3043(4-I-3)	-1354(4-II-3)
15	15	-0.57(5-II-4)	2.01(4-II-3)	-0.65(5-II-4)	83(2)	-1148(4-II-3)	373(1)
15	16	0.34(5-II-4)	-3.60(4-I-3)	1.00(5-I-4)	130(4-II-3)	1550(4-I-3)	625(3)
15	17	0.26(5-II-4)	-4.70(4-I-3)	0.94(5-I-4)	80(5-II-4)	1988(4-I-3)	457(3)
15	18	0.14(5-II-4)	-5.30(4-I-3)	0.84(5-I-4)	74(2)	2249(3)	346(3)
15	19	0.09(5-II-4)	-6.41(3)	0.75(5-I-4)	59(2)	2736(3)	268(2)
15	20	0.06(5-II-4)	-7.20(3)	0.66(5-I-4)	48(2)	3075(3)	193(2)
15	21	0.05(5-II-4)	-7.65(3)	0.55(5-I-4)	41(2)	3266(3)	135(4-II-3)
15	22	0.04(5-II-3)	-7.78(2)	0.43(5-I-4)	36(2)	3324(2)	94(4-II-3)
15	23	0.03(5-II-3)	-7.65(1)	0.29(5-I-4)	33(2)	3275(1)	-119(4-I-3)
15	24	0.03(5-II-3)	-7.25(1)	0.15(5-I-4)	29(2)	3113(1)	-194(4-I-3)
15	25	0.03(4-I-3)	-6.55(1)	-0.26(1)	48(4-II-3)	2825(1)	-299(4-I-3)
15	26	0.07(4-I-3)	-5.48(1)	-0.37(1)	41(5-II-3)	2383(1)	-442(4-I-3)
15	27	0.38(5-II-1)	-4.50(4-II-3)	-0.45(4-I-3)	183(4-I-3)	1946(4-II-3)	-637(4-I-3)
15	28	0.22(5-I-1)	1.78(4-I-3)	0.94(4-II-3)	108(4-I-3)	-1176(4-I-3)	-680(3)
16	1	3.63(5-I-4)	0.67(4-I-1)	-1.57(4-I-1)	-2018(5-I-4)	128(4-II-1)	-435(4-II-1)
16	2	6.19(5-I-4)	1.10(4-I-1)	-2.94(4-I-1)	-3149(5-I-4)	-939(4-I-1)	1934(4-I-1)
16	3	3.18(5-I-4)	0.63(4-II-1)	-1.69(4-I-1)	-1271(5-I-4)	146(4-I-1)	-676(2)
16	4	3.40(5-I-4)	0.49(4-II-1)	0.65(4-II-1)	-1416(5-I-4)	-516(4-II-1)	1377(4-I-1)
16	5	-1.84(5-II-4)	-0.14(4-I-1)	-1.20(4-I-1)	843(5-II-4)	83(4-II-1)	-560(2)
16	6	-1.80(5-II-4)	-0.26(4-I-1)	0.44(4-II-3)	813(5-II-4)	255(4-I-1)	1154(4-I-1)
16	7	-2.50(5-II-4)	-0.11(4-I-1)	-0.87(4-I-1)	1143(5-II-4)	38(4-II-1)	-461(3)
16	8	-2.51(5-II-4)	-0.22(4-I-1)	0.33(4-II-3)	1137(5-II-4)	211(4-I-1)	860(4-I-1)
16	9	-3.10(2)	-0.08(4-I-1)	-0.58(4-I-1)	1452(2)	-28(4-I-1)	-332(1)
16	10	-3.06(2)	-0.18(4-I-1)	0.27(5-I-1)	1447(2)	175(4-I-1)	591(4-I-1)
16	11	-3.75(2)	-0.08(4-I-1)	-0.33(4-I-1)	1726(2)	-23(4-I-1)	-215(5-I-4)
16	12	-3.71(2)	-0.17(4-I-1)	0.25(5-I-1)	1714(2)	166(4-I-1)	339(4-I-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
16	13	-3.95(1)	-0.11(4-I-1)	0.16(1)	1801(2)	33(4-II-2)	-143(5-I-4)
16	14	-3.89(1)	-0.18(4-I-1)	0.29(5-I-1)	1767(2)	171(4-I-1)	-109(1)
16	15	-3.86(1)	-0.12(4-I-1)	0.41(1)	1754(1)	61(4-II-1)	165(5-II-4)
16	16	-3.71(1)	-0.14(4-I-3)	0.32(5-I-1)	1679(1)	180(4-I-1)	-337(1)
16	17	-3.36(1)	0.52(4-II-1)	0.49(4-I-3)	1534(1)	78(5-II-4)	333(2)
16	18	-3.18(1)	0.55(4-II-3)	-0.30(4-II-1)	1452(1)	-431(4-II-1)	-429(1)
16	19	-1.83(1)	0.45(4-I-1)	-0.71(4-II-3)	417(1)	61(4-II-1)	426(3)
16	20	-3.48(5-I-4)	0.90(4-I-1)	-1.78(4-I-3)	1325(5-I-4)	-622(4-I-1)	647(4-II-3)
17	1	-2.39(5-II-4)	0.52(4-I-1)	0.85(4-II-1)	777(5-II-4)	54(4-II-3)	-486(4-II-1)
17	2	-3.87(5-II-4)	1.01(4-I-1)	1.92(4-II-1)	-1587(5-I-4)	-758(4-I-1)	1028(4-I-1)
17	3	-3.72(5-II-4)	0.59(4-II-1)	-1.18(4-I-1)	1646(5-II-4)	95(5-I-4)	-375(2)
17	4	-3.63(5-II-4)	0.58(4-II-1)	-0.59(4-I-1)	1622(5-II-4)	-472(4-II-1)	1004(4-I-1)
17	5	-3.55(5-II-4)	-0.10(4-I-1)	-0.91(4-I-1)	1559(5-II-4)	68(4-II-1)	-175(5-I-4)
17	6	-3.44(5-II-4)	0.15(4-II-1)	-0.72(4-I-2)	1499(5-II-4)	161(4-I-1)	867(4-I-1)
17	7	-3.31(1)	-0.12(4-I-1)	-0.64(4-I-1)	1509(1)	32(4-II-1)	138(5-II-4)
17	8	-3.33(1)	-0.20(4-I-1)	-0.71(3)	1514(1)	188(4-I-1)	600(4-I-1)
17	9	-2.86(1)	-0.15(4-I-1)	-0.32(5-I-4)	1330(1)	-24(4-I-2)	199(5-II-4)
17	10	-2.94(1)	-0.25(4-I-1)	-0.58(3)	1355(1)	224(4-I-1)	322(5-I-4)
17	11	-2.19(1)	-0.16(4-I-1)	0.22(1)	1043(1)	50(4-II-2)	256(5-II-4)
17	12	-2.17(1)	-0.22(4-I-3)	-0.44(5-II-2)	1031(1)	239(4-I-2)	-163(4-I-3)
17	13	-1.28(5-I-4)	0.46(4-II-4)	0.53(4-I-3)	657(1)	73(5-II-4)	393(3)
17	14	-1.30(5-I-4)	0.41(4-II-3)	-0.49(4-II-1)	643(5-I-4)	-341(4-II-4)	-421(4-I-3)
17	15	0.97(3)	0.39(4-I-4)	-0.80(4-II-3)	-744(3)	61(4-II-1)	436(3)
17	16	2.37(5-II-4)	0.67(4-I-2)	-1.82(4-II-3)	-1358(5-II-4)	-519(4-I-3)	679(4-II-3)
18	1	1.75(5-I-4)	-0.45(4-II-1)	0.95(4-II-1)	-1209(5-I-4)	36(4-II-3)	-648(2)
18	2	3.32(5-I-4)	0.88(4-I-1)	2.21(4-II-1)	-1918(5-I-4)	-644(4-I-1)	-782(4-II-1)
18	3	-3.15(5-II-4)	0.57(4-II-1)	-0.97(4-I-1)	1399(5-II-4)	76(5-I-4)	-572(2)
18	4	-3.09(5-I-4)	0.55(4-II-1)	0.54(4-II-1)	1397(5-II-4)	-435(4-II-4)	852(4-I-1)
18	5	-3.52(1)	0.08(4-II-2)	-0.77(4-I-1)	1567(1)	66(4-II-1)	-308(5-I-4)
18	6	-3.38(1)	0.14(4-II-1)	-0.30(4-I-1)	1510(1)	-152(4-II-1)	742(4-I-1)
18	7	-4.13(1)	-0.08(4-I-3)	-0.54(4-I-1)	1828(1)	36(4-II-1)	-233(5-I-4)
18	8	-4.12(1)	-0.14(4-I-2)	-0.25(4-I-1)	1810(1)	126(4-I-1)	524(4-I-1)
18	9	-4.51(1)	-0.07(4-I-2)	-0.38(5-I-4)	1997(2)	26(4-II-1)	-176(5-I-4)
18	10	-4.51(1)	-0.15(4-I-2)	-0.14(5-II-2)	1988(2)	127(4-I-2)	376(5-I-4)
18	11	-4.68(2)	-0.07(4-I-2)	-0.23(5-I-4)	2065(2)	26(4-II-3)	-121(5-I-4)
18	12	-4.66(2)	-0.13(4-I-2)	0.16(1)	2052(2)	117(4-I-2)	234(5-I-4)
18	13	-4.54(2)	-0.07(4-I-1)	0.37(4-I-3)	2007(2)	38(4-II-3)	150(5-II-4)
18	14	-4.51(2)	-0.10(4-I-2)	0.20(1)	1980(2)	101(4-I-3)	-333(4-I-3)
18	15	-4.10(1)	0.10(4-II-2)	0.56(4-I-3)	1808(1)	64(4-II-3)	240(5-II-4)
18	16	-3.93(1)	0.17(4-II-3)	-0.27(4-II-3)	1736(1)	-171(4-II-3)	-517(4-I-3)
18	17	-3.23(5-I-4)	0.57(4-II-3)	0.72(4-I-3)	1446(5-I-4)	77(5-II-4)	505(3)
18	18	-3.17(5-I-4)	0.56(4-II-3)	-0.79(4-II-3)	1445(5-I-4)	-435(4-II-3)	-599(4-I-3)
18	19	-1.30(5-I-4)	-0.47(4-II-3)	-1.09(4-II-3)	-817(5-II-4)	52(4-II-1)	657(3)
18	20	-3.20(5-I-4)	0.90(4-I-3)	-2.48(4-II-3)	-1502(5-II-4)	-642(4-I-3)	954(4-II-3)
19	1	0.79(4-II-3)	0.40(4-I-4)	0.66(4-I-1)	-789(5-I-4)	57(4-II-3)	-469(2)
19	2	-2.48(5-II-4)	0.76(4-I-2)	1.69(4-II-1)	-1468(5-I-4)	-606(4-I-1)	813(4-I-1)
19	3	-2.14(1)	0.49(4-II-3)	-0.93(4-I-1)	990(1)	85(5-I-4)	-541(3)
19	4	-2.13(5-I-4)	0.50(4-II-1)	0.34(4-II-1)	966(5-II-4)	-390(4-II-4)	803(4-I-1)
19	5	-3.30(1)	-0.14(4-I-3)	-0.67(3)	1485(1)	52(4-II-3)	-369(5-I-4)
19	6	-3.25(1)	-0.19(4-I-1)	0.18(5-I-2)	1464(1)	203(4-I-2)	626(3)
19	7	-4.15(1)	-0.10(4-I-3)	-0.42(3)	1847(1)	28(4-II-1)	-297(5-I-4)
19	8	-4.17(1)	-0.18(4-I-3)	0.17(5-I-2)	1850(1)	169(4-I-2)	426(3)
19	9	-4.70(1)	-0.08(4-I-3)	-0.25(5-I-4)	2081(1)	-22(4-I-3)	-215(5-I-4)
19	10	-4.69(1)	-0.16(4-I-3)	0.17(5-I-2)	2079(1)	155(4-I-3)	262(5-I-4)
19	11	-4.87(1)	-0.06(4-I-3)	0.24(4-I-3)	2148(1)	23(4-II-3)	-132(5-I-4)
19	12	-4.86(1)	-0.13(4-I-3)	0.17(4-I-3)	2147(1)	134(4-I-3)	-221(4-I-3)
19	13	-4.59(1)	-0.09(4-I-3)	0.46(4-I-3)	2023(1)	35(4-II-3)	155(5-II-4)
19	14	-4.63(1)	-0.15(4-I-3)	-0.25(4-I-3)	2033(1)	149(4-I-3)	-406(4-I-3)
19	15	-4.04(5-I-4)	0.13(4-II-3)	0.72(4-I-3)	1780(5-I-4)	-41(4-I-3)	240(5-II-4)
19	16	-3.97(5-I-4)	0.20(4-II-3)	-0.34(4-II-3)	1740(1)	178(4-I-3)	-657(4-I-3)
19	17	-3.55(5-I-4)	0.28(4-II-4)	0.94(4-I-3)	1577(5-I-4)	109(5-II-4)	468(2)
19	18	-3.72(5-I-4)	0.31(4-II-3)	-0.91(4-II-3)	1651(5-I-4)	-246(4-II-1)	-733(4-I-3)
19	19	-2.23(5-I-4)	0.46(4-I-3)	0.70(4-I-3)	-935(5-II-4)	57(5-II-4)	336(4-II-3)
19	20	-3.19(5-I-4)	0.81(4-I-3)	-1.31(4-II-3)	-1579(5-II-4)	-675(4-I-3)	-860(4-I-3)
20	1	-1.60(1)	0.34(4-I-3)	0.42(4-II-1)	364(1)	38(5-I-4)	-383(3)
20	2	-2.18(1)	0.73(4-I-3)	1.14(4-II-1)	625(5-II-4)	-503(4-I-3)	-344(4-II-1)
20	3	-3.40(1)	0.34(4-II-3)	-0.36(4-I-4)	1554(1)	74(5-I-4)	-407(3)
20	4	-3.26(1)	0.29(4-II-1)	0.56(4-II-3)	1486(1)	-267(4-II-3)	314(4-I-3)
20	5	-4.18(1)	0.16(4-II-3)	-0.28(3)	1874(1)	54(4-II-3)	-167(5-I-4)
20	6	-4.09(1)	0.18(4-II-2)	-0.33(5-II-3)	1838(1)	-186(4-II-3)	268(3)
20	7	-4.04(1)	-0.12(4-I-3)	0.16(4-I-3)	1829(1)	37(4-II-3)	108(5-II-4)
20	8	-3.94(1)	-0.18(4-I-3)	-0.36(5-I-3)	1786(1)	186(4-I-3)	-158(4-I-3)
20	9	-3.31(1)	0.08(4-II-3)	0.48(4-I-3)	1525(1)	34(4-II-3)	241(1)
20	10	-3.27(1)	-0.15(4-I-3)	-0.37(5-II-3)	1510(1)	157(4-I-3)	-462(4-I-3)
20	11	-2.60(5-I-4)	-0.18(4-I-3)	0.77(4-I-3)	1164(5-I-4)	67(4-II-3)	392(1)
20	12	-2.66(5-I-4)	-0.20(4-I-3)	-0.60(4-II-1)	1173(5-I-4)	230(4-I-3)	-727(4-I-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
20	13	1.84(5-II-4)	0.37(4-II-3)	1.31(4-I-3)	818(5-I-4)	111(2)	432(1)
20	14	1.98(5-II-4)	0.24(4-II-3)	-0.69(4-II-3)	-808(5-II-4)	-298(4-II-3)	-1100(4-I-3)
20	15	2.46(5-II-4)	0.68(4-I-3)	1.19(4-I-3)	-1313(5-II-4)	79(4-II-3)	313(4-II-3)
20	16	4.01(5-II-4)	0.92(4-I-3)	1.95(4-I-3)	-1996(5-II-4)	-795(4-I-3)	-1363(4-I-3)
21	1	-4.22(4-I-3)	0.73(5-II-4)	1.80(5-II-4)	1445(4-I-3)	442(5-I-4)	483(5-I-4)
21	2	-5.58(3)	-1.14(5-I-4)	-1.04(5-I-4)	1981(4-I-3)	1525(1)	896(5-I-4)
21	3	-4.44(4-I-3)	0.68(5-II-4)	-1.05(5-I-4)	1773(4-I-3)	-346(5-II-4)	-608(5-II-4)
21	4	-6.67(3)	-0.84(1)	-0.72(5-I-4)	2625(3)	1354(1)	775(5-I-4)
21	5	-5.02(4-I-3)	-0.81(5-I-4)	-1.13(5-I-4)	2095(4-I-3)	-569(3)	-551(5-II-4)
21	6	-7.09(3)	-0.94(1)	-0.75(5-I-4)	3099(3)	1358(1)	646(5-I-4)
21	7	-6.12(3)	-0.82(5-I-4)	-1.16(5-I-4)	2533(3)	-604(3)	-422(5-II-4)
21	8	-7.39(3)	-1.05(1)	-0.74(5-I-4)	3344(3)	1426(1)	562(5-I-4)
21	9	-6.95(3)	-0.97(1)	-1.11(5-I-4)	2901(3)	-566(3)	-308(5-II-4)
21	10	-7.57(3)	-1.18(1)	-0.72(5-I-4)	3462(3)	1500(1)	485(5-I-4)
21	11	-7.49(3)	-1.10(1)	-0.98(5-I-4)	3130(3)	-527(3)	-216(5-II-4)
21	12	-7.65(3)	-1.30(1)	-0.70(5-I-4)	3504(3)	1561(1)	403(5-I-4)
21	13	-7.75(3)	-1.20(1)	-0.80(5-I-4)	3239(3)	-501(3)	166(4-I-1)
21	14	-7.66(2)	-1.38(1)	-0.68(4-I-1)	3497(2)	1594(1)	322(5-I-4)
21	15	-7.79(2)	-1.28(1)	-0.60(5-I-4)	3255(2)	-487(3)	209(4-I-1)
21	16	-7.57(2)	-1.43(1)	-0.70(4-I-1)	3447(2)	1613(1)	241(5-I-4)
21	17	-7.62(1)	-1.34(1)	-0.38(5-I-4)	3176(2)	-484(2)	243(4-I-1)
21	18	-7.36(1)	-1.46(1)	-0.75(4-I-1)	3338(1)	1620(1)	165(5-I-4)
21	19	-7.22(1)	-1.39(1)	0.49(1)	3005(1)	-504(1)	267(4-I-1)
21	20	-7.03(1)	-1.47(1)	-0.80(4-I-1)	3190(1)	1633(1)	-208(1)
21	21	-6.57(1)	-1.38(1)	0.71(1)	2744(1)	-604(1)	302(4-I-1)
21	22	-6.57(1)	-1.44(1)	-0.89(4-I-1)	3030(1)	1678(1)	-299(1)
21	23	-5.67(1)	-1.25(1)	0.83(1)	2355(1)	-814(1)	445(4-I-2)
21	24	-5.98(1)	-1.27(1)	-1.05(4-I-2)	2860(1)	1684(1)	-394(1)
21	25	-4.59(4-II-3)	-0.90(5-I-2)	0.92(4-II-3)	1897(4-II-3)	-1183(2)	749(4-I-3)
21	26	-5.26(1)	-1.10(5-I-3)	-1.32(4-I-3)	2448(1)	1722(1)	-418(1)
21	27	-6.60(4-II-3)	1.27(5-II-1)	-2.66(4-I-3)	-2656(4-I-3)	-589(5-II-1)	1403(4-I-3)
21	28	-4.80(1)	-1.03(5-I-4)	-1.44(4-I-3)	1331(1)	1639(1)	358(4-I-3)
22	1	-3.24(1)	-2.88(3)	1.04(5-I-3)	634(1)	-653(1)	-1417(1)
22	2	-2.12(1)	-3.55(3)	1.03(5-I-4)	542(1)	-1453(1)	-1558(3)
22	3	-1.47(5-I-4)	-3.75(4-I-3)	0.99(5-I-4)	402(4-II-3)	-2814(1)	-1098(3)
22	4	-1.26(5-I-4)	-3.40(4-I-2)	-1.02(5-II-4)	-704(4-I-3)	-1628(1)	-700(5-I-4)
22	5	1.17(4-I-3)	-2.78(4-I-2)	-1.64(5-II-4)	-534(4-I-3)	-1410(4-II-1)	977(5-II-4)
22	6	-3.05(1)	-3.79(4-I-1)	-0.84(5-II-4)	1257(1)	2478(3)	649(4-I-3)
22	7	-3.75(1)	-2.57(4-I-1)	-0.61(5-II-4)	2082(1)	2910(3)	227(5-II-4)
22	8	-3.55(1)	-2.33(3)	1.50(5-I-4)	1686(1)	2656(3)	729(2)
22	9	-2.21(4-I-3)	-1.38(1)	1.41(1)	735(5-II-4)	660(1)	-346(5-II-4)
22	10	-3.01(1)	-1.73(4-I-2)	1.26(1)	962(1)	544(4-I-2)	-1253(1)
22	11	-3.39(1)	-2.21(3)	0.93(1)	1009(1)	571(4-I-2)	-1155(1)
22	12	-2.75(1)	-2.72(3)	0.81(5-I-4)	1271(1)	698(5-I-3)	-970(1)
22	13	-2.43(1)	-3.13(4-I-2)	0.77(5-I-4)	1150(1)	1087(4-I-3)	-896(1)
23	1	-6.02(1)	-4.73(1)	1.11(3)	5808(3)	2071(1)	646(2)
23	2	-5.56(1)	-4.29(1)	0.68(4-I-1)	6477(3)	2445(1)	380(1)
23	3	-5.35(1)	-3.99(1)	0.42(5-II-2)	6478(3)	2553(1)	293(1)
23	4	-5.16(1)	-3.74(1)	-0.32(1)	6177(3)	2682(1)	176(1)
23	5	-4.98(1)	-3.44(1)	-0.55(1)	5396(1)	2759(1)	-216(4-II-3)
23	6	-4.71(1)	-3.17(1)	-0.94(1)	5550(1)	3038(1)	628(1)
23	7	-4.96(1)	-3.48(1)	-0.62(1)	5664(3)	2781(1)	211(1)
23	8	-5.18(1)	-3.82(1)	-0.45(1)	6231(3)	2770(1)	208(1)
23	9	-5.36(1)	-4.13(1)	-0.29(1)	6364(3)	2748(1)	277(1)
23	10	-5.54(1)	-4.43(1)	0.38(5-II-2)	6010(3)	2688(1)	302(1)
23	11	-5.70(1)	-4.58(1)	0.53(3)	5357(3)	2535(1)	241(1)
23	12	-5.85(1)	-4.49(1)	0.59(3)	4557(3)	2207(1)	149(1)
23	13	-5.93(2)	-4.17(1)	0.48(3)	3786(3)	1823(1)	130(1)
23	14	-5.55(2)	-3.78(1)	-0.44(1)	2826(3)	1204(1)	220(1)
23	15	-4.74(3)	-3.27(1)	-0.83(1)	1951(3)	851(1)	234(1)
23	16	-3.07(4-I-2)	-3.00(1)	-0.96(1)	774(4-I-3)	337(4-I-1)	232(5-I-3)
23	17	3.87(4-II-3)	-2.26(1)	-1.60(5-I-4)	-1999(4-II-4)	-991(5-II-4)	-1625(3)
23	18	-3.13(4-I-3)	-2.99(1)	-1.95(1)	1384(4-I-3)	-328(4-II-1)	-1761(3)
23	19	-5.09(3)	-3.39(1)	-1.77(1)	2686(3)	935(1)	-1094(3)
23	20	-6.93(3)	-3.62(1)	-1.03(1)	3372(3)	1132(1)	-855(3)
23	21	-7.84(3)	-3.95(1)	0.70(4-I-1)	3917(2)	1300(1)	-588(3)
23	22	-7.81(2)	-4.43(1)	1.66(3)	4193(2)	1492(1)	202(4-I-3)
23	23	-5.57(1)	-4.44(1)	0.54(3)	6172(3)	2517(1)	366(2)
23	24	-5.43(1)	-4.21(1)	0.39(5-II-2)	6383(3)	2645(1)	320(1)
23	25	-5.55(1)	-4.48(1)	0.46(5-II-2)	6040(3)	2614(1)	314(1)
23	26	-6.17(2)	-4.05(1)	0.36(5-II-2)	3814(3)	1446(1)	-239(5-II-2)
23	27	-6.36(1)	-4.54(1)	0.87(3)	5050(3)	1968(1)	132(5-I-2)
23	28	-5.98(1)	-4.56(1)	0.75(3)	4823(3)	2147(1)	125(5-I-2)
23	29	-6.68(2)	-4.29(1)	0.72(3)	4410(3)	1693(1)	-221(3)
23	30	-5.74(1)	-4.66(1)	0.67(3)	5502(3)	2449(1)	242(4-I-3)
23	31	-5.88(1)	-4.70(1)	0.86(3)	5564(3)	2279(1)	254(4-I-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
24	1	-3.62(1)	-4.03(1)	-0.62(3)	2072(1)	3809(1)	1731(3)
24	2	-4.17(1)	-3.93(1)	-0.42(3)	2930(2)	5419(2)	2067(3)
24	3	-4.75(1)	-3.89(1)	-0.26(3)	3246(2)	6166(2)	2098(3)
24	4	-5.54(3)	-3.91(1)	-0.28(3)	3291(3)	6347(2)	2357(3)
24	5	-5.19(1)	-3.20(1)	0.41(2)	2695(2)	6718(2)	2284(3)
24	6	-4.36(1)	-2.28(1)	1.33(3)	2588(1)	6876(2)	2026(3)
24	7	-3.33(1)	-1.05(1)	2.16(3)	1915(1)	6491(2)	1545(3)
24	8	-2.07(1)	0.91(4-II-3)	2.21(3)	1401(1)	5812(2)	1320(3)
24	9	-1.02(1)	0.95(4-II-3)	1.73(5-I-3)	-660(4-II-1)	4295(2)	455(5-II-3)
24	10	-2.56(1)	0.87(4-II-3)	1.42(5-I-3)	-971(3)	2253(1)	-666(5-I-3)
24	11	-2.71(1)	-1.17(1)	1.33(3)	416(1)	1107(1)	-311(4-I-3)
24	12	-2.96(1)	-4.01(2)	0.37(4-II-3)	244(1)	-2483(3)	-299(4-I-3)
24	13	-3.23(1)	-4.09(1)	-0.59(3)	1025(1)	1899(1)	980(3)
24	14	-3.28(1)	-2.21(1)	0.90(3)	1682(1)	3922(2)	909(3)
24	15	-3.87(1)	-3.32(1)	0.43(1)	2419(1)	5439(2)	1641(3)
25	1	-4.90(1)	-3.94(3)	0.64(4-I-3)	2490(1)	4452(3)	-727(3)
25	2	-4.74(1)	-5.76(3)	1.29(3)	2320(1)	4681(3)	-1099(3)
25	3	-4.56(1)	-7.61(3)	2.06(3)	2123(1)	3598(3)	-1145(3)
25	4	-3.81(1)	-7.57(3)	1.59(3)	2156(1)	3410(3)	-1190(3)
25	5	-3.10(1)	-6.82(3)	0.81(4-I-3)	2204(1)	2923(3)	-1394(3)
25	6	-2.10(1)	-6.67(3)	-0.46(4-II-3)	2119(1)	1172(4-I-3)	-1241(3)
25	7	-1.20(1)	-5.04(3)	-0.89(4-II-3)	860(1)	-1040(4-II-3)	-560(3)
25	8	0.70(4-II-3)	-3.43(4-I-3)	-1.87(5-II-4)	-541(3)	-2969(4-II-3)	866(5-II-4)
25	9	-1.56(1)	-4.20(3)	-0.63(5-II-4)	-946(3)	-2234(2)	1527(1)
25	10	-2.49(1)	-4.68(3)	-0.40(1)	-122(3)	-2081(3)	1725(2)
25	11	-3.35(1)	-4.51(3)	-0.59(1)	442(1)	-1722(3)	1867(2)
25	12	-4.06(1)	-3.99(3)	-0.78(1)	621(1)	-1338(3)	1911(2)
25	13	-4.53(1)	-3.27(3)	-0.92(5-I-4)	726(5-I-3)	-976(3)	1894(2)
25	14	-4.65(1)	-2.52(3)	-1.11(5-I-4)	793(5-I-3)	-675(3)	1808(2)
25	15	-4.36(1)	-2.22(3)	-1.15(5-I-4)	930(5-I-3)	-371(5-II-4)	1337(1)
25	16	-3.56(1)	-1.26(3)	-1.13(5-I-4)	983(5-I-3)	395(5-I-4)	1209(1)
25	17	-3.22(5-I-4)	-1.04(5-I-4)	-1.54(5-I-4)	1166(5-I-4)	495(5-I-4)	-708(5-II-4)
25	18	-3.88(1)	-2.20(3)	-1.14(1)	2003(1)	2467(3)	-474(5-II-4)
25	19	-4.56(1)	-2.99(3)	-0.46(1)	2354(1)	3562(3)	-362(5-II-4)
25	20	-2.80(1)	-4.95(3)	0.42(4-I-3)	1073(1)	1876(3)	-533(3)
25	21	-2.41(1)	-4.08(3)	-0.47(1)	438(4-I-3)	1045(4-I-3)	-135(4-I-1)
25	22	-3.08(1)	-4.38(3)	0.32(4-I-3)	907(1)	1513(3)	-135(4-I-1)
25	23	-4.02(1)	-4.10(3)	0.33(5-I-1)	711(1)	838(4-I-3)	662(1)
25	24	-2.19(1)	-4.01(3)	0.50(5-I-1)	-419(4-II-3)	451(4-I-3)	896(1)
25	25	-2.77(1)	-4.24(3)	0.29(5-I-1)	303(1)	-531(4-II-3)	1293(2)
25	26	-4.45(1)	-2.62(3)	-0.74(1)	1367(1)	642(3)	1274(1)
25	27	-4.35(1)	-3.38(3)	-0.32(1)	1824(1)	2153(3)	775(1)
25	28	-4.27(1)	-3.41(3)	-0.58(1)	1252(1)	568(3)	1339(1)
25	29	-3.96(1)	-3.90(3)	-0.28(1)	1118(1)	413(4-I-1)	1302(1)
25	30	-3.40(1)	-4.19(3)	-0.13(1)	759(1)	246(4-I-4)	1286(1)
25	31	-3.54(1)	-4.09(3)	0.35(3)	1170(1)	1342(3)	595(1)
25	32	-4.06(1)	-3.78(3)	0.26(5-II-2)	1718(1)	1973(3)	552(1)
25	33	-3.52(1)	-4.25(3)	0.41(4-I-3)	1393(1)	2210(3)	-200(4-I-4)
25	34	-4.27(1)	-4.20(3)	0.59(3)	2045(1)	3331(3)	-367(4-I-3)
25	35	-3.54(1)	-5.25(3)	0.57(4-I-3)	1759(1)	2863(3)	-704(3)
26	1	-3.25(5-I-2)	-0.65(4-II-3)	-1.28(4-II-1)	1365(5-I-2)	-126(4-I-3)	469(4-II-1)
26	2	-3.74(1)	-0.73(4-II-3)	-1.10(3)	1533(1)	131(4-II-3)	460(3)
26	3	-3.64(1)	-1.05(2)	-0.83(3)	1496(1)	135(4-II-4)	532(3)
26	4	-3.08(1)	-0.97(4-I-3)	-1.15(5-I-2)	1134(1)	-722(4-I-3)	526(5-I-2)
26	5	-2.86(5-II-2)	0.84(4-II-3)	-2.67(4-I-3)	1169(5-II-2)	-736(4-I-2)	1031(4-I-3)
26	6	-2.76(1)	3.04(4-I-3)	-0.82(3)	1233(1)	180(5-I-2)	217(4-I-2)
26	7	-3.50(1)	0.93(4-I-3)	-1.00(3)	1533(1)	371(4-II-3)	275(3)
26	8	-3.68(1)	-0.52(4-II-3)	-1.13(3)	1563(1)	402(4-II-3)	492(4-II-4)
26	9	-3.24(5-I-2)	-0.58(4-II-3)	-1.25(4-II-1)	1385(5-I-2)	457(4-II-3)	628(4-II-4)
26	10	-2.63(5-I-2)	-0.85(4-II-3)	-1.26(4-II-1)	1140(5-I-2)	627(4-II-3)	780(4-II-4)
26	11	2.15(5-II-2)	-0.74(4-II-3)	-1.11(4-II-1)	-1012(5-II-2)	493(4-II-3)	746(4-II-4)
26	12	7.34(5-II-2)	2.81(4-I-3)	2.47(4-I-2)	-3154(5-II-2)	-1300(4-I-3)	-1111(4-I-2)
26	13	1.99(5-II-2)	1.11(4-I-3)	-1.50(4-II-4)	815(5-I-2)	-426(4-I-3)	-373(4-I-1)
26	14	-2.73(5-I-2)	-0.72(4-II-3)	-1.47(4-II-1)	1162(5-I-2)	-270(4-I-3)	418(4-II-1)
27	1	-5.41(2)	-2.94(3)	-0.47(4-II-3)	7749(2)	1997(3)	555(4-I-3)
27	2	-5.42(2)	-2.91(3)	-0.48(4-II-3)	7594(2)	2031(3)	581(4-II-3)
27	3	-5.47(2)	-2.86(3)	-0.48(4-II-3)	6918(2)	2033(3)	589(4-II-3)
27	4	-5.52(2)	-2.81(3)	-0.46(4-II-3)	5732(3)	1999(3)	564(4-II-4)
27	5	-5.56(2)	-2.80(3)	-0.43(4-II-4)	4054(3)	1881(3)	493(4-II-1)
27	6	-5.54(2)	-2.82(3)	-0.39(1)	2345(4-II-2)	1605(3)	383(4-II-1)
27	7	-5.43(2)	-2.77(3)	-0.32(1)	-1535(4-I-2)	979(3)	203(4-II-1)
27	8	-5.26(1)	-2.42(3)	-0.30(1)	-4327(1)	371(4-II-1)	-134(5-I-4)
27	9	-5.14(1)	-2.63(5-I-2)	-0.89(4-I-1)	-8538(2)	-1838(5-II-2)	1264(5-II-2)
27	10	-5.56(1)	-2.56(3)	0.68(5-II-2)	-6893(2)	498(4-II-1)	816(3)
27	11	-5.61(1)	-3.76(3)	0.83(5-II-2)	-5853(1)	856(3)	636(3)
27	12	-5.61(1)	-4.40(3)	0.67(5-II-2)	-5720(1)	1229(3)	554(3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
27	13	-5.70 (1)	-4.46 (3)	-0.58 (4-II-1)	-5873 (1)	1290 (5-II-2)	462 (4-II-3)
27	14	-5.95 (1)	-3.98 (3)	-0.91 (4-II-1)	-6229 (1)	1266 (5-II-2)	410 (4-II-3)
27	15	-6.04 (2)	-3.80 (5-II-2)	-0.96 (4-II-1)	-7139 (2)	951 (5-II-2)	497 (4-II-3)
27	16	-5.16 (1)	-3.71 (5-II-2)	1.74 (4-I-3)	-8824 (2)	-2283 (5-I-2)	-816 (5-I-2)
27	17	-5.11 (2)	-3.04 (3)	0.77 (4-I-3)	-2463 (4-I-1)	-629 (5-I-2)	891 (5-II-2)
27	18	-5.43 (2)	-3.20 (3)	0.48 (4-I-3)	2197 (4-II-1)	948 (5-II-2)	762 (5-II-2)
27	19	-5.62 (2)	-3.15 (3)	0.37 (4-I-3)	4558 (3)	1587 (3)	669 (4-II-3)
27	20	-5.72 (2)	-3.09 (3)	0.34 (4-I-3)	6384 (3)	2062 (3)	686 (4-II-3)
27	21	-5.77 (2)	-3.06 (3)	-0.35 (4-II-3)	7482 (2)	2306 (3)	711 (4-II-3)
27	22	-5.79 (2)	-3.03 (3)	-0.36 (4-II-3)	7957 (2)	2330 (3)	722 (4-II-3)
27	23	-5.77 (2)	-3.00 (3)	-0.37 (4-II-3)	7766 (2)	2140 (3)	658 (4-II-3)
27	24	-5.80 (2)	-2.93 (3)	-0.36 (4-II-3)	6951 (2)	1830 (3)	549 (4-II-3)
27	25	-5.82 (2)	-2.87 (3)	0.37 (4-I-3)	5234 (1)	1366 (3)	505 (4-II-3)
27	26	-5.60 (2)	-2.90 (3)	0.36 (4-I-3)	6632 (2)	1772 (3)	427 (4-II-3)
27	27	-5.52 (2)	-2.97 (3)	-0.43 (4-II-3)	7425 (2)	1899 (3)	522 (4-II-3)
27	28	-5.65 (2)	-2.98 (3)	-0.39 (4-II-3)	7827 (2)	2079 (3)	621 (4-II-3)
27	29	-5.55 (2)	-2.97 (3)	-0.41 (4-II-3)	7808 (2)	2082 (3)	626 (4-II-3)
27	30	-5.70 (2)	-3.03 (3)	-0.36 (4-II-3)	7509 (2)	2203 (3)	702 (4-II-3)
27	31	-5.70 (2)	-3.01 (3)	-0.37 (4-II-3)	7891 (2)	2223 (3)	684 (4-II-3)
27	32	-5.63 (2)	-3.00 (3)	-0.38 (4-II-3)	7654 (2)	2138 (3)	679 (4-II-3)
27	33	-5.52 (2)	-2.95 (3)	-0.42 (4-II-3)	7380 (2)	2056 (3)	651 (4-II-3)
27	34	-5.60 (2)	-3.00 (3)	0.39 (4-I-3)	7030 (3)	2045 (3)	707 (3)
27	35	-5.66 (2)	-3.05 (3)	0.39 (4-I-3)	6683 (3)	2028 (3)	715 (4-II-3)
27	36	-5.62 (2)	-3.07 (3)	0.47 (4-I-3)	5145 (3)	1720 (3)	790 (3)
27	37	-5.89 (2)	-3.36 (3)	-0.50 (4-II-1)	-3437 (1)	1538 (5-II-2)	771 (3)
27	38	-5.84 (2)	-3.09 (5-II-2)	0.74 (4-I-3)	-3055 (1)	1244 (5-II-2)	1030 (3)
27	39	-5.79 (2)	-3.07 (3)	0.63 (4-I-4)	-1038 (4-I-1)	1499 (5-II-2)	1000 (3)
27	40	-5.61 (2)	-3.06 (3)	0.62 (4-I-3)	2729 (4-II-1)	1325 (5-II-2)	950 (3)
27	41	-5.64 (2)	-2.89 (3)	-0.40 (4-II-3)	4850 (3)	1989 (3)	684 (3)
27	42	-5.55 (2)	-2.92 (3)	-0.41 (4-II-3)	6415 (3)	2017 (3)	691 (3)
27	43	-5.60 (2)	-2.99 (3)	0.45 (4-I-3)	5781 (3)	1906 (3)	789 (3)
27	44	-5.68 (2)	-2.97 (3)	0.49 (4-I-3)	3775 (3)	1810 (3)	859 (3)
27	45	-5.72 (2)	-2.90 (3)	-0.38 (4-II-4)	2874 (4-II-2)	1963 (3)	593 (4-II-1)
27	46	-5.82 (2)	-3.01 (3)	0.47 (4-I-4)	1858 (4-II-2)	1821 (3)	791 (3)
27	47	-5.79 (2)	-3.67 (3)	0.46 (4-I-1)	-3403 (1)	1707 (3)	516 (4-II-1)
27	48	-5.85 (2)	-3.67 (3)	-0.44 (4-II-1)	-3389 (1)	1746 (3)	634 (4-II-1)
27	49	-5.87 (2)	-3.19 (3)	0.39 (4-I-1)	-1402 (4-I-2)	1967 (3)	625 (4-II-1)
27	50	-5.76 (2)	-2.97 (3)	-0.33 (4-II-1)	1369 (4-II-2)	1849 (3)	481 (4-II-1)
27	51	-5.71 (2)	-3.12 (3)	0.32 (4-I-1)	-2672 (1)	1538 (3)	352 (4-II-1)
28	1	-7.20 (3)	-4.12 (3)	-0.78 (1)	5072 (3)	2258 (3)	692 (2)
28	2	-6.66 (3)	-4.15 (3)	-1.11 (1)	5526 (3)	4008 (3)	975 (2)
28	3	-6.54 (3)	-4.04 (2)	-1.41 (1)	5701 (3)	5277 (3)	1417 (2)
28	4	-6.79 (3)	-4.07 (1)	-2.13 (2)	7305 (3)	7738 (3)	2866 (2)
28	5	-6.84 (3)	-3.85 (2)	-1.48 (1)	6447 (2)	5174 (3)	1374 (2)
28	6	-6.85 (3)	-3.84 (2)	-1.13 (1)	6339 (2)	4434 (3)	856 (2)
28	7	-6.94 (3)	-3.76 (3)	-0.97 (1)	6106 (2)	3576 (3)	569 (4-II-3)
28	8	-6.95 (3)	-3.66 (3)	-0.95 (5-II-2)	5712 (2)	2817 (3)	343 (4-II-3)
28	9	-6.80 (3)	-3.49 (3)	-1.04 (5-II-2)	5044 (2)	2018 (3)	-294 (5-I-2)
28	10	-6.54 (3)	-3.32 (3)	-1.20 (5-II-2)	4245 (2)	1162 (3)	-480 (5-I-2)
28	11	-5.99 (3)	-3.09 (3)	-1.46 (5-II-2)	3229 (2)	510 (5-II-2)	-652 (1)
28	12	-5.07 (3)	-2.78 (3)	-1.87 (2)	2234 (4-II-1)	-844 (1)	-738 (5-I-2)
28	13	-4.08 (4-II-1)	-2.26 (3)	-2.26 (2)	1537 (4-II-1)	-1701 (2)	-858 (5-I-2)
28	14	-3.35 (4-II-1)	-2.13 (5-II-2)	-2.43 (5-II-2)	-1509 (4-I-1)	-2606 (2)	-919 (5-I-2)
28	15	5.83 (4-I-1)	-1.61 (5-II-2)	-2.78 (5-II-2)	-3093 (4-I-1)	-4068 (2)	-2118 (2)
28	16	-3.34 (4-II-1)	-1.97 (5-II-2)	-3.20 (3)	1122 (4-II-1)	-3506 (3)	-2234 (2)
28	17	-4.29 (4-II-1)	-2.60 (3)	-3.47 (2)	1819 (4-II-1)	-2904 (3)	-1810 (2)
28	18	-5.78 (3)	-2.77 (3)	-3.30 (2)	2082 (4-II-1)	-2955 (2)	-1633 (2)
28	19	-7.44 (3)	-3.03 (3)	-3.02 (2)	2929 (3)	-3070 (2)	-1487 (2)
28	20	-8.61 (3)	-3.14 (3)	-2.58 (1)	3632 (2)	-3007 (2)	-1061 (1)
28	21	-9.45 (3)	-3.17 (3)	-2.04 (1)	4009 (3)	-2950 (1)	-656 (4-I-3)
28	22	-9.90 (3)	-3.23 (3)	-1.46 (4-I-1)	4236 (3)	-2884 (1)	-374 (4-I-3)
28	23	-9.87 (3)	-3.30 (3)	-1.02 (4-I-1)	4310 (3)	-2657 (1)	473 (4-II-3)
28	24	-9.55 (3)	-3.26 (3)	0.68 (4-II-1)	4077 (3)	-2586 (1)	685 (4-II-3)
28	25	-8.06 (3)	-3.96 (3)	-0.65 (4-I-1)	4687 (3)	277 (5-II-2)	514 (2)
28	26	-6.39 (3)	-3.19 (3)	-1.76 (1)	3480 (2)	-581 (1)	-613 (5-I-2)
28	27	-5.68 (3)	-3.02 (3)	-2.23 (2)	2618 (3)	-1590 (1)	-785 (1)
28	28	-6.87 (3)	-3.21 (3)	-2.26 (1)	3400 (2)	-1698 (1)	-663 (1)
28	29	-6.99 (3)	-3.40 (3)	-1.45 (1)	4318 (2)	406 (5-II-2)	-463 (5-I-2)
28	30	-7.67 (3)	-3.33 (3)	-1.93 (1)	4138 (2)	-1213 (1)	-464 (5-I-2)
28	31	-8.30 (3)	-3.50 (3)	-1.60 (1)	4628 (2)	-1004 (1)	-283 (4-I-3)
28	32	-7.25 (3)	-3.71 (3)	-1.06 (1)	5490 (2)	1951 (3)	291 (5-II-2)
28	33	-7.16 (3)	-3.63 (3)	-1.20 (1)	4931 (2)	1091 (3)	-307 (5-I-2)
28	34	-7.61 (3)	-3.68 (3)	-1.23 (1)	5043 (2)	657 (5-II-2)	-230 (5-I-2)
28	35	-7.98 (3)	-3.83 (3)	-1.04 (1)	5286 (2)	845 (5-II-2)	420 (5-II-2)
28	36	-8.57 (3)	-3.70 (3)	-1.03 (4-I-1)	4903 (2)	-702 (1)	409 (4-II-3)
28	37	-8.05 (3)	-3.83 (3)	-0.80 (1)	5045 (2)	602 (5-II-2)	501 (5-II-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
28	38	-8.68 (3)	-3.60 (3)	-1.26 (1)	4844 (2)	-988 (1)	290 (4-II-3)
28	39	-7.92 (3)	-3.72 (3)	-1.17 (1)	5233 (2)	724 (5-II-2)	335 (5-II-2)
28	40	-7.48 (3)	-3.96 (2)	-1.01 (1)	5577 (2)	1962 (3)	487 (5-II-2)
28	41	-7.14 (3)	-3.91 (2)	-1.01 (1)	5899 (2)	2891 (3)	516 (5-II-2)
28	42	-7.40 (3)	-3.82 (3)	-1.04 (1)	5606 (2)	1952 (3)	399 (5-II-2)
28	43	-7.39 (3)	-4.02 (3)	-0.92 (1)	5461 (2)	2191 (3)	561 (5-II-2)
28	44	-6.96 (3)	-4.06 (2)	-1.09 (1)	5963 (2)	3624 (3)	693 (2)
29	1	-9.45 (3)	-1.96 (1)	0.60 (3)	4256 (3)	982 (1)	-401 (4-I-1)
29	2	-8.62 (3)	-2.36 (1)	1.11 (3)	4693 (3)	1347 (1)	-290 (4-I-1)
29	3	-7.59 (3)	-2.67 (1)	1.67 (3)	4989 (3)	1640 (1)	229 (1)
29	4	-6.43 (3)	-2.92 (1)	2.12 (3)	5032 (3)	1782 (1)	403 (1)
29	5	-5.23 (3)	-3.17 (1)	2.24 (3)	4747 (3)	1795 (1)	483 (1)
29	6	-3.96 (2)	-3.33 (1)	2.19 (3)	3978 (3)	1657 (1)	497 (1)
29	7	-2.48 (4-I-1)	-3.47 (1)	1.93 (3)	2479 (3)	1392 (5-II-4)	294 (1)
29	8	-1.40 (4-I-1)	-3.41 (1)	1.58 (4-I-3)	1366 (4-I-1)	1339 (5-II-4)	-345 (4-I-2)
29	9	2.40 (4-II-1)	-4.18 (5-II-4)	1.37 (4-I-3)	-1287 (4-II-1)	-1634 (5-I-4)	801 (4-II-3)
29	10	-1.89 (4-I-1)	-3.49 (5-II-4)	1.68 (4-I-1)	-1831 (3)	1569 (5-II-4)	-271 (4-I-3)
29	11	-2.79 (3)	-3.31 (1)	1.49 (4-I-1)	-1856 (3)	1389 (5-II-4)	-364 (4-I-1)
29	12	-3.56 (3)	-3.33 (1)	0.96 (4-I-1)	-2391 (3)	1186 (1)	-321 (5-II-2)
29	13	-3.95 (3)	-3.03 (1)	0.35 (5-I-4)	-2775 (3)	939 (1)	-349 (5-II-2)
29	14	-4.02 (3)	-2.41 (1)	-0.82 (1)	-2734 (3)	570 (1)	-306 (5-II-2)
29	15	-3.56 (3)	-1.46 (1)	-1.35 (1)	-2795 (3)	-284 (5-II-4)	-201 (4-II-1)
29	16	2.26 (4-II-1)	-1.58 (5-I-4)	-1.79 (5-I-4)	-2472 (4-II-1)	-1376 (5-II-4)	-1090 (5-II-4)
29	17	-3.57 (4-I-1)	-1.84 (1)	-2.30 (1)	1079 (4-I-1)	-724 (3)	-953 (3)
29	18	-5.53 (2)	-2.24 (1)	-2.58 (1)	2339 (2)	-302 (4-II-3)	-1114 (3)
29	19	-7.42 (3)	-2.19 (1)	-2.37 (1)	3456 (2)	259 (1)	-913 (3)
29	20	-8.78 (3)	-1.98 (1)	-1.92 (1)	4138 (3)	454 (1)	-542 (3)
29	21	-9.53 (3)	-1.88 (1)	-1.33 (1)	4520 (3)	613 (1)	-106 (3)
29	22	-9.80 (3)	-1.72 (1)	-0.79 (1)	4562 (3)	668 (1)	379 (1)
29	23	-9.63 (3)	-1.59 (1)	0.45 (4-I-1)	4183 (3)	592 (1)	524 (1)
29	24	-8.87 (1)	-1.55 (1)	0.49 (4-I-1)	4025 (3)	470 (1)	698 (1)
29	25	-8.31 (1)	-1.52 (1)	-0.34 (1)	2719 (1)	427 (1)	151 (1)
29	26	-9.47 (3)	-1.40 (1)	-0.44 (1)	3111 (1)	443 (1)	-715 (3)
29	27	-9.88 (3)	-1.57 (1)	0.31 (4-I-1)	3719 (1)	551 (1)	-495 (4-I-1)
29	28	-9.21 (3)	-2.00 (1)	-0.68 (1)	4943 (3)	749 (1)	197 (1)
29	29	-9.51 (3)	-1.79 (1)	-0.45 (1)	4594 (3)	614 (1)	-219 (4-I-1)
29	30	-9.10 (3)	-2.07 (1)	0.31 (4-I-1)	4852 (3)	893 (1)	-201 (4-I-1)
29	31	-8.08 (3)	-2.22 (1)	-1.25 (1)	4693 (3)	708 (1)	144 (1)
29	32	-8.77 (3)	-2.15 (1)	-0.93 (1)	4966 (3)	772 (1)	198 (1)
29	33	-7.91 (3)	-2.44 (1)	-0.59 (1)	4945 (3)	1072 (1)	209 (1)
29	34	-8.10 (3)	-2.40 (1)	0.48 (4-I-1)	4986 (3)	1259 (1)	-169 (4-I-1)
29	35	-6.92 (3)	-2.40 (1)	-1.32 (1)	4139 (2)	679 (1)	-132 (4-I-1)
29	36	-6.68 (3)	-2.45 (1)	-0.40 (1)	4426 (3)	1160 (1)	169 (1)
29	37	-6.26 (3)	-2.75 (1)	1.39 (3)	4579 (3)	1863 (1)	188 (1)
29	38	-6.51 (3)	-2.52 (1)	0.74 (3)	4479 (3)	1543 (1)	157 (1)
29	39	-7.22 (3)	-2.60 (1)	1.00 (3)	4901 (3)	1637 (1)	164 (1)
29	40	-5.53 (3)	-2.37 (1)	0.29 (5-II-2)	3254 (2)	1050 (1)	-144 (4-I-1)
29	41	-5.41 (3)	-2.27 (1)	-1.10 (1)	2914 (2)	544 (1)	-160 (5-II-2)
29	42	-4.87 (3)	-2.15 (1)	0.39 (5-II-2)	1019 (4-I-1)	1113 (1)	-135 (4-I-1)
29	43	-4.61 (3)	-2.09 (1)	-0.29 (1)	893 (4-I-1)	846 (1)	-173 (4-I-1)
29	44	-4.60 (3)	-1.95 (1)	-0.27 (1)	-618 (4-II-1)	922 (1)	-156 (5-II-2)
29	45	-5.08 (3)	-1.99 (1)	0.38 (5-II-2)	1940 (2)	1105 (1)	124 (1)
29	46	-4.10 (3)	-1.78 (1)	-0.84 (1)	1007 (4-I-1)	386 (1)	184 (1)
29	47	-5.21 (3)	-2.28 (1)	0.66 (5-II-2)	2504 (2)	1370 (1)	-136 (4-I-1)
29	48	-5.67 (3)	-2.46 (1)	0.68 (5-II-2)	3630 (2)	1464 (1)	138 (1)
29	49	-5.45 (3)	-2.49 (1)	1.02 (3)	3270 (2)	1692 (1)	164 (1)
29	50	-5.40 (3)	-2.77 (1)	1.50 (3)	3898 (3)	1956 (1)	186 (1)
29	51	-4.83 (3)	-2.28 (1)	0.57 (5-I-1)	1272 (2)	1345 (1)	-153 (4-I-1)
29	52	-4.47 (3)	-2.44 (1)	0.46 (4-I-1)	-574 (4-II-1)	1243 (1)	-189 (4-I-1)
29	53	-3.54 (3)	-2.87 (1)	1.34 (3)	921 (4-I-1)	1829 (1)	-308 (4-I-1)
29	54	-4.20 (3)	-2.71 (1)	0.90 (4-I-1)	265 (4-I-1)	1540 (1)	-270 (4-I-1)
29	55	-4.47 (3)	-2.84 (1)	1.50 (3)	2727 (2)	1943 (1)	-146 (4-I-1)
29	56	-4.81 (3)	-2.50 (1)	0.99 (3)	1935 (2)	1657 (1)	-177 (4-I-1)
30	1	-5.63 (3)	-1.70 (1)	0.84 (5-II-4)	1219 (4-I-2)	-257 (4-II-1)	1453 (1)
30	2	-5.99 (3)	-2.54 (1)	0.51 (5-II-4)	1995 (2)	932 (2)	1368 (1)
30	3	-6.18 (3)	-3.11 (1)	0.36 (5-II-4)	2880 (2)	1638 (2)	1212 (1)
30	4	-6.29 (3)	-3.52 (1)	0.30 (5-II-4)	3581 (2)	2253 (2)	962 (1)
30	5	-6.38 (3)	-3.79 (1)	0.30 (5-II-1)	4102 (3)	2800 (3)	662 (1)
30	6	-6.46 (3)	-3.87 (1)	0.35 (5-II-1)	4443 (3)	3245 (3)	276 (1)
30	7	-6.61 (3)	-3.81 (1)	0.42 (5-II-1)	4722 (3)	3698 (3)	-367 (5-II-1)
30	8	-6.76 (3)	-3.62 (1)	0.56 (5-II-1)	4967 (3)	4006 (3)	-713 (2)
30	9	-6.95 (3)	-3.64 (3)	0.95 (5-II-1)	5741 (3)	4746 (3)	-2011 (3)
30	10	-6.11 (3)	-3.68 (3)	0.70 (5-II-1)	3883 (3)	4254 (3)	-1178 (3)
30	11	-5.62 (3)	-3.71 (3)	0.64 (4-I-4)	2477 (3)	2914 (2)	-784 (4-I-1)
30	12	-4.95 (3)	-3.75 (3)	0.74 (4-I-1)	669 (3)	1018 (2)	532 (4-II-1)
30	13	-4.10 (3)	-3.55 (3)	1.51 (4-I-1)	-1031 (2)	-1644 (4-I-1)	1353 (4-II-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
30	14	-4.97(4-II-1)	-4.47(4-II-1)	5.36(4-I-1)	-2823(4-I-1)	-6468(4-I-1)	3202(4-II-1)
30	15	-3.85(4-II-1)	-4.81(3)	2.00(4-I-1)	-830(4-I-1)	-4389(3)	2387(3)
30	16	-4.33(3)	-5.28(3)	-1.09(4-II-1)	812(4-II-1)	-3315(3)	2130(3)
30	17	-5.46(3)	-5.27(3)	-1.16(1)	1251(3)	-2888(3)	2306(3)
30	18	-6.52(3)	-4.93(3)	-1.35(1)	1572(3)	-2557(3)	2535(3)
30	19	-7.39(3)	-4.41(1)	-1.31(1)	1662(2)	-2221(3)	2716(3)
30	20	-8.00(3)	-3.82(1)	-1.08(1)	1573(2)	-1906(3)	2848(3)
30	21	-8.31(3)	-3.14(1)	-0.88(4-I-1)	1326(2)	-1637(3)	2929(3)
30	22	-8.28(3)	-2.45(1)	-0.68(4-I-1)	1085(4-I-2)	-1393(3)	3008(3)
30	23	-7.92(3)	-1.72(1)	0.99(4-II-1)	729(4-I-1)	-1215(3)	2986(3)
30	24	-7.03(3)	-0.90(1)	1.41(4-II-1)	-1018(4-II-1)	-1137(3)	2652(3)
30	25	-5.58(3)	0.26(5-II-4)	2.05(4-II-1)	-1398(4-II-1)	-951(3)	2568(3)
30	26	-4.29(4-I-1)	0.94(3)	2.60(4-II-1)	-2584(4-II-1)	-1182(3)	2552(3)
30	27	3.69(4-II-1)	1.47(5-II-4)	3.35(4-II-1)	-4124(4-II-1)	-1796(3)	2083(4-I-1)
30	28	-4.19(4-I-1)	0.42(4-I-1)	1.96(4-II-1)	-1933(4-II-1)	-1674(3)	1217(1)
30	29	-4.74(3)	-0.71(1)	1.26(5-II-4)	-854(4-II-1)	-830(3)	1443(1)
30	30	-7.05(3)	-2.29(1)	0.77(4-II-1)	1522(4-I-2)	-621(3)	2164(3)
30	31	-6.27(3)	-1.83(1)	0.98(4-II-1)	1258(4-I-2)	-595(4-II-1)	1929(3)
30	32	-6.43(3)	-2.51(1)	0.61(4-II-1)	1919(2)	338(4-I-1)	1722(3)
30	33	-7.39(3)	-3.44(1)	-0.45(4-I-1)	2500(2)	-248(3)	2079(3)
30	34	-7.29(3)	-2.86(1)	0.47(4-II-1)	2163(2)	-339(4-II-1)	2091(3)
30	35	-6.79(3)	-3.71(1)	0.20(5-II-4)	3103(2)	1074(2)	1533(3)
30	36	-6.58(3)	-3.55(1)	0.29(5-II-4)	3206(2)	1533(2)	1313(3)
30	37	-6.53(3)	-3.80(1)	0.26(5-II-4)	3705(2)	2146(2)	1014(1)
30	38	-6.62(3)	-3.09(1)	0.36(4-II-1)	2636(2)	866(2)	1593(3)
30	39	-7.29(3)	-3.91(1)	-0.54(1)	2581(2)	-384(3)	2089(3)
30	40	-6.93(3)	-4.28(1)	-0.64(1)	2554(3)	-452(4-I-3)	2016(3)
30	41	-6.52(3)	-4.05(1)	0.27(5-II-1)	3663(3)	2165(3)	850(1)
30	42	-6.55(3)	-3.94(1)	0.25(5-II-1)	3712(3)	2111(3)	958(1)
30	43	-6.45(3)	-3.97(1)	0.34(5-II-1)	4090(3)	2840(3)	557(1)
30	44	-6.83(3)	-3.95(1)	-0.23(1)	3188(3)	1031(2)	1475(3)
30	45	-6.65(3)	-4.15(1)	-0.23(1)	3168(3)	1102(2)	1365(3)
30	46	-6.22(3)	-3.99(1)	0.54(4-I-4)	3594(3)	2783(3)	261(1)
30	47	-6.48(3)	-3.85(1)	0.61(4-I-3)	4282(3)	3700(3)	-419(5-II-1)
30	48	-6.09(3)	-3.95(3)	0.64(4-I-3)	3831(3)	3360(3)	-453(5-II-1)
30	49	-6.40(3)	-4.06(1)	0.40(4-I-3)	3662(3)	2483(3)	589(1)
30	50	-6.43(3)	-3.95(1)	0.47(4-I-3)	4228(3)	3297(3)	173(5-I-1)
30	51	-6.35(3)	-4.25(3)	0.21(4-I-3)	3085(3)	1295(2)	1152(3)
30	52	-6.39(3)	-4.55(3)	-0.59(1)	2407(3)	-503(4-I-1)	1862(3)
30	53	-5.16(3)	-4.27(3)	0.79(4-I-1)	1448(3)	374(4-II-1)	1199(3)
30	54	-5.77(3)	-4.62(3)	-0.44(4-II-1)	2082(3)	-505(4-I-1)	1612(3)
30	55	-5.74(3)	-4.04(3)	0.64(4-I-1)	2668(3)	2204(2)	255(4-II-1)
30	56	-6.01(3)	-4.20(3)	0.48(4-I-1)	2906(3)	1609(2)	805(3)
31	1	-4.83(1)	-7.54(1)	-0.82(4-I-1)	1560(1)	3605(2)	426(4-I-1)
31	2	-5.52(1)	-7.27(1)	-0.70(4-I-1)	1901(1)	3217(3)	-332(1)
31	3	-6.31(1)	-6.68(1)	-0.64(4-I-1)	2373(1)	2712(3)	-361(1)
31	4	-6.98(1)	-5.73(1)	-0.57(4-I-1)	2837(1)	2159(3)	-320(1)
31	5	-7.70(1)	-4.52(2)	-0.44(4-I-1)	3213(1)	1692(3)	-230(4-II-1)
31	6	-7.19(1)	-5.50(1)	0.69(1)	3116(1)	2411(1)	-247(4-II-1)
31	7	-6.49(1)	-6.47(1)	0.98(1)	3084(1)	2855(1)	-387(4-II-1)
31	8	-5.78(1)	-7.24(1)	1.30(1)	2995(1)	3267(1)	-558(4-II-1)
31	9	-4.84(1)	-7.82(1)	1.59(1)	2663(1)	3471(1)	-797(1)
31	10	-3.71(1)	-9.17(1)	2.27(1)	1793(1)	3522(1)	-939(1)
31	11	-2.69(1)	-8.91(1)	-0.68(4-I-1)	931(1)	3045(1)	404(4-I-1)
31	12	-2.16(1)	-8.49(1)	-1.38(4-I-1)	804(1)	2626(1)	787(3)
31	13	-2.40(1)	-8.00(1)	-2.42(3)	877(1)	3054(1)	1257(3)
31	14	-3.23(1)	-7.67(1)	-1.54(4-I-1)	1098(1)	3683(1)	766(3)
31	15	-4.02(1)	-7.72(1)	-1.04(4-I-1)	1283(1)	3804(1)	579(4-I-1)
31	16	-5.38(1)	-7.34(1)	-0.57(4-I-1)	2198(1)	3370(2)	-410(1)
31	17	-6.00(1)	-6.87(1)	-0.55(4-I-1)	2603(1)	3072(3)	-394(1)
31	18	-5.50(1)	-7.30(1)	0.81(1)	2545(1)	3454(1)	-495(1)
31	19	-4.66(1)	-8.05(1)	0.87(1)	2086(1)	3817(1)	-578(1)
31	20	-3.91(1)	-8.04(1)	-0.74(4-I-1)	1376(1)	3663(1)	-275(1)
31	21	-4.67(1)	-7.74(1)	-0.62(4-I-1)	1846(1)	3658(1)	-324(1)
32	1	-5.13(3)	-5.91(3)	-1.41(3)	2753(3)	3836(2)	1232(1)
32	2	-6.08(3)	-5.53(3)	-1.84(3)	1703(3)	2343(2)	2224(3)
32	3	-6.98(3)	-5.29(1)	-2.58(3)	-563(4-II-1)	1109(2)	3184(3)
32	4	-7.01(3)	-4.42(1)	-1.98(4-II-1)	-935(4-II-1)	871(4-I-1)	2961(3)
32	5	-6.89(3)	-3.51(1)	-1.87(4-I-1)	-1457(4-II-1)	739(4-I-1)	2867(3)
32	6	-6.57(3)	-2.71(1)	-1.75(4-I-1)	-2520(4-II-1)	-1027(4-II-1)	2738(3)
32	7	-5.59(3)	-2.35(4-I-1)	2.85(4-II-1)	-3797(4-II-1)	-1542(4-II-1)	3274(3)
32	8	-7.28(4-I-1)	-3.06(4-I-1)	5.69(4-II-1)	-7142(4-II-1)	-3416(3)	3362(4-I-1)
32	9	-5.31(4-I-1)	-3.01(1)	1.82(4-II-1)	-1923(4-II-1)	-2305(3)	1700(3)
32	10	-5.03(3)	-3.67(1)	-0.97(4-I-1)	1413(4-I-1)	-685(4-II-1)	776(4-I-1)
32	11	-4.82(3)	-4.51(3)	-0.81(4-I-1)	2242(3)	1682(2)	-377(4-II-1)
32	12	-4.50(3)	-5.23(3)	-0.68(4-I-1)	2918(3)	3175(2)	-701(4-II-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
32	13	-4.06(3)	-5.94(3)	-0.63(1)	3313(3)	4684(3)	-889(3)
32	14	-3.56(3)	-6.53(3)	-0.54(2)	3425(3)	5828(3)	-1043(3)
32	15	-2.75(1)	-7.06(3)	-1.19(3)	3655(3)	8666(3)	-1515(3)
32	16	-3.78(3)	-6.52(3)	-0.89(3)	3818(3)	6522(3)	-483(4-I-1)
32	17	-4.47(3)	-6.18(3)	-1.09(3)	3339(3)	5209(3)	379(1)
32	18	-5.88(3)	-4.30(1)	-1.45(4-I-1)	1148(4-I-1)	1125(4-I-1)	1719(3)
32	19	-5.50(3)	-3.74(1)	-1.35(4-I-1)	1100(4-I-1)	643(4-I-1)	1560(3)
32	20	-5.22(3)	-4.46(1)	-1.11(4-I-1)	1767(3)	1505(2)	807(1)
32	21	-5.22(3)	-5.48(3)	-1.25(4-I-1)	2401(3)	3240(2)	1092(1)
32	22	-5.92(3)	-5.06(3)	-1.60(4-I-1)	1423(3)	2000(2)	2023(3)
32	23	-5.66(3)	-4.87(3)	-1.35(4-I-1)	1673(3)	2106(2)	1377(3)
32	24	-4.96(3)	-5.11(3)	-0.99(4-I-1)	2440(3)	2809(2)	391(4-I-1)
32	25	-4.65(3)	-5.73(3)	-0.94(2)	2998(3)	4197(3)	222(4-I-1)
33	1	-2.67(3)	-3.13(1)	0.31(4-II-3)	2277(3)	-2805(4-II-1)	-776(4-II-4)
33	2	-3.25(3)	-3.49(2)	0.43(4-II-3)	2649(3)	-1589(4-II-2)	-669(4-II-4)
33	3	-2.92(3)	-2.81(1)	0.49(4-II-4)	1719(3)	-3227(4-II-2)	733(4-I-1)
33	4	-3.28(3)	-3.03(1)	0.53(4-II-3)	2496(3)	-1764(4-II-2)	502(4-I-1)
33	5	-2.98(3)	-2.80(1)	0.70(4-II-4)	1558(3)	-3609(4-II-2)	1365(3)
33	6	-3.31(3)	-2.92(1)	0.79(4-II-4)	2302(3)	-2433(4-II-2)	962(4-I-1)
33	7	-3.33(3)	-3.35(1)	1.50(3)	546(1)	-6236(4-II-2)	3148(3)
33	8	-2.84(3)	-3.40(1)	1.01(4-II-4)	1746(3)	-3534(4-II-2)	1683(3)
34	1	-1.77(1)	-4.44(3)	0.57(4-I-3)	-1010(5-II-3)	1150(5-I-3)	-1896(4-II-1)
34	2	-2.60(1)	-3.86(3)	0.97(4-I-3)	-773(5-II-3)	2019(3)	-1447(3)
34	3	-3.33(1)	-3.58(3)	1.06(4-I-3)	685(1)	2808(3)	-1620(3)
34	4	-4.14(3)	-3.41(3)	1.07(3)	1572(1)	3344(3)	-1848(3)
34	5	-2.04(1)	-4.43(3)	-0.72(4-II-3)	-666(4-II-1)	-1369(5-II-3)	-2148(3)
34	6	-2.62(1)	-3.82(3)	-0.42(4-II-3)	-899(5-II-3)	1472(3)	-988(3)
34	7	-2.93(1)	-3.55(3)	0.46(4-I-3)	-743(5-II-3)	2345(3)	-970(3)
34	8	-3.08(1)	-3.64(3)	0.50(4-I-3)	-462(5-II-3)	2763(3)	-933(3)
34	9	-2.68(1)	-4.51(3)	-1.48(2)	1000(1)	-1597(5-II-3)	-2847(3)
34	10	-3.24(1)	-3.86(3)	-1.12(4-II-3)	-782(4-II-1)	658(5-II-2)	-941(3)
34	11	-3.43(1)	-3.70(3)	-0.81(4-II-3)	-780(4-II-1)	1454(3)	-618(4-I-1)
34	12	-3.36(1)	-3.80(3)	-0.62(4-II-3)	-586(4-II-1)	2192(3)	-536(5-I-4)
34	13	-4.06(2)	-4.58(3)	-2.53(2)	-1181(4-II-1)	-3180(5-II-2)	-4562(3)
34	14	-4.37(2)	-4.30(3)	-1.92(2)	-1702(4-II-1)	516(5-II-2)	-857(4-I-1)
34	15	-4.50(2)	-3.75(3)	-1.56(2)	997(4-I-1)	2047(3)	677(4-II-4)
34	16	-4.99(2)	-3.17(3)	-1.41(2)	2389(1)	2810(3)	1420(1)
35	1	-2.94(3)	-2.12(3)	-0.98(3)	3528(3)	2700(3)	1487(3)
35	2	-2.85(3)	-1.89(1)	-1.22(3)	3838(3)	2236(1)	2324(3)
35	3	-2.72(3)	-1.58(1)	-1.33(3)	4614(3)	1745(1)	2421(3)
35	4	-2.78(3)	-1.18(1)	-1.42(3)	4254(3)	1049(1)	1674(3)
35	5	-2.79(3)	-1.96(3)	-0.95(3)	3052(3)	3009(3)	1174(3)
35	6	-2.73(3)	-1.87(1)	-1.34(3)	3170(3)	2298(1)	1836(3)
35	7	-2.64(3)	-1.61(1)	-1.49(3)	3485(3)	1542(1)	2254(3)
35	8	-2.59(3)	-1.26(1)	-1.70(3)	3244(3)	979(4-II-1)	1500(3)
35	9	-2.57(3)	-1.99(3)	-1.01(3)	2675(3)	2966(3)	1031(3)
35	10	-2.60(3)	-1.90(1)	-1.42(3)	2477(3)	2296(1)	1460(3)
35	11	-2.58(3)	-1.64(1)	-1.66(3)	2163(3)	1638(1)	1948(3)
35	12	-2.31(3)	-1.32(1)	-1.89(3)	2014(3)	-1067(4-I-1)	1450(3)
35	13	-2.33(3)	-2.21(3)	-0.98(3)	2404(3)	2699(3)	740(3)
35	14	-2.42(3)	-2.02(1)	-1.55(3)	1940(3)	2195(1)	949(3)
35	15	-2.41(3)	-1.74(1)	-1.82(3)	777(1)	1648(1)	1120(3)
35	16	-2.22(3)	-1.43(4-II-1)	-1.86(3)	741(1)	1247(4-II-1)	1167(3)
36	1	-2.18(1)	-4.11(3)	1.74(3)	1152(1)	1250(5-I-3)	-1246(4-II-1)
36	2	-1.71(1)	-4.30(3)	1.29(3)	751(1)	1274(5-I-3)	-1476(4-II-1)
36	3	-2.72(1)	-3.82(3)	1.49(3)	706(1)	1901(3)	-1511(3)
36	4	-3.48(3)	-3.79(3)	1.48(3)	854(3)	2829(3)	-1648(3)
36	5	-4.00(3)	-4.64(3)	1.38(3)	1343(3)	4927(3)	-1842(3)
36	6	-3.58(3)	-4.13(3)	1.44(3)	384(3)	3682(3)	-1105(3)
36	7	-3.28(3)	-3.92(3)	1.68(3)	194(3)	2116(3)	-495(5-II-2)
36	8	-2.49(3)	-4.06(3)	1.95(3)	1298(3)	1017(5-I-3)	1160(1)
36	9	-2.45(3)	-3.90(3)	1.88(3)	1162(1)	1491(3)	-623(4-II-1)
37	1	-2.60(3)	-1.36(4-I-1)	-1.19(3)	4943(3)	-1349(4-II-1)	275(5-I-4)
37	2	-1.87(1)	-1.54(1)	-1.54(3)	7040(3)	1464(4-I-1)	-2771(2)
37	3	-1.62(1)	-1.98(1)	-1.76(3)	7726(3)	2293(1)	-4219(2)
37	4	-1.40(1)	-2.55(1)	-2.01(3)	9800(3)	2923(3)	-5375(2)
37	5	-2.40(3)	-1.69(4-I-1)	-1.06(3)	3925(3)	-3276(4-II-1)	1062(3)
37	6	-1.69(1)	-1.89(1)	-1.40(3)	5909(3)	-1168(4-II-1)	-1320(2)
37	7	-1.38(1)	-2.32(1)	-1.56(3)	6846(3)	1625(4-I-1)	-2154(2)
37	8	-0.90(1)	-3.20(1)	-1.39(3)	7543(3)	1701(4-I-1)	-2745(2)
37	9	-2.28(3)	-1.83(1)	-1.01(3)	2714(3)	-4559(4-II-1)	1807(3)
37	10	-1.52(1)	-2.13(1)	-1.28(3)	4615(3)	-1874(4-II-1)	-571(1)
37	11	-1.30(1)	-2.59(1)	-1.32(3)	5606(3)	1379(4-I-1)	-1043(4-II-2)
37	12	-1.10(1)	-3.32(2)	-0.95(3)	5816(3)	1258(4-I-1)	-1703(4-II-2)
37	13	-1.75(3)	-1.90(1)	-0.91(3)	1528(3)	-5558(2)	2435(3)
37	14	-1.54(1)	-2.31(1)	-1.10(3)	3363(3)	-2395(4-II-1)	380(5-II-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
37	15	-1.35 (1)	-2.75 (1)	-1.11 (3)	4384 (3)	-1229 (4-II-1)	-556 (4-II-2)
37	16	-1.24 (1)	-3.30 (1)	-0.71 (3)	4630 (3)	-1350 (4-II-1)	-1234 (4-II-2)
38	1	-1.81 (3)	-1.93 (1)	-0.76 (3)	2146 (3)	3394 (3)	1156 (3)
38	2	-1.62 (3)	-1.95 (1)	-0.97 (3)	2191 (3)	2498 (1)	1744 (3)
38	3	-1.35 (1)	-1.92 (1)	-1.07 (3)	2226 (3)	1653 (4-II-1)	1757 (3)
38	4	-1.20 (5-II-1)	-1.81 (1)	-1.16 (4-I-1)	2330 (3)	-1998 (4-I-1)	1453 (3)
38	5	-1.27 (1)	-1.93 (1)	-0.85 (4-I-1)	1614 (3)	4377 (3)	1159 (3)
38	6	-1.33 (1)	-2.04 (1)	-0.93 (4-I-1)	1444 (3)	2683 (3)	1639 (3)
38	7	-1.42 (1)	-2.11 (1)	-0.92 (4-I-1)	1260 (3)	1443 (4-II-1)	1659 (3)
38	8	-1.53 (1)	-2.33 (1)	-0.85 (4-I-1)	939 (5-II-1)	-3412 (4-I-1)	1712 (3)
38	9	-1.17 (1)	-1.39 (1)	-0.91 (4-I-1)	1559 (3)	5020 (3)	1213 (3)
38	10	-1.44 (1)	-1.51 (1)	-0.86 (4-I-1)	1437 (3)	3096 (3)	1941 (3)
38	11	-1.70 (1)	-1.58 (1)	-0.78 (4-I-1)	1284 (3)	1428 (4-II-1)	2132 (3)
38	12	-1.95 (1)	-1.67 (1)	-0.74 (4-I-1)	846 (3)	-3464 (4-I-1)	1707 (3)
38	13	-1.50 (1)	-0.44 (1)	-0.75 (4-I-1)	2022 (3)	8440 (3)	991 (5-I-1)
38	14	-2.08 (1)	-0.42 (1)	-0.42 (4-I-1)	1248 (3)	3989 (3)	2253 (3)
38	15	-2.15 (1)	-0.78 (1)	0.31 (1)	888 (4-II-1)	1694 (4-II-1)	2383 (3)
38	16	-2.11 (1)	-1.17 (1)	0.35 (1)	721 (4-II-1)	-4555 (4-I-1)	2020 (3)
39	1	-2.73 (1)	0.77 (4-II-1)	1.72 (1)	1109 (4-II-1)	6363 (3)	4638 (3)
39	2	-2.41 (1)	-0.86 (1)	1.15 (1)	1361 (5-II-1)	3075 (3)	2735 (3)
39	3	-2.29 (1)	-1.28 (1)	1.02 (1)	1069 (5-II-1)	-1946 (4-I-1)	1711 (5-I-4)
39	4	-2.13 (1)	-1.40 (1)	0.88 (1)	-888 (5-I-1)	-5245 (4-I-1)	1628 (5-I-4)
39	5	-2.45 (1)	-2.50 (1)	1.14 (1)	1577 (5-II-1)	987 (1)	2943 (3)
39	6	-2.15 (1)	-2.07 (1)	1.29 (1)	1973 (5-II-1)	1285 (4-II-1)	2554 (3)
39	7	-2.11 (1)	-2.02 (1)	1.14 (1)	2007 (5-II-1)	-2519 (4-I-1)	1617 (5-I-4)
39	8	-2.05 (1)	-2.03 (1)	1.04 (1)	1861 (5-II-1)	-5049 (4-I-1)	1773 (4-I-1)
39	9	-2.60 (1)	-2.99 (1)	0.90 (1)	2170 (5-II-1)	-1048 (5-II-1)	2616 (3)
39	10	-2.22 (1)	-2.81 (1)	1.03 (1)	2590 (5-II-1)	-1534 (4-I-1)	2425 (3)
39	11	-2.04 (1)	-2.65 (1)	1.05 (1)	3014 (5-II-1)	-2750 (4-I-1)	1817 (3)
39	12	-1.97 (1)	-2.56 (1)	1.01 (1)	3010 (5-II-1)	-4569 (4-I-1)	2094 (4-I-1)
39	13	-2.76 (1)	-3.30 (1)	0.75 (1)	2617 (3)	-1634 (5-II-1)	2731 (3)
39	14	-2.30 (1)	-3.16 (1)	0.87 (1)	3282 (5-II-1)	-1883 (4-I-1)	2753 (3)
39	15	-2.03 (1)	-3.05 (1)	0.92 (1)	4036 (5-II-1)	-2622 (4-I-1)	2322 (3)
39	16	-1.86 (1)	-3.06 (1)	0.85 (1)	4528 (5-II-1)	-3615 (4-I-1)	2459 (4-I-1)
40	1	-1.27 (5-II-1)	-2.54 (1)	-0.99 (4-I-1)	1423 (3)	-6077 (4-II-1)	1834 (3)
40	2	-1.48 (1)	-2.58 (1)	-0.83 (4-I-1)	1464 (3)	-3550 (4-II-1)	1315 (3)
40	3	-1.66 (1)	-2.84 (1)	-0.68 (4-I-4)	1983 (3)	-2481 (4-II-1)	827 (4-I-1)
40	4	-1.92 (1)	-3.14 (1)	-0.43 (4-I-4)	2191 (3)	-2567 (4-II-1)	-509 (4-I-1)
40	5	-1.71 (1)	-2.12 (1)	-0.70 (4-I-1)	817 (4-I-1)	-5972 (4-II-1)	1739 (3)
40	6	-1.82 (3)	-2.43 (1)	-0.55 (4-I-1)	984 (4-I-1)	-4687 (4-II-1)	1603 (3)
40	7	-2.11 (3)	-2.60 (1)	-0.42 (4-I-1)	1010 (3)	-3915 (4-II-1)	1160 (3)
40	8	-2.48 (3)	-2.75 (1)	-0.30 (4-I-4)	1185 (3)	-3728 (4-II-1)	820 (4-I-1)
40	9	-2.10 (3)	-1.87 (1)	-0.43 (4-I-1)	722 (4-I-1)	-6172 (4-II-1)	1928 (3)
40	10	-2.21 (3)	-2.14 (1)	0.35 (4-II-1)	885 (4-I-1)	-5096 (4-II-1)	1415 (3)
40	11	-2.42 (3)	-2.30 (1)	0.43 (1)	864 (4-I-1)	-4379 (4-II-1)	1328 (3)
40	12	-2.83 (3)	-2.26 (1)	0.45 (4-II-1)	954 (3)	-4471 (4-II-2)	1176 (3)
40	13	-2.12 (1)	-1.61 (1)	0.67 (1)	331 (4-I-1)	-7668 (4-II-1)	1909 (3)
40	14	-1.42 (1)	-1.62 (1)	0.74 (1)	356 (4-I-1)	-5120 (4-I-1)	1404 (3)
40	15	-2.63 (3)	-1.61 (1)	0.82 (1)	720 (5-II-1)	-3400 (4-II-1)	1719 (3)
40	16	-3.05 (3)	-1.70 (1)	0.99 (1)	771 (1)	-1920 (4-II-1)	2164 (2)
41	1	-5.01 (3)	-4.34 (3)	-0.60 (4-II-3)	1924 (3)	4522 (3)	-189 (4-I-3)
41	2	-4.92 (3)	-4.23 (3)	-0.47 (4-II-4)	1445 (4-I-1)	2923 (3)	-526 (4-I-3)
41	3	-4.48 (3)	-3.92 (3)	0.74 (4-I-1)	1133 (4-I-1)	1226 (3)	-823 (4-I-4)
41	4	-3.79 (1)	-3.72 (3)	1.35 (4-I-1)	-1589 (4-II-1)	-1264 (3)	-1100 (4-I-1)
41	5	-2.72 (4-I-1)	-2.97 (5-II-1)	3.64 (4-I-1)	-2777 (2)	-6108 (3)	1858 (4-II-1)
41	6	-3.98 (1)	-3.41 (3)	1.27 (4-I-1)	-1127 (2)	-549 (5-I-3)	754 (4-II-1)
41	7	-4.40 (3)	-3.87 (3)	1.03 (4-I-1)	334 (4-II-1)	2555 (3)	657 (4-II-1)
41	8	-4.45 (3)	-4.02 (3)	0.91 (4-I-3)	824 (1)	5112 (3)	-643 (4-I-1)
41	9	-4.47 (3)	-4.43 (3)	1.15 (4-I-3)	1146 (3)	6114 (3)	-715 (4-I-1)
41	10	-4.31 (3)	-4.76 (3)	1.84 (3)	1507 (3)	7166 (3)	-799 (3)
41	11	-3.88 (3)	-4.50 (3)	0.77 (4-I-3)	792 (3)	6576 (3)	-559 (4-I-1)
41	12	-3.97 (1)	-4.84 (3)	-0.87 (4-II-3)	927 (1)	6291 (3)	-352 (4-I-4)
41	13	-4.64 (2)	-5.14 (3)	-2.07 (2)	2015 (3)	6850 (3)	1033 (1)
41	14	-5.02 (3)	-4.74 (3)	-1.47 (2)	2680 (3)	6194 (3)	710 (1)
41	15	-5.06 (3)	-4.59 (3)	-0.96 (1)	2443 (3)	5727 (3)	556 (1)
41	16	-4.33 (3)	-3.44 (3)	0.70 (4-I-1)	-803 (4-II-1)	1969 (3)	-1084 (4-I-1)
41	17	-4.50 (3)	-3.78 (3)	0.64 (4-I-3)	323 (1)	4606 (3)	-870 (4-I-1)
41	18	-4.62 (3)	-4.40 (3)	-0.53 (4-II-3)	1071 (4-I-1)	4754 (3)	-613 (4-I-4)
41	19	-4.30 (1)	-4.37 (3)	-0.66 (4-II-3)	948 (1)	5602 (3)	-544 (3)
41	20	-4.52 (3)	-4.06 (3)	0.38 (4-I-3)	745 (4-I-1)	4985 (3)	-757 (4-I-1)
41	21	-4.59 (3)	-4.46 (3)	-0.81 (4-II-3)	1353 (3)	5532 (3)	-300 (4-I-3)
41	22	-4.92 (3)	-4.70 (3)	-1.06 (4-II-3)	1952 (3)	6013 (3)	326 (1)
41	23	-4.53 (3)	-3.88 (3)	0.52 (4-I-4)	759 (4-I-1)	3163 (3)	-945 (4-I-1)
41	24	-4.73 (3)	-4.14 (3)	-0.46 (4-II-3)	1220 (4-I-1)	3978 (3)	-582 (4-I-3)
41	25	-4.85 (3)	-4.49 (3)	-0.72 (4-II-3)	1534 (3)	4545 (3)	-381 (4-I-3)
42	1	-7.57 (2)	-3.31 (3)	1.68 (3)	8704 (3)	1865 (3)	-666 (1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
42	2	-6.82 (2)	-3.15 (3)	1.46 (3)	6465 (2)	1681 (1)	-1007 (1)
42	3	-6.01 (2)	-3.45 (3)	1.57 (2)	5392 (1)	1818 (1)	-1235 (1)
42	4	-5.44 (1)	-3.51 (3)	1.52 (2)	4779 (1)	1766 (1)	-1341 (1)
42	5	-5.44 (1)	-3.56 (3)	1.31 (2)	6338 (2)	2513 (2)	-1751 (1)
42	6	-5.41 (1)	-3.61 (3)	1.23 (2)	7183 (2)	2910 (2)	-1897 (1)
42	7	-5.37 (1)	-3.65 (3)	1.20 (2)	7338 (3)	3115 (2)	-1894 (2)
42	8	-5.34 (1)	-3.66 (3)	1.17 (2)	6857 (3)	3070 (3)	-1748 (2)
42	9	-5.31 (1)	-3.67 (3)	1.12 (2)	5759 (3)	2726 (3)	-1435 (2)
42	10	-5.26 (1)	-3.68 (3)	1.04 (2)	4045 (3)	2013 (3)	-930 (2)
42	11	-5.16 (1)	-3.64 (3)	0.92 (2)	2149 (4-II-2)	952 (4-II-1)	-372 (4-II-1)
42	12	-5.03 (1)	-3.45 (3)	1.08 (4-II-1)	-2174 (4-I-2)	-883 (4-I-1)	792 (1)
42	13	-4.74 (1)	-4.00 (5-I-2)	1.47 (4-II-1)	-6511 (2)	-3296 (4-I-1)	3438 (2)
42	14	-5.33 (1)	-4.58 (3)	1.01 (2)	-5036 (2)	-1691 (4-I-1)	3348 (2)
42	15	-5.56 (1)	-5.07 (3)	0.74 (2)	-4314 (2)	-946 (4-I-1)	3393 (3)
42	16	-5.90 (2)	-4.91 (3)	0.29 (4-I-1)	-4088 (1)	-400 (4-I-1)	3186 (3)
42	17	-6.28 (2)	-4.22 (3)	-0.34 (4-II-3)	-3993 (1)	255 (4-II-1)	2848 (3)
42	18	-6.53 (2)	-3.13 (3)	-0.59 (5-II-2)	-3919 (1)	342 (5-II-2)	2421 (3)
42	19	-6.51 (2)	-1.88 (5-II-2)	-0.74 (5-II-2)	-3782 (2)	352 (5-II-2)	1901 (3)
42	20	-6.01 (3)	-0.82 (5-II-2)	-0.81 (5-II-2)	-3561 (2)	-605 (5-I-2)	1300 (3)
42	21	-4.82 (3)	2.12 (5-I-2)	1.51 (5-I-2)	-3609 (2)	-898 (4-II-1)	1132 (5-II-2)
42	22	-3.43 (4-II-1)	4.19 (4-II-1)	3.04 (5-I-2)	-4518 (2)	-2156 (2)	-1178 (5-I-2)
42	23	-4.06 (4-II-4)	0.54 (4-II-1)	-1.09 (5-II-2)	-2122 (4-I-2)	-1369 (2)	-491 (5-I-2)
42	24	-4.74 (3)	-1.11 (3)	0.67 (5-I-2)	-1221 (4-I-2)	-270 (5-I-2)	-651 (5-I-2)
42	25	-5.44 (2)	-2.08 (3)	0.71 (5-I-2)	1263 (4-II-2)	1157 (3)	-886 (4-II-1)
42	26	-5.92 (2)	-2.84 (3)	0.77 (5-I-2)	2119 (4-II-2)	2085 (3)	-1101 (2)
42	27	-6.19 (2)	-3.30 (3)	0.92 (3)	3293 (3)	2919 (3)	-1147 (2)
42	28	-6.39 (2)	-3.57 (3)	1.00 (3)	4414 (3)	3482 (3)	-1095 (2)
42	29	-6.57 (2)	-3.69 (3)	0.99 (3)	5450 (3)	3882 (3)	-955 (1)
42	30	-6.72 (2)	-3.65 (3)	0.93 (3)	6300 (2)	4149 (3)	-699 (1)
42	31	-6.91 (2)	-3.53 (3)	0.88 (3)	7096 (2)	4254 (3)	-336 (1)
42	32	-7.24 (2)	-3.24 (3)	0.86 (3)	7837 (2)	4322 (3)	395 (4-II-3)
42	33	-8.15 (2)	-3.10 (3)	1.28 (3)	9821 (3)	3324 (3)	613 (4-II-2)
42	34	-6.04 (2)	-3.65 (3)	1.26 (3)	6477 (3)	4073 (3)	-891 (2)
42	35	-6.21 (2)	-3.62 (3)	1.25 (3)	7195 (3)	3997 (3)	-832 (1)
42	36	-6.37 (2)	-3.63 (3)	1.16 (3)	6900 (3)	4179 (3)	-694 (1)
42	37	-6.52 (2)	-3.65 (3)	1.03 (3)	6606 (3)	4229 (3)	-640 (1)
42	38	-6.35 (2)	-3.67 (3)	1.08 (3)	5833 (3)	4128 (3)	-817 (1)
42	39	-6.19 (2)	-3.66 (3)	1.19 (3)	6185 (3)	4183 (3)	-792 (1)
42	40	-7.14 (2)	-3.38 (3)	1.44 (3)	8095 (2)	2993 (3)	-388 (1)
42	41	-6.53 (2)	-3.55 (3)	1.17 (3)	7335 (3)	4111 (3)	-567 (1)
42	42	-6.64 (2)	-3.46 (3)	1.13 (3)	7654 (3)	3996 (3)	-487 (1)
42	43	-6.71 (2)	-3.58 (3)	1.07 (3)	7286 (2)	4182 (3)	-479 (1)
42	44	-6.43 (2)	-3.55 (3)	1.27 (3)	7654 (3)	3896 (3)	-663 (1)
42	45	-6.88 (2)	-3.44 (3)	1.26 (3)	8043 (2)	3589 (3)	-323 (1)
42	46	-6.54 (2)	-3.46 (3)	1.44 (3)	7402 (2)	2552 (3)	-1007 (1)
42	47	-6.40 (2)	-3.53 (3)	1.40 (3)	7881 (2)	3117 (3)	-892 (1)
42	48	-6.18 (2)	-3.60 (3)	1.32 (3)	7793 (3)	3510 (3)	-967 (1)
42	49	-5.87 (2)	-3.64 (3)	1.33 (3)	7694 (2)	3209 (2)	-1376 (1)
42	50	-5.61 (1)	-3.64 (3)	1.30 (2)	7466 (2)	3024 (2)	-1690 (1)
42	51	-6.01 (2)	-3.49 (3)	1.46 (3)	6752 (2)	2426 (2)	-1423 (1)
42	52	-5.74 (1)	-3.57 (3)	1.39 (3)	6955 (2)	2642 (2)	-1647 (1)
42	53	-6.00 (2)	-3.56 (3)	1.41 (3)	7557 (2)	2890 (2)	-1346 (1)
42	54	-5.99 (2)	-3.63 (3)	1.30 (3)	7399 (3)	3751 (3)	-1086 (2)
42	55	-5.87 (2)	-3.64 (3)	1.30 (3)	6662 (3)	3851 (3)	-1106 (2)
42	56	-5.68 (2)	-3.65 (3)	1.27 (2)	6770 (3)	3568 (3)	-1351 (2)
42	57	-5.50 (1)	-3.66 (3)	1.22 (2)	6835 (3)	3293 (3)	-1585 (2)
42	58	-5.55 (1)	-3.66 (3)	1.26 (2)	7421 (3)	3264 (2)	-1689 (2)
42	59	-5.76 (2)	-3.65 (3)	1.30 (3)	7460 (3)	3479 (3)	-1405 (2)
42	60	-5.66 (2)	-3.62 (3)	1.25 (2)	5490 (3)	3409 (3)	-1133 (2)
42	61	-5.48 (1)	-3.64 (3)	1.18 (2)	5651 (3)	3044 (3)	-1332 (2)
42	62	-5.80 (2)	-3.62 (3)	1.30 (2)	5479 (3)	3750 (3)	-946 (2)
42	63	-5.96 (2)	-3.73 (3)	1.08 (2)	-802 (4-I-1)	1997 (3)	1205 (3)
42	64	-5.97 (2)	-4.17 (3)	0.79 (2)	-2285 (1)	1014 (3)	2238 (3)
42	65	-5.51 (1)	-3.48 (3)	0.97 (5-I-2)	-1549 (4-I-2)	835 (4-II-1)	844 (1)
42	66	-5.61 (1)	-3.81 (3)	1.21 (2)	-2718 (1)	742 (4-II-1)	1806 (3)
42	67	-5.75 (2)	-3.65 (3)	1.11 (2)	-978 (4-I-2)	1501 (3)	817 (1)
42	68	-5.87 (2)	-3.74 (3)	1.11 (2)	-944 (4-I-1)	1787 (3)	1073 (1)
42	69	-5.77 (2)	-4.17 (3)	0.98 (2)	-2605 (1)	851 (4-II-1)	2205 (3)
42	70	-5.48 (1)	-3.53 (3)	1.00 (2)	2103 (4-II-2)	1653 (3)	-356 (4-II-1)
42	71	-5.48 (1)	-3.60 (3)	1.10 (2)	3916 (3)	2493 (3)	-888 (2)
42	72	-5.90 (2)	-3.57 (3)	1.24 (2)	1866 (4-II-2)	2730 (3)	406 (4-I-1)
42	73	-5.71 (2)	-3.53 (3)	1.13 (2)	2087 (4-II-2)	2249 (3)	-196 (4-II-1)
42	74	-5.85 (2)	-3.57 (3)	1.21 (2)	1943 (4-II-2)	2546 (3)	299 (4-I-1)
42	75	-5.84 (2)	-3.54 (3)	1.30 (2)	2930 (3)	3269 (3)	-291 (4-II-1)
42	76	-5.81 (2)	-3.58 (3)	1.31 (2)	4228 (3)	3589 (3)	-640 (2)
42	77	-5.80 (2)	-3.55 (3)	1.27 (2)	3384 (3)	3173 (3)	-399 (4-II-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
42	78	-5.67 (2)	-3.56 (3)	1.20 (2)	3777 (3)	2978 (3)	-706 (2)
42	79	-5.81 (2)	-3.38 (3)	1.23 (3)	2948 (3)	3329 (3)	-522 (4-II-1)
42	80	-5.92 (2)	-3.35 (3)	1.11 (3)	3147 (3)	3247 (3)	-810 (2)
42	81	-5.96 (2)	-3.50 (3)	1.18 (3)	3940 (3)	3692 (3)	-756 (2)
42	82	-6.15 (2)	-3.62 (3)	1.13 (3)	4825 (3)	3888 (3)	-876 (2)
42	83	-6.03 (2)	-3.63 (3)	1.24 (3)	5261 (3)	4075 (3)	-787 (2)
42	84	-5.92 (2)	-3.63 (3)	1.30 (3)	5486 (3)	4010 (3)	-823 (2)
42	85	-5.89 (2)	-3.57 (3)	1.28 (3)	4223 (3)	3845 (3)	-647 (2)
42	86	-5.82 (2)	-3.46 (3)	1.30 (2)	3029 (3)	3450 (3)	-390 (4-II-1)
42	87	-5.85 (2)	-3.51 (3)	1.33 (2)	3012 (3)	3426 (3)	-316 (4-II-1)
42	88	-5.86 (2)	-3.58 (3)	1.33 (2)	4344 (3)	3800 (3)	-618 (2)
42	89	-6.13 (2)	-3.77 (3)	0.63 (2)	-1980 (1)	1187 (3)	2057 (3)
42	90	-5.98 (2)	-3.55 (3)	1.06 (2)	725 (4-II-1)	2138 (3)	1103 (3)
42	91	-5.88 (2)	-3.49 (3)	1.26 (2)	1908 (4-II-2)	2883 (3)	386 (4-I-1)
42	92	-6.13 (2)	-3.10 (3)	0.68 (5-I-2)	-1670 (1)	1220 (3)	1704 (3)
42	93	-5.88 (2)	-3.21 (3)	1.07 (2)	894 (4-II-2)	2174 (3)	809 (3)
42	94	-5.79 (2)	-3.34 (3)	1.26 (2)	1984 (4-II-2)	2919 (3)	279 (4-I-1)
42	95	-5.70 (2)	-3.17 (3)	1.20 (2)	2041 (4-II-2)	2808 (3)	-326 (4-II-1)
42	96	-5.67 (2)	-3.02 (3)	1.01 (2)	2099 (4-II-2)	2551 (3)	-628 (4-II-1)
42	97	-5.88 (2)	-2.33 (3)	0.85 (5-I-2)	-1413 (4-I-2)	1046 (3)	1216 (3)
42	98	-5.20 (2)	-1.51 (3)	1.04 (5-I-2)	-1324 (4-I-2)	694 (5-II-2)	669 (5-II-2)
42	99	-5.64 (2)	-2.82 (3)	1.06 (2)	1047 (4-II-2)	2041 (3)	472 (5-II-2)
42	100	-5.42 (2)	-2.46 (3)	0.98 (5-I-2)	1175 (4-II-2)	1690 (3)	-389 (5-I-2)
43	1	-3.05 (1)	-5.92 (3)	0.69 (1)	2307 (1)	3533 (2)	686 (3)
43	2	-3.15 (3)	-6.65 (3)	-0.44 (4-I-3)	2704 (3)	4368 (2)	737 (3)
43	3	-3.41 (3)	-6.93 (3)	-0.77 (4-I-3)	3069 (3)	4834 (3)	813 (3)
43	4	-3.73 (3)	-6.91 (3)	-1.05 (4-I-3)	3390 (3)	4968 (3)	904 (3)
43	5	-3.99 (3)	-6.69 (3)	-1.28 (4-I-3)	3769 (3)	4851 (3)	1069 (3)
43	6	-4.22 (3)	-6.51 (3)	-1.48 (4-I-3)	3934 (3)	4482 (3)	1166 (3)
43	7	-4.01 (3)	-6.95 (3)	-1.86 (3)	4940 (3)	4802 (3)	2127 (3)
43	8	-4.34 (3)	-6.29 (3)	-1.51 (4-I-3)	4706 (3)	4451 (3)	1069 (3)
43	9	-4.36 (3)	-6.05 (3)	-1.30 (4-I-3)	4283 (3)	4532 (3)	770 (3)
43	10	-4.33 (3)	-5.87 (3)	-1.17 (4-I-3)	3731 (3)	4583 (3)	543 (5-II-1)
43	11	-4.17 (3)	-5.73 (3)	-1.12 (5-II-1)	3094 (3)	4447 (3)	403 (5-II-4)
43	12	-3.91 (3)	-5.60 (3)	-1.16 (5-II-1)	2423 (2)	4144 (2)	275 (5-II-4)
43	13	-3.57 (3)	-5.35 (3)	-1.25 (5-II-1)	1657 (2)	3576 (2)	-257 (5-I-4)
43	14	-3.19 (3)	-4.97 (3)	-1.36 (5-II-1)	924 (5-II-4)	2805 (2)	-397 (5-I-4)
43	15	-2.55 (3)	-4.37 (3)	-1.52 (5-II-1)	441 (5-II-4)	1788 (4-I-1)	-507 (5-I-1)
43	16	-1.98 (5-II-4)	-3.54 (4-I-1)	-1.75 (5-II-1)	-1009 (5-I-4)	761 (4-I-1)	-509 (5-I-1)
43	17	-1.62 (5-II-4)	-3.01 (4-I-1)	-2.01 (4-I-3)	-1608 (5-I-4)	-1720 (4-II-1)	-501 (5-I-1)
43	18	5.77 (5-I-4)	-2.97 (4-I-1)	-2.30 (4-I-2)	-3286 (5-I-4)	-3379 (3)	-1424 (4-II-3)
43	19	2.48 (5-I-4)	-3.40 (4-I-1)	-2.44 (4-I-2)	-1194 (5-I-4)	-3408 (3)	-817 (4-II-2)
43	20	-2.07 (5-II-4)	-4.04 (3)	-2.41 (3)	-947 (5-I-4)	-3479 (3)	-776 (4-II-2)
43	21	-2.61 (5-II-4)	-4.46 (3)	-2.21 (3)	799 (5-II-4)	-3905 (3)	-822 (1)
43	22	-3.10 (2)	-4.69 (3)	-1.69 (4-I-1)	1110 (2)	-3867 (3)	-640 (1)
43	23	-3.66 (2)	-4.69 (3)	-1.21 (4-I-1)	1267 (2)	-3806 (3)	-457 (1)
43	24	-3.86 (1)	-4.51 (3)	-0.61 (4-I-1)	1347 (1)	-3750 (3)	-343 (5-I-3)
43	25	-3.67 (1)	-4.10 (3)	0.37 (1)	1300 (1)	-3477 (3)	-234 (5-I-4)
43	26	-3.25 (1)	-3.17 (3)	0.92 (1)	1118 (1)	-3236 (3)	322 (5-II-4)
43	27	-3.42 (5-I-4)	-1.96 (4-I-1)	1.48 (5-I-4)	1272 (5-I-4)	-2571 (3)	932 (5-II-4)
43	28	-2.99 (1)	-3.30 (4-I-1)	1.33 (1)	1164 (1)	824 (4-I-1)	572 (5-II-1)
43	29	-3.08 (1)	-4.68 (3)	1.04 (1)	1844 (1)	2220 (2)	648 (5-II-1)
43	30	-2.09 (5-II-4)	-4.61 (3)	-1.44 (4-I-3)	1097 (5-II-4)	-792 (4-II-1)	-417 (4-II-2)
43	31	-1.97 (5-II-4)	-4.10 (3)	-1.43 (5-II-1)	766 (5-II-4)	-773 (4-II-1)	-445 (4-II-2)
43	32	-2.09 (5-II-4)	-4.61 (3)	-1.34 (5-II-1)	1097 (5-II-4)	956 (4-I-1)	-352 (4-II-3)
43	33	-1.85 (5-II-4)	-4.43 (3)	-1.70 (4-I-3)	810 (5-II-4)	-1547 (3)	-495 (4-II-1)
43	34	-2.28 (5-II-4)	-4.67 (3)	-1.65 (4-I-2)	1096 (5-II-4)	-2193 (3)	-442 (4-II-1)
43	35	-2.50 (2)	-4.96 (3)	-1.36 (4-I-2)	1446 (2)	-1709 (3)	-320 (4-II-1)
43	36	-2.20 (5-II-4)	-4.84 (3)	-1.34 (4-I-3)	1320 (5-II-4)	-803 (4-II-1)	-361 (4-II-1)
43	37	-2.35 (2)	-5.05 (3)	-1.15 (5-II-1)	1709 (2)	1067 (4-I-1)	-301 (4-II-2)
43	38	-2.66 (1)	-5.49 (3)	-0.96 (5-II-1)	2470 (2)	1975 (2)	216 (4-I-1)
43	39	-2.56 (1)	-5.29 (3)	-1.03 (5-II-1)	2077 (2)	981 (4-I-1)	-201 (4-II-1)
43	40	-2.67 (1)	-5.43 (3)	-0.93 (5-II-1)	2274 (2)	1067 (4-I-1)	204 (4-I-1)
43	41	-2.77 (1)	-5.26 (3)	-0.90 (5-II-1)	2092 (2)	-445 (4-II-1)	153 (4-I-1)
43	42	-2.60 (2)	-5.18 (3)	-1.10 (4-I-2)	1762 (2)	-877 (3)	-239 (4-II-1)
43	43	-2.99 (1)	-5.06 (3)	-0.96 (4-I-2)	1805 (2)	-1802 (3)	-188 (4-II-1)
43	44	-2.72 (1)	-5.45 (3)	-0.84 (5-II-1)	2386 (2)	1407 (2)	287 (4-I-1)
43	45	-2.81 (1)	-5.56 (3)	-0.73 (5-II-1)	2564 (3)	2206 (2)	405 (4-I-2)
43	46	-2.82 (1)	-5.60 (3)	-0.85 (5-II-1)	2692 (3)	2564 (2)	331 (4-I-2)
43	47	-2.93 (1)	-5.70 (3)	-0.53 (5-II-1)	2565 (1)	3000 (2)	509 (4-I-2)
43	48	-3.14 (1)	-4.98 (3)	-0.66 (5-II-1)	1857 (2)	-1650 (3)	147 (5-II-2)
43	49	-2.82 (1)	-5.26 (3)	-0.78 (5-II-1)	2162 (2)	498 (4-I-1)	227 (4-I-1)
43	50	-2.80 (1)	-5.21 (3)	-0.66 (5-II-1)	2193 (1)	989 (4-I-1)	303 (5-II-2)
43	51	-2.86 (1)	-5.00 (3)	0.45 (5-I-1)	2092 (1)	1575 (2)	417 (5-II-1)
43	52	-3.03 (1)	-4.71 (3)	-0.47 (5-II-1)	1851 (1)	-1133 (3)	191 (5-II-2)
43	53	-2.85 (1)	-4.08 (3)	0.61 (5-I-1)	1707 (1)	-746 (4-II-1)	231 (5-II-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
43	54	-2.51 (2)	-4.71 (3)	-1.26 (5-II-1)	1102 (5-II-4)	1721 (4-I-1)	-379 (1)
43	55	-2.71 (2)	-5.14 (3)	-1.10 (5-II-1)	1976 (2)	2223 (2)	-224 (5-I-1)
43	56	-3.01 (3)	-5.07 (3)	-1.17 (5-II-1)	1688 (2)	2802 (2)	-285 (5-I-1)
43	57	-3.74 (3)	-5.58 (3)	-1.07 (5-II-1)	2873 (2)	4187 (2)	320 (5-II-1)
43	58	-3.39 (3)	-5.36 (3)	-1.12 (5-II-1)	2251 (2)	3542 (2)	185 (5-II-1)
43	59	-3.39 (3)	-5.53 (3)	-1.01 (5-II-1)	2886 (2)	3813 (2)	315 (5-II-1)
43	60	-2.93 (1)	-5.47 (3)	-0.99 (5-II-1)	2589 (2)	2941 (2)	219 (5-II-1)
43	61	-3.15 (1)	-6.09 (3)	-0.67 (5-II-1)	2988 (3)	3980 (2)	571 (5-II-1)
43	62	-3.07 (1)	-5.77 (3)	-0.87 (5-II-1)	3004 (3)	3537 (2)	404 (5-II-1)
43	63	-3.51 (3)	-6.28 (3)	-0.86 (4-I-3)	3394 (3)	4620 (2)	666 (3)
43	64	-3.50 (3)	-5.86 (3)	-0.92 (5-II-1)	3325 (3)	4296 (2)	479 (5-II-1)
43	65	-3.97 (3)	-5.76 (3)	-1.05 (5-II-1)	3365 (3)	4490 (3)	450 (5-II-1)
43	66	-3.86 (3)	-5.92 (3)	-1.01 (4-I-3)	3612 (3)	4609 (3)	555 (5-II-1)
43	67	-4.12 (3)	-5.94 (3)	-1.10 (4-I-3)	3784 (3)	4695 (3)	588 (5-II-1)
43	68	-3.85 (3)	-6.30 (3)	-1.03 (4-I-3)	3709 (3)	4850 (3)	757 (3)
43	69	-4.12 (3)	-6.25 (3)	-1.18 (4-I-3)	4030 (3)	4765 (3)	829 (3)
44	1	-6.92 (2)	-2.43 (1)	-1.63 (1)	3424 (2)	2018 (1)	-2218 (3)
44	2	-8.18 (3)	-2.45 (3)	-0.90 (4-I-4)	4056 (3)	2082 (1)	-1839 (3)
44	3	-8.81 (3)	-2.72 (3)	1.02 (4-I-4)	4385 (3)	2060 (3)	-1522 (3)
44	4	-9.20 (3)	-2.95 (3)	1.64 (4-I-4)	4223 (3)	1869 (3)	-1275 (3)
44	5	-8.93 (3)	-3.33 (3)	2.22 (4-I-4)	4064 (3)	1588 (3)	-1015 (3)
44	6	-8.02 (3)	-3.77 (3)	2.70 (3)	3693 (3)	1320 (3)	-711 (3)
44	7	-6.82 (3)	-4.22 (3)	3.36 (3)	3049 (3)	876 (3)	-491 (3)
44	8	-6.10 (3)	-4.39 (3)	2.26 (3)	3447 (3)	1819 (3)	-1112 (3)
44	9	-6.21 (3)	-4.23 (3)	1.86 (3)	3705 (3)	2700 (3)	-1558 (3)
44	10	-6.49 (3)	-3.90 (3)	1.93 (3)	3915 (3)	3085 (3)	-2062 (3)
44	11	-6.38 (3)	-4.36 (3)	1.71 (4-I-3)	4143 (3)	3767 (3)	-1435 (3)
44	12	-6.85 (3)	-4.17 (3)	1.72 (4-I-2)	4413 (3)	3202 (3)	-1260 (3)
44	13	-7.49 (3)	-3.72 (3)	1.51 (4-I-2)	4662 (3)	2962 (3)	-1182 (3)
44	14	-7.81 (3)	-3.25 (3)	1.13 (4-I-4)	4606 (3)	2718 (3)	-1133 (3)
44	15	-7.44 (3)	-2.87 (3)	0.59 (4-I-4)	4218 (3)	2503 (3)	-1128 (3)
44	16	-6.56 (3)	-2.55 (3)	-0.96 (1)	3486 (2)	2239 (1)	-1193 (3)
44	17	-4.97 (2)	-2.51 (1)	-1.67 (1)	2381 (2)	1837 (1)	-1351 (3)
44	18	-3.30 (4-I-1)	-2.91 (1)	-2.04 (1)	1213 (4-I-1)	1170 (1)	-1617 (3)
44	19	5.41 (4-II-1)	-2.53 (1)	-3.36 (5-I-4)	-2556 (4-II-1)	333 (4-I-1)	-2257 (5-II-4)
44	20	-3.12 (4-I-1)	-2.70 (1)	-2.68 (1)	1347 (4-I-1)	1049 (1)	-2813 (3)
44	21	-5.04 (2)	-2.49 (1)	-2.27 (1)	2443 (2)	1768 (1)	-2606 (3)
44	22	-7.33 (3)	-4.01 (3)	2.12 (3)	4198 (3)	2318 (3)	-1175 (3)
44	23	-8.19 (3)	-3.55 (3)	1.84 (4-I-2)	4524 (3)	2235 (3)	-1192 (3)
45	1	-9.69 (3)	-2.48 (3)	1.17 (3)	4341 (3)	1235 (3)	-788 (4-I-4)
45	2	-10.13 (3)	-2.40 (1)	1.09 (3)	4393 (3)	1146 (3)	-545 (4-I-3)
45	3	-9.96 (3)	-2.41 (1)	1.05 (3)	4195 (3)	1147 (1)	-300 (4-I-3)
45	4	-9.13 (3)	-2.53 (1)	1.02 (5-II-1)	3730 (3)	1192 (1)	286 (1)
45	5	-7.65 (3)	-2.72 (1)	1.03 (5-II-1)	3012 (2)	1243 (1)	444 (1)
45	6	-5.45 (2)	-2.95 (1)	1.03 (5-II-1)	2073 (2)	1282 (1)	522 (1)
45	7	-3.34 (4-I-1)	-3.10 (1)	0.93 (5-II-1)	1221 (4-I-1)	1028 (1)	497 (1)
45	8	5.06 (4-II-1)	-2.24 (1)	-2.26 (5-I-4)	-2091 (4-II-1)	933 (1)	781 (5-I-4)
45	9	-3.22 (4-I-1)	-2.31 (5-II-4)	1.01 (5-II-1)	1345 (4-I-1)	1078 (1)	-864 (3)
45	10	-5.41 (2)	-2.57 (1)	0.68 (5-II-1)	2282 (2)	984 (1)	-994 (3)
45	11	-7.66 (3)	-2.62 (1)	0.74 (5-II-1)	3212 (3)	959 (1)	-1012 (3)
45	12	-9.17 (3)	-2.51 (1)	0.80 (4-I-3)	3905 (3)	906 (1)	-916 (3)
45	13	-10.04 (3)	-2.39 (1)	0.96 (4-I-3)	4307 (3)	875 (1)	-752 (3)
45	14	-10.28 (3)	-2.33 (1)	1.19 (4-I-3)	4446 (3)	873 (1)	-576 (3)
45	15	-9.95 (3)	-2.36 (3)	1.47 (3)	4321 (3)	846 (1)	-427 (3)
45	16	-8.74 (3)	-2.35 (3)	1.85 (3)	3838 (3)	893 (3)	-215 (3)
45	17	-7.45 (3)	-2.41 (3)	1.69 (3)	2780 (3)	929 (3)	-257 (3)
45	18	-7.93 (3)	-2.38 (3)	1.54 (3)	2328 (3)	1040 (3)	-457 (3)
45	19	-7.89 (3)	-2.65 (3)	1.45 (3)	1247 (3)	854 (3)	-382 (3)
45	20	-7.69 (3)	-2.48 (3)	1.53 (3)	2927 (3)	951 (1)	-1494 (2)
45	21	-8.41 (3)	-2.52 (3)	1.04 (3)	3776 (3)	1124 (3)	-818 (3)
45	22	-8.38 (3)	-2.27 (3)	1.46 (3)	3625 (3)	1039 (1)	-725 (3)
46	1	-7.62 (3)	-4.40 (1)	-3.47 (3)	3859 (3)	1634 (1)	1474 (3)
46	2	-8.14 (3)	-4.20 (1)	-3.47 (3)	3810 (3)	1955 (1)	1590 (3)
46	3	-8.50 (3)	-3.72 (1)	-3.21 (2)	3423 (3)	2208 (1)	1595 (2)
46	4	-8.52 (3)	-3.01 (1)	-2.72 (2)	2861 (3)	2211 (1)	1470 (2)
46	5	-8.11 (3)	-2.39 (1)	-1.94 (2)	2272 (3)	2052 (1)	1295 (2)
46	6	-6.94 (3)	-1.76 (1)	-1.25 (4-I-1)	1508 (4-I-2)	1446 (1)	894 (2)
46	7	-4.75 (3)	-1.18 (1)	0.94 (4-II-1)	1003 (4-I-3)	1078 (1)	723 (2)
46	8	-2.55 (4-I-3)	-1.08 (1)	2.33 (4-II-1)	-1692 (4-II-3)	-268 (4-II-1)	-1250 (4-II-1)
46	9	-3.88 (4-I-3)	-2.51 (1)	-1.20 (5-I-4)	1664 (4-I-3)	-778 (3)	-837 (3)
46	10	-5.63 (3)	-3.33 (1)	-2.21 (2)	2105 (3)	-337 (5-I-4)	-312 (4-II-1)
46	11	-6.56 (3)	-4.05 (1)	-2.82 (3)	2802 (3)	442 (1)	370 (4-I-1)
46	12	-7.23 (3)	-4.26 (1)	-3.04 (3)	3190 (3)	897 (1)	683 (2)
46	13	-7.64 (3)	-4.30 (1)	-3.03 (3)	3399 (3)	1311 (1)	1019 (2)
46	14	-7.75 (3)	-4.24 (1)	-2.92 (3)	3555 (3)	1776 (1)	1339 (2)
46	15	-7.61 (3)	-4.07 (1)	-2.81 (3)	3517 (3)	2153 (1)	1635 (2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
46	16	-7.33(3)	-3.87(1)	-2.82(1)	3309(3)	2383(1)	1809(2)
46	17	-7.11(3)	-3.59(1)	-2.96(1)	2732(3)	2197(1)	1599(3)
46	18	-6.44(3)	-3.26(1)	-2.77(1)	2772(3)	2062(1)	1536(1)
46	19	-6.10(3)	-2.99(1)	-2.57(1)	1768(3)	1098(1)	749(1)
46	20	-7.19(3)	-3.38(1)	-3.13(1)	1726(3)	644(1)	615(1)
46	21	-7.42(3)	-3.63(1)	-3.14(1)	2023(3)	904(1)	751(1)
46	22	-7.00(3)	-3.71(1)	-2.96(1)	2400(3)	1008(1)	763(1)
46	23	-7.26(3)	-4.23(1)	-3.27(1)	3345(3)	1358(1)	1232(1)
46	24	-7.34(3)	-3.29(1)	-2.22(2)	3211(3)	1511(1)	1281(2)
46	25	-6.29(3)	-3.10(1)	-1.82(2)	2663(3)	831(1)	907(2)
46	26	-6.89(3)	-3.77(1)	-2.48(3)	3211(3)	1178(1)	1136(2)
46	27	-7.95(3)	-3.92(1)	-2.89(2)	3859(3)	2082(1)	1643(2)
46	28	-7.77(3)	-3.61(1)	-2.64(2)	3567(3)	1879(1)	1489(2)
46	29	-7.49(3)	-3.99(1)	-2.69(3)	3833(3)	1979(1)	1556(2)
46	30	-7.26(3)	-4.14(1)	-2.74(3)	3637(3)	1635(1)	1390(2)
46	31	-7.81(3)	-4.09(1)	-3.06(3)	4035(3)	2113(1)	1704(2)
46	32	-7.52(3)	-4.14(1)	-2.87(3)	4037(3)	2184(1)	1684(2)
46	33	-7.50(3)	-4.25(1)	-2.94(3)	3895(3)	2015(1)	1615(2)
46	34	-7.41(3)	-4.22(1)	-2.90(3)	4004(3)	2154(1)	1674(2)
46	35	-7.44(3)	-4.30(1)	-2.87(3)	3843(3)	1812(1)	1517(2)
46	36	-7.19(3)	-3.89(1)	-2.96(1)	3438(3)	2145(1)	1651(3)
46	37	-7.43(3)	-4.10(1)	-2.97(3)	3828(3)	2203(1)	1707(2)
46	38	-7.49(3)	-4.10(1)	-2.95(3)	4031(3)	2161(1)	1700(3)
46	39	-7.63(3)	-4.12(1)	-3.10(3)	4016(3)	2027(1)	1685(3)
46	40	-7.40(3)	-3.83(1)	-3.16(1)	3375(3)	1876(1)	1542(3)
46	41	-7.43(3)	-4.12(1)	-2.97(3)	3926(3)	2212(1)	1722(3)
46	42	-7.39(3)	-4.01(1)	-3.00(1)	3728(3)	1836(1)	1565(3)
47	1	-6.78(3)	-2.80(1)	-0.95(1)	3295(3)	836(1)	1034(1)
47	2	-7.11(3)	-3.62(1)	-1.75(1)	4165(3)	1153(1)	1278(1)
47	3	-6.66(3)	-4.30(1)	-2.18(1)	4708(3)	1418(1)	1374(1)
47	4	-5.93(1)	-4.67(1)	-2.39(1)	5037(3)	1680(1)	1308(1)
47	5	-5.19(1)	-4.80(1)	-2.33(1)	5050(3)	1638(1)	1057(1)
47	6	-4.57(1)	-4.43(1)	-2.13(1)	4964(3)	1602(1)	712(1)
47	7	-4.31(1)	-3.79(1)	-1.91(1)	4618(1)	1172(1)	350(1)
47	8	-4.32(1)	-4.12(1)	-2.12(1)	4424(3)	795(1)	299(1)
47	9	-3.92(1)	-4.67(1)	-2.67(1)	4172(3)	622(1)	275(1)
47	10	-4.23(1)	-5.57(1)	-4.64(3)	3983(3)	-788(4-I-1)	-629(3)
47	11	-5.92(1)	-5.14(1)	-4.42(3)	4051(3)	-858(4-I-1)	255(1)
47	12	-7.25(3)	-4.80(1)	-4.10(2)	4394(3)	-579(4-I-1)	706(1)
47	13	-8.05(3)	-4.26(1)	-3.55(2)	4363(3)	-320(5-I-4)	1145(1)
47	14	-8.37(3)	-3.62(1)	-2.70(2)	4061(3)	574(1)	1482(1)
47	15	-8.17(3)	-2.97(1)	-1.67(2)	3675(3)	882(1)	1701(1)
47	16	-7.63(3)	-2.22(1)	-0.65(4-I-4)	2734(3)	1089(1)	1850(1)
47	17	-6.22(3)	-1.67(1)	0.74(4-II-1)	1538(4-I-2)	1119(1)	2010(2)
47	18	-3.82(4-I-1)	-1.23(5-II-4)	1.54(3)	-908(4-II-4)	759(1)	2141(2)
47	19	4.52(4-II-3)	-0.68(1)	2.42(5-II-4)	-3150(4-II-3)	-223(5-I-1)	1755(5-I-4)
47	20	-3.81(4-I-2)	-1.75(1)	0.83(5-II-1)	853(4-I-4)	-343(5-I-4)	787(2)
47	21	-5.73(3)	-2.17(3)	-0.27(5-I-2)	2086(3)	502(1)	875(1)
47	22	-5.49(1)	-4.84(1)	-2.93(1)	4797(3)	1137(1)	1089(1)
47	23	-5.45(1)	-5.11(1)	-3.24(1)	4471(3)	588(1)	906(1)
47	24	-6.37(1)	-4.89(1)	-3.40(2)	4559(3)	563(1)	1173(1)
47	25	-6.99(3)	-4.58(1)	-3.17(2)	4652(3)	713(1)	1363(1)
47	26	-7.12(3)	-4.33(1)	-2.69(2)	4686(3)	975(1)	1451(1)
47	27	-6.30(3)	-4.65(1)	-2.75(1)	4871(3)	1226(1)	1335(1)
48	1	-1.01(4-I-3)	1.52(3)	3.66(3)	86(3)	317(3)	-95(4-I-3)
48	2	-3.33(3)	1.52(3)	4.11(3)	170(3)	453(3)	65(3)
48	3	-4.39(3)	1.23(4-I-3)	4.31(3)	200(3)	342(3)	37(2)
48	4	-4.49(3)	1.09(4-I-3)	4.34(3)	202(3)	167(3)	43(1)
48	5	-1.57(5-II-3)	1.47(3)	3.76(3)	67(4-I-3)	281(3)	-53(1)
48	6	-3.58(3)	1.38(3)	4.40(3)	151(3)	423(3)	139(3)
48	7	-4.42(3)	1.26(4-I-3)	4.59(3)	193(3)	324(3)	98(3)
48	8	-4.53(3)	1.27(4-I-3)	4.54(3)	196(3)	163(3)	90(1)
48	9	-2.42(3)	-0.81(1)	3.76(3)	-99(1)	278(3)	-45(1)
48	10	-3.99(3)	0.87(4-I-3)	4.51(3)	-68(1)	376(3)	173(3)
48	11	-4.51(3)	1.08(4-I-3)	4.64(3)	-55(1)	266(3)	116(3)
48	12	-4.50(3)	1.26(4-I-3)	4.60(3)	-56(1)	117(3)	97(1)
48	13	-3.85(3)	-1.63(1)	3.65(3)	-171(3)	-215(1)	-139(4-II-3)
48	14	-3.97(3)	-1.26(1)	4.06(3)	-345(3)	247(3)	-49(4-II-3)
48	15	-4.48(3)	-0.69(1)	4.34(3)	-438(3)	160(3)	-122(4-II-3)
48	16	-4.52(3)	1.20(5-II-3)	4.42(3)	-476(2)	53(4-II-3)	-158(3)
49	1	2.01(1)	1.44(3)	2.72(3)	-39(4-I-3)	455(3)	-193(3)
49	2	-3.16(3)	0.71(3)	2.70(3)	-221(2)	382(3)	-89(3)
49	3	-4.43(3)	-0.39(1)	2.77(3)	-375(2)	219(3)	-99(3)
49	4	-4.53(3)	-0.94(1)	2.79(3)	-465(2)	-86(1)	-98(5-II-3)
49	5	1.22(1)	1.78(3)	3.20(3)	89(3)	339(3)	-166(3)
49	6	-2.92(3)	1.40(3)	3.33(3)	67(5-II-3)	405(3)	40(1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
49	7	-4.29(3)	0.88(4-I-3)	3.22(3)	-51(1)	277(3)	39(1)
49	8	-4.58(3)	-0.71(1)	3.18(3)	-91(1)	119(5-II-3)	56(3)
49	9	-1.02(4-I-3)	1.89(3)	3.42(3)	100(3)	309(3)	-140(3)
49	10	-3.07(3)	1.64(3)	3.67(3)	165(3)	439(3)	45(1)
49	11	-4.32(3)	1.19(3)	3.69(3)	190(3)	320(3)	38(1)
49	12	-4.63(3)	0.96(4-I-3)	3.66(3)	179(3)	153(3)	56(3)
49	13	-1.41(5-II-3)	1.77(3)	3.50(3)	104(3)	259(3)	-118(3)
49	14	-3.23(3)	1.41(3)	3.87(3)	150(3)	426(3)	38(1)
49	15	-4.34(3)	1.16(4-I-3)	4.03(3)	189(3)	329(3)	19(1)
49	16	-4.70(3)	1.13(4-I-3)	4.07(3)	192(3)	167(3)	27(1)
50	1	2.19(1)	1.27(3)	1.88(1)	-82(1)	-386(1)	63(1)
50	2	-2.73(3)	0.84(3)	2.12(1)	112(4-I-4)	422(3)	166(1)
50	3	-4.69(3)	-0.96(1)	2.07(3)	172(3)	446(3)	114(1)
50	4	-5.39(3)	-1.16(1)	1.94(5-II-3)	224(3)	318(3)	31(1)
50	5	1.44(1)	1.20(3)	1.95(1)	-148(1)	-351(1)	82(2)
50	6	-2.86(3)	0.88(3)	2.51(3)	96(4-I-4)	400(3)	198(1)
50	7	-4.52(3)	-0.72(1)	2.45(3)	144(4-I-4)	394(3)	160(1)
50	8	-5.10(3)	-0.92(1)	2.17(5-II-3)	190(3)	261(3)	90(1)
50	9	-1.07(4-I-3)	-0.78(1)	2.13(3)	-147(1)	-276(1)	97(2)
50	10	-3.11(3)	-0.66(1)	2.72(3)	-121(1)	368(3)	224(3)
50	11	-4.41(3)	-0.58(1)	2.70(3)	-110(1)	315(3)	175(1)
50	12	-4.84(3)	-0.74(1)	2.45(3)	-101(1)	178(3)	114(1)
50	13	-1.62(3)	-1.15(1)	2.32(3)	-77(2)	-278(1)	-55(5-II-3)
50	14	-3.04(3)	-0.99(1)	2.56(3)	-267(2)	281(3)	60(2)
50	15	-4.25(3)	-0.78(4-II-3)	2.72(3)	-400(3)	215(3)	-54(5-II-3)
50	16	-4.65(3)	-0.70(4-II-3)	2.66(3)	-469(2)	91(5-II-3)	-97(5-II-3)
51	1	2.80(1)	-1.53(1)	-0.41(5-I-3)	260(1)	-415(1)	-67(4-I-3)
51	2	-2.29(3)	-3.37(1)	-0.56(5-I-3)	279(1)	429(3)	-92(3)
51	3	-4.11(2)	-5.35(1)	-0.47(5-I-3)	432(1)	550(3)	-76(3)
51	4	-5.63(2)	-7.68(1)	1.45(1)	621(1)	1214(1)	-254(1)
51	5	2.50(1)	-1.69(1)	0.87(5-II-3)	81(3)	-485(1)	-81(4-I-4)
51	6	-2.43(3)	-2.41(1)	1.15(1)	225(3)	465(3)	-82(4-I-4)
51	7	-4.63(3)	-3.38(1)	1.46(1)	351(3)	577(3)	-56(4-I-4)
51	8	-5.73(2)	-3.44(1)	1.32(5-II-3)	409(1)	589(1)	-111(1)
51	9	2.12(1)	-1.29(1)	1.28(1)	-77(1)	-504(1)	91(1)
51	10	-2.54(3)	-1.71(1)	1.63(1)	216(3)	462(3)	136(1)
51	11	-4.68(3)	-1.95(1)	1.67(1)	349(3)	562(3)	76(1)
51	12	-5.64(2)	-2.02(1)	1.51(5-II-3)	416(3)	476(3)	-70(3)
51	13	1.71(1)	1.20(3)	1.56(1)	-85(1)	-476(1)	92(1)
51	14	-2.67(3)	-1.11(1)	1.83(1)	140(3)	429(3)	168(1)
51	15	-4.63(3)	-1.39(1)	1.78(5-II-3)	230(3)	502(3)	97(1)
51	16	-5.43(3)	-1.51(1)	1.74(5-II-3)	293(3)	397(3)	-38(3)
52	1	0.79(1)	1.09(3)	-3.44(3)	49(3)	-441(1)	-64(1)
52	2	-3.00(3)	-1.57(1)	-4.03(3)	103(2)	574(3)	-247(1)
52	3	-4.36(3)	-2.17(1)	-4.32(1)	119(2)	697(1)	-208(1)
52	4	-4.02(2)	-2.56(1)	-4.64(1)	79(1)	1137(1)	17(5-II-3)
52	5	1.90(1)	-1.39(1)	-3.00(3)	68(3)	-449(1)	-43(1)
52	6	-2.55(3)	-2.05(1)	-3.67(1)	213(2)	579(3)	-208(1)
52	7	-4.27(3)	-2.58(1)	-4.13(1)	292(1)	735(1)	-229(1)
52	8	-4.49(2)	-3.14(1)	-4.22(1)	259(1)	1266(1)	-77(1)
52	9	2.84(1)	-1.60(1)	-2.45(3)	136(3)	-430(1)	49(5-I-3)
52	10	-2.20(3)	-2.53(1)	-3.00(1)	269(1)	534(3)	-111(3)
52	11	-4.18(3)	-3.92(1)	-3.49(1)	454(1)	693(1)	-214(3)
52	12	-4.88(2)	-4.95(1)	-3.64(1)	463(1)	1466(1)	-178(1)
52	13	3.49(1)	-1.14(1)	-1.65(1)	290(1)	-321(1)	64(5-I-3)
52	14	-2.19(3)	-3.14(1)	-1.63(1)	308(1)	468(3)	-32(5-II-3)
52	15	-3.85(3)	-5.61(1)	-1.76(1)	440(1)	575(1)	-118(3)
52	16	-5.16(2)	-8.94(1)	-2.46(1)	691(1)	1666(1)	-196(1)
53	1	-3.85(3)	-2.04(1)	-4.11(3)	-164(2)	-301(1)	119(3)
53	2	-4.11(3)	-1.40(1)	-4.43(3)	-406(3)	350(3)	-70(1)
53	3	-4.66(3)	0.61(3)	-4.47(3)	-509(3)	316(3)	49(3)
53	4	-2.75(2)	1.70(3)	-5.20(3)	-481(3)	774(1)	191(1)
53	5	-2.04(2)	-1.30(1)	-4.23(3)	-171(1)	289(3)	-57(2)
53	6	-3.90(3)	-1.17(1)	-5.11(3)	-139(1)	460(3)	-277(1)
53	7	-4.48(3)	0.77(3)	-5.35(3)	-129(3)	388(3)	-159(1)
53	8	-4.25(2)	0.62(4-II-3)	-5.03(3)	-179(3)	740(1)	102(2)
53	9	-0.87(4-I-4)	-1.10(1)	-4.16(3)	-120(1)	-306(1)	-56(1)
53	10	-3.48(3)	-1.10(1)	-5.05(3)	-56(1)	517(3)	-264(1)
53	11	-4.58(3)	-1.13(1)	-5.24(3)	26(4-I-3)	512(3)	-164(1)
53	12	-5.03(2)	-0.97(1)	-4.83(3)	-68(4-II-2)	814(1)	67(2)
53	13	1.78(1)	-1.22(1)	-3.97(3)	-71(1)	-345(1)	-48(1)
53	14	-3.04(3)	-1.57(1)	-4.54(3)	51(4-I-4)	556(3)	-240(1)
53	15	-4.75(3)	-1.83(1)	-4.73(3)	22(4-I-3)	580(1)	-174(1)
53	16	-5.89(3)	-1.85(1)	-4.71(3)	-33(5-II-3)	907(1)	44(2)
54	1	-3.19(3)	2.20(3)	-5.23(3)	131(3)	475(3)	277(3)
54	2	-4.20(3)	2.20(3)	-5.69(3)	130(3)	478(3)	85(3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
54	3	-4.36(3)	2.24(3)	-5.58(3)	121(4-I-4)	316(3)	121(3)
54	4	-2.67(2)	2.16(3)	-5.03(3)	-177(1)	131(1)	97(3)
54	5	-2.17(2)	2.07(3)	-5.30(3)	141(3)	554(3)	292(3)
54	6	-3.97(3)	1.90(3)	-5.76(3)	128(3)	492(3)	66(5-II-3)
54	7	-4.77(3)	1.82(3)	-5.71(3)	80(4-I-4)	283(3)	57(5-II-3)
54	8	-4.38(2)	1.61(3)	-4.68(3)	-201(1)	96(1)	-35(5-I-3)
54	9	-1.38(2)	1.75(3)	-5.05(3)	104(3)	585(3)	293(3)
54	10	-3.77(3)	1.30(3)	-5.36(3)	-83(1)	447(3)	46(5-II-4)
54	11	-5.02(3)	-1.12(1)	-5.45(3)	-182(1)	222(3)	-26(1)
54	12	-6.10(2)	-0.87(1)	-4.41(3)	-221(3)	121(1)	-87(3)
54	13	1.70(1)	1.11(3)	-4.34(3)	-140(2)	710(3)	319(3)
54	14	-3.84(3)	-0.85(1)	-4.40(3)	-363(2)	406(3)	119(3)
54	15	-5.06(3)	-2.22(1)	-4.37(3)	-571(3)	87(3)	103(3)
54	16	-8.68(2)	-3.18(1)	-4.90(3)	-428(3)	-312(3)	110(1)
55	1	-5.42(3)	-0.60(1)	-3.82(3)	-234(3)	-259(1)	212(1)
55	2	-4.72(3)	1.36(3)	-3.97(3)	-302(3)	184(3)	108(3)
55	3	-4.55(3)	3.01(3)	-4.07(3)	-297(3)	109(5-II-3)	174(3)
55	4	-2.73(4-I-4)	4.67(3)	-4.70(3)	-243(4-I-4)	82(4-II-2)	165(3)
55	5	-4.13(3)	1.73(3)	-4.40(3)	-70(1)	341(3)	166(1)
55	6	-4.78(3)	2.38(3)	-4.99(3)	70(2)	322(3)	-34(4-I-2)
55	7	-4.40(3)	3.43(3)	-5.15(3)	125(2)	183(3)	73(4-II-4)
55	8	-2.65(3)	4.12(3)	-5.26(3)	203(1)	67(5-II-3)	102(3)
55	9	-3.22(3)	2.19(3)	-4.83(3)	121(3)	409(3)	199(1)
55	10	-4.47(3)	2.76(3)	-5.39(3)	219(3)	402(3)	43(4-II-4)
55	11	-4.40(3)	3.14(3)	-5.60(3)	256(3)	252(3)	116(1)
55	12	-3.10(3)	3.39(3)	-5.33(3)	282(3)	75(4-I-3)	153(1)
55	13	-2.21(2)	1.75(3)	-5.07(3)	109(3)	488(3)	251(3)
55	14	-4.21(3)	2.40(3)	-5.53(3)	181(3)	457(3)	79(4-II-4)
55	15	-4.59(3)	2.88(3)	-5.52(3)	152(3)	263(3)	136(3)
55	16	-4.48(3)	3.04(3)	-5.37(3)	200(4-I-4)	58(4-I-3)	200(1)
56	1	-4.66(3)	1.76(3)	-2.96(4-II-4)	209(3)	427(3)	123(3)
56	2	-4.90(3)	1.86(3)	-3.13(4-II-4)	275(3)	400(3)	-19(4-II-1)
56	3	-4.75(3)	2.25(3)	-3.31(4-II-4)	303(3)	278(3)	7(4-I-1)
56	4	-4.19(3)	2.63(3)	-3.20(4-II-4)	289(3)	153(3)	-23(4-II-2)
56	5	-4.41(3)	2.10(3)	-2.86(3)	271(3)	465(3)	183(3)
56	6	-4.78(3)	2.41(3)	-3.31(3)	325(3)	402(3)	28(4-I-1)
56	7	-4.75(3)	2.58(3)	-3.45(1)	341(3)	261(3)	-36(1)
56	8	-4.43(3)	2.79(3)	-3.25(3)	314(3)	121(3)	-63(1)
56	9	-3.47(3)	2.09(3)	-3.18(3)	146(3)	456(3)	240(3)
56	10	-4.52(3)	2.47(3)	-3.39(3)	188(3)	337(3)	42(4-I-1)
56	11	-4.74(3)	2.61(3)	-3.58(1)	151(3)	202(3)	-51(1)
56	12	-4.79(3)	2.96(3)	-3.59(1)	125(4-II-2)	78(5-II-3)	-74(1)
56	13	-2.76(3)	2.18(3)	-3.21(3)	-174(2)	546(3)	313(3)
56	14	-4.76(3)	2.50(3)	-3.32(3)	-254(3)	275(3)	146(3)
56	15	-4.68(3)	2.72(3)	-3.36(3)	-288(3)	108(5-II-3)	133(3)
56	16	-5.10(3)	3.10(3)	-4.23(1)	-285(3)	-210(1)	69(3)
57	1	-6.04(3)	-0.84(4-II-4)	-2.34(4-II-4)	-312(3)	226(3)	85(1)
57	2	-5.36(3)	0.57(4-I-2)	-2.40(4-II-4)	-425(3)	176(3)	56(1)
57	3	-4.96(3)	1.52(3)	-2.58(4-II-4)	-460(3)	111(3)	102(4-II-4)
57	4	-4.28(3)	2.53(3)	-2.67(4-II-4)	-428(2)	69(4-II-3)	126(4-II-4)
57	5	-5.22(3)	0.97(3)	-2.50(4-II-4)	-43(1)	386(3)	-53(4-I-4)
57	6	-5.37(3)	1.33(3)	-2.90(4-II-4)	-33(1)	298(3)	-88(3)
57	7	-4.96(3)	1.97(3)	-2.92(4-II-4)	-47(1)	204(3)	-33(4-II-2)
57	8	-4.12(3)	2.55(3)	-2.94(4-II-4)	-59(1)	122(3)	15(4-I-2)
57	9	-4.66(3)	1.38(3)	-2.64(4-II-4)	170(3)	430(3)	55(1)
57	10	-5.15(3)	1.75(3)	-3.03(4-II-4)	236(3)	370(3)	-85(3)
57	11	-4.84(3)	2.10(3)	-3.13(4-II-4)	230(3)	263(3)	-39(4-II-2)
57	12	-4.02(3)	2.50(3)	-3.11(4-II-4)	192(3)	157(3)	-26(4-II-2)
57	13	-4.04(3)	1.26(3)	-2.75(4-II-4)	163(3)	463(3)	91(1)
57	14	-4.98(3)	1.83(3)	-3.07(4-II-4)	257(3)	413(3)	-45(4-II-2)
57	15	-4.79(3)	2.13(3)	-3.20(4-II-4)	265(3)	285(3)	-11(4-II-2)
57	16	-3.99(3)	2.33(3)	-3.17(4-II-4)	241(3)	157(3)	-15(4-II-2)
58	1	-5.30(3)	1.53(3)	-1.55(4-II-4)	194(3)	494(3)	69(4-II-4)
58	2	-5.43(3)	2.08(3)	-1.74(4-II-4)	260(3)	414(3)	35(2)
58	3	-4.98(3)	2.67(3)	-1.81(4-II-4)	259(3)	290(3)	24(1)
58	4	-4.00(3)	3.23(3)	-1.81(4-II-4)	220(3)	181(3)	18(1)
58	5	-5.12(3)	1.79(3)	-1.80(4-II-4)	233(3)	513(3)	113(3)
58	6	-5.38(3)	2.25(3)	-2.02(4-II-4)	273(3)	393(3)	48(2)
58	7	-4.99(3)	2.73(3)	-2.06(4-II-4)	244(3)	270(3)	-23(4-II-3)
58	8	-4.04(3)	3.21(3)	-2.01(4-II-4)	184(3)	169(3)	-43(4-II-3)
58	9	-4.95(3)	1.70(3)	-1.96(4-II-4)	104(3)	487(3)	150(3)
58	10	-5.33(3)	2.08(3)	-2.19(4-II-4)	81(3)	320(3)	45(4-I-3)
58	11	-5.00(3)	2.51(3)	-2.21(4-II-4)	27(5-II-2)	213(3)	-44(4-II-3)
58	12	-4.09(3)	3.03(3)	-2.18(4-II-4)	-35(1)	126(3)	-68(4-II-3)
58	13	-4.55(3)	1.18(3)	-1.96(4-II-4)	-311(3)	467(3)	180(4-II-4)
58	14	-5.44(3)	1.64(3)	-2.15(4-II-4)	-386(3)	251(3)	78(3)

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
58	15	-5.06(3)	2.08(3)	-2.31(4-II-4)	-443(3)	140(3)	83(4-II-4)
58	16	-4.09(3)	2.62(3)	-2.39(4-II-4)	-421(2)	71(4-II-3)	78(4-II-4)
59	1	-5.29(3)	0.91(5-I-3)	0.85(5-I-3)	-298(3)	390(3)	-125(5-I-3)
59	2	-5.55(3)	1.70(3)	0.99(5-I-3)	-382(3)	211(3)	-44(5-I-3)
59	3	-5.08(3)	2.47(3)	1.04(5-I-3)	-406(3)	112(4-I-4)	-30(5-I-3)
59	4	-4.13(3)	3.33(4-II-2)	1.04(5-I-3)	-345(3)	52(4-I-4)	54(5-II-3)
59	5	-5.30(3)	1.69(3)	-0.82(5-II-3)	120(3)	468(3)	-123(3)
59	6	-5.49(3)	2.20(3)	-1.00(5-II-3)	123(3)	315(3)	-46(5-II-2)
59	7	-5.04(3)	2.83(3)	-1.04(5-II-3)	95(2)	208(3)	37(1)
59	8	-4.07(3)	3.48(3)	-1.08(5-II-3)	74(2)	124(3)	75(3)
59	9	-5.25(3)	1.83(3)	-1.04(5-II-3)	256(3)	505(3)	-70(5-I-3)
59	10	-5.45(3)	2.39(3)	-1.20(5-II-3)	321(3)	398(3)	-38(5-II-2)
59	11	-4.99(3)	2.93(3)	-1.27(5-II-3)	309(3)	275(3)	29(1)
59	12	-3.99(3)	3.47(3)	-1.31(5-II-3)	262(2)	172(3)	52(3)
59	13	-5.17(3)	1.56(3)	-1.24(4-II-4)	204(3)	505(3)	34(5-II-3)
59	14	-5.43(3)	2.20(3)	-1.39(4-II-4)	285(3)	426(3)	18(1)
59	15	-4.98(3)	2.80(3)	-1.49(4-II-4)	288(3)	297(3)	26(1)
59	16	-3.97(3)	3.33(3)	-1.55(4-II-4)	251(2)	186(3)	32(4-II-1)
60	1	-4.65(3)	1.56(3)	2.16(5-I-3)	197(3)	510(3)	-95(3)
60	2	-5.29(3)	2.25(3)	2.40(5-I-3)	286(3)	433(3)	-14(1)
60	3	-4.99(3)	2.80(3)	2.53(5-I-3)	294(3)	297(3)	-43(1)
60	4	-4.10(3)	3.31(4-II-3)	2.58(5-I-3)	265(2)	177(2)	-48(1)
60	5	-5.06(3)	1.79(3)	1.95(5-I-3)	230(3)	482(3)	-51(1)
60	6	-5.39(3)	2.36(3)	2.22(5-I-3)	309(3)	395(3)	40(5-I-3)
60	7	-5.02(3)	2.93(3)	2.32(5-I-3)	310(3)	275(3)	-25(5-II-3)
60	8	-4.14(3)	3.57(4-II-3)	2.34(5-I-3)	276(2)	171(2)	-54(3)
60	9	-5.40(3)	1.52(3)	1.69(5-I-3)	81(5-II-3)	432(3)	64(5-II-3)
60	10	-5.53(3)	2.09(3)	1.96(5-I-3)	103(3)	312(3)	53(2)
60	11	-5.07(3)	2.86(3)	1.99(5-I-3)	89(3)	209(3)	-32(5-II-2)
60	12	-4.18(3)	3.65(4-II-2)	2.00(5-I-3)	87(2)	127(2)	-68(3)
60	13	-5.84(3)	0.62(5-II-3)	1.40(5-I-3)	-311(3)	299(3)	69(5-II-3)
60	14	-5.53(3)	1.59(4-II-2)	1.44(5-I-3)	-392(3)	193(3)	-30(1)
60	15	-5.07(3)	2.57(4-II-2)	1.52(5-I-3)	-408(3)	113(3)	-55(1)
60	16	-4.23(3)	3.61(4-II-2)	1.53(5-I-3)	-338(3)	62(2)	-73(5-I-3)
61	1	-3.34(3)	1.73(3)	2.82(3)	-240(3)	588(3)	-291(3)
61	2	-5.18(3)	1.92(4-II-3)	3.05(3)	-357(3)	308(3)	-154(3)
61	3	-5.04(3)	2.12(4-II-3)	3.23(3)	-436(3)	151(3)	-173(3)
61	4	-4.17(3)	2.40(4-II-3)	3.31(3)	-436(3)	44(5-I-2)	-167(3)
61	5	-4.16(3)	2.01(3)	2.92(3)	137(3)	531(3)	-238(3)
61	6	-4.99(3)	2.30(3)	3.13(3)	105(3)	352(3)	-57(4-I-3)
61	7	-4.95(3)	2.53(3)	3.11(3)	41(5-I-3)	218(3)	25(4-II-3)
61	8	-4.24(3)	2.89(4-II-3)	3.08(3)	-21(5-II-2)	109(2)	50(4-II-3)
61	9	-4.59(3)	2.00(3)	2.75(3)	237(3)	534(3)	-198(3)
61	10	-5.13(3)	2.42(3)	2.98(3)	281(3)	415(3)	-55(2)
61	11	-4.97(3)	2.81(3)	2.99(3)	257(3)	272(3)	-30(4-I-3)
61	12	-4.22(3)	3.14(4-II-3)	2.93(3)	204(2)	155(2)	32(4-II-3)
61	13	-5.08(3)	1.73(3)	2.46(3)	199(3)	489(3)	-146(3)
61	14	-5.24(3)	2.19(3)	2.69(3)	262(3)	423(3)	-45(2)
61	15	-4.97(3)	2.75(3)	2.76(3)	270(3)	291(3)	-50(2)
61	16	-4.25(3)	3.34(4-II-3)	2.75(3)	239(2)	176(2)	-44(1)
62	1	-2.82(3)	1.39(3)	3.85(3)	123(3)	466(3)	-127(3)
62	2	-4.55(3)	1.78(3)	4.32(3)	205(3)	456(3)	28(4-II-3)
62	3	-4.79(3)	1.93(3)	4.55(3)	211(3)	317(3)	-40(1)
62	4	-4.24(3)	2.14(5-II-3)	4.63(4-II-3)	191(3)	164(3)	-52(3)
62	5	-3.72(3)	1.43(3)	3.75(3)	119(3)	417(3)	-93(1)
62	6	-4.77(3)	1.68(3)	4.32(3)	185(3)	401(3)	84(3)
62	7	-4.82(3)	1.93(3)	4.48(3)	189(3)	283(3)	19(5-I-3)
62	8	-4.34(3)	2.38(5-II-3)	4.48(3)	168(3)	151(3)	-18(5-II-3)
62	9	-4.55(3)	-0.91(1)	3.57(3)	-73(1)	373(3)	-84(1)
62	10	-5.09(3)	1.23(5-II-3)	4.17(3)	-48(1)	328(3)	90(3)
62	11	-4.93(3)	1.85(5-II-3)	4.21(3)	-38(1)	217(3)	23(5-I-3)
62	12	-4.37(3)	2.44(5-II-3)	4.20(3)	-39(3)	108(3)	-30(5-II-3)
62	13	-5.79(3)	-1.53(1)	3.29(3)	-277(3)	-216(1)	-163(1)
62	14	-5.02(3)	-0.90(1)	3.47(3)	-420(3)	191(3)	-103(1)
62	15	-4.87(3)	1.51(5-II-3)	3.69(3)	-470(3)	116(3)	-174(3)
62	16	-4.48(3)	2.46(4-II-4)	3.76(3)	-447(3)	44(5-I-2)	-208(3)
63	1	-1.50(4-I-3)	1.83(3)	3.67(3)	-106(5-II-3)	631(3)	-294(3)
63	2	-4.20(3)	1.49(3)	3.89(3)	-266(3)	397(3)	-140(3)
63	3	-4.68(3)	1.28(5-II-3)	4.09(3)	-394(3)	210(3)	-162(3)
63	4	-4.26(3)	1.24(5-II-3)	4.19(3)	-464(2)	53(4-II-3)	-159(3)
63	5	-2.19(3)	2.03(3)	4.05(3)	157(3)	506(3)	-237(3)
63	6	-3.96(3)	1.95(3)	4.33(3)	132(3)	421(3)	-28(4-I-4)
63	7	-4.60(3)	1.70(3)	4.32(3)	70(4-II-3)	270(3)	30(5-II-2)
63	8	-4.34(3)	1.73(5-II-3)	4.31(3)	-46(1)	114(3)	53(5-II-3)
63	9	-2.79(3)	1.99(3)	4.08(3)	197(3)	484(3)	-195(3)
63	10	-4.19(3)	2.07(3)	4.45(3)	258(3)	466(3)	-20(4-I-3)

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
63	11	-4.65 (3)	2.02 (3)	4.55 (4-II-3)	255 (3)	316 (3)	13 (5-II-2)
63	12	-4.37 (3)	1.99 (5-II-3)	4.54 (4-II-3)	211 (3)	158 (3)	31 (5-II-2)
63	13	-3.57 (3)	1.70 (3)	3.95 (3)	156 (3)	413 (3)	-153 (3)
63	14	-4.40 (3)	1.70 (3)	4.39 (3)	208 (3)	441 (3)	-9 (1)
63	15	-4.68 (3)	1.86 (3)	4.61 (3)	230 (3)	315 (3)	-42 (1)
63	16	-4.44 (3)	2.20 (5-II-3)	4.68 (4-II-3)	210 (3)	168 (3)	-41 (1)
64	1	-4.33 (2)	1.06 (4-I-3)	4.22 (3)	185 (3)	-120 (1)	59 (1)
64	2	-4.59 (2)	1.12 (4-I-3)	3.98 (3)	174 (2)	-52 (1)	55 (1)
64	3	-5.52 (1)	1.27 (4-I-3)	3.55 (3)	186 (1)	477 (1)	-16 (4-I-2)
64	4	-4.86 (1)	1.38 (4-I-3)	3.08 (3)	350 (1)	1649 (1)	-235 (3)
64	5	-4.33 (2)	1.31 (4-I-3)	4.39 (3)	181 (3)	-109 (1)	105 (1)
64	6	-4.38 (2)	1.45 (4-I-3)	4.00 (3)	179 (3)	-62 (1)	98 (1)
64	7	-5.13 (1)	1.68 (4-I-3)	3.53 (3)	237 (1)	414 (1)	-31 (4-I-2)
64	8	-4.35 (1)	1.82 (4-I-3)	3.06 (3)	360 (1)	1594 (1)	-258 (3)
64	9	-4.16 (2)	1.49 (5-II-3)	4.39 (3)	-61 (1)	-114 (1)	116 (1)
64	10	-4.02 (2)	1.91 (5-II-3)	3.85 (3)	-35 (1)	-95 (1)	125 (1)
64	11	-4.80 (1)	2.42 (5-II-3)	3.22 (3)	89 (1)	279 (1)	33 (1)
64	12	-4.50 (1)	2.78 (3)	3.23 (3)	241 (1)	1548 (1)	-298 (3)
64	13	-4.07 (2)	1.88 (5-II-3)	4.16 (3)	-485 (2)	-121 (1)	-142 (3)
64	14	-3.76 (2)	2.67 (5-II-3)	3.61 (3)	-467 (2)	-111 (1)	-116 (5-II-3)
64	15	-4.59 (1)	3.44 (5-II-3)	2.85 (3)	-394 (1)	201 (1)	-74 (5-II-3)
64	16	-4.94 (1)	3.95 (5-II-3)	2.98 (3)	-194 (2)	1482 (1)	-304 (3)
65	1	-4.24 (2)	-1.59 (4-II-3)	2.71 (3)	-485 (2)	-159 (1)	-87 (3)
65	2	-4.13 (2)	-2.89 (1)	2.71 (3)	-447 (2)	-64 (1)	-99 (1)
65	3	-5.21 (1)	-5.03 (1)	2.83 (3)	-323 (2)	505 (1)	-67 (1)
65	4	-7.11 (1)	-6.80 (1)	3.14 (3)	81 (1)	2183 (1)	-239 (3)
65	5	-4.47 (2)	-1.32 (1)	3.23 (3)	-103 (1)	-127 (1)	66 (3)
65	6	-4.65 (2)	-2.10 (1)	3.40 (3)	-55 (1)	28 (4-II-3)	54 (3)
65	7	-5.56 (1)	-2.84 (4-II-3)	3.78 (3)	74 (1)	597 (1)	42 (5-I-3)
65	8	-4.95 (1)	-2.80 (4-II-3)	2.95 (3)	303 (1)	2092 (1)	-189 (3)
65	9	-4.50 (2)	-1.00 (1)	3.70 (3)	161 (3)	-115 (1)	71 (3)
65	10	-4.64 (2)	-1.38 (4-II-3)	3.78 (3)	166 (2)	47 (4-II-3)	67 (3)
65	11	-5.48 (1)	-1.43 (4-II-3)	3.73 (3)	247 (1)	607 (1)	45 (4-II-2)
65	12	-4.17 (1)	-1.04 (4-II-3)	3.15 (3)	303 (1)	1944 (1)	-217 (3)
65	13	-4.58 (2)	1.01 (4-I-3)	4.01 (3)	180 (3)	-109 (1)	41 (1)
65	14	-4.57 (2)	0.96 (4-I-3)	3.89 (3)	175 (2)	56 (4-II-3)	42 (1)
65	15	-5.13 (1)	1.05 (4-I-3)	3.52 (3)	206 (1)	583 (1)	32 (4-II-2)
65	16	-3.71 (1)	1.25 (4-I-3)	3.18 (3)	295 (1)	1818 (1)	-252 (3)
66	1	-5.29 (2)	-1.41 (1)	1.73 (5-II-3)	293 (3)	158 (3)	-72 (1)
66	2	-4.67 (2)	-1.59 (1)	1.58 (5-II-3)	396 (3)	167 (3)	-145 (1)
66	3	-3.76 (2)	-1.82 (1)	1.68 (5-II-3)	462 (2)	788 (1)	-130 (1)
66	4	-1.43 (2)	-2.27 (1)	1.98 (5-II-3)	504 (1)	2131 (1)	-84 (5-II-3)
66	5	-5.00 (2)	-1.31 (1)	1.93 (5-II-3)	247 (3)	123 (5-II-3)	-14 (4-I-3)
66	6	-4.66 (2)	-1.70 (1)	1.73 (5-II-3)	343 (3)	147 (3)	-73 (1)
66	7	-4.26 (1)	-1.66 (1)	1.86 (5-II-3)	441 (3)	780 (1)	-136 (1)
66	8	-1.59 (1)	-1.74 (1)	2.40 (3)	496 (1)	2279 (1)	-145 (3)
66	9	-4.70 (2)	-1.21 (1)	2.14 (5-II-3)	-62 (1)	80 (5-II-3)	45 (1)
66	10	-4.51 (2)	-1.98 (1)	1.86 (5-II-3)	90 (3)	96 (3)	-31 (2)
66	11	-4.66 (1)	-2.37 (1)	1.86 (5-II-3)	250 (3)	698 (1)	-111 (2)
66	12	-2.32 (1)	-2.11 (1)	2.77 (3)	406 (1)	2423 (1)	-228 (3)
66	13	-4.49 (3)	-1.06 (4-II-3)	2.33 (3)	-470 (2)	-86 (1)	-113 (5-II-3)
66	14	-4.45 (2)	-2.09 (1)	2.05 (5-II-3)	-406 (2)	66 (5-II-3)	-120 (3)
66	15	-5.01 (1)	-3.91 (1)	1.80 (5-II-3)	-231 (1)	614 (1)	-110 (3)
66	16	-3.48 (1)	-5.04 (1)	2.76 (3)	51 (1)	2521 (1)	-276 (3)
67	1	-6.03 (2)	-3.88 (1)	2.32 (5-II-3)	432 (1)	128 (1)	-478 (1)
67	2	-5.08 (2)	-1.07 (1)	2.62 (3)	-166 (4-I-1)	127 (1)	-230 (1)
67	3	-3.71 (3)	1.60 (3)	2.25 (3)	-442 (3)	309 (1)	-288 (1)
67	4	1.61 (1)	3.77 (1)	1.06 (5-II-3)	-81 (5-I-3)	1455 (1)	-73 (1)
67	5	-5.70 (2)	-2.91 (1)	1.61 (5-II-3)	421 (1)	329 (1)	-261 (1)
67	6	-4.86 (2)	-1.16 (1)	1.90 (5-II-3)	340 (1)	167 (1)	-255 (1)
67	7	-3.47 (2)	1.26 (3)	1.58 (5-II-3)	348 (1)	420 (1)	-166 (1)
67	8	0.84 (1)	1.67 (3)	1.10 (5-II-3)	532 (1)	1744 (1)	197 (2)
67	9	-5.59 (2)	-1.88 (1)	1.52 (5-II-3)	456 (2)	268 (1)	-212 (1)
67	10	-4.80 (2)	-1.18 (1)	1.52 (5-II-3)	481 (2)	187 (1)	-262 (1)
67	11	-3.41 (2)	0.39 (5-I-3)	1.38 (5-II-3)	549 (1)	599 (1)	-117 (1)
67	12	0.28 (5-II-3)	-0.32 (5-II-3)	1.43 (5-II-3)	567 (1)	1860 (1)	160 (2)
67	13	-5.34 (2)	-1.51 (1)	1.59 (5-II-3)	360 (3)	218 (3)	-146 (1)
67	14	-4.73 (2)	-1.36 (1)	1.47 (5-II-3)	447 (2)	184 (1)	-214 (1)
67	15	-3.64 (2)	-1.38 (1)	1.41 (5-II-3)	514 (2)	719 (1)	-122 (1)
67	16	-0.55 (5-I-3)	-2.04 (1)	1.82 (5-II-3)	503 (1)	1984 (1)	52 (5-I-3)
68	1	-5.10 (2)	0.57 (4-II-2)	-1.33 (1)	-184 (1)	-228 (1)	-227 (1)
68	2	-5.19 (3)	1.02 (4-II-4)	-0.98 (1)	-196 (1)	123 (3)	-193 (3)
68	3	-5.08 (3)	2.06 (4-II-4)	0.22 (5-II-3)	-191 (1)	146 (3)	-143 (3)
68	4	-3.27 (3)	4.36 (1)	0.61 (1)	-77 (1)	123 (1)	79 (1)
68	5	-4.77 (2)	-0.58 (1)	-1.51 (1)	24 (4-I-4)	-300 (1)	-233 (1)
68	6	-5.36 (3)	0.85 (4-II-2)	-1.54 (1)	147 (3)	180 (3)	-173 (3)

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68	7	-5.59(3)	1.90(4-II-4)	-1.12(1)	204(3)	240(3)	-115(3)
68	8	-4.07(3)	2.87(3)	0.26(5-II-3)	191(3)	277(1)	132(1)
68	9	-4.35(2)	-1.22(1)	-1.66(1)	187(1)	-349(1)	-185(1)
68	10	-5.52(3)	0.47(4-II-3)	-1.98(1)	424(1)	225(3)	-91(3)
68	11	-5.95(3)	1.05(4-II-3)	-1.70(1)	537(1)	314(1)	-108(3)
68	12	-5.92(3)	1.42(4-II-3)	0.53(1)	461(3)	448(1)	85(1)
68	13	-3.61(2)	-2.42(1)	-1.95(1)	602(1)	-104(1)	73(2)
68	14	-5.40(3)	-1.11(1)	-2.32(1)	791(1)	218(1)	273(1)
68	15	-6.61(3)	0.41(4-II-2)	-1.67(1)	976(1)	322(1)	214(1)
68	16	-10.27(1)	0.86(3)	0.75(5-II-3)	928(1)	649(1)	155(1)
69	1	-6.43(3)	-1.34(4-I-4)	-2.46(3)	-558(3)	156(4-I-4)	-43(2)
69	2	-2.67(2)	-1.48(3)	-0.75(3)	-705(3)	61(5-I-2)	65(3)
69	3	-1.32(2)	-2.44(3)	0.91(1)	-861(3)	87(4-II-2)	-13(1)
69	4	-1.28(2)	-4.62(3)	2.67(3)	-1534(3)	-59(4-I-2)	79(2)
69	5	-5.14(2)	-0.62(4-I-4)	-1.56(3)	-307(1)	195(4-I-4)	-91(3)
69	6	-3.12(2)	-1.20(4-I-4)	-0.83(3)	-467(1)	71(4-I-4)	18(4-II-1)
69	7	-2.61(2)	-1.28(3)	1.29(1)	-672(1)	44(4-II-2)	-18(5-I-3)
69	8	-5.05(3)	-0.76(3)	1.79(3)	-1003(3)	-35(4-I-2)	-37(5-I-3)
69	9	-4.85(2)	0.53(4-II-4)	-1.22(3)	-215(1)	178(4-I-4)	-123(3)
69	10	-4.24(2)	-0.66(4-I-4)	-0.68(5-I-3)	-375(1)	88(4-I-4)	-84(3)
69	11	-3.88(3)	0.63(4-II-4)	1.33(1)	-519(1)	52(4-II-3)	-94(3)
69	12	-3.38(3)	0.31(4-II-4)	1.61(1)	-605(3)	-26(4-I-4)	-115(3)
69	13	-4.54(2)	0.51(4-II-4)	-1.10(3)	-197(1)	124(4-I-4)	-173(3)
69	14	-4.83(3)	0.72(4-II-4)	-0.64(5-I-3)	-347(1)	94(4-I-4)	-158(3)
69	15	-4.88(3)	1.62(4-II-4)	0.68(3)	-402(1)	61(4-II-3)	-138(3)
69	16	-3.86(3)	3.67(1)	2.52(1)	-307(1)	-47(4-I-3)	-129(3)
70	1	-2.96(2)	1.50(3)	-4.49(3)	-235(1)	-270(4-II-4)	153(1)
70	2	-0.68(4-I-3)	0.89(3)	-3.36(3)	84(4-I-4)	-91(1)	192(1)
70	3	1.08(5-I-1)	0.34(3)	-2.09(3)	138(3)	-255(3)	263(3)
70	4	1.11(4-II-3)	-0.32(1)	0.65(1)	168(3)	-344(3)	276(3)
70	5	-2.97(2)	-0.71(1)	-4.26(3)	-288(1)	-205(4-I-4)	195(1)
70	6	-1.09(2)	-1.37(1)	-3.12(3)	-244(1)	-102(1)	253(1)
70	7	-0.42(2)	-1.73(1)	-1.86(3)	-224(1)	-246(3)	310(3)
70	8	-1.21(1)	-1.99(3)	0.73(1)	-146(1)	-431(3)	320(3)
70	9	-3.41(2)	-1.34(1)	-3.65(3)	-275(1)	119(4-I-4)	173(1)
70	10	-1.79(2)	-2.13(1)	-2.52(3)	-437(1)	-132(1)	224(1)
70	11	-1.14(2)	-3.72(3)	-1.32(3)	-539(1)	-205(3)	308(3)
70	12	-2.85(3)	-4.41(3)	0.75(1)	-448(3)	-533(3)	394(3)
70	13	-2.87(2)	-1.86(1)	-3.12(3)	-386(3)	194(4-I-4)	43(1)
70	14	-2.32(2)	-3.03(3)	-1.42(3)	-720(2)	-180(1)	110(1)
70	15	-2.37(2)	-4.80(3)	0.33(1)	-942(3)	-243(3)	115(3)
70	16	-5.85(3)	-7.29(3)	0.89(1)	-1031(3)	-657(3)	340(3)
71	1	3.00(1)	6.23(3)	-3.97(3)	403(1)	59(4-II-1)	98(3)
71	2	2.02(1)	6.91(3)	-2.50(3)	454(1)	-203(3)	26(4-I-2)
71	3	3.18(3)	9.23(3)	-1.08(3)	517(1)	-547(3)	-65(3)
71	4	8.28(3)	14.12(3)	-3.45(3)	557(1)	-1140(3)	432(3)
71	5	1.92(1)	4.45(3)	-4.39(3)	310(1)	-48(3)	64(3)
71	6	1.77(1)	5.65(3)	-3.14(3)	389(1)	-212(3)	38(4-I-2)
71	7	2.52(3)	7.34(3)	-2.98(3)	486(1)	-548(3)	89(1)
71	8	5.50(3)	6.15(3)	-1.28(3)	546(1)	-576(3)	382(3)
71	9	-1.21(4-I-4)	3.39(3)	-4.67(3)	278(2)	-109(1)	90(1)
71	10	1.18(1)	4.12(3)	-3.71(3)	289(2)	-194(3)	67(1)
71	11	2.10(3)	4.21(3)	-2.76(3)	377(2)	-442(3)	168(2)
71	12	3.42(3)	3.27(3)	-0.57(4-II-2)	431(3)	-436(3)	365(3)
71	13	-0.97(4-I-4)	2.12(3)	-4.83(3)	181(4-I-4)	-227(1)	125(1)
71	14	0.80(1)	2.16(3)	-3.55(3)	179(3)	-159(3)	122(1)
71	15	1.06(4-II-3)	2.10(3)	-2.35(3)	296(3)	-366(3)	213(3)
71	16	1.45(4-II-3)	1.55(3)	0.49(1)	315(3)	-406(3)	304(3)
72	1	-3.03(2)	2.61(3)	-2.64(4-II-4)	232(3)	-90(1)	-72(3)
72	2	-0.98(2)	1.56(4-I-2)	-1.73(4-II-4)	138(3)	-205(1)	-152(3)
72	3	1.71(4-II-3)	-1.93(4-II-2)	-1.05(3)	-173(1)	-544(3)	-223(3)
72	4	-4.14(1)	-5.66(4-II-2)	1.41(4-II-2)	-582(4-II-3)	-974(3)	207(5-I-3)
72	5	-3.59(2)	2.84(3)	-2.39(4-II-4)	260(3)	-116(1)	-127(3)
72	6	-1.54(2)	1.94(3)	-1.01(4-II-4)	193(3)	-229(1)	-196(3)
72	7	-1.06(1)	-0.87(4-II-2)	0.71(5-I-3)	122(3)	-578(3)	-281(3)
72	8	-6.05(1)	-0.50(4-II-4)	0.35(5-I-3)	81(2)	-367(3)	-225(3)
72	9	-4.64(2)	3.43(3)	-2.28(4-II-4)	125(4-II-3)	-150(1)	-135(3)
72	10	-2.47(2)	3.08(3)	-0.57(4-II-4)	154(4-II-3)	-263(3)	-195(3)
72	11	-1.69(1)	2.75(3)	1.56(5-I-3)	247(3)	-603(3)	-231(3)
72	12	-5.34(1)	0.39(3)	0.49(5-I-3)	442(3)	-378(3)	-372(3)
72	13	-6.21(3)	3.92(3)	-2.44(4-II-4)	-203(2)	-217(3)	-58(1)
72	14	-3.10(2)	4.28(3)	-0.63(4-II-4)	99(4-II-2)	-327(3)	-114(3)
72	15	-2.13(1)	6.08(3)	0.99(5-I-3)	292(4-II-2)	-673(3)	-175(3)
72	16	-5.73(1)	9.85(3)	3.01(3)	815(4-II-4)	-1138(3)	-684(3)
73	1	-2.95(2)	3.70(3)	-2.67(4-II-4)	-359(2)	-67(1)	126(4-II-4)
73	2	-1.09(2)	5.61(3)	-2.76(4-II-4)	-290(2)	-215(2)	126(4-II-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
73	3	1.39(4-II-3)	8.64(3)	-2.78(4-II-4)	-292(2)	-797(3)	134(4-II-2)
73	4	-2.42(1)	11.43(3)	-1.96(4-II-3)	-303(3)	-1886(3)	231(4-II-3)
73	5	-2.72(2)	3.20(3)	-3.06(4-II-4)	-89(1)	65(4-II-3)	21(4-I-3)
73	6	-0.93(4-I-3)	3.88(3)	-3.38(4-II-4)	-158(1)	-210(1)	-17(1)
73	7	1.37(4-II-3)	4.58(3)	-3.83(4-II-4)	-262(2)	-798(3)	113(4-II-2)
73	8	-3.61(1)	5.98(3)	-2.24(4-II-3)	-409(3)	-1886(3)	289(4-II-3)
73	9	-2.69(2)	2.75(3)	-3.12(4-II-4)	110(3)	77(4-II-3)	-35(1)
73	10	-0.89(2)	2.51(3)	-3.20(4-II-4)	-127(1)	-212(1)	-60(1)
73	11	1.12(4-II-3)	1.74(4-I-2)	-3.50(4-II-4)	-275(3)	-703(3)	90(4-II-2)
73	12	-4.77(2)	1.93(4-I-2)	-3.45(4-II-3)	-546(3)	-1856(3)	300(4-II-3)
73	13	-2.69(2)	2.36(3)	-2.91(4-II-4)	172(3)	-87(1)	-48(4-II-2)
73	14	-0.84(2)	1.62(4-I-2)	-2.56(4-II-4)	-89(1)	-222(1)	-99(3)
73	15	-0.98(1)	-1.54(4-II-2)	-2.17(3)	-252(1)	-621(3)	-82(3)
73	16	-5.72(2)	-5.84(4-II-2)	-3.36(4-II-3)	-686(3)	-1752(3)	307(4-II-2)
74	1	-2.44(2)	3.77(3)	-1.72(4-II-4)	149(2)	51(5-II-3)	13(1)
74	2	-0.81(4-I-3)	4.13(3)	-1.52(4-II-4)	69(4-I-2)	-288(3)	16(4-II-2)
74	3	1.54(4-II-2)	4.03(3)	-1.24(4-II-4)	-129(4-II-2)	-981(3)	-46(1)
74	4	-2.33(3)	3.21(3)	0.89(1)	-255(4-II-3)	-2121(4-II-3)	-72(1)
74	5	-2.51(2)	3.73(3)	-1.85(4-II-4)	93(2)	-54(1)	-48(4-II-3)
74	6	-0.80(4-I-3)	4.07(3)	-1.45(4-II-4)	-88(4-II-2)	-294(3)	-40(3)
74	7	1.67(4-II-3)	3.85(3)	-0.92(4-II-4)	-179(4-II-2)	-1001(3)	-48(4-I-3)
74	8	-2.78(3)	4.26(3)	-0.82(4-II-2)	-265(4-II-3)	-2132(4-II-3)	91(4-II-3)
74	9	-2.64(2)	3.70(3)	-2.00(4-II-4)	-76(2)	-67(1)	-80(3)
74	10	-0.91(4-I-3)	4.51(3)	-1.46(4-II-4)	-150(3)	-292(3)	-60(3)
74	11	1.26(4-II-3)	5.22(3)	-0.80(4-II-4)	-213(4-II-2)	-991(3)	40(4-II-3)
74	12	-2.46(3)	5.83(3)	-1.21(4-II-2)	-290(4-II-3)	-2152(4-II-3)	139(4-II-3)
74	13	-2.76(2)	3.52(3)	-2.24(4-II-4)	-360(2)	-89(1)	61(1)
74	14	-1.11(2)	5.08(3)	-1.84(4-II-4)	-297(2)	-304(3)	64(4-II-4)
74	15	0.85(4-II-3)	7.53(3)	-1.17(4-II-4)	-281(2)	-988(3)	113(4-II-4)
74	16	-2.27(3)	9.80(3)	-1.36(4-II-2)	-329(3)	-2183(3)	221(4-II-3)
75	1	-2.74(2)	4.56(4-II-2)	0.89(5-I-3)	-219(2)	-45(1)	70(4-II-2)
75	2	-1.11(4-I-3)	6.31(4-II-3)	-0.99(5-II-3)	-107(4-I-4)	-227(3)	73(4-II-2)
75	3	2.18(4-II-3)	8.61(4-II-3)	-1.13(5-II-3)	-63(4-I-4)	-764(4-II-3)	-43(1)
75	4	1.69(4-II-4)	10.52(4-II-3)	-0.74(5-II-3)	-155(3)	-2075(4-II-3)	-173(5-I-3)
75	5	-2.55(2)	4.24(3)	-1.21(5-II-3)	53(2)	34(5-II-3)	100(3)
75	6	-0.91(4-I-3)	5.09(4-II-2)	-1.45(5-II-3)	-26(5-I-3)	-229(3)	86(4-II-2)
75	7	2.24(4-II-3)	5.78(4-II-2)	-1.66(4-II-4)	-110(4-II-2)	-851(4-II-3)	-61(1)
75	8	-0.77(4-I-4)	6.12(4-II-2)	-0.89(5-II-3)	-219(4-II-2)	-2134(4-II-3)	-155(5-I-3)
75	9	-2.41(2)	4.01(3)	-1.39(5-II-3)	186(2)	51(5-II-3)	69(3)
75	10	-0.77(4-I-3)	4.34(3)	-1.56(4-II-4)	83(4-I-2)	-252(3)	58(4-II-2)
75	11	2.13(4-II-3)	4.12(3)	-1.59(4-II-4)	-148(4-II-2)	-932(4-II-3)	-64(1)
75	12	-1.17(3)	4.03(3)	-0.93(5-II-3)	-226(4-II-2)	-2140(4-II-3)	-123(5-I-2)
75	13	-2.38(2)	3.83(3)	-1.56(4-II-4)	182(2)	50(5-II-3)	39(4-II-4)
75	14	0.79(4-II-3)	4.09(3)	-1.54(4-II-4)	91(4-I-2)	-273(3)	33(4-II-2)
75	15	2.02(4-II-3)	3.95(3)	-1.29(4-II-4)	-142(4-II-2)	-973(4-II-3)	-49(1)
75	16	-1.85(3)	3.33(3)	-0.78(4-II-4)	-189(4-II-2)	-2156(4-II-3)	-84(1)
76	1	-2.80(2)	4.05(4-II-3)	2.52(5-I-3)	206(2)	53(4-I-3)	-39(3)
76	2	-1.39(4-I-3)	4.70(4-II-3)	2.28(5-I-3)	113(2)	-202(4-II-3)	-23(3)
76	3	1.41(4-II-2)	5.16(4-II-3)	1.70(5-I-3)	-104(4-II-3)	-754(4-II-3)	-37(3)
76	4	-1.65(1)	5.68(4-II-3)	0.97(5-I-3)	-189(4-II-3)	-1711(4-II-3)	-169(5-I-3)
76	5	-2.78(2)	4.39(4-II-3)	2.34(5-I-3)	217(2)	58(2)	-66(3)
76	6	-1.24(4-I-3)	5.12(4-II-3)	2.21(5-I-3)	122(2)	-193(4-II-3)	-59(3)
76	7	1.94(4-II-2)	5.36(4-II-3)	1.70(5-I-3)	-113(4-II-3)	-767(4-II-3)	-67(3)
76	8	-1.13(4-I-2)	5.51(4-II-3)	0.79(5-I-3)	-209(4-II-3)	-1805(4-II-3)	-178(5-I-3)
76	9	-2.75(2)	4.69(4-II-3)	2.01(5-I-3)	85(2)	40(4-I-3)	-89(3)
76	10	-1.13(4-I-3)	5.86(4-II-3)	1.95(5-I-3)	71(1)	-187(4-II-3)	-88(3)
76	11	2.25(4-II-2)	6.68(4-II-3)	1.69(5-I-3)	-76(4-II-3)	-757(4-II-3)	-81(2)
76	12	0.90(4-II-2)	6.78(4-II-3)	0.71(5-I-3)	-171(4-II-3)	-1886(4-II-3)	-171(5-I-3)
76	13	-2.81(2)	4.88(4-II-3)	1.46(5-I-3)	-205(2)	13(4-I-3)	-74(5-I-3)
76	14	-1.06(4-I-3)	6.74(4-II-3)	1.33(5-I-3)	-88(4-I-4)	-173(4-II-3)	-65(2)
76	15	2.38(4-II-2)	9.05(4-II-3)	1.14(5-I-3)	-53(4-I-4)	-722(4-II-3)	-59(2)
76	16	1.99(4-II-2)	10.78(4-II-3)	0.77(5-I-3)	-68(4-II-3)	-1959(4-II-3)	-134(5-I-3)
77	1	-3.11(2)	3.11(5-II-3)	3.10(3)	-384(2)	-80(1)	-139(1)
77	2	-2.15(2)	4.06(5-II-3)	2.62(3)	-334(2)	-241(3)	-100(1)
77	3	-2.27(1)	5.20(5-II-3)	1.83(3)	-290(2)	-562(4-II-3)	-72(3)
77	4	-4.26(1)	6.23(5-II-3)	1.41(4-II-3)	-256(3)	-1327(4-II-3)	-266(4-II-3)
77	5	-3.14(2)	3.44(4-II-3)	2.94(3)	-66(3)	-42(1)	72(4-II-3)
77	6	-1.95(2)	4.01(4-II-3)	2.51(3)	-122(3)	-183(3)	70(4-II-2)
77	7	-1.73(1)	4.34(4-II-3)	2.01(1)	-194(4-II-3)	-565(4-II-3)	18(4-I-3)
77	8	-2.96(1)	4.58(5-II-3)	1.17(4-II-3)	-243(4-II-3)	-1397(4-II-3)	-241(4-I-3)
77	9	-3.01(2)	3.69(4-II-3)	2.81(3)	132(2)	36(4-I-4)	50(4-II-3)
77	10	-1.63(2)	4.18(4-II-3)	2.46(1)	60(4-I-3)	-174(4-II-3)	48(4-II-2)
77	11	-1.24(1)	4.43(4-II-3)	1.95(1)	-150(4-II-3)	-642(4-II-3)	-24(4-II-3)
77	12	-2.07(1)	4.61(4-II-3)	1.19(5-I-3)	-217(4-II-3)	-1469(4-II-3)	-210(4-II-2)
77	13	-2.97(2)	3.96(4-II-3)	2.65(5-I-3)	181(2)	54(2)	-30(1)
77	14	-1.40(4-I-3)	4.55(4-II-3)	2.38(5-I-3)	97(2)	-172(4-II-3)	9(5-II-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
77	15	1.57 (4-II-2)	5.05 (4-II-3)	1.83 (5-I-3)	-104 (4-II-3)	-681 (4-II-3)	-22 (4-II-3)
77	16	-1.40 (1)	5.72 (4-II-3)	1.30 (5-I-3)	-170 (4-II-3)	-1557 (4-II-3)	-172 (5-I-3)
78	1	-3.47 (2)	2.54 (5-II-3)	4.59 (4-II-3)	147 (2)	-63 (1)	-43 (3)
78	2	-2.99 (2)	2.98 (5-II-3)	4.37 (4-II-3)	87 (5-I-3)	-121 (3)	-19 (5-II-3)
78	3	-3.57 (1)	3.41 (5-II-3)	3.68 (4-II-3)	-55 (5-II-3)	-334 (5-II-3)	16 (1)
78	4	-4.92 (1)	3.83 (5-II-3)	3.23 (4-II-3)	-210 (4-II-3)	698 (1)	-95 (4-II-3)
78	5	-3.52 (2)	2.92 (5-II-3)	4.48 (4-II-3)	131 (2)	-47 (1)	-29 (5-II-3)
78	6	-2.77 (2)	3.50 (5-II-3)	4.33 (4-II-3)	90 (5-I-3)	-106 (5-II-3)	31 (1)
78	7	-3.01 (1)	3.95 (5-II-3)	3.84 (4-II-3)	67 (1)	-335 (5-II-3)	-37 (3)
78	8	-3.66 (1)	5.11 (3)	2.40 (4-II-3)	-182 (4-II-3)	-685 (5-II-3)	-190 (4-II-3)
78	9	-3.42 (2)	3.20 (5-II-3)	4.14 (3)	-40 (5-II-3)	-45 (1)	-44 (5-II-3)
78	10	-2.44 (2)	4.17 (3)	3.98 (4-II-3)	-50 (5-II-3)	-107 (3)	-40 (5-II-3)
78	11	-2.37 (1)	5.34 (4-II-4)	3.52 (4-II-3)	-77 (5-II-3)	-353 (5-II-3)	-57 (4-II-2)
78	12	-2.75 (1)	6.33 (3)	1.84 (4-II-3)	-132 (4-II-3)	-707 (5-II-3)	-241 (4-II-3)
78	13	-3.48 (2)	3.64 (4-II-3)	3.58 (3)	-371 (2)	-42 (1)	-193 (3)
78	14	-2.21 (2)	5.32 (4-II-3)	3.21 (4-II-3)	-282 (2)	-96 (5-II-3)	-148 (3)
78	15	-1.66 (1)	7.42 (4-II-3)	2.58 (4-II-3)	-227 (2)	-327 (5-II-3)	-97 (4-II-3)
78	16	1.96 (4-II-2)	9.09 (4-II-3)	1.91 (4-II-3)	-171 (3)	-732 (5-II-3)	-256 (4-II-3)
79	1	-3.68 (2)	1.43 (4-I-3)	4.03 (3)	-502 (2)	-156 (1)	-124 (3)
79	2	-3.44 (2)	1.59 (4-I-3)	3.68 (3)	-525 (2)	-234 (2)	-92 (3)
79	3	-4.88 (1)	-1.74 (1)	3.13 (3)	-503 (2)	-279 (5-II-3)	-46 (5-II-2)
79	4	-9.11 (1)	-2.57 (1)	3.39 (3)	-190 (3)	1000 (1)	-237 (4-II-4)
79	5	-3.78 (2)	1.77 (5-II-3)	4.27 (3)	-104 (1)	-109 (1)	73 (3)
79	6	-3.51 (2)	1.76 (5-II-3)	4.05 (3)	-143 (1)	-149 (1)	82 (3)
79	7	-4.65 (1)	1.58 (4-I-3)	3.79 (3)	-140 (3)	-242 (5-II-3)	80 (2)
79	8	-7.10 (1)	1.79 (4-I-3)	2.77 (3)	114 (1)	999 (1)	-180 (4-II-3)
79	9	-3.72 (2)	2.08 (5-II-3)	4.50 (3)	138 (3)	-84 (1)	47 (3)
79	10	-3.27 (2)	2.12 (5-II-3)	4.31 (3)	79 (5-I-3)	-113 (3)	68 (3)
79	11	-4.19 (1)	2.14 (5-II-3)	3.83 (3)	74 (1)	-271 (5-II-3)	88 (2)
79	12	-5.82 (1)	2.18 (5-II-3)	2.55 (3)	192 (1)	926 (1)	-165 (4-II-3)
79	13	-3.74 (2)	2.45 (5-II-3)	4.61 (4-II-3)	158 (2)	-65 (1)	-21 (1)
79	14	-3.05 (2)	2.67 (5-II-3)	4.33 (3)	106 (2)	-88 (5-II-3)	17 (1)
79	15	-3.66 (1)	2.90 (5-II-3)	3.74 (3)	-54 (5-II-3)	-277 (5-II-3)	56 (1)
79	16	-4.58 (1)	3.14 (5-II-3)	2.73 (3)	131 (1)	867 (1)	-127 (4-II-3)
80	1	0.25 (4-I-1)	-4.03 (1)	0.63 (5-I-4)	-62 (3)	678 (1)	387 (1)
80	2	-0.75 (1)	-5.77 (1)	0.82 (5-I-4)	203 (1)	-90 (1)	483 (1)
80	3	-1.87 (1)	-7.68 (1)	1.35 (3)	245 (1)	-1334 (1)	225 (2)
80	4	-3.88 (1)	-6.89 (3)	1.40 (3)	-204 (2)	-4739 (1)	-290 (1)
80	5	-0.32 (5-I-3)	-2.90 (1)	2.04 (3)	-67 (1)	1062 (1)	289 (1)
80	6	-1.34 (1)	-3.29 (2)	2.27 (3)	-509 (1)	-237 (1)	381 (1)
80	7	-2.27 (1)	-3.11 (3)	1.94 (3)	-863 (1)	-2010 (1)	168 (1)
80	8	-1.39 (1)	-3.11 (3)	1.19 (5-I-4)	-928 (1)	-4693 (1)	40 (5-I-4)
80	9	-1.36 (5-I-3)	-2.86 (1)	2.49 (3)	70 (2)	1310 (1)	-41 (1)
80	10	-1.00 (1)	-2.67 (1)	2.47 (5-I-4)	-420 (1)	-276 (1)	57 (4-II-1)
80	11	-1.51 (1)	-2.27 (2)	1.82 (5-I-4)	-823 (1)	-1980 (1)	185 (1)
80	12	-1.12 (1)	-2.17 (3)	1.15 (3)	-983 (1)	-4885 (1)	503 (3)
80	13	-2.12 (5-I-3)	-3.76 (1)	2.44 (5-I-4)	728 (1)	1197 (1)	278 (4-II-4)
80	14	-0.46 (1)	-2.86 (1)	1.78 (3)	493 (1)	-274 (1)	-327 (1)
80	15	-0.67 (1)	-2.65 (1)	1.33 (5-I-4)	697 (1)	-1175 (1)	-81 (1)
80	16	-2.65 (1)	1.31 (5-I-4)	0.81 (5-I-4)	143 (1)	-4861 (1)	680 (3)
81	1	3.47 (3)	-2.47 (3)	-2.79 (3)	-1512 (3)	-2986 (3)	-609 (3)
81	2	2.79 (3)	-2.18 (3)	-2.74 (3)	-1765 (3)	-2908 (3)	-711 (3)
81	3	4.36 (3)	-1.53 (1)	-2.44 (3)	-1368 (3)	-1854 (1)	-563 (1)
81	4	4.54 (3)	-1.45 (1)	-1.97 (3)	-1431 (3)	-1926 (1)	-674 (1)
81	5	4.87 (3)	-1.34 (3)	-1.76 (3)	-1064 (3)	-1934 (1)	-699 (1)
81	6	5.16 (3)	-1.68 (3)	-1.55 (3)	-937 (3)	-1692 (1)	-709 (3)
81	7	3.43 (3)	-2.30 (3)	-1.87 (3)	-1601 (3)	-2761 (3)	-566 (3)
81	8	4.05 (3)	-1.63 (3)	-2.59 (3)	-1589 (3)	-2014 (3)	-569 (3)
82	1	3.35 (3)	-3.09 (3)	0.77 (5-II-3)	-1262 (3)	-3278 (3)	79 (5-II-3)
82	2	3.36 (3)	-3.16 (3)	-0.38 (5-I-3)	-1270 (3)	-3057 (3)	-193 (5-I-3)
82	3	4.07 (3)	-1.45 (3)	-0.37 (5-I-3)	-831 (3)	-1132 (2)	432 (3)
82	4	4.95 (3)	-1.35 (3)	0.56 (5-II-3)	-906 (3)	-1201 (1)	517 (3)
82	5	4.76 (3)	-1.18 (3)	0.81 (5-II-3)	-1098 (3)	-1350 (1)	479 (3)
82	6	4.95 (3)	-1.37 (3)	1.05 (3)	-1305 (3)	-1482 (2)	416 (1)
82	7	3.72 (3)	-2.76 (3)	0.71 (5-II-3)	-1430 (3)	-3020 (3)	97 (5-II-3)
82	8	3.98 (3)	-2.02 (3)	0.71 (5-II-3)	-1405 (3)	-1963 (3)	158 (5-II-3)
83	1	-3.26 (1)	0.38 (1)	-1.47 (3)	-375 (3)	369 (3)	-360 (1)
83	2	-3.02 (1)	-0.33 (5-II-3)	-1.89 (3)	361 (1)	-160 (5-II-3)	-507 (4-II-4)
83	3	-2.02 (1)	1.00 (1)	-2.48 (3)	456 (1)	789 (1)	-494 (4-II-4)
83	4	-2.99 (1)	1.73 (1)	-2.39 (3)	-677 (3)	730 (1)	-569 (3)
83	5	-2.84 (1)	0.91 (3)	-1.16 (4-II-4)	-524 (3)	535 (3)	-429 (1)
83	6	-3.54 (1)	-0.31 (5-II-3)	-1.70 (3)	-350 (3)	629 (3)	-709 (1)
83	7	-3.11 (1)	0.38 (1)	-1.67 (3)	407 (1)	383 (3)	-375 (1)
83	8	-3.05 (1)	0.44 (1)	-1.48 (4-II-4)	-668 (3)	313 (3)	-367 (1)
83	9	-3.71 (1)	0.26 (1)	-1.44 (3)	-273 (3)	590 (3)	-620 (1)
84	1	2.91 (3)	-1.23 (3)	1.83 (3)	-802 (3)	-884 (2)	667 (3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
84	2	2.59(3)	-2.30(3)	2.33(3)	-998(3)	-2549(3)	499(3)
84	3	2.90(3)	-1.04(3)	2.08(3)	-921(3)	-845(2)	584(3)
84	4	2.35(3)	-2.00(3)	2.48(3)	-1106(3)	-2602(3)	532(3)
84	5	2.91(3)	-0.83(2)	2.29(3)	-1013(3)	-761(2)	558(1)
84	6	2.10(3)	-1.77(3)	2.61(3)	-1244(3)	-2662(3)	567(3)
84	7	2.75(3)	-0.47(2)	2.36(3)	-1116(3)	-642(2)	527(1)
84	8	1.78(3)	-1.61(3)	2.74(3)	-1402(3)	-2731(3)	607(3)
85	1	1.75(3)	-1.05(3)	1.41(3)	-493(3)	-604(1)	737(3)
85	2	2.30(3)	-2.43(3)	1.86(3)	-719(3)	-2029(3)	412(1)
85	3	2.02(3)	-0.90(3)	1.89(3)	-728(3)	-632(2)	800(3)
85	4	2.09(3)	-2.12(3)	2.10(3)	-831(3)	-2097(3)	433(1)
85	5	2.32(3)	-0.89(2)	2.11(3)	-846(3)	-688(2)	790(3)
85	6	1.92(3)	-1.86(3)	2.35(3)	-909(3)	-2182(3)	489(3)
85	7	2.43(3)	-0.75(2)	2.28(3)	-924(3)	-683(2)	736(3)
85	8	1.67(3)	-1.68(3)	2.60(3)	-1000(3)	-2283(3)	571(3)
86	1	-2.68(3)	2.51(3)	2.67(3)	-2908(3)	-1203(3)	453(1)
86	2	-1.89(3)	4.30(3)	1.48(1)	-1602(3)	-1253(3)	629(3)
86	3	-3.01(3)	3.62(3)	2.42(1)	-2908(3)	-1173(3)	475(3)
87	1	1.14(5-II-3)	0.45(3)	-2.66(3)	-1052(3)	138(3)	-600(1)
87	2	-0.77(1)	-0.47(5-II-3)	-3.43(3)	-1257(3)	-1742(3)	-557(3)
87	3	1.25(5-II-3)	-0.25(5-II-3)	-2.95(3)	-856(3)	-188(1)	-619(1)
87	4	0.80(5-II-3)	-0.68(5-II-3)	-3.45(3)	-1019(3)	-1700(3)	-518(3)
87	5	1.15(5-II-3)	-0.50(3)	-2.94(3)	-689(3)	-245(1)	-636(1)
87	6	1.08(3)	-0.96(5-II-3)	-3.42(3)	-832(3)	-1662(3)	-490(3)
87	7	1.09(5-II-3)	-0.82(3)	-2.80(3)	-516(3)	-290(1)	-640(3)
87	8	1.42(3)	-1.40(3)	-3.35(3)	-687(3)	-1630(3)	-468(1)
88	1	5.11(3)	-1.66(3)	0.49(5-II-3)	-1188(3)	-1704(3)	268(1)
88	2	3.81(3)	-3.24(3)	0.46(5-II-3)	-1434(3)	-3330(3)	-157(5-I-3)
88	3	5.09(3)	-1.69(3)	0.72(5-II-3)	-1247(3)	-1828(1)	277(1)
88	4	3.93(3)	-3.18(3)	0.69(5-II-3)	-1450(3)	-3352(3)	-115(5-I-3)
88	5	4.99(3)	-1.74(3)	0.96(3)	-1242(3)	-1943(1)	275(1)
88	6	4.03(3)	-3.20(3)	0.91(5-II-3)	-1473(3)	-3381(3)	107(5-II-3)
88	7	4.91(3)	-1.76(3)	1.55(3)	-1175(3)	-2020(1)	275(1)
88	8	4.15(3)	-3.26(3)	1.12(5-II-3)	-1458(3)	-3426(3)	143(5-II-3)
89	1	-0.67(1)	-0.30(5-II-3)	-2.88(3)	-599(3)	-190(5-II-3)	-642(3)
89	2	-0.93(1)	-0.79(5-II-3)	-3.38(3)	-620(3)	-1405(3)	-510(3)
89	3	-0.74(1)	-0.48(5-II-3)	-2.84(3)	-496(3)	-237(5-II-3)	-691(3)
89	4	0.75(5-II-3)	-1.01(5-II-3)	-3.23(3)	-507(3)	-1346(3)	-459(4-II-4)
89	5	-0.94(1)	-0.52(5-II-3)	-2.71(3)	-378(3)	-242(5-II-3)	-711(3)
89	6	0.95(5-II-3)	-1.34(3)	-3.12(1)	-423(3)	-1296(3)	-433(1)
89	7	-1.07(1)	-0.70(4-II-4)	-2.41(3)	322(1)	-205(5-II-3)	-677(3)
89	8	1.23(4-II-4)	-1.74(3)	-3.00(1)	488(1)	-1259(3)	-427(1)
90	1	3.97(3)	-0.99(3)	-2.29(3)	-1257(3)	-1304(1)	-794(3)
90	2	3.27(3)	-2.47(3)	-2.43(1)	-1271(3)	-2612(3)	-492(1)
90	3	3.85(3)	-1.10(3)	-2.08(3)	-1135(3)	-1197(1)	-821(3)
90	4	3.30(3)	-2.63(3)	-2.20(1)	-1182(3)	-2483(3)	-404(1)
90	5	3.53(3)	-1.18(3)	-1.78(1)	-956(3)	-1064(1)	-817(3)
90	6	3.30(3)	-2.87(3)	-2.00(1)	-1109(3)	-2380(3)	-336(1)
90	7	3.40(3)	-1.44(1)	-1.23(1)	-651(3)	-932(1)	-762(3)
90	8	3.38(3)	-3.18(3)	-1.83(1)	-1006(3)	-2300(3)	-311(1)
91	1	-1.70(5-II-3)	-0.42(5-II-3)	2.30(3)	-290(4-I-4)	341(5-II-3)	708(3)
91	2	0.64(5-I-3)	-0.88(5-I-3)	2.55(3)	390(1)	-736(4-I-4)	468(3)
91	3	-1.53(5-II-3)	-0.33(5-I-3)	2.39(3)	-397(3)	263(5-II-3)	749(3)
91	4	-0.71(1)	-0.65(5-I-3)	2.69(3)	-443(3)	-763(3)	500(3)
91	5	-1.45(5-II-3)	-0.31(5-I-3)	2.33(3)	-488(3)	216(5-II-3)	737(3)
91	6	-0.94(1)	-0.43(5-I-3)	2.81(3)	-516(3)	-803(3)	549(3)
91	7	-1.51(5-II-3)	-0.19(4-I-4)	2.24(3)	-567(3)	208(5-II-3)	691(3)
91	8	-1.20(1)	0.44(1)	2.89(3)	-596(3)	-849(3)	600(3)
92	1	-3.31(1)	0.39(1)	-1.64(4-II-4)	-328(5-II-3)	251(3)	-520(4-II-4)
92	2	-2.74(1)	1.27(1)	-2.46(4-II-4)	454(1)	1032(1)	-529(3)
92	3	-3.17(1)	0.25(1)	-1.81(4-II-4)	303(1)	269(3)	-564(3)
92	4	-2.45(1)	1.01(1)	-2.45(4-II-4)	529(1)	1050(1)	-493(3)
92	5	-3.12(1)	0.23(1)	-1.95(4-II-4)	342(1)	334(3)	-583(3)
92	6	-2.21(1)	0.79(1)	-2.41(4-II-4)	604(1)	1066(1)	-456(3)
92	7	-3.09(1)	0.27(5-I-3)	-2.09(3)	397(1)	437(3)	-546(3)
92	8	-1.96(1)	0.59(1)	-2.36(4-II-4)	676(1)	1082(1)	-448(4-II-4)
93	1	-3.96(1)	0.79(3)	0.69(5-I-3)	302(1)	719(3)	101(5-I-3)
93	2	-3.09(1)	1.45(1)	-0.87(5-II-3)	542(1)	1420(1)	-199(5-II-3)
93	3	-3.92(1)	0.52(1)	-0.61(5-II-3)	356(1)	569(3)	-107(5-II-3)
93	4	-2.78(1)	1.35(1)	-0.94(5-II-3)	619(1)	1401(1)	-186(5-II-3)
93	5	-4.04(1)	0.37(1)	-0.89(4-II-4)	386(1)	470(3)	-162(5-II-3)
93	6	-2.60(1)	1.25(1)	-0.99(4-II-4)	657(1)	1385(1)	-171(5-II-3)
93	7	-4.17(1)	0.29(1)	-1.06(4-II-4)	395(1)	426(4-II-3)	-216(5-II-3)
93	8	-2.47(1)	1.20(1)	-1.06(4-II-4)	680(1)	1375(1)	-154(5-II-3)
94	1	0.74(1)	-1.59(1)	2.28(4-II-4)	1175(1)	801(1)	459(1)
94	2	0.54(1)	-3.32(1)	1.72(4-II-4)	545(1)	459(1)	405(3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
94	3	-0.49(5-II-3)	-1.24(1)	2.11(4-II-4)	1154(1)	700(1)	357(1)
95	1	-4.16(1)	0.33(4-II-4)	-0.65(5-II-3)	394(1)	493(4-II-3)	-205(5-II-3)
95	2	-2.74(1)	1.40(1)	-0.77(5-II-3)	659(1)	1432(1)	-131(5-II-3)
95	3	-3.97(1)	0.34(1)	-0.85(4-II-4)	390(1)	540(4-II-3)	-255(5-II-3)
95	4	-2.75(1)	1.38(1)	-0.77(5-II-3)	647(1)	1388(1)	-114(1)
95	5	-3.79(1)	0.53(4-II-3)	-1.08(4-II-4)	354(1)	631(4-II-3)	-286(5-II-3)
95	6	-2.76(1)	1.41(1)	-0.79(4-II-4)	619(1)	1346(1)	-118(1)
95	7	-3.91(3)	0.92(3)	-1.35(4-II-4)	-272(4-I-4)	747(4-II-3)	-280(5-II-3)
95	8	-2.73(1)	1.47(1)	-0.83(4-II-4)	567(1)	1307(1)	-113(1)
96	1	-3.66(4-II-4)	0.55(4-II-4)	1.92(3)	360(1)	676(4-II-3)	432(3)
96	2	-2.15(1)	0.96(4-II-4)	1.59(3)	587(1)	1240(1)	247(3)
96	3	-3.54(4-II-4)	0.38(4-II-4)	1.52(3)	329(1)	580(4-II-3)	427(3)
96	4	-2.24(1)	1.00(1)	1.57(3)	545(1)	1222(1)	255(3)
96	5	-3.56(4-II-4)	0.28(4-II-4)	1.25(5-I-3)	294(1)	526(4-II-3)	375(3)
96	6	-2.31(1)	1.11(1)	1.54(3)	498(1)	1205(1)	273(3)
96	7	-3.69(4-II-4)	0.36(4-II-3)	1.11(5-I-3)	-300(4-I-4)	520(4-II-3)	315(5-I-3)
96	8	-2.38(1)	1.28(1)	1.48(3)	451(1)	1188(1)	293(3)
97	1	-3.42(4-II-4)	-0.21(4-I-4)	1.47(3)	-286(4-I-4)	450(4-II-4)	323(3)
97	2	-1.90(1)	1.00(1)	1.76(3)	423(1)	1089(1)	324(3)
97	3	-3.15(4-II-4)	0.31(4-II-4)	1.29(3)	-327(4-I-4)	510(4-II-4)	313(1)
97	4	-2.15(1)	1.19(4-II-4)	1.67(3)	-399(4-I-4)	1052(1)	328(3)
97	5	-2.93(4-II-4)	0.60(4-II-3)	1.10(5-I-3)	-367(4-I-4)	603(4-II-4)	295(1)
97	6	-2.35(1)	1.46(4-II-3)	1.57(3)	-488(3)	1017(1)	335(3)
97	7	-3.08(4-II-4)	1.12(3)	0.74(5-I-3)	-497(3)	712(4-II-4)	279(1)
97	8	-2.58(1)	1.74(3)	1.47(3)	-669(3)	985(1)	354(3)
98	1	1.59(3)	1.52(3)	-0.25(4-II-3)	-395(3)	-422(3)	68(4-II-3)
98	2	1.78(3)	1.40(3)	-0.28(4-II-3)	-474(3)	-249(3)	75(4-II-3)
98	3	1.66(3)	1.35(3)	0.11(1)	-452(3)	-352(3)	-52(1)
98	4	1.50(3)	1.53(3)	-0.34(4-II-3)	-410(3)	-566(3)	86(4-II-3)
98	5	1.59(3)	1.53(3)	-0.26(4-II-3)	-357(3)	-323(3)	115(4-II-3)
98	6	1.59(3)	1.53(3)	-0.24(4-II-3)	-380(3)	-277(3)	64(4-II-3)
98	7	1.58(3)	1.53(3)	-0.24(4-II-3)	-407(3)	-524(3)	76(4-II-3)
98	8	1.58(3)	1.52(3)	-0.25(4-II-3)	-394(3)	-436(3)	115(4-II-3)
99	1	-1.17(5-II-3)	-0.65(2)	2.30(3)	-452(3)	-294(5-I-3)	689(3)
99	2	0.82(5-I-3)	-0.73(5-I-3)	2.88(3)	-599(3)	-1122(3)	605(3)
99	3	-1.02(5-II-3)	-0.43(2)	2.33(3)	-577(3)	-244(5-I-3)	594(3)
99	4	-0.66(1)	-0.46(5-I-3)	2.89(3)	-743(3)	-1158(3)	619(3)
99	5	-0.86(5-II-3)	-0.22(5-I-3)	2.25(3)	-701(3)	197(5-II-3)	520(1)
99	6	-0.93(1)	0.44(1)	2.85(3)	-924(3)	-1197(3)	637(3)
99	7	-0.94(5-II-3)	0.57(5-II-3)	1.89(3)	-864(3)	309(5-II-3)	471(1)
99	8	-1.26(1)	0.71(1)	2.80(3)	-1156(3)	-1237(3)	665(3)
100	1	1.78(3)	1.73(3)	-0.32(3)	-441(3)	-476(3)	79(3)
100	2	1.94(3)	1.60(3)	-0.30(3)	-525(3)	-338(3)	99(3)
100	3	1.79(3)	1.40(3)	-0.17(5-II-3)	-485(3)	-364(3)	26(5-II-3)
100	4	1.68(3)	1.73(3)	-0.35(3)	-454(3)	-577(3)	77(4-II-3)
100	5	1.80(3)	1.74(3)	-0.32(3)	-407(3)	-402(3)	137(3)
100	6	1.77(3)	1.73(3)	-0.29(3)	-434(3)	-363(3)	87(3)
100	7	1.75(3)	1.74(3)	-0.30(3)	-447(3)	-551(3)	78(3)
100	8	1.77(3)	1.72(3)	-0.32(3)	-428(3)	-474(3)	126(3)
101	1	1.18(3)	1.22(3)	0.54(1)	-275(3)	-310(3)	-145(1)
101	2	0.94(3)	1.34(3)	0.59(1)	-288(3)	-489(3)	-145(1)
101	3	1.37(3)	1.31(3)	0.39(1)	-405(3)	-361(3)	-76(1)
101	4	1.29(3)	1.17(3)	0.66(1)	-301(3)	304(1)	-231(3)
101	5	1.15(3)	1.22(3)	0.55(1)	-246(3)	-397(3)	-198(1)
101	6	1.18(3)	1.22(3)	0.54(1)	-309(3)	-448(3)	-132(1)
101	7	1.20(3)	1.22(3)	0.54(1)	-243(3)	246(1)	-168(3)
101	8	1.18(3)	1.22(3)	0.55(1)	-193(3)	-270(3)	-204(1)
102	1	1.18(3)	1.56(3)	0.58(1)	-283(3)	-400(3)	-153(1)
102	2	0.96(3)	1.72(3)	0.57(1)	-288(3)	-577(3)	-150(1)
102	3	1.33(3)	1.61(3)	0.39(1)	-388(3)	-442(3)	-74(1)
102	4	1.31(3)	1.55(3)	0.67(1)	-310(3)	-271(3)	-238(3)
102	5	1.14(3)	1.55(3)	0.59(1)	-253(3)	-477(3)	-210(1)
102	6	1.18(3)	1.56(3)	0.57(1)	-314(3)	-528(3)	-142(1)
102	7	1.21(3)	1.55(3)	0.57(1)	-254(3)	-285(3)	-180(3)
102	8	1.18(3)	1.57(3)	0.59(1)	-206(3)	-371(3)	-213(1)
103	1	0.85(3)	0.90(3)	0.53(1)	-249(3)	-337(3)	-126(1)
103	2	1.36(3)	1.16(3)	0.27(1)	-403(3)	-306(3)	-49(1)
103	3	1.14(3)	-1.00(1)	0.48(1)	-251(3)	369(1)	-153(3)
104	1	1.20(3)	2.03(3)	0.38(3)	-288(3)	-530(3)	-111(3)
104	2	0.98(3)	2.13(3)	0.48(3)	-297(3)	-693(3)	-118(1)
104	3	1.31(3)	1.88(3)	0.23(3)	-376(3)	-509(3)	-42(5-II-3)
104	4	1.26(3)	2.00(3)	0.54(3)	-301(3)	-379(3)	-201(3)
104	5	1.19(3)	2.04(3)	0.39(3)	-274(3)	-617(3)	-151(1)
104	6	1.19(3)	2.02(3)	0.40(3)	-319(3)	-657(3)	-101(1)
104	7	1.20(3)	2.04(3)	0.40(3)	-260(3)	-419(3)	-145(3)
104	8	1.19(3)	2.02(3)	0.39(3)	-222(3)	-488(3)	-161(1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
105	1	1.80 (3)	2.16 (3)	-0.41 (3)	-466 (3)	-612 (3)	93 (1)
105	2	1.93 (3)	2.10 (3)	-0.41 (3)	-503 (3)	-517 (3)	128 (3)
105	3	1.81 (3)	1.47 (3)	-0.21 (3)	-489 (3)	-391 (3)	43 (3)
106	1	1.74 (3)	2.36 (3)	-0.39 (3)	-443 (3)	-635 (3)	97 (3)
106	2	1.78 (3)	2.26 (3)	-0.36 (3)	-490 (3)	-600 (3)	118 (3)
106	3	1.70 (3)	1.73 (3)	-0.26 (1)	-459 (3)	-454 (3)	71 (1)
106	4	1.73 (3)	2.29 (3)	-0.35 (3)	-452 (3)	-606 (3)	103 (1)
106	5	1.76 (3)	2.37 (3)	-0.39 (3)	-425 (3)	-629 (3)	118 (3)
106	6	1.73 (3)	2.36 (3)	-0.38 (3)	-451 (3)	-625 (3)	115 (3)
106	7	1.72 (3)	2.38 (3)	-0.37 (3)	-436 (3)	-634 (3)	89 (1)
106	8	1.74 (3)	2.36 (3)	-0.38 (3)	-415 (3)	-621 (3)	100 (3)
107	1	1.50 (3)	2.71 (3)	-0.25 (1)	-406 (3)	-740 (3)	85 (3)
107	2	1.52 (3)	1.85 (3)	-0.18 (1)	-413 (3)	-483 (3)	65 (1)
107	3	1.58 (3)	2.65 (3)	-0.22 (3)	-400 (3)	-677 (3)	70 (1)
108	1	1.35 (3)	2.64 (3)	0.12 (4-II-3)	-323 (3)	-736 (3)	-58 (4-II-3)
108	2	1.09 (3)	3.00 (3)	0.11 (4-II-3)	-292 (3)	-765 (3)	-56 (1)
108	3	1.33 (3)	1.87 (3)	0.20 (4-II-3)	-380 (3)	-477 (3)	27 (1)
109	1	0.95 (3)	-1.10 (1)	0.30 (1)	-212 (3)	310 (1)	-72 (1)
109	2	0.74 (3)	-0.98 (1)	0.31 (1)	-231 (3)	-321 (3)	-76 (1)
109	3	1.28 (3)	1.03 (3)	0.13 (1)	-384 (3)	-289 (3)	23 (5-II-3)
109	4	1.06 (3)	-1.12 (1)	0.31 (1)	-244 (3)	435 (1)	-134 (3)
109	5	0.89 (3)	-1.11 (1)	0.31 (1)	-177 (3)	236 (1)	-133 (1)
109	6	0.95 (3)	-1.10 (1)	0.27 (1)	-237 (3)	-266 (5-II-3)	-70 (1)
109	7	0.97 (3)	-1.12 (1)	0.27 (1)	-187 (3)	401 (1)	-87 (3)
109	8	0.93 (3)	-1.10 (1)	0.28 (1)	166 (1)	319 (1)	-122 (1)
110	1	0.85 (3)	-1.57 (1)	0.31 (4-II-4)	-182 (3)	430 (1)	-111 (4-II-4)
110	2	-0.72 (1)	-1.45 (1)	0.24 (4-II-4)	-187 (3)	353 (1)	-50 (1)
110	3	1.13 (3)	1.16 (3)	-0.11 (4-I-2)	-351 (3)	-308 (3)	36 (3)
111	1	0.96 (3)	-0.86 (1)	-0.22 (5-I-3)	-213 (3)	218 (1)	54 (5-I-3)
111	2	1.06 (3)	-0.85 (1)	-0.20 (5-I-3)	-291 (3)	289 (1)	68 (3)
111	3	1.08 (3)	1.35 (3)	-0.10 (5-I-3)	-307 (3)	-361 (3)	-27 (5-II-3)
111	4	0.85 (3)	0.85 (3)	-0.27 (5-I-3)	-231 (3)	-336 (3)	91 (1)
111	5	0.95 (3)	-0.85 (1)	-0.22 (5-I-3)	-175 (3)	267 (1)	90 (5-I-3)
111	6	0.96 (3)	-0.85 (1)	-0.20 (5-I-3)	-202 (3)	301 (1)	51 (5-I-3)
111	7	0.93 (3)	-0.85 (1)	-0.21 (5-I-3)	-224 (3)	-266 (3)	59 (1)
111	8	0.93 (3)	-0.88 (1)	-0.24 (5-I-3)	-208 (3)	206 (1)	96 (3)
112	1	0.80 (3)	-1.10 (1)	-0.17 (5-I-3)	210 (1)	285 (1)	41 (5-I-3)
112	2	0.88 (3)	-1.05 (1)	-0.17 (5-I-3)	-247 (3)	313 (1)	64 (5-I-3)
112	3	0.98 (3)	1.29 (3)	-0.17 (1)	-286 (3)	-348 (3)	31 (1)
112	4	-0.86 (1)	-0.95 (1)	-0.24 (5-I-3)	217 (1)	-252 (3)	81 (1)
112	5	-0.78 (1)	-1.09 (1)	-0.16 (5-I-3)	199 (1)	313 (1)	72 (5-I-3)
112	6	0.80 (3)	-1.09 (1)	-0.15 (5-I-3)	223 (1)	337 (1)	40 (5-I-3)
112	7	-0.80 (1)	-1.09 (1)	-0.16 (5-I-3)	196 (1)	241 (1)	48 (1)
112	8	-0.80 (1)	-1.12 (1)	-0.18 (5-I-3)	177 (1)	280 (1)	74 (5-I-3)
113	1	-0.79 (1)	-1.37 (1)	-0.14 (4-I-2)	215 (1)	361 (1)	35 (4-I-2)
113	2	-0.77 (1)	-1.26 (1)	-0.12 (4-I-2)	-213 (3)	334 (1)	57 (4-I-2)
113	3	0.96 (3)	1.22 (3)	-0.21 (1)	-287 (3)	-331 (3)	53 (1)
113	4	-0.84 (1)	-1.22 (1)	-0.17 (5-I-3)	220 (1)	318 (1)	57 (1)
113	5	-0.80 (1)	-1.35 (1)	-0.13 (4-I-2)	206 (1)	363 (1)	52 (5-I-3)
113	6	-0.79 (1)	-1.36 (1)	-0.12 (4-I-2)	222 (1)	373 (1)	39 (4-I-2)
113	7	-0.80 (1)	-1.35 (1)	-0.13 (4-I-2)	208 (1)	348 (1)	37 (1)
113	8	-0.81 (1)	-1.38 (1)	-0.16 (5-I-3)	195 (1)	363 (1)	54 (5-I-3)
114	1	1.14 (3)	1.01 (3)	-0.23 (4-II-3)	-265 (3)	-287 (3)	57 (4-II-3)
114	2	1.30 (3)	0.97 (3)	-0.22 (4-II-3)	-348 (3)	250 (1)	69 (4-II-3)
114	3	1.25 (3)	1.36 (3)	-0.09 (4-II-2)	-346 (3)	-356 (3)	-40 (1)
114	4	1.02 (3)	1.12 (3)	-0.31 (4-II-3)	-284 (3)	-452 (3)	84 (1)
114	5	1.14 (3)	1.03 (3)	-0.24 (4-II-3)	-233 (3)	-195 (3)	105 (3)
114	6	1.14 (3)	1.02 (3)	-0.21 (4-II-3)	-250 (3)	237 (1)	52 (4-II-3)
114	7	1.11 (3)	1.02 (3)	-0.22 (4-II-3)	-281 (3)	-387 (3)	67 (4-II-3)
114	8	1.12 (3)	0.99 (3)	-0.25 (4-II-3)	-272 (3)	-291 (3)	109 (4-II-3)
115	1	-0.80 (1)	-1.60 (1)	0.24 (4-II-4)	222 (1)	430 (1)	-62 (4-II-4)
115	2	-0.81 (1)	-1.39 (1)	0.23 (4-II-2)	214 (1)	331 (1)	52 (4-I-2)
115	3	1.02 (3)	1.16 (3)	-0.18 (1)	-313 (3)	-318 (3)	54 (1)
115	4	-0.79 (1)	-1.40 (1)	0.16 (4-II-4)	218 (1)	411 (1)	-90 (4-II-4)
115	5	-0.85 (1)	-1.59 (1)	0.26 (4-II-4)	225 (1)	407 (1)	-77 (4-II-4)
115	6	-0.81 (1)	-1.60 (1)	0.25 (4-II-4)	221 (1)	400 (1)	-52 (4-II-4)
115	7	-0.80 (1)	-1.60 (1)	0.23 (4-II-4)	222 (1)	454 (1)	-78 (4-II-4)
115	8	-0.83 (1)	-1.62 (1)	0.20 (4-II-4)	224 (1)	440 (1)	-66 (4-II-4)
116	1	1.36 (3)	1.25 (3)	-0.26 (4-II-3)	-331 (3)	-352 (3)	68 (4-II-3)
116	2	1.54 (3)	1.18 (3)	-0.26 (4-II-3)	-411 (3)	221 (1)	75 (4-II-3)
116	3	1.47 (3)	1.36 (3)	0.14 (1)	-401 (3)	-358 (3)	-61 (1)
116	4	1.26 (3)	1.33 (3)	-0.35 (4-II-3)	-347 (3)	-508 (3)	90 (4-II-3)
116	5	1.36 (3)	1.26 (3)	-0.26 (4-II-3)	-292 (3)	-254 (3)	114 (4-II-3)
116	6	1.37 (3)	1.26 (3)	-0.25 (4-II-3)	-315 (3)	-203 (3)	62 (4-II-3)
116	7	1.34 (3)	1.26 (3)	-0.26 (4-II-3)	-346 (3)	-456 (3)	77 (4-II-3)
116	8	1.34 (3)	1.23 (3)	-0.28 (4-II-3)	-333 (3)	-359 (3)	120 (4-II-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
117	1	14.83(1)	2.84(3)	5.94(3)	260(1)	196(1)	-67(3)
117	2	-0.38(1)	0.47(5-I-4)	4.29(3)	479(1)	255(3)	157(1)
117	3	-5.23(1)	-3.42(1)	4.46(3)	385(1)	567(3)	384(3)
117	4	-9.04(3)	-0.80(4-II-1)	3.15(3)	391(3)	970(5-I-4)	786(3)
117	5	3.87(4-II-4)	0.24(3)	2.45(1)	199(5-I-4)	68(5-I-3)	83(1)
117	6	1.05(4-II-2)	1.71(1)	6.13(1)	171(5-I-4)	395(3)	111(3)
117	7	-2.94(1)	3.26(1)	5.21(3)	157(5-I-4)	944(3)	225(3)
117	8	-2.88(3)	3.17(3)	3.19(1)	159(5-I-4)	1698(3)	537(3)
117	9	-3.35(3)	-0.65(1)	1.47(3)	211(5-I-4)	83(3)	55(1)
117	10	-2.23(1)	0.99(3)	3.72(1)	229(5-I-4)	493(3)	70(1)
117	11	-1.29(1)	2.19(3)	4.40(1)	241(5-I-4)	1265(3)	116(1)
117	12	-0.59(1)	3.10(3)	3.94(1)	229(5-I-4)	2259(3)	297(1)
117	13	-7.19(1)	-1.90(1)	1.24(1)	81(1)	104(3)	-50(3)
117	14	-3.57(1)	2.27(3)	1.41(1)	60(1)	495(3)	44(1)
117	15	-2.51(3)	4.76(3)	2.02(1)	46(1)	1231(3)	-54(5-I-4)
117	16	0.56(4-II-3)	6.01(3)	3.90(3)	200(3)	2867(3)	204(1)
118	1	-4.92(1)	-3.39(1)	0.37(4-I-1)	3865(1)	1823(1)	-690(3)
118	2	-4.99(1)	-3.46(1)	0.48(4-I-1)	5447(3)	1894(1)	-279(3)
118	3	-4.98(1)	-3.75(1)	0.63(4-I-1)	6339(3)	2047(1)	270(1)
118	4	-5.09(1)	-4.09(1)	0.85(4-I-1)	6840(3)	2316(1)	494(1)
118	5	-5.14(1)	-4.54(1)	1.38(3)	6997(3)	2288(2)	592(2)
118	6	-4.93(1)	-4.04(1)	0.83(4-I-1)	6932(3)	2285(1)	574(2)
118	7	-4.77(1)	-3.78(1)	0.61(4-I-1)	6226(3)	1895(1)	315(1)
118	8	-4.69(1)	-3.38(1)	0.45(4-I-1)	4327(3)	1257(1)	-352(3)
118	9	-4.82(3)	-3.54(1)	0.52(4-I-1)	1530(1)	413(1)	-848(3)
118	10	-5.61(3)	-4.13(1)	1.70(3)	-3589(3)	-845(3)	-1688(3)
118	11	-4.00(3)	-4.56(1)	1.35(3)	-4023(3)	-347(5-II-3)	-1500(3)
118	12	-3.44(2)	-5.21(1)	0.58(5-II-2)	-3761(3)	901(1)	-1475(3)
118	13	-3.90(1)	-6.01(1)	-1.72(1)	-2747(3)	1956(1)	-1458(3)
118	14	-4.33(1)	-4.27(1)	-0.76(1)	-664(4-II-3)	1910(1)	-1461(3)
118	15	-4.70(1)	-3.50(1)	-0.42(1)	2119(1)	1761(1)	-1136(3)
118	16	-4.79(1)	-3.51(1)	0.46(4-I-1)	3924(1)	1562(1)	-506(3)
118	17	-4.64(1)	-3.66(1)	0.47(5-II-2)	1909(1)	1201(1)	-1169(3)
118	18	-4.29(1)	-4.22(1)	0.47(5-II-2)	423(1)	806(1)	-1143(3)
118	19	-4.32(1)	-4.33(1)	-0.45(1)	-841(5-II-2)	1197(1)	-1401(3)
119	1	-5.01(1)	-3.61(1)	0.83(3)	5078(1)	3028(1)	-1503(3)
119	2	-5.08(1)	-4.00(1)	0.88(3)	5730(2)	2940(2)	-1659(3)
119	3	-5.09(1)	-4.42(1)	0.92(3)	6055(2)	2796(2)	-1557(3)
119	4	-4.77(1)	-5.26(3)	1.30(3)	6370(2)	2627(2)	-1608(3)
119	5	-4.91(1)	-4.51(1)	0.99(3)	6193(2)	2778(2)	-1581(3)
119	6	-4.94(1)	-4.02(1)	0.98(3)	5712(2)	2836(2)	-1716(3)
119	7	-4.94(1)	-3.67(1)	1.01(3)	4880(1)	2790(2)	-1624(3)
119	8	-4.89(1)	-3.41(1)	0.98(3)	3566(1)	2704(1)	-1327(3)
119	9	-4.98(1)	-3.09(1)	0.77(3)	2005(1)	2846(1)	-761(3)
119	10	-5.10(1)	-2.88(1)	0.40(5-I-4)	-814(5-I-4)	2738(1)	396(1)
119	11	-4.96(1)	-2.91(1)	-1.40(1)	-2343(3)	3547(1)	796(1)
119	12	-4.72(1)	-2.41(1)	-0.65(1)	-1159(4-II-3)	3485(1)	692(1)
119	13	-4.78(1)	-2.35(1)	0.26(5-I-1)	1579(1)	2992(1)	600(1)
119	14	-4.87(1)	-2.34(1)	0.51(3)	3803(1)	2571(1)	-325(5-I-4)
119	15	-4.94(1)	-3.12(1)	0.69(3)	4460(1)	3089(1)	-1132(3)
119	16	-4.80(1)	-3.04(1)	0.67(3)	3101(1)	2912(1)	-788(3)
119	17	-4.94(1)	-3.44(1)	0.89(3)	4390(1)	2952(1)	-1463(3)
120	1	-9.01(2)	-3.62(1)	1.51(3)	2766(2)	1220(1)	-1018(3)
120	2	-8.78(2)	-3.98(1)	2.00(3)	3155(2)	1691(1)	-753(3)
120	3	-8.21(2)	-4.39(1)	1.99(3)	3565(2)	2119(1)	-947(3)
120	4	-8.48(2)	-3.98(1)	1.76(3)	4349(2)	1801(1)	-1308(3)
120	5	-8.48(2)	-3.72(1)	1.22(3)	4865(3)	1712(1)	-1091(3)
120	6	-8.26(2)	-3.89(1)	0.57(5-II-3)	5328(3)	1740(1)	-663(3)
120	7	-8.40(2)	-4.17(1)	0.36(5-II-3)	5442(3)	1948(1)	-257(5-II-3)
120	8	-9.27(2)	-4.25(1)	0.51(5-II-3)	4719(3)	1854(1)	221(5-I-3)
120	9	-8.89(2)	-3.99(1)	0.54(5-II-3)	4340(2)	1705(1)	616(2)
120	10	-7.97(2)	-3.02(1)	0.30(5-II-3)	3140(1)	1068(1)	831(2)
120	11	-6.88(1)	-1.69(1)	-0.87(5-I-3)	1620(1)	470(1)	721(3)
120	12	-8.67(2)	-2.02(1)	-0.59(5-I-3)	1030(1)	-402(5-II-3)	-481(3)
120	13	-9.19(2)	-2.88(1)	0.72(5-II-3)	2139(1)	998(1)	-966(3)
120	14	-8.30(2)	-3.17(1)	-0.49(5-I-3)	3529(2)	930(1)	-124(5-II-3)
120	15	-8.52(2)	-3.48(1)	0.39(5-II-3)	4226(2)	1228(1)	-531(3)
120	16	-8.39(2)	-3.75(1)	-0.39(5-I-3)	4742(2)	1596(1)	169(5-I-3)
121	1	-1.53(3)	1.49(3)	2.23(1)	-101(1)	-75(4-I-1)	26(1)
121	2	-2.25(2)	-0.44(1)	3.71(1)	57(5-I-3)	-22(5-II-2)	49(1)
121	3	-2.68(1)	-2.23(1)	4.86(1)	71(5-I-3)	73(4-I-4)	108(1)
121	4	-4.98(1)	-3.45(1)	5.62(1)	278(3)	-271(1)	455(1)
121	5	-6.52(1)	-0.58(1)	3.04(1)	35(1)	500(1)	70(1)
121	6	-4.98(1)	-1.92(1)	5.63(1)	36(5-I-3)	152(1)	-66(1)
121	7	-3.74(1)	-2.28(1)	6.63(1)	38(3)	-62(1)	-84(1)
121	8	-2.05(1)	-2.89(1)	5.77(1)	30(4-I-4)	-177(1)	468(1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
121	9	-13.83(1)	-3.59(1)	3.02(1)	-171(3)	597(1)	205(1)
121	10	-8.36(1)	-3.93(1)	6.47(1)	-236(1)	-45(5-I-4)	16(4-I-1)
121	11	-2.51(1)	-3.78(1)	6.19(1)	-267(1)	-250(1)	-88(1)
121	12	1.57(3)	-3.41(1)	4.62(1)	-469(1)	137(3)	232(1)
121	13	-22.32(1)	-10.73(1)	4.46(1)	-2430(1)	603(1)	226(1)
121	14	-6.73(1)	-5.34(1)	2.39(1)	-2227(1)	-172(1)	338(3)
121	15	-1.05(3)	-1.74(3)	1.56(1)	-1830(1)	-439(1)	349(3)
121	16	3.85(1)	1.80(1)	1.80(1)	-1790(1)	-180(1)	220(1)
122	1	-3.93(3)	-4.21(1)	-1.36(1)	2411(3)	2369(3)	1158(4-II-2)
122	2	-4.02(3)	-4.21(1)	-1.40(1)	3500(3)	3444(3)	1732(2)
122	3	-4.05(2)	-4.18(1)	-1.38(1)	4210(3)	4115(3)	2281(2)
122	4	-4.07(2)	-4.18(1)	-1.33(1)	4693(2)	4539(3)	2666(2)
122	5	-4.07(2)	-4.17(1)	-1.29(1)	4925(2)	4663(3)	2858(2)
122	6	-4.06(2)	-4.16(1)	-1.24(1)	4894(2)	4545(3)	2845(2)
122	7	-4.03(2)	-4.18(1)	-1.18(1)	4464(2)	4085(2)	2586(1)
122	8	-4.12(3)	-4.10(1)	-1.21(1)	3962(1)	3514(2)	2226(1)
122	9	-4.34(3)	-4.03(1)	-1.27(1)	2838(1)	2812(1)	1645(1)
122	10	-3.66(2)	-4.13(1)	-1.09(1)	3270(1)	2742(1)	1687(1)
122	11	-3.19(1)	-4.36(1)	-1.24(1)	3444(1)	2751(1)	1819(1)
122	12	-3.10(1)	-4.47(1)	-1.71(1)	3153(1)	2363(1)	1571(1)
122	13	-3.33(1)	-4.33(1)	-1.66(2)	3991(2)	3165(1)	2253(1)
122	14	-3.48(1)	-4.16(1)	-1.60(2)	4561(2)	3710(2)	2562(1)
122	15	-3.61(1)	-4.06(1)	-1.49(2)	4732(2)	4065(3)	2728(1)
122	16	-3.71(2)	-4.00(1)	-1.36(2)	4424(2)	4069(3)	2654(2)
122	17	-3.78(2)	-4.00(1)	-1.22(2)	3678(3)	3692(3)	2355(2)
122	18	-3.78(2)	-3.95(1)	-1.11(1)	2471(3)	2832(3)	1802(2)
122	19	-3.68(3)	-3.90(1)	-1.05(1)	1153(4-II-1)	1696(4-II-3)	1144(4-II-2)
122	20	-3.41(3)	-3.69(1)	-1.15(4-II-1)	-1640(1)	-1156(4-I-3)	604(4-II-2)
122	21	-3.25(4-II-1)	-2.92(1)	-1.54(4-II-3)	-5806(2)	-3993(1)	-2322(4-I-3)
122	22	-3.48(3)	-3.98(1)	-1.31(1)	-1330(1)	-1332(4-I-2)	-949(4-I-2)
122	23	-3.75(3)	-4.13(1)	-1.30(1)	1140(4-II-2)	1356(4-II-2)	693(4-II-2)
122	24	-3.71(3)	-4.09(1)	-1.19(1)	1861(3)	1993(4-II-3)	1258(4-II-2)
122	25	-3.81(2)	-4.18(1)	-1.29(1)	3132(3)	2905(3)	1685(2)
122	26	-3.76(2)	-4.06(1)	-1.23(2)	3794(3)	3620(3)	2338(2)
122	27	-3.75(2)	-4.06(1)	-1.19(1)	2920(3)	2918(3)	1892(2)
122	28	-3.76(2)	-4.12(1)	-1.25(1)	3663(3)	3386(3)	2146(2)
122	29	-3.86(2)	-4.20(1)	-1.35(1)	4088(3)	3786(3)	2243(2)
122	30	-3.71(2)	-4.09(1)	-1.33(2)	4450(2)	4017(3)	2642(2)
122	31	-3.76(2)	-4.16(1)	-1.33(2)	4388(3)	3960(3)	2540(2)
122	32	-3.60(2)	-4.15(1)	-1.43(2)	4793(2)	4117(3)	2780(2)
122	33	-3.66(2)	-4.22(1)	-1.38(2)	4817(2)	4231(3)	2785(2)
122	34	-3.90(2)	-4.21(1)	-1.32(1)	4833(2)	4475(3)	2741(2)
122	35	-3.76(2)	-4.24(1)	-1.34(1)	4843(2)	4341(3)	2767(2)
122	36	-3.90(2)	-4.20(1)	-1.36(1)	4549(2)	4204(3)	2566(2)
122	37	-3.84(2)	-4.19(1)	-1.26(1)	4664(2)	4102(2)	2683(1)
122	38	-3.86(2)	-4.21(1)	-1.28(1)	4929(2)	4485(3)	2830(2)
122	39	-3.67(2)	-4.24(1)	-1.31(1)	4902(2)	4275(3)	2791(2)
122	40	-3.53(2)	-4.26(1)	-1.27(1)	4484(2)	3786(2)	2533(1)
122	41	-3.51(2)	-4.31(1)	-1.42(2)	4713(2)	3908(2)	2693(1)
122	42	-3.43(1)	-4.27(1)	-1.50(2)	4621(2)	3776(2)	2637(1)
123	1	-0.70(1)	-2.51(3)	0.66(4-I-1)	2334(1)	2193(3)	-838(2)
123	2	-1.54(1)	-2.35(3)	0.74(4-I-1)	1030(1)	2539(3)	-903(2)
123	3	-2.20(1)	-2.18(3)	0.90(3)	-1118(4-II-1)	3121(3)	-722(4-I-4)
123	4	-2.91(1)	-1.98(1)	1.20(3)	-1991(3)	4355(3)	944(4-II-2)
123	5	-1.32(1)	-2.62(3)	-0.46(1)	-2341(4-II-1)	1594(5-II-1)	-2052(3)
123	6	-1.72(1)	-2.20(3)	0.48(4-I-1)	-2363(4-II-1)	2604(5-II-1)	-2140(3)
123	7	-2.33(1)	-1.90(1)	0.51(4-I-1)	-2627(4-II-1)	3796(5-II-1)	-2154(3)
123	8	-2.75(1)	-1.58(1)	0.35(5-I-4)	-2906(4-II-2)	5700(3)	-2385(3)
123	9	-1.55(1)	-2.32(3)	-0.64(1)	-4835(4-II-1)	1209(5-II-1)	-2193(3)
123	10	-1.94(1)	-2.10(1)	-0.49(1)	-4551(4-II-1)	2504(5-II-1)	-2568(3)
123	11	-2.34(1)	-1.87(1)	-0.41(1)	-4257(4-II-2)	3926(5-II-1)	-2749(3)
123	12	-2.73(1)	-1.60(1)	-0.39(1)	-3940(4-II-2)	5179(5-II-1)	-2892(3)
123	13	-1.80(1)	-1.76(1)	-0.71(1)	-8104(4-II-1)	-1083(5-I-1)	-1459(4-I-1)
123	14	-1.99(1)	-2.09(1)	-0.63(1)	-7157(4-II-1)	2017(5-II-1)	-1865(4-I-1)
123	15	-2.36(1)	-2.05(1)	-0.63(1)	-6220(4-II-2)	3415(5-II-1)	-2247(4-I-1)
123	16	-2.70(1)	-1.94(1)	-0.67(1)	-4746(4-II-2)	5075(5-II-1)	-2880(4-I-1)
124	1	-3.78(1)	-2.46(3)	-0.78(4-II-4)	-4291(4-II-2)	1665(3)	-2099(3)
124	2	-3.82(1)	-2.39(3)	-0.56(4-II-4)	-4448(4-II-2)	2206(3)	-2180(3)
124	3	-3.77(1)	-2.34(3)	-0.44(4-II-4)	-4390(4-II-2)	3165(3)	-2110(3)
124	4	-3.65(1)	-2.33(3)	-0.31(4-II-1)	-4173(4-II-2)	4487(3)	-1637(3)
124	5	-4.48(1)	-2.55(3)	-0.84(4-II-3)	-8170(4-II-2)	1329(3)	-2726(3)
124	6	-4.05(1)	-2.47(3)	-0.70(4-II-4)	-7183(4-II-2)	1806(3)	-2780(3)
124	7	-3.80(1)	-2.30(3)	-0.71(4-II-4)	-6342(4-II-2)	2641(3)	-3024(3)
124	8	-3.69(1)	-1.98(1)	-0.94(3)	-5616(4-II-2)	3962(3)	-3459(3)
125	1	-8.76(3)	-4.07(1)	-1.24(2)	4535(3)	1822(1)	775(2)
125	2	-9.11(3)	-3.89(1)	-0.91(2)	4222(3)	1680(1)	594(2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
125	3	-9.23(3)	-3.86(1)	-0.42(1)	3965(3)	1686(1)	164(1)
125	4	-8.96(3)	-4.06(1)	-0.81(2)	3474(3)	1627(1)	507(2)
125	5	-8.57(3)	-4.33(1)	-1.06(2)	2913(3)	1809(1)	802(2)
125	6	-7.84(3)	-4.19(1)	-1.17(2)	2035(3)	1751(1)	796(2)
125	7	-6.42(3)	-3.30(1)	-1.03(4-I-3)	959(4-I-2)	1491(1)	851(3)
125	8	-3.25(4-I-3)	-3.14(5-I-4)	-1.31(4-I-1)	-975(4-II-3)	1054(5-I-4)	-439(4-II-1)
125	9	-5.28(3)	-4.47(1)	-2.04(2)	2519(3)	1166(1)	407(5-I-3)
125	10	-7.52(3)	-4.89(1)	-2.22(2)	3582(3)	1714(1)	528(2)
125	11	-8.39(3)	-5.11(1)	-2.16(2)	4146(3)	2080(1)	874(2)
125	12	-7.86(3)	-5.00(1)	-1.69(2)	4664(3)	2420(1)	1060(2)
125	13	-8.15(3)	-4.42(1)	-1.40(2)	4721(3)	2206(1)	929(2)
125	14	-8.24(3)	-4.36(1)	-1.22(2)	4350(3)	2077(1)	943(2)
125	15	-7.40(3)	-4.51(1)	-1.07(4-I-3)	4113(3)	2257(1)	849(2)
126	1	-5.03(1)	-4.23(3)	-1.04(5-II-4)	1746(1)	2361(3)	659(3)
126	2	-2.79(1)	-2.68(4-I-1)	0.80(4-II-3)	833(4-I-3)	813(4-I-2)	-598(4-II-3)
126	3	-4.36(1)	-5.30(3)	-1.27(3)	2016(1)	668(4-I-3)	196(5-II-4)
126	4	-4.80(1)	-6.44(3)	-1.07(5-II-4)	1963(1)	1121(4-I-2)	362(4-I-3)
126	5	-4.39(1)	-6.09(3)	-1.31(3)	1830(1)	1915(3)	726(3)
126	6	-4.81(1)	-6.29(3)	-1.13(3)	2623(1)	3200(3)	804(2)
126	7	-5.14(1)	-6.93(3)	-0.95(5-II-4)	2761(1)	3553(3)	927(2)
126	8	-5.58(1)	-7.79(3)	-1.78(3)	2528(1)	3928(2)	933(3)
126	9	-5.75(1)	-6.06(3)	-1.92(3)	2201(1)	3175(3)	667(3)
127	1	-8.08(3)	-3.63(1)	-1.04(5-I-4)	3228(3)	-175(5-II-1)	273(4-I-1)
127	2	-8.10(3)	-3.84(1)	-0.89(5-I-4)	3231(3)	-223(5-II-1)	314(4-I-1)
127	3	-8.05(2)	-3.97(1)	-0.75(5-I-4)	3243(2)	-240(5-II-4)	372(4-I-1)
127	4	-7.94(2)	-4.07(1)	-0.62(5-I-4)	3189(2)	-259(5-II-4)	442(4-I-1)
127	5	-7.79(2)	-4.11(1)	-0.48(5-I-4)	3094(2)	-342(4-I-3)	540(4-I-1)
127	6	-7.58(1)	-4.11(1)	-0.35(5-I-4)	2961(2)	-399(4-I-3)	652(4-I-1)
127	7	-7.29(1)	-4.08(1)	0.35(1)	2805(1)	-381(4-I-3)	690(4-I-1)
127	8	-7.08(1)	-3.99(1)	-0.36(4-I-1)	2644(1)	-223(4-I-3)	595(4-I-1)
127	9	-7.01(1)	-3.96(1)	-0.46(4-I-1)	2619(1)	629(1)	506(4-I-1)
127	10	-6.63(1)	-3.91(1)	-0.52(4-I-1)	2718(1)	860(1)	551(4-I-1)
127	11	-6.26(1)	-3.65(1)	-0.86(4-I-1)	2239(1)	1752(1)	512(4-I-2)
127	12	-7.26(1)	-4.09(1)	-0.92(4-I-1)	2894(1)	2623(1)	463(4-I-1)
127	13	-7.99(2)	-4.51(1)	-1.05(4-I-1)	3526(2)	2610(1)	539(3)
127	14	-8.88(3)	-4.58(1)	-1.35(5-I-3)	3811(2)	2356(1)	542(5-I-3)
127	15	-8.51(2)	-4.32(1)	-1.23(5-I-3)	3735(3)	2427(1)	412(5-I-4)
127	16	-8.28(3)	-3.60(1)	-1.20(5-I-3)	3339(3)	1933(1)	258(5-I-4)
127	17	-7.87(3)	-2.77(1)	-1.09(5-I-4)	2997(3)	1203(1)	268(5-I-4)
127	18	-8.00(3)	-3.37(1)	-1.11(5-I-4)	3112(3)	439(1)	273(5-I-4)
127	19	-8.05(3)	-3.50(1)	-1.13(5-I-4)	3196(3)	102(5-I-1)	245(5-I-4)
127	20	-7.97(2)	-3.97(1)	-0.89(5-I-4)	3367(3)	373(5-I-4)	306(5-I-4)
127	21	-7.89(2)	-4.06(1)	-0.87(5-I-4)	3465(2)	726(1)	322(5-I-4)
127	22	-8.04(2)	-4.26(1)	-1.12(5-I-3)	3726(3)	2092(1)	407(5-I-4)
127	23	-7.89(2)	-4.07(1)	-0.95(5-I-4)	3540(3)	1164(1)	326(5-I-4)
127	24	-7.98(2)	-3.96(1)	-1.01(5-I-4)	3557(3)	1431(1)	324(5-I-4)
127	25	-7.99(3)	-3.85(1)	-0.96(5-I-4)	3394(3)	550(1)	323(5-I-4)
127	26	-7.95(3)	-3.57(1)	-1.10(5-I-4)	3368(3)	742(1)	340(5-I-4)
127	27	-7.92(2)	-4.05(1)	-0.80(5-I-4)	3373(2)	362(5-I-4)	329(4-I-1)
127	28	-7.43(1)	-4.14(1)	-0.43(5-I-4)	3080(2)	212(4-II-3)	473(4-I-1)
127	29	-7.27(1)	-4.18(1)	-0.57(4-I-1)	3115(1)	753(1)	494(4-I-1)
127	30	-7.44(1)	-4.18(1)	-0.63(4-I-1)	3385(2)	1037(1)	381(4-I-1)
127	31	-7.80(2)	-4.27(1)	-0.93(5-I-4)	3635(2)	1779(1)	394(5-I-4)
127	32	-7.48(2)	-4.34(1)	-0.76(5-I-4)	3493(2)	1488(1)	353(5-I-4)
127	33	-7.69(2)	-4.42(1)	-0.97(4-I-1)	3598(2)	2087(1)	406(5-I-4)
127	34	-7.58(2)	-4.28(1)	-0.60(5-I-4)	3354(2)	685(1)	371(4-I-1)
127	35	-7.67(2)	-4.20(1)	-0.56(5-I-4)	3220(2)	246(5-I-4)	416(4-I-1)
127	36	-7.50(1)	-4.17(1)	-0.53(5-I-4)	3180(2)	359(5-I-4)	426(4-I-1)
127	37	-7.71(2)	-4.20(1)	-0.72(5-I-4)	3400(2)	770(1)	348(4-I-1)
127	38	-7.82(2)	-4.16(1)	-0.75(5-I-4)	3390(2)	535(1)	344(4-I-1)
127	39	-7.79(2)	-4.17(1)	-0.67(5-I-4)	3317(2)	339(5-I-4)	370(4-I-1)
127	40	-7.83(2)	-4.17(1)	-0.88(5-I-4)	3558(2)	1364(1)	369(5-I-4)
127	41	-7.80(2)	-4.16(1)	-0.82(5-I-4)	3479(2)	920(1)	350(5-I-4)
127	42	-7.69(2)	-4.26(1)	-0.79(5-I-4)	3471(2)	1119(1)	351(5-I-4)
128	1	-7.74(1)	-4.83(1)	1.76(4-I-2)	3450(1)	1393(1)	-660(4-I-2)
128	2	-8.35(1)	-4.25(1)	3.00(2)	3392(1)	1451(1)	-1128(2)
128	3	-7.08(1)	-5.24(1)	3.02(3)	2809(1)	2140(1)	-1070(2)
128	4	-6.54(1)	-6.60(1)	2.98(3)	2799(1)	3028(1)	-1119(2)
128	5	-5.89(1)	-7.71(1)	2.51(2)	2542(1)	3566(3)	-1123(3)
128	6	-6.44(1)	-6.66(1)	1.65(2)	2922(3)	3266(2)	-1037(3)
128	7	-6.50(1)	-5.85(1)	1.24(4-I-1)	2482(3)	2693(1)	-661(4-I-1)
128	8	-5.47(1)	-5.26(1)	1.00(4-I-1)	1866(3)	1869(1)	-498(4-I-1)
128	9	-6.91(1)	-5.31(1)	1.13(4-I-1)	2899(3)	1423(1)	-570(4-I-2)
128	10	-6.68(1)	-5.73(1)	1.58(4-I-1)	3249(3)	2365(1)	-662(4-I-1)
128	11	-7.03(1)	-5.57(1)	2.09(2)	3440(1)	2201(1)	-829(3)
128	12	-6.56(1)	-6.17(1)	2.10(2)	3250(1)	2725(1)	-972(3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
129	1	-2.88 (1)	-3.54 (1)	0.76 (1)	3048 (3)	-1850 (2)	2812 (3)
129	2	-2.80 (1)	-3.69 (1)	0.80 (1)	2814 (1)	-1584 (4-I-1)	2804 (3)
129	3	-2.29 (1)	-3.53 (1)	0.79 (1)	4089 (3)	-2132 (2)	3775 (3)
129	4	-2.01 (1)	-3.35 (1)	0.88 (1)	4780 (3)	-2392 (3)	3354 (3)
129	5	-1.98 (1)	-3.04 (1)	0.91 (1)	5318 (5-II-1)	-3173 (3)	2659 (3)
129	6	-2.13 (1)	-3.20 (1)	0.81 (1)	4428 (5-II-1)	-2415 (3)	3028 (3)
129	7	-2.43 (1)	-3.34 (1)	0.77 (1)	3790 (3)	-1977 (4-I-1)	3203 (3)
129	8	-2.83 (1)	-3.37 (1)	0.74 (1)	3029 (3)	-1898 (2)	2826 (3)
129	9	-2.88 (1)	-3.48 (1)	0.72 (1)	3118 (3)	-1956 (2)	2826 (3)
129	10	-2.61 (1)	-3.46 (1)	0.76 (1)	3684 (3)	-1991 (2)	3458 (3)
130	1	-3.42 (1)	-1.56 (1)	0.56 (3)	-3652 (3)	7500 (3)	2460 (3)
130	2	-3.37 (1)	-1.53 (1)	0.46 (3)	-3355 (5-I-4)	6482 (3)	2589 (3)
130	3	-3.59 (1)	-1.76 (1)	0.43 (4-I-1)	-3691 (3)	6418 (3)	1939 (3)
130	4	-3.74 (1)	-2.07 (1)	0.45 (3)	-4200 (3)	6376 (3)	1203 (1)
130	5	-4.09 (1)	-2.18 (1)	0.54 (3)	-3208 (3)	5185 (3)	-365 (3)
130	6	-3.47 (1)	-2.28 (1)	0.51 (3)	-4700 (3)	5936 (3)	451 (4-II-2)
130	7	-3.23 (1)	-2.36 (1)	0.44 (3)	-4884 (3)	6556 (2)	1034 (1)
130	8	-3.24 (1)	-2.18 (1)	0.52 (5-I-1)	-3831 (3)	10299 (2)	2463 (1)
130	9	-3.34 (1)	-1.53 (1)	0.53 (5-I-1)	-4162 (3)	8498 (3)	2551 (3)
130	10	-3.49 (1)	-1.80 (1)	0.49 (3)	-4114 (3)	7289 (3)	2036 (3)
130	11	-3.52 (1)	-2.11 (1)	0.50 (3)	-4661 (3)	7098 (3)	1363 (1)
130	12	-3.38 (1)	-2.03 (1)	0.47 (3)	-4654 (3)	7897 (3)	1857 (1)
131	1	-3.24 (1)	-1.03 (1)	0.22 (5-I-4)	-3849 (4-II-2)	7848 (3)	-3258 (3)
131	2	-3.19 (1)	-1.12 (1)	0.28 (4-II-3)	-3329 (4-II-2)	7697 (3)	-2638 (3)
131	3	-3.09 (1)	-1.05 (1)	0.75 (4-II-3)	-2297 (3)	8820 (3)	-1360 (4-I-2)
131	4	-3.14 (1)	-1.22 (1)	0.23 (5-I-4)	-3265 (4-II-2)	6717 (3)	-2731 (3)
131	5	-3.15 (1)	-1.35 (1)	-0.40 (1)	-3702 (4-II-2)	6593 (3)	-3148 (3)
131	6	-3.21 (1)	-1.36 (1)	-0.65 (1)	-3497 (4-II-2)	6456 (3)	-3369 (3)
131	7	-3.32 (1)	-1.26 (1)	-0.59 (1)	-3258 (4-II-2)	7215 (3)	-3711 (3)
131	8	-3.36 (1)	-1.21 (1)	-0.66 (1)	-3300 (4-II-2)	8095 (3)	-4215 (3)
131	9	-2.96 (1)	-1.64 (1)	-1.04 (1)	-2684 (4-II-2)	10752 (1)	-3824 (3)
131	10	-3.42 (1)	-0.75 (1)	-0.76 (1)	-3153 (4-II-2)	8651 (1)	-4075 (3)
131	11	-3.26 (1)	-1.02 (1)	-0.33 (1)	-3748 (4-II-2)	8155 (3)	-3880 (3)
131	12	-3.25 (1)	-1.17 (1)	-0.44 (1)	-3620 (4-II-2)	7579 (3)	-3525 (3)
132	1	-2.12 (1)	-1.90 (1)	1.33 (1)	-2046 (5-I-4)	5626 (3)	6103 (3)
132	2	-2.08 (1)	-1.97 (2)	1.42 (1)	-1875 (5-I-4)	6897 (3)	5685 (3)
132	3	-2.02 (1)	-0.82 (1)	1.34 (1)	2044 (1)	8171 (2)	4963 (1)
132	4	-1.85 (2)	-2.62 (2)	1.06 (1)	-4152 (4-II-3)	7671 (3)	4629 (3)
132	5	-2.11 (1)	-1.99 (1)	0.94 (1)	-2178 (5-I-4)	4840 (3)	6361 (3)
132	6	-2.35 (1)	-2.35 (1)	1.38 (3)	-1198 (5-I-1)	4779 (3)	6168 (3)
132	7	-1.52 (1)	-1.81 (1)	2.11 (3)	4600 (5-II-1)	5562 (3)	7355 (3)
132	8	-2.43 (1)	-1.77 (1)	1.10 (3)	1311 (5-II-1)	4616 (3)	5593 (3)
132	9	-2.24 (1)	-1.74 (1)	1.04 (1)	-1650 (5-I-1)	5570 (3)	5763 (3)
132	10	-2.26 (1)	-2.24 (1)	1.04 (1)	-1255 (5-I-1)	5120 (3)	5594 (3)
133	1	-1.78 (1)	-2.97 (1)	1.29 (3)	7042 (3)	-3417 (4-II-2)	3557 (3)
133	2	-0.93 (1)	-2.83 (1)	1.85 (3)	9988 (3)	-3238 (4-II-2)	5062 (3)
133	3	-1.46 (1)	-3.08 (1)	0.93 (3)	7329 (3)	-3746 (4-II-2)	3674 (3)
133	4	-1.69 (1)	-2.78 (1)	0.88 (3)	6744 (3)	-4150 (4-II-2)	3935 (3)
133	5	-2.01 (1)	-2.53 (1)	0.83 (3)	3886 (1)	-6008 (4-II-2)	6750 (3)
133	6	-1.99 (1)	-2.57 (1)	1.26 (3)	5453 (3)	-3362 (4-II-2)	3048 (3)
133	7	-1.90 (1)	-2.80 (1)	1.34 (3)	5228 (3)	-2892 (4-II-2)	2526 (3)
133	8	-1.71 (1)	-3.45 (1)	1.11 (3)	4584 (3)	1760 (4-I-2)	1897 (3)
133	9	-1.89 (1)	-3.10 (1)	1.25 (3)	6050 (3)	-3174 (4-II-2)	2359 (3)
134	1	-3.58 (1)	-2.12 (1)	-0.30 (4-II-1)	-3544 (4-II-2)	5455 (3)	-995 (4-I-1)
134	2	-3.60 (1)	-2.20 (1)	-0.31 (3)	-3922 (4-II-2)	4960 (3)	-1222 (4-I-1)
134	3	-3.32 (1)	-1.92 (1)	-0.79 (3)	-4400 (4-II-2)	8013 (3)	-3042 (3)
134	4	-3.50 (1)	-1.81 (1)	-0.70 (3)	-3663 (4-II-2)	6405 (3)	-1847 (4-I-1)
134	5	-3.48 (1)	-1.88 (1)	-0.44 (3)	-3318 (4-II-2)	6000 (3)	-1294 (4-I-1)
134	6	-3.75 (1)	-1.73 (1)	-0.35 (4-II-1)	-2412 (4-II-2)	5675 (3)	-1126 (4-I-1)
134	7	-3.67 (1)	-1.89 (1)	-0.33 (4-II-1)	-2935 (4-II-2)	5728 (3)	-764 (4-I-1)
135	1	-4.25 (3)	-0.45 (4-II-3)	-1.92 (3)	1176 (1)	7835 (1)	-3781 (3)
135	2	-1.59 (3)	-0.55 (4-II-3)	-2.13 (3)	2501 (1)	6352 (1)	-3474 (3)
135	3	-1.54 (4-II-4)	-0.19 (4-II-2)	-2.24 (3)	2475 (1)	4788 (1)	-3616 (3)
135	4	-2.35 (4-II-2)	-0.54 (1)	-1.45 (3)	1921 (1)	4219 (1)	-4018 (3)
135	5	-1.37 (4-II-1)	-0.36 (4-II-2)	-1.50 (3)	1500 (1)	8999 (1)	-2527 (3)
135	6	-1.34 (3)	-0.49 (4-II-2)	-2.08 (3)	2279 (1)	6251 (1)	-3688 (3)
135	7	-1.96 (3)	-0.99 (4-II-3)	-1.96 (3)	2357 (4-I-2)	4000 (1)	-4335 (3)
135	8	-3.91 (3)	-1.43 (4-II-3)	-2.48 (3)	1702 (4-I-3)	-1915 (5-I-1)	-4121 (3)
136	1	-3.57 (1)	-6.08 (2)	1.73 (4-II-3)	-475 (5-II-2)	1203 (4-I-3)	754 (1)
136	2	-3.78 (1)	-6.47 (2)	1.73 (4-II-3)	498 (1)	1555 (4-I-3)	740 (1)
136	3	-4.29 (1)	-6.51 (2)	1.39 (4-II-3)	1131 (1)	1667 (4-I-3)	794 (1)
136	4	-4.96 (1)	-6.23 (2)	0.86 (4-II-3)	1715 (1)	1921 (2)	852 (1)
136	5	-5.55 (1)	-5.94 (1)	-1.29 (1)	2076 (1)	2108 (2)	900 (1)
136	6	-6.19 (1)	-5.37 (1)	-1.92 (1)	2536 (1)	2406 (1)	904 (1)
136	7	-5.94 (1)	-5.32 (2)	-0.92 (1)	2542 (1)	3230 (1)	459 (1)
136	8	-5.86 (1)	-5.25 (2)	1.07 (4-II-3)	2566 (1)	3634 (1)	-510 (4-II-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
136	9	-5.85 (1)	-5.28 (2)	1.52 (4-II-3)	2674 (1)	3900 (1)	-842 (4-II-3)
136	10	-5.54 (1)	-5.64 (2)	1.80 (3)	2551 (1)	3695 (1)	-1001 (4-II-3)
136	11	-4.96 (1)	-6.49 (2)	1.94 (3)	2240 (1)	3463 (1)	-1113 (3)
136	12	-4.14 (1)	-7.30 (2)	1.94 (3)	2002 (1)	3288 (1)	-1063 (3)
136	13	-3.39 (1)	-8.37 (1)	2.00 (1)	1311 (1)	3422 (1)	-936 (1)
136	14	-3.97 (1)	-7.82 (1)	1.46 (3)	1993 (1)	3505 (2)	-809 (3)
136	15	-3.84 (1)	-6.85 (1)	1.09 (4-II-3)	2401 (1)	2859 (2)	-807 (3)
136	16	-3.56 (1)	-5.43 (2)	0.79 (5-I-1)	1785 (1)	1572 (2)	-220 (5-I-2)
136	17	-3.77 (1)	-5.71 (2)	1.46 (4-II-3)	525 (1)	1088 (4-I-2)	343 (1)
136	18	-4.81 (1)	-6.16 (2)	1.50 (4-II-3)	2241 (1)	3328 (1)	-1173 (3)
136	19	-4.42 (1)	-6.24 (2)	1.38 (4-II-3)	1985 (1)	2911 (2)	-1065 (3)
136	20	-4.67 (1)	-5.99 (2)	1.47 (4-II-3)	1811 (1)	2909 (2)	-961 (4-II-3)
136	21	-3.94 (1)	-6.10 (2)	1.43 (4-II-3)	951 (1)	2053 (2)	-604 (4-II-3)
136	22	-4.41 (1)	-6.09 (2)	1.48 (4-II-3)	1175 (1)	2317 (2)	-657 (4-II-3)
136	23	-5.30 (1)	-5.73 (2)	1.54 (4-II-3)	2368 (1)	3482 (1)	-1054 (4-II-3)
136	24	-5.04 (1)	-5.81 (2)	1.47 (4-II-3)	1980 (1)	3098 (2)	-908 (4-II-3)
136	25	-5.44 (1)	-5.63 (2)	1.43 (4-II-3)	2328 (1)	3450 (1)	-872 (4-II-3)
136	26	-4.79 (1)	-6.01 (2)	1.39 (4-II-3)	1519 (1)	2606 (2)	-567 (4-II-3)
136	27	-5.38 (1)	-5.72 (2)	1.17 (4-II-3)	2075 (1)	3017 (1)	-489 (4-II-3)
137	1	-4.32 (3)	-5.32 (1)	-2.23 (3)	1799 (3)	1160 (1)	233 (4-I-1)
137	2	-4.76 (3)	-5.66 (1)	-1.83 (3)	2415 (3)	2151 (2)	312 (4-I-1)
137	3	-5.01 (3)	-5.75 (1)	-1.37 (1)	2598 (3)	3067 (2)	499 (4-I-1)
137	4	-4.69 (3)	-5.77 (1)	-1.11 (1)	3227 (3)	3768 (2)	910 (3)
137	5	-4.15 (3)	-6.02 (1)	-0.98 (1)	3602 (3)	4213 (2)	1469 (3)
137	6	-3.76 (1)	-6.12 (1)	-0.93 (3)	3834 (3)	4438 (1)	1734 (3)
137	7	-3.40 (1)	-6.09 (1)	-0.94 (3)	3937 (3)	4322 (1)	1844 (3)
137	8	-2.97 (1)	-5.89 (1)	-0.97 (3)	3882 (3)	3909 (1)	1803 (3)
137	9	-2.61 (1)	-5.64 (1)	-1.11 (3)	3696 (3)	2967 (1)	1699 (1)
137	10	-2.94 (1)	-6.15 (1)	-1.01 (3)	3789 (3)	3628 (1)	1840 (3)
137	11	-3.27 (1)	-6.45 (1)	-1.12 (3)	3717 (3)	4019 (1)	1906 (3)
137	12	-3.63 (1)	-6.65 (1)	-1.39 (3)	3391 (3)	4006 (1)	1901 (3)
137	13	-3.97 (3)	-6.52 (1)	-1.72 (3)	2959 (3)	3658 (1)	1821 (3)
137	14	-4.24 (3)	-6.03 (1)	-1.96 (3)	2529 (3)	3102 (1)	1642 (3)
137	15	-4.33 (3)	-5.20 (1)	-2.01 (3)	2037 (3)	2158 (1)	1333 (3)
137	16	-3.97 (3)	-4.05 (1)	-1.80 (3)	1470 (3)	1114 (1)	903 (3)
137	17	-2.95 (4-I-3)	-2.62 (1)	-1.50 (4-I-1)	703 (4-I-3)	-337 (4-II-3)	511 (4-I-1)
137	18	2.95 (5-I-4)	-1.32 (1)	-1.46 (4-I-1)	-1710 (5-I-4)	-1341 (3)	-1427 (4-II-1)
137	19	-2.55 (4-I-3)	-3.18 (1)	-1.78 (3)	1052 (4-I-3)	-1151 (3)	-1094 (1)
137	20	-3.49 (3)	-4.57 (1)	-2.33 (3)	1731 (3)	515 (4-I-3)	-365 (4-II-1)
137	21	-4.16 (3)	-6.00 (1)	-1.72 (3)	2720 (3)	3054 (2)	1374 (3)
137	22	-4.16 (3)	-5.62 (1)	-1.90 (3)	2331 (3)	2221 (2)	1026 (3)
137	23	-4.33 (3)	-5.90 (1)	-1.66 (3)	2708 (3)	2775 (2)	1045 (3)
137	24	-3.82 (1)	-6.31 (1)	-1.17 (3)	3509 (3)	4150 (1)	1699 (3)
137	25	-4.01 (3)	-6.29 (1)	-1.47 (3)	3090 (3)	3657 (1)	1545 (3)
137	26	-4.11 (3)	-6.11 (1)	-1.15 (3)	3409 (3)	3953 (2)	1426 (3)
137	27	-4.24 (3)	-6.06 (1)	-1.40 (3)	3062 (3)	3474 (2)	1239 (3)
137	28	-4.49 (3)	-5.93 (1)	-1.25 (3)	3200 (3)	3465 (2)	1047 (3)
138	1	-5.66 (1)	-4.07 (1)	-1.00 (1)	5963 (3)	2565 (1)	468 (1)
138	2	-5.99 (1)	-4.25 (1)	-0.80 (1)	5465 (3)	2558 (1)	437 (1)
138	3	-6.18 (1)	-4.31 (1)	-0.61 (1)	4237 (3)	2472 (2)	501 (1)
138	4	-5.92 (1)	-4.05 (1)	-0.74 (1)	5454 (3)	2589 (1)	472 (1)
138	5	-5.60 (1)	-4.05 (1)	-0.88 (1)	6023 (3)	2663 (1)	456 (1)
138	6	-5.27 (1)	-3.87 (1)	-0.98 (1)	6039 (3)	2624 (1)	383 (1)
138	7	-4.92 (1)	-3.49 (1)	-1.10 (1)	5718 (1)	2660 (1)	328 (1)
138	8	-4.64 (1)	-3.05 (1)	-1.26 (1)	5695 (1)	1984 (1)	443 (1)
138	9	-4.82 (1)	-2.75 (1)	-1.29 (1)	5479 (1)	1715 (1)	-492 (5-I-4)
138	10	-4.94 (1)	-2.75 (1)	-1.30 (1)	5117 (1)	1513 (1)	-691 (3)
138	11	-5.01 (1)	-2.82 (1)	-1.40 (1)	4922 (1)	1446 (1)	-732 (3)
138	12	-5.18 (1)	-3.37 (1)	-1.30 (1)	5582 (1)	2155 (1)	-272 (5-I-4)
138	13	-5.38 (1)	-3.82 (1)	-1.15 (1)	5953 (3)	2477 (1)	362 (1)
138	14	-4.98 (1)	-3.15 (1)	-1.27 (1)	5573 (1)	2188 (1)	-274 (5-I-4)
139	1	-5.31 (1)	-4.05 (2)	1.11 (3)	2417 (2)	1251 (3)	-304 (5-II-3)
139	2	-5.51 (1)	-4.64 (2)	1.00 (3)	3288 (2)	2019 (3)	-546 (3)
139	3	-5.50 (1)	-4.86 (2)	0.90 (3)	4032 (2)	2521 (3)	-771 (3)
139	4	-5.49 (1)	-4.79 (2)	0.74 (3)	4830 (2)	2925 (3)	-1023 (3)
139	5	-5.49 (1)	-4.48 (1)	0.60 (3)	5419 (2)	3152 (3)	-1240 (3)
139	6	-5.49 (1)	-4.09 (1)	0.49 (3)	5657 (2)	3288 (3)	-1402 (3)
139	7	-5.42 (1)	-3.69 (1)	0.42 (3)	5555 (1)	3343 (3)	-1465 (3)
139	8	-5.26 (1)	-3.25 (1)	0.37 (3)	5337 (1)	3256 (3)	-1373 (3)
139	9	-5.24 (1)	-2.69 (1)	0.35 (3)	5630 (1)	3081 (3)	-1195 (3)
139	10	-5.43 (1)	-3.15 (1)	0.32 (3)	5332 (1)	3280 (3)	-1433 (3)
139	11	-5.61 (1)	-3.56 (1)	0.32 (3)	5550 (1)	3348 (3)	-1435 (3)
139	12	-5.81 (1)	-3.87 (1)	0.38 (3)	5506 (2)	3244 (3)	-1340 (3)
139	13	-5.98 (1)	-4.17 (1)	0.46 (3)	5085 (2)	3028 (3)	-1084 (3)
139	14	-6.07 (1)	-4.63 (1)	0.56 (3)	4209 (2)	2576 (3)	-680 (3)
139	15	-6.28 (1)	-4.83 (2)	0.40 (3)	3053 (2)	2161 (3)	-338 (4-I-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
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R.37.12

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
139	16	-6.36(1)	-4.58(2)	0.69(3)	2343(2)	1791(3)	597(1)
139	17	-6.02(1)	-4.07(2)	1.14(3)	1648(2)	1323(3)	839(1)
139	18	-5.28(1)	-3.22(2)	1.40(3)	1005(4-I-2)	918(3)	1247(1)
139	19	-3.72(1)	-2.15(2)	1.36(5-II-3)	-954(4-II-1)	428(5-I-4)	1893(1)
139	20	2.91(4-II-1)	-1.73(5-I-4)	2.08(5-II-4)	-2808(4-II-1)	-423(5-II-4)	1732(1)
139	21	-3.31(4-I-1)	-2.34(2)	0.97(5-II-3)	661(4-I-1)	-431(5-II-4)	739(1)
139	22	-4.73(1)	-3.32(2)	0.93(3)	1533(2)	640(4-I-1)	387(1)
139	23	-5.62(1)	-4.45(1)	0.58(3)	5214(2)	3101(3)	-1152(3)
139	24	-5.66(1)	-4.15(1)	0.48(3)	5519(2)	3241(3)	-1292(3)
139	25	-5.79(1)	-4.38(1)	0.54(3)	5098(2)	3041(3)	-1082(3)
139	26	-5.57(1)	-4.50(2)	1.07(3)	2801(2)	1572(3)	140(1)
139	27	-5.82(1)	-4.65(2)	0.62(3)	4469(2)	2750(3)	-796(3)
139	28	-5.61(1)	-4.72(2)	0.69(3)	4692(2)	2856(3)	-913(3)
139	29	-5.84(1)	-4.72(2)	0.82(3)	3304(2)	1979(3)	-244(4-I-1)
139	30	-5.62(1)	-4.80(2)	0.80(3)	4003(2)	2473(3)	-630(3)
139	31	-5.90(1)	-4.75(2)	0.69(3)	3855(2)	2390(3)	-438(3)
140	1	-4.89(1)	-2.31(2)	0.90(1)	2221(2)	3059(2)	293(5-I-4)
140	2	-4.90(1)	-3.24(2)	0.96(1)	2631(1)	3324(2)	273(5-I-4)
140	3	-5.07(1)	-4.33(2)	0.56(1)	2378(1)	3240(2)	149(5-I-4)
140	4	-4.76(1)	-3.42(2)	-0.34(5-II-2)	2295(1)	3288(2)	-308(1)
140	5	-4.54(1)	-2.53(2)	-0.49(4-I-1)	1741(1)	3007(2)	-365(1)
140	6	-4.04(1)	-1.66(4-I-3)	-0.59(4-I-1)	1146(5-II-4)	1934(2)	-303(1)
140	7	-3.14(1)	-1.00(4-I-2)	-0.54(4-I-2)	985(5-II-4)	1103(4-I-1)	326(4-I-1)
140	8	-3.81(5-II-4)	2.04(4-II-1)	1.51(4-II-3)	-1941(5-I-4)	-1039(4-II-1)	-899(4-II-3)
140	9	-3.20(5-II-4)	-1.37(4-I-1)	-1.05(4-I-1)	1342(5-II-4)	-1642(3)	-721(1)
140	10	-3.70(1)	-1.90(2)	-1.07(4-I-1)	1329(1)	-1598(3)	-453(1)
140	11	-4.25(1)	-2.51(2)	-0.87(5-I-4)	1604(1)	-1786(3)	-387(1)
140	12	-4.55(1)	-2.70(2)	-0.63(5-I-4)	1764(2)	-1838(1)	-290(1)
140	13	-4.68(1)	-2.62(2)	0.62(5-II-4)	1838(2)	-1801(1)	-197(1)
140	14	-4.61(1)	-2.31(2)	0.91(1)	1818(2)	-1677(1)	144(4-II-3)
140	15	-4.21(1)	-1.67(2)	1.08(1)	1637(1)	-1417(3)	299(4-II-3)
140	16	-3.27(1)	-1.15(4-I-3)	0.91(4-I-3)	1437(1)	-1428(2)	544(3)
140	17	-3.87(5-I-4)	2.00(4-II-3)	-1.49(4-II-1)	-1466(5-II-4)	-942(4-II-3)	825(4-II-1)
140	18	-3.75(1)	-0.87(4-I-2)	0.48(4-I-3)	1171(5-I-4)	1119(4-I-3)	-284(1)
140	19	-4.55(1)	-1.48(4-I-1)	0.72(1)	1543(1)	2036(2)	242(4-II-3)
140	20	-4.40(1)	-2.56(2)	0.78(1)	2230(2)	-165(4-II-1)	173(4-II-3)
140	21	-4.26(1)	-2.03(2)	0.75(1)	2186(2)	503(4-I-1)	236(4-II-3)
140	22	-4.49(1)	-2.62(2)	0.78(1)	2474(2)	1469(2)	215(4-II-3)
140	23	-4.14(1)	-2.81(2)	-0.44(4-I-1)	2153(1)	1315(2)	-275(1)
140	24	-3.76(1)	-2.25(2)	-0.60(4-I-1)	1852(1)	402(4-I-3)	-215(1)
140	25	-4.07(1)	-2.75(2)	-0.54(4-I-1)	1962(1)	-238(4-II-3)	-189(1)
140	26	-4.50(1)	-3.14(2)	0.71(1)	2538(2)	1874(2)	142(5-I-4)
140	27	-4.36(1)	-3.25(2)	0.28(1)	2385(1)	1817(2)	-211(1)
140	28	-4.37(1)	-2.90(2)	0.55(1)	2221(2)	241(4-I-1)	-139(1)
140	29	-4.25(1)	-2.98(2)	-0.33(5-I-4)	2119(2)	213(4-I-4)	-171(1)
141	1	-9.27(1)	-0.76(1)	1.77(4-II-4)	-1972(4-II-3)	654(1)	579(4-I-3)
141	2	-8.99(1)	0.69(4-II-3)	1.49(4-II-4)	-4199(4-II-3)	-1112(4-II-3)	-1211(4-II-3)
141	3	-9.79(1)	-1.10(1)	1.52(4-II-4)	-5061(4-II-3)	-1135(4-II-3)	-1995(4-II-3)
141	4	-9.48(1)	-1.64(1)	1.58(4-II-2)	-3952(4-II-3)	922(4-I-3)	-1889(4-II-3)
141	5	-9.12(1)	-2.09(1)	1.82(4-II-1)	-2256(4-II-3)	928(4-I-3)	-1695(4-II-2)
141	6	-10.06(1)	-1.57(1)	1.36(4-II-2)	3124(1)	1360(1)	-784(4-II-4)
141	7	-9.83(1)	-0.97(1)	1.94(4-II-4)	2021(1)	1110(1)	-572(4-II-2)
141	8	-9.78(1)	-0.83(1)	1.15(4-II-4)	-2740(4-II-3)	-864(4-II-3)	-1518(4-II-2)
142	1	-7.03(1)	-3.74(1)	-1.54(1)	6244(1)	1234(4-I-3)	-331(4-I-3)
142	2	-6.35(1)	-3.77(1)	-2.87(1)	6504(1)	1816(1)	403(4-II-3)
142	3	-7.67(1)	-3.83(1)	-2.86(1)	3839(1)	1593(1)	-248(5-II-3)
142	4	-8.48(1)	-2.61(1)	-1.12(1)	5326(1)	-1229(4-II-3)	-858(4-II-2)
142	5	-7.33(1)	-3.91(1)	-1.71(1)	6907(1)	1210(4-I-3)	423(1)
142	6	-7.43(1)	-3.54(1)	-1.78(1)	6306(1)	1621(1)	513(1)
142	7	-7.05(1)	-3.41(1)	-1.47(1)	5796(1)	1205(4-I-3)	-452(3)
142	8	-6.74(1)	-3.48(1)	-1.35(1)	6537(1)	-1263(4-II-3)	-377(4-I-3)
143	1	0.67(5-II-3)	-9.56(1)	-1.21(4-II-4)	3605(1)	2834(1)	361(1)
143	2	-0.75(1)	-11.18(1)	-2.32(4-II-4)	3534(1)	3339(1)	517(4-II-1)
143	3	-0.70(1)	-9.03(1)	-0.71(3)	3735(1)	4746(1)	2268(3)
143	4	1.08(5-II-3)	-9.23(1)	-1.00(4-II-4)	3650(1)	3868(1)	820(1)
143	5	0.74(5-II-3)	-10.26(1)	-1.12(4-II-4)	4258(1)	2458(1)	-1216(3)
143	6	1.13(5-II-3)	-10.09(1)	-1.61(4-II-4)	3808(1)	2251(1)	482(1)
143	7	0.92(5-II-3)	-9.92(1)	-1.44(4-II-4)	3781(1)	3588(1)	189(1)
143	8	0.94(5-II-3)	-8.63(1)	-1.32(4-II-4)	4132(1)	1834(1)	-735(3)
144	1	-5.56(1)	-8.15(1)	-1.98(4-II-1)	2393(1)	3290(1)	961(4-II-1)
144	2	-5.78(1)	-7.82(1)	-1.28(4-II-1)	2382(2)	3254(1)	615(4-II-1)
144	3	-5.35(1)	-7.81(1)	-0.72(4-II-1)	2084(2)	3283(1)	420(4-II-1)
144	4	-4.40(2)	-8.06(1)	0.70(4-I-1)	1722(2)	3253(1)	-321(4-I-1)
144	5	-5.02(1)	-8.19(1)	-0.85(4-II-1)	2157(2)	3322(1)	289(4-II-1)
144	6	-5.31(1)	-8.36(1)	-1.28(4-II-1)	2332(1)	3479(1)	607(4-II-1)
144	7	-5.00(1)	-8.89(1)	-1.63(4-II-1)	2232(1)	3985(1)	937(4-II-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
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144	8	-3.91(1)	-9.39(1)	-1.90(4-II-1)	1642(1)	4428(1)	915(4-II-1)
144	9	-2.90(1)	-10.12(1)	-1.53(4-II-1)	1218(1)	4600(1)	478(4-II-1)
144	10	-3.61(1)	-9.95(1)	-2.33(4-II-1)	1380(1)	3876(1)	769(4-II-1)
144	11	-4.03(1)	-9.52(1)	-2.98(4-II-4)	1498(1)	3986(1)	903(1)
144	12	-4.92(1)	-9.80(1)	-3.57(1)	2019(1)	3597(1)	1520(1)
144	13	-5.59(1)	-8.57(1)	-2.62(1)	2368(1)	3353(1)	1294(4-II-4)
145	1	0.58(5-II-3)	-7.39(1)	-1.33(3)	4401(1)	4107(1)	1621(1)
145	2	0.29(5-II-3)	-7.88(1)	-2.28(3)	4633(1)	3531(1)	1617(1)
145	3	-0.96(1)	-7.92(1)	-1.78(3)	3839(1)	4574(1)	1873(3)
145	4	1.02(5-II-3)	-7.45(1)	-1.33(5-II-3)	4459(1)	5150(1)	1135(2)
145	5	0.60(5-II-3)	-8.02(1)	-1.37(3)	4964(1)	3742(1)	383(1)
145	6	0.88(5-II-3)	-7.51(1)	-2.00(3)	4310(1)	3141(1)	1721(1)
145	7	0.84(5-II-3)	-7.80(1)	-1.65(3)	4667(1)	4997(1)	1252(1)
145	8	0.90(5-II-3)	-6.83(1)	-1.32(5-II-3)	5148(1)	3453(1)	688(1)
146	1	-5.27(1)	-4.70(1)	-4.46(1)	6261(1)	1937(1)	455(4-II-3)
146	2	-5.00(1)	-4.86(1)	-4.55(1)	5660(1)	2123(1)	979(4-II-3)
146	3	-4.23(1)	-4.67(1)	-4.21(1)	5843(1)	2841(1)	875(4-II-3)
147	1	-3.59(1)	-4.11(1)	1.66(3)	4191(1)	2066(1)	329(4-I-1)
147	2	-2.94(1)	-4.06(1)	1.48(4-II-1)	3517(1)	1932(2)	279(4-I-4)
147	3	-2.30(1)	-3.83(1)	1.31(4-II-1)	2282(1)	1533(2)	219(4-I-4)
147	4	-1.72(1)	-3.43(1)	1.22(4-II-1)	1374(1)	1382(5-I-2)	-435(4-II-4)
147	5	-1.28(4-II-3)	-3.08(5-I-2)	1.47(4-II-4)	304(4-II-3)	1035(5-I-2)	-456(4-II-4)
147	6	-1.98(1)	-3.52(1)	1.42(4-II-3)	-713(1)	1422(5-I-2)	256(4-I-1)
147	7	-2.59(1)	-3.95(1)	1.11(4-II-4)	-1183(1)	1587(1)	-191(4-II-1)
147	8	-3.05(1)	-3.73(1)	0.61(4-II-1)	-1767(1)	1458(1)	-243(5-I-2)
147	9	-2.86(1)	-3.05(1)	0.31(5-I-2)	-2373(2)	1080(1)	-310(4-I-3)
147	10	2.72(4-I-3)	-2.67(1)	-1.15(5-II-2)	-2612(4-I-3)	449(1)	-1181(5-I-2)
147	11	-3.28(4-II-3)	-3.05(1)	-1.20(1)	1066(4-II-3)	-440(5-II-3)	-730(5-I-2)
147	12	-4.67(1)	-2.96(1)	-1.33(1)	1839(4-II-3)	766(1)	-1002(3)
147	13	-6.21(1)	-2.87(1)	-0.92(1)	3099(1)	1152(1)	-1103(3)
147	14	-7.47(1)	-2.78(1)	0.77(4-II-1)	3842(1)	1307(1)	-867(3)
147	15	-8.38(1)	-2.80(1)	1.49(3)	4228(1)	1251(1)	-718(3)
147	16	-6.39(1)	-3.66(1)	1.64(3)	4661(1)	1740(1)	-530(4-II-1)
147	17	-4.72(1)	-4.06(1)	1.71(3)	4590(1)	2016(1)	-301(4-II-1)
147	18	-3.38(1)	-3.45(1)	1.03(4-II-1)	714(4-II-3)	1901(1)	152(1)
147	19	-3.38(1)	-3.54(1)	1.22(4-II-1)	2018(2)	2166(1)	260(1)
147	20	-2.92(1)	-3.61(1)	1.18(4-II-1)	836(4-II-3)	1999(1)	228(1)
147	21	-3.79(1)	-3.64(1)	1.32(3)	2889(2)	2156(1)	253(1)
147	22	-3.22(1)	-3.13(1)	0.81(5-I-2)	996(4-II-3)	1413(1)	247(1)
147	23	-4.32(1)	-3.46(1)	0.85(4-II-1)	2880(2)	1661(1)	-319(4-II-1)
147	24	-4.15(1)	-3.18(1)	0.85(5-I-2)	2231(2)	1560(1)	-279(4-II-1)
147	25	-3.80(1)	-3.42(1)	0.93(4-II-1)	2556(2)	1821(1)	-208(4-II-1)
147	26	-3.99(1)	-3.31(1)	0.54(4-II-1)	2743(2)	1258(1)	-401(4-II-1)
147	27	-4.67(1)	-3.44(1)	0.99(4-II-1)	3359(1)	1795(1)	-358(4-II-1)
147	28	-4.87(1)	-3.62(1)	1.23(4-II-1)	3825(1)	2104(1)	-364(4-II-1)
147	29	-4.26(1)	-3.65(1)	1.22(4-II-1)	3337(1)	2098(1)	-310(4-II-1)
147	30	-5.28(1)	-3.20(1)	0.65(4-II-1)	3486(1)	1397(1)	-455(4-II-1)
147	31	-5.95(1)	-3.39(1)	1.04(4-II-1)	4076(1)	1686(1)	-502(4-II-1)
148	1	-8.28(1)	-5.62(1)	2.17(4-II-1)	3469(1)	2437(1)	-833(4-II-1)
148	2	-8.04(1)	-5.79(1)	1.62(4-II-1)	3242(1)	2520(1)	-661(4-II-1)
148	3	-8.22(1)	-5.17(2)	1.15(4-II-1)	3219(1)	2239(1)	-510(1)
148	4	-8.13(1)	-4.18(3)	0.79(4-II-1)	3441(1)	1694(3)	-352(4-II-1)
148	5	-7.83(1)	-4.92(1)	1.03(4-II-1)	3427(1)	1942(2)	-419(4-II-1)
148	6	-7.95(1)	-5.59(1)	1.44(4-II-1)	3388(1)	2235(2)	-612(4-II-1)
148	7	-8.26(1)	-5.49(1)	1.83(4-II-1)	3431(1)	2310(2)	-825(4-II-1)
148	8	-8.65(1)	-5.07(1)	2.17(4-II-1)	3577(1)	2266(2)	-1064(4-II-1)
148	9	-9.39(1)	-4.28(1)	2.20(4-II-1)	3766(1)	2034(2)	-1198(4-II-1)
148	10	-9.47(1)	-3.77(1)	2.15(4-II-1)	4109(1)	1661(1)	-1292(3)
148	11	-9.84(1)	-2.80(1)	2.13(3)	4092(1)	1178(1)	-975(3)
148	12	-9.62(1)	-3.65(1)	2.77(3)	3996(1)	1411(1)	-1097(3)
148	13	-8.87(1)	-4.87(1)	2.62(3)	3677(1)	2042(1)	-1065(4-II-1)
148	14	-8.99(1)	-4.28(1)	2.21(4-II-1)	3865(1)	1933(1)	-1143(4-II-1)
149	1	-3.73(1)	-8.48(1)	1.20(1)	1122(2)	2645(2)	-1436(1)
149	2	-3.26(1)	-8.34(1)	0.93(1)	1076(2)	2362(3)	-1438(1)
149	3	-2.76(1)	-7.95(1)	0.81(4-II-3)	989(2)	2007(3)	-1350(1)
149	4	-2.30(1)	-7.30(1)	0.68(4-II-3)	834(2)	1663(4-II-1)	-1155(1)
149	5	-1.77(1)	-6.34(2)	0.56(4-II-3)	521(1)	1428(4-II-1)	-801(1)
149	6	-1.26(1)	-5.02(2)	-0.88(5-I-2)	286(1)	1265(4-II-1)	-669(1)
149	7	-0.91(5-I-2)	-3.45(4-II-1)	-0.95(5-I-2)	-266(4-II-3)	824(4-II-1)	489(5-I-2)
149	8	-1.88(1)	-4.63(2)	0.98(5-II-2)	508(1)	1395(4-II-1)	610(5-I-2)
149	9	-2.68(1)	-5.87(2)	1.36(1)	852(1)	1634(3)	457(5-I-2)
149	10	-3.39(1)	-6.63(1)	1.73(1)	1001(1)	1857(3)	472(4-I-3)
149	11	-3.82(1)	-7.18(1)	1.90(1)	1251(1)	2704(3)	432(4-I-3)
149	12	-4.10(1)	-7.74(1)	1.98(1)	1388(1)	3255(1)	-305(4-II-3)
149	13	-4.07(1)	-8.26(1)	2.20(1)	1247(1)	3470(1)	-549(4-II-3)
149	14	-3.57(1)	-8.63(1)	2.50(1)	1321(1)	3808(1)	-967(1)

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
149	15	-3.71(1)	-8.50(1)	1.92(1)	1638(1)	4534(1)	-813(1)
149	16	-4.09(1)	-8.28(1)	1.35(1)	1931(1)	4755(1)	-616(1)
149	17	-4.39(1)	-8.04(1)	0.97(1)	2206(1)	4844(1)	-424(1)
149	18	-4.63(1)	-7.84(1)	0.93(1)	2275(1)	4718(1)	-272(1)
149	19	-4.72(1)	-7.70(1)	1.10(1)	2208(1)	4426(1)	-252(1)
149	20	-4.68(1)	-7.64(1)	1.48(1)	1982(1)	3931(1)	-434(1)
149	21	-4.59(1)	-7.53(1)	1.94(1)	1699(2)	3238(1)	-862(1)
149	22	-4.46(1)	-8.04(1)	1.72(1)	1335(2)	3067(1)	-1210(1)
149	23	-4.11(1)	-8.39(1)	1.47(1)	1171(2)	2850(1)	-1356(1)
149	24	-4.14(1)	-7.84(1)	1.40(1)	2149(1)	4302(1)	-542(1)
149	25	-4.31(1)	-7.83(1)	1.14(1)	2324(1)	4522(1)	-471(1)
149	26	-4.13(1)	-7.72(1)	1.25(1)	2257(1)	4134(1)	-491(1)
149	27	-4.38(1)	-7.84(1)	1.02(1)	2267(1)	4346(1)	-489(1)
149	28	-4.12(1)	-7.77(1)	1.08(1)	2148(1)	3942(1)	-611(1)
149	29	-3.97(1)	-8.01(1)	1.05(1)	1711(1)	3494(1)	-906(1)
149	30	-4.48(1)	-7.92(1)	1.34(1)	1768(1)	3753(1)	-801(1)
149	31	-4.24(1)	-8.06(1)	1.20(1)	1713(1)	3656(1)	-903(1)
149	32	-4.45(1)	-7.85(1)	1.09(1)	2076(1)	4134(1)	-596(1)
149	33	-3.67(1)	-6.87(1)	1.51(1)	1435(1)	2848(3)	-281(4-II-3)
149	34	-4.05(1)	-7.50(1)	1.29(1)	2135(1)	3780(1)	-478(1)
149	35	-3.92(1)	-7.21(1)	1.40(1)	1834(1)	3328(3)	-393(1)
149	36	-4.09(1)	-7.54(1)	1.57(1)	1902(1)	3771(1)	-418(1)
149	37	-3.63(1)	-7.81(1)	0.93(1)	1558(1)	3160(2)	-912(1)
149	38	-3.91(1)	-7.53(1)	1.08(1)	2001(1)	3530(2)	-623(1)
149	39	-2.91(1)	-6.89(1)	0.77(4-II-3)	1131(1)	2435(3)	-676(1)
149	40	-2.80(1)	-6.11(1)	0.79(4-II-3)	944(1)	2144(3)	-417(4-II-3)
149	41	-3.32(1)	-6.74(1)	1.11(1)	1407(1)	2699(3)	-407(4-II-3)
149	42	-3.24(1)	-7.43(1)	0.82(1)	1366(1)	2804(3)	-818(1)
149	43	-3.64(1)	-7.18(1)	1.12(1)	1775(1)	3117(3)	-527(1)
150	1	-3.46(1)	2.18(4-II-3)	1.03(4-I-4)	4063(1)	-2612(4-II-3)	-1233(3)
150	2	-3.61(1)	2.61(4-II-3)	-0.76(1)	3864(1)	-2964(4-II-3)	720(1)
150	3	-2.63(1)	2.39(4-II-3)	-1.01(1)	2907(1)	-2204(4-II-3)	1389(1)
150	4	-2.99(1)	2.82(4-II-3)	0.61(4-I-4)	3137(1)	-3049(4-II-3)	669(1)
150	5	-3.44(1)	2.35(4-II-3)	1.10(3)	3272(1)	-2437(4-II-3)	-1004(4-I-3)
150	6	-3.19(1)	1.80(4-II-3)	1.68(3)	3031(1)	-1776(4-II-3)	-1697(3)
150	7	-2.91(1)	1.18(4-II-2)	2.11(3)	2581(1)	-1060(4-II-2)	-2408(3)
150	8	-2.79(1)	1.05(4-II-2)	2.27(3)	2285(1)	-1359(5-I-1)	-2886(3)
150	9	-3.30(1)	0.69(4-II-2)	1.98(3)	3074(1)	-1008(5-I-1)	-2247(3)
150	10	-3.99(1)	-1.66(1)	1.52(2)	4401(1)	1653(1)	-1904(2)
150	11	-4.52(1)	-1.61(1)	2.02(2)	5638(1)	1753(1)	-2079(2)
150	12	-2.54(1)	-1.19(1)	2.11(3)	3455(1)	1466(1)	-1900(3)
150	13	-3.06(1)	1.65(4-II-3)	1.70(3)	3640(1)	-2133(4-II-3)	-1987(3)
150	14	-3.28(1)	-0.90(1)	2.07(3)	3276(1)	1054(1)	-2291(3)
151	1	1.63(4-II-3)	-3.28(1)	-1.15(3)	-2137(4-II-3)	3109(1)	1916(4-I-3)
151	2	-1.31(1)	-2.93(1)	-1.49(3)	-1106(4-II-2)	2780(1)	2120(3)
151	3	-2.02(1)	-2.86(1)	-1.63(3)	2086(1)	3274(1)	1693(3)
151	4	1.23(4-II-3)	-2.81(1)	-1.22(3)	1247(1)	3540(1)	911(3)
151	5	1.79(4-II-3)	-3.03(1)	-0.90(4-I-4)	-1906(4-II-3)	4361(1)	677(4-I-1)
151	6	-2.19(1)	-3.73(1)	1.11(1)	2784(1)	5108(1)	-1687(1)
151	7	1.76(4-II-3)	-3.79(1)	0.91(1)	2179(1)	4686(1)	-1468(1)
151	8	2.01(4-II-3)	-3.17(1)	0.91(1)	1836(1)	3578(1)	-1585(1)
151	9	2.09(4-II-3)	-2.67(1)	1.12(1)	-1984(4-II-3)	1504(1)	-1043(1)
151	10	2.32(4-II-3)	-4.11(1)	1.03(1)	-3529(4-II-3)	2137(1)	1060(4-I-3)
151	11	2.09(4-II-3)	-3.84(1)	-0.67(4-I-1)	-2794(4-II-3)	2900(1)	1620(4-I-3)
152	1	-2.40(1)	-1.58(1)	1.45(1)	-5404(4-II-3)	2604(1)	-2267(4-II-2)
152	2	2.02(4-II-2)	-1.50(1)	0.55(1)	-5127(4-II-3)	4838(1)	-2834(1)
152	3	1.67(4-II-2)	-1.61(1)	0.39(1)	-4579(3)	7548(3)	-1862(1)
152	4	1.52(4-II-2)	-2.10(1)	-0.39(4-I-3)	-4921(3)	6578(2)	1219(4-I-2)
152	5	1.05(4-II-1)	-2.96(1)	0.48(1)	-5524(3)	5362(1)	1095(4-I-2)
152	6	1.10(4-II-2)	-2.36(1)	-0.49(5-II-3)	-5349(3)	6564(2)	1127(4-I-2)
152	7	1.42(4-II-2)	-1.71(1)	-0.49(4-I-3)	-4638(3)	8232(3)	-2023(4-II-2)
152	8	1.95(4-II-2)	-1.18(1)	0.61(1)	-3702(5-II-3)	7762(3)	-3796(4-II-2)
152	9	2.26(4-II-2)	-1.01(1)	1.00(1)	-2399(5-II-3)	6238(3)	-4869(4-II-2)
152	10	2.05(4-II-2)	0.38(4-II-3)	1.14(4-II-3)	2861(1)	1947(1)	-2882(4-II-2)
152	11	-2.22(1)	-0.39(1)	0.90(4-II-3)	-2058(5-II-3)	1590(1)	-1476(4-II-2)
152	12	-2.30(1)	-0.92(1)	0.69(3)	-3302(5-II-3)	1477(1)	-1118(4-II-2)
152	13	-2.09(1)	-1.33(1)	0.84(1)	-3428(5-II-3)	3752(3)	-3980(4-II-2)
153	1	-0.92(1)	-1.94(1)	-0.87(4-II-3)	3225(2)	-3084(5-II-3)	5817(3)
153	2	-0.81(1)	-2.62(1)	-0.79(4-II-3)	-1200(4-II-3)	-3666(5-II-3)	4377(3)
153	3	-0.53(1)	-2.65(1)	-0.64(5-I-3)	-1609(4-II-3)	-4098(5-II-3)	3843(3)
153	4	-0.57(1)	-2.30(1)	-0.78(5-I-3)	-1335(4-II-3)	-5434(4-II-3)	3523(3)
153	5	-0.59(1)	-2.01(1)	-0.72(5-I-3)	1399(1)	-6293(4-II-3)	3807(3)
153	6	-0.76(1)	-1.94(1)	-0.86(5-I-3)	3515(2)	-4009(5-II-3)	5678(3)
153	7	-0.94(1)	-1.91(1)	-1.25(5-I-3)	4378(3)	-3358(3)	4890(3)
153	8	-1.81(1)	-1.32(1)	-1.40(5-I-3)	3131(1)	-3923(3)	3557(3)
153	9	-1.26(1)	-1.74(1)	-1.20(5-I-3)	4313(2)	-2692(5-II-3)	4843(3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
153	10	-0.86(1)	-2.16(1)	-0.62(5-I-3)	2571(1)	-4062(5-II-3)	5716(3)
154	1	-0.74(1)	2.04(4-II-2)	-1.08(1)	1908(1)	-7314(4-II-3)	1041(1)
154	2	-0.73(1)	1.52(4-II-2)	-0.84(1)	-2221(4-II-3)	-7311(4-II-3)	-1069(4-II-2)
154	3	0.71(5-II-3)	1.38(4-II-2)	0.84(4-II-2)	-2213(4-II-3)	-7857(4-II-3)	-1649(4-II-2)
154	4	1.47(5-II-3)	1.23(4-II-2)	1.29(4-II-2)	-3233(4-II-3)	-8669(4-II-3)	-3535(4-II-2)
154	5	2.56(4-II-3)	-1.00(1)	0.90(4-II-4)	-6247(4-II-3)	-7774(3)	-4217(4-II-3)
154	6	2.46(4-II-3)	-0.51(5-II-2)	-0.42(1)	-5895(4-II-3)	-6460(3)	-3610(3)
154	7	2.33(4-II-3)	-0.38(5-II-2)	-0.33(1)	-5912(4-II-3)	-5614(4-II-3)	-4318(3)
154	8	1.91(4-II-3)	-0.25(5-II-1)	-0.32(1)	-7351(3)	-4386(4-II-3)	-5468(3)
154	9	1.18(5-II-3)	-0.60(5-II-2)	-0.49(4-II-2)	-10837(3)	-2491(4-II-3)	-4866(3)
154	10	1.15(5-II-3)	0.15(5-I-1)	-0.30(4-II-2)	-9054(3)	-969(4-II-2)	-3200(3)
154	11	0.87(5-II-2)	0.16(5-I-4)	0.33(4-I-2)	-7881(3)	716(1)	-2959(3)
154	12	0.52(5-II-2)	0.37(4-II-3)	0.57(4-I-2)	-6878(4-II-3)	2036(2)	-2366(4-I-2)
154	13	-1.45(1)	-0.57(1)	0.61(3)	-7309(4-II-3)	4108(3)	-3398(3)
154	14	-1.59(1)	-1.37(1)	0.47(3)	-7725(4-II-3)	4022(3)	-2700(3)
154	15	-1.30(1)	-2.55(1)	0.54(5-I-1)	-6539(4-II-3)	2184(5-II-2)	-1589(4-I-3)
154	16	-0.98(1)	-2.02(1)	-1.28(1)	1899(1)	-4275(3)	-1475(3)
154	17	-1.52(1)	-1.62(1)	-1.62(1)	6434(3)	-5975(3)	1459(1)
154	18	-1.75(1)	0.86(4-II-2)	-1.68(5-I-3)	4898(3)	-4671(3)	2165(1)
154	19	-1.25(1)	-1.53(1)	-1.23(1)	6549(3)	-6666(3)	2107(1)
154	20	-0.98(1)	-1.06(1)	-1.06(1)	6099(3)	-8679(3)	2564(1)
154	21	-0.57(1)	-1.82(1)	-1.05(1)	4204(1)	-7154(3)	2225(1)
154	22	0.96(4-II-3)	-0.35(1)	0.26(4-I-1)	-8392(4-II-3)	1229(1)	-3827(3)
154	23	0.92(4-II-3)	-0.88(1)	0.40(4-I-2)	-8323(4-II-3)	2380(3)	-3635(3)
154	24	0.98(4-II-3)	-0.56(1)	0.21(5-I-1)	-8596(4-II-3)	1221(1)	-3849(3)
154	25	1.30(4-II-3)	-0.40(1)	-0.31(1)	-9037(4-II-3)	-1387(4-II-2)	-4314(3)
154	26	1.10(4-II-3)	-0.38(1)	-0.20(4-II-2)	-8731(3)	-608(4-II-2)	-4016(3)
154	27	1.22(4-II-3)	-0.47(1)	-0.30(1)	-8696(4-II-3)	537(1)	-4144(3)
154	28	1.95(4-II-3)	-0.58(1)	-0.59(1)	-6148(4-II-3)	-5315(3)	-4496(3)
154	29	1.85(4-II-3)	-0.42(1)	-0.50(1)	-6761(4-II-3)	-4280(3)	-4885(3)
154	30	1.59(4-II-3)	-0.58(1)	-0.59(1)	-7001(4-II-3)	-3410(3)	-4811(3)
154	31	1.47(4-II-3)	-0.40(1)	-0.38(1)	-8255(4-II-3)	-2439(3)	-5029(3)
154	32	1.33(4-II-3)	-0.58(1)	-0.52(1)	-8229(4-II-3)	-1549(5-I-2)	-4449(3)
154	33	1.12(4-II-3)	-0.60(1)	-0.33(1)	-8652(4-II-3)	822(1)	-4088(3)
154	34	-0.74(1)	-1.71(1)	-1.13(1)	4739(1)	-8764(3)	1580(1)
154	35	0.70(5-II-3)	-1.31(1)	-1.04(1)	3738(1)	-9287(3)	1025(1)
154	36	1.30(4-II-3)	-1.22(1)	0.81(4-II-2)	2237(1)	-8921(3)	-3574(4-II-2)
154	37	0.86(5-II-3)	-1.24(1)	-0.99(1)	3646(1)	-9246(3)	-1513(4-II-2)
154	38	1.21(5-II-3)	-1.42(1)	-0.84(1)	3063(1)	-7168(3)	-4773(4-II-2)
154	39	1.29(5-II-3)	-1.35(1)	-0.82(1)	2681(1)	-7428(3)	-4820(4-II-2)
154	40	1.34(4-II-3)	-1.30(1)	-0.88(1)	2457(1)	-6640(3)	-4908(3)
154	41	0.96(4-II-3)	-1.42(1)	-1.02(1)	4096(1)	-8756(3)	-1766(4-II-2)
154	42	1.05(5-II-3)	-1.35(1)	-0.82(1)	3153(1)	-8905(3)	-3100(4-II-2)
154	43	0.97(4-II-3)	-1.50(1)	-0.84(1)	3270(1)	-8192(3)	-2760(4-II-2)
154	44	1.25(5-II-3)	-1.36(1)	-0.86(1)	2961(1)	-8478(3)	-4046(4-II-2)
154	45	1.09(5-II-3)	-1.42(1)	-0.87(1)	3322(1)	-8067(3)	-3663(4-II-2)
154	46	1.29(4-II-3)	-1.35(1)	-0.93(1)	-2729(4-II-3)	-5586(3)	-4818(3)
154	47	1.16(5-II-3)	-1.46(1)	-0.97(1)	3307(1)	-6159(3)	-4866(3)
154	48	-0.90(1)	-1.75(1)	-1.06(1)	3548(1)	-5244(3)	-3694(3)
154	49	0.85(4-II-3)	-1.69(1)	-1.17(1)	3979(1)	-8557(3)	-1610(4-II-4)
154	50	-0.95(1)	-1.61(1)	-0.93(1)	3484(1)	-7509(3)	-3226(4-II-2)
154	51	1.44(4-II-3)	-1.22(1)	-0.73(1)	-2619(4-II-3)	-7387(3)	-4880(4-II-2)
154	52	1.68(4-II-3)	-1.33(1)	-0.75(1)	-3748(4-II-3)	-7486(3)	-4654(4-II-2)
154	53	1.38(5-II-3)	-1.25(1)	0.72(4-II-2)	-2301(4-II-3)	-8196(3)	-4477(4-II-2)
154	54	1.55(4-II-3)	-1.29(1)	-0.82(1)	-3395(4-II-3)	-6823(3)	-4892(3)
154	55	1.49(4-II-3)	-1.22(1)	-0.89(1)	-3993(4-II-3)	-5718(3)	-4740(3)
154	56	1.08(4-II-3)	-0.75(1)	-0.79(1)	-7924(4-II-3)	-1010(5-I-2)	-2868(3)
154	57	1.02(4-II-3)	-1.33(1)	-0.91(1)	-5475(4-II-3)	-3048(5-I-2)	-3005(3)
154	58	1.09(4-II-3)	-0.91(1)	-0.81(1)	-7371(4-II-3)	-1912(5-I-2)	-3329(3)
154	59	1.14(4-II-3)	-1.24(1)	-0.94(1)	-3823(4-II-3)	-4114(3)	-4183(3)
154	60	1.35(4-II-3)	-1.08(1)	-0.87(1)	-4844(4-II-3)	-4395(3)	-4665(3)
154	61	1.26(4-II-3)	-0.97(1)	-0.78(1)	-6245(4-II-3)	-3444(3)	-3665(3)
154	62	1.93(4-II-3)	-1.05(1)	-0.73(1)	-5202(4-II-3)	-7014(3)	-4544(3)
154	63	1.94(4-II-3)	-0.86(1)	-0.76(1)	-5846(4-II-3)	-5554(3)	-4552(3)
154	64	1.74(4-II-3)	-1.02(1)	-0.76(1)	-4775(4-II-3)	-5718(3)	-4771(3)
154	65	1.52(4-II-3)	-0.89(1)	-0.78(1)	-5492(4-II-3)	-4764(3)	-4765(3)
154	66	0.98(4-II-3)	-1.08(1)	-0.54(1)	-8285(4-II-3)	1816(3)	-3356(3)
154	67	1.17(4-II-3)	-0.71(1)	-0.64(1)	-7926(4-II-3)	-1176(5-I-2)	-3832(3)
154	68	1.39(4-II-3)	-0.73(1)	-0.73(1)	-6785(4-II-3)	-3243(3)	-4267(3)
155	1	-0.49(1)	-2.32(2)	2.14(3)	141(4-II-4)	-258(4-I-4)	688(3)
155	2	-0.33(1)	-2.27(2)	1.99(3)	247(5-II-3)	-334(3)	844(3)
155	3	0.25(5-II-3)	-2.22(2)	1.83(1)	679(1)	-471(3)	953(1)
155	4	0.66(3)	-1.76(2)	1.41(1)	1156(1)	-743(3)	798(1)
155	5	0.95(3)	-1.18(2)	1.17(1)	1276(1)	-1018(1)	276(1)
155	6	1.18(3)	-1.00(1)	1.17(1)	-517(1)	-2192(1)	-368(2)
155	7	1.07(3)	-1.17(1)	1.09(1)	-411(1)	-1192(1)	678(1)

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
155	8	0.74(3)	-0.83(3)	0.97(1)	-1130(1)	-1269(3)	786(1)
155	9	0.25(3)	-0.79(3)	0.87(3)	-1934(1)	-1214(3)	901(1)
155	10	0.22(4-I-1)	-0.47(5-I-3)	1.32(3)	-2767(1)	-1044(1)	941(1)
155	11	-0.55(1)	-0.54(5-I-3)	0.99(1)	-2098(1)	-288(1)	799(1)
155	12	4.46(3)	-1.17(5-I-3)	0.87(5-II-3)	-1456(1)	460(4-II-4)	699(1)
155	13	1.42(4-II-2)	-0.49(3)	0.92(3)	-258(3)	248(1)	265(3)
155	14	-0.30(1)	-1.29(2)	2.13(3)	-129(1)	-357(2)	327(3)
155	15	-0.36(1)	-0.26(4-I-1)	1.71(3)	-970(1)	-274(1)	59(1)
155	16	-0.51(1)	-0.42(2)	1.97(3)	-321(1)	-199(3)	66(3)
155	17	-0.46(1)	-1.09(2)	2.02(3)	-340(1)	-178(3)	105(1)
155	18	0.33(5-II-2)	-1.01(3)	1.47(3)	-1168(1)	-569(1)	239(1)
155	19	-0.23(1)	-0.73(3)	1.30(1)	-1711(1)	-711(1)	342(1)
155	20	0.95(3)	-1.28(3)	1.35(3)	-1310(1)	-786(1)	439(1)
155	21	-0.39(1)	-0.62(2)	1.64(1)	-1222(1)	-473(1)	148(1)
155	22	0.91(3)	-1.30(2)	1.49(1)	-151(1)	-699(1)	79(1)
155	23	0.80(3)	-0.99(2)	1.17(3)	-971(1)	-676(1)	201(1)
155	24	0.59(3)	-1.11(2)	1.53(1)	-695(1)	-537(1)	148(1)
155	25	0.48(3)	-1.48(2)	1.63(1)	249(2)	-458(3)	261(1)
155	26	0.33(5-II-3)	-1.12(2)	1.76(1)	-532(1)	-341(3)	141(1)
155	27	-0.23(1)	-1.40(2)	1.85(3)	-93(1)	-336(3)	214(1)
156	1	-1.19(3)	-4.66(1)	1.83(3)	7781(1)	2639(1)	729(3)
156	2	-3.56(1)	-7.33(1)	-0.61(1)	9341(1)	6739(1)	534(4-I-3)
156	3	-3.70(3)	-5.15(1)	0.41(4-I-1)	7321(1)	5673(1)	1058(3)
156	4	-3.81(1)	-4.93(1)	0.46(3)	4488(1)	3476(1)	133(5-II-4)
156	5	-3.50(1)	-4.83(1)	0.55(3)	1989(4-II-4)	2702(1)	-414(5-I-4)
156	6	-3.20(1)	-4.37(1)	0.92(3)	709(4-II-1)	2069(1)	-595(3)
156	7	-2.89(1)	-3.32(5-I-2)	1.37(3)	-1628(1)	1529(5-I-2)	-666(5-I-3)
156	8	-2.48(4-II-3)	4.39(5-II-2)	1.97(4-II-4)	-4084(1)	-2341(5-II-2)	810(5-II-2)
156	9	-2.77(1)	-3.83(5-I-2)	2.06(3)	-3575(1)	1520(5-I-2)	472(5-II-2)
156	10	-3.31(1)	-4.49(1)	1.76(3)	-2445(1)	2035(1)	-500(5-I-3)
156	11	-3.30(1)	-5.87(1)	1.46(5-II-2)	-2269(1)	2383(1)	-537(5-I-3)
156	12	-3.43(1)	-6.71(1)	1.28(5-II-2)	-2611(1)	2859(1)	-675(5-I-3)
156	13	-3.52(1)	-7.10(1)	0.99(5-II-2)	-2977(1)	3012(1)	-945(5-I-3)
156	14	-3.58(1)	-6.99(1)	-0.82(5-I-2)	-3399(1)	2746(1)	-1313(1)
156	15	-3.78(1)	-6.24(1)	-0.89(5-I-2)	-4005(1)	1988(1)	-1673(1)
156	16	-4.07(1)	-4.92(1)	0.74(4-I-1)	-5132(1)	-1096(4-I-3)	-1595(1)
156	17	-3.85(1)	2.82(5-I-2)	2.19(4-I-3)	-7298(1)	-2859(5-I-2)	-1706(5-I-2)
156	18	-4.17(1)	-3.71(1)	1.63(2)	-1614(4-I-2)	-2116(4-I-4)	-339(5-I-3)
156	19	-4.74(1)	-4.18(1)	2.38(2)	4265(1)	-1536(4-I-4)	-336(5-I-4)
156	20	-6.15(1)	-5.32(1)	3.45(1)	8600(1)	3286(1)	244(5-II-4)
156	21	-1.61(3)	-4.37(1)	2.19(3)	7545(1)	1726(1)	758(1)
156	22	-3.46(1)	-5.16(1)	1.27(3)	1861(4-II-4)	2156(1)	-369(5-I-4)
156	23	-3.96(1)	-4.65(1)	0.98(4-I-1)	-2001(4-I-3)	1741(1)	-493(5-I-4)
156	24	-3.73(1)	-4.52(1)	1.89(3)	1383(4-II-2)	1027(1)	334(5-II-4)
156	25	-3.62(1)	-5.66(1)	0.69(4-I-3)	-1695(4-I-3)	2752(1)	-675(1)
156	26	-3.29(1)	-5.56(1)	0.86(4-I-1)	1742(4-II-4)	3068(1)	-460(5-I-4)
156	27	-2.77(1)	-5.66(1)	0.94(4-I-1)	3786(1)	3254(1)	-437(5-I-4)
156	28	-2.22(3)	-5.66(1)	0.98(4-I-1)	6119(1)	3144(1)	-436(5-I-4)
156	29	-3.36(1)	-4.84(1)	2.27(3)	3834(1)	1513(1)	413(5-II-4)
156	30	-2.14(3)	-5.58(1)	2.26(3)	5651(1)	1994(1)	349(5-II-4)
156	31	-2.78(1)	-5.35(1)	1.63(3)	3443(1)	2169(1)	-330(5-I-4)
156	32	-3.74(1)	-5.24(1)	0.52(5-II-2)	2235(1)	3970(1)	173(4-II-1)
156	33	-3.62(1)	-5.33(1)	0.76(5-II-2)	865(4-II-1)	3088(1)	-336(5-I-4)
156	34	-3.68(1)	-5.85(1)	0.77(5-II-2)	-538(4-I-1)	3639(1)	-326(5-I-4)
156	35	-3.67(1)	-6.11(1)	0.59(5-II-2)	-1193(4-I-3)	3501(1)	-663(1)
156	36	-3.77(1)	-6.07(1)	0.66(5-II-2)	-734(4-I-2)	3833(1)	-449(5-I-4)
156	37	-3.80(1)	-5.36(1)	0.44(4-I-1)	3527(1)	4912(1)	-264(5-I-4)
156	38	-4.00(1)	-5.16(1)	0.49(4-I-1)	2882(1)	4685(1)	211(5-II-4)
156	39	-4.10(1)	-5.32(1)	0.46(4-I-1)	4826(1)	5398(1)	177(5-II-4)
156	40	-3.80(1)	-5.49(1)	0.47(4-I-1)	1892(4-II-4)	4321(1)	-279(5-I-4)
156	41	-3.23(1)	-5.47(1)	0.52(4-I-1)	6056(1)	5018(1)	-522(1)
156	42	-3.54(1)	-5.69(1)	0.60(4-I-1)	1737(4-II-4)	3914(1)	-467(1)
156	43	-3.38(1)	-5.52(1)	0.57(4-I-1)	3818(1)	4373(1)	-469(1)
157	1	-8.42(1)	-3.04(1)	2.58(3)	5222(1)	3431(1)	-131(1)
157	2	-7.81(1)	-3.45(1)	3.34(1)	3724(1)	684(1)	551(5-I-3)
157	3	-2.38(1)	-2.02(1)	1.03(3)	2314(1)	1200(1)	-1201(1)
157	4	-2.02(1)	-2.18(1)	0.99(3)	2654(1)	1921(1)	-1908(1)
157	5	-0.88(3)	-1.62(1)	-0.34(5-II-4)	2994(1)	2592(1)	-2446(1)
157	6	-7.94(1)	-1.74(1)	0.84(3)	8865(1)	2846(1)	-2677(1)
157	7	-8.57(1)	-3.21(1)	2.55(3)	7118(1)	3709(1)	-1885(1)
157	8	-4.55(1)	-3.44(1)	1.52(3)	3857(1)	2257(1)	-1808(1)
158	1	-3.83(1)	-3.44(1)	-0.57(5-II-2)	2678(1)	1681(1)	988(5-II-2)
158	2	-4.16(1)	-2.22(1)	-0.77(4-II-3)	1574(5-I-2)	-475(4-I-1)	580(5-II-2)
158	3	-4.01(5-I-2)	1.15(4-I-3)	-1.48(4-II-3)	-2657(5-II-2)	-2066(3)	-1123(4-I-3)
158	4	-4.05(1)	-2.23(1)	-0.94(5-II-2)	1552(5-I-2)	-973(4-I-1)	-533(1)
158	5	-4.05(1)	-3.31(1)	-0.63(5-II-2)	2395(1)	1179(4-II-1)	609(5-II-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
158	6	-3.91(1)	-3.84(1)	0.57(1)	3593(1)	2657(1)	1045(3)
158	7	-3.88(1)	-4.06(1)	0.66(1)	4699(1)	4222(1)	1914(3)
158	8	-4.28(1)	-4.47(1)	-0.66(5-II-2)	5902(1)	5024(1)	3736(1)
158	9	-1.65(1)	-3.34(1)	0.87(1)	6373(1)	1606(1)	1945(2)
158	10	-2.77(1)	-4.12(1)	0.69(1)	5327(1)	2873(1)	2378(3)
158	11	-3.36(1)	-4.07(1)	0.40(1)	4084(1)	2849(1)	1627(3)
159	1	-3.54(1)	-2.89(3)	2.81(3)	3792(1)	5860(1)	868(1)
159	2	-2.87(1)	-3.25(1)	3.11(1)	3085(1)	6041(1)	-335(5-II-2)
159	3	-1.95(1)	-6.50(1)	2.77(1)	2349(1)	6025(1)	-322(5-II-2)
159	4	-2.78(1)	-3.93(1)	2.91(1)	2973(1)	6005(1)	-504(5-II-2)
159	5	-3.22(1)	-2.09(3)	2.42(1)	3213(1)	5754(1)	441(1)
159	6	-2.32(1)	-0.55(4-II-4)	1.45(3)	1681(1)	5518(1)	1340(1)
159	7	-2.10(1)	-0.35(4-II-4)	1.79(3)	1966(1)	5728(1)	1246(3)
159	8	-2.73(1)	-1.13(3)	1.75(3)	2814(1)	5906(1)	1405(3)
159	9	-3.26(1)	-1.11(3)	2.20(3)	3181(1)	5687(1)	881(1)
160	1	-6.58(1)	-2.32(1)	-1.62(4-II-3)	2441(3)	2602(1)	1178(3)
160	2	-6.38(1)	-1.55(1)	-0.98(4-II-3)	1098(4-II-1)	1681(1)	1066(5-II-2)
160	3	-4.96(1)	0.90(4-I-1)	1.58(4-I-3)	-1018(4-I-1)	1470(1)	1383(3)
160	4	-3.54(4-II-1)	1.47(4-I-3)	3.09(4-I-3)	-2929(4-I-1)	-531(5-II-3)	970(5-II-2)
160	5	-4.07(1)	-2.10(1)	0.90(1)	1416(4-II-1)	-675(5-II-2)	630(5-II-2)
160	6	-4.17(1)	-3.21(1)	-0.47(4-II-3)	3273(2)	1384(1)	898(5-II-2)
160	7	-3.36(1)	-4.10(1)	-0.76(3)	5183(1)	1944(1)	947(5-II-2)
160	8	-2.04(1)	-4.41(1)	-1.06(3)	6359(1)	2027(1)	736(5-II-3)
160	9	-0.82(1)	-3.55(1)	-1.29(3)	6052(1)	1796(1)	-541(1)
160	10	-2.20(1)	-3.96(1)	-2.06(3)	6002(1)	2587(1)	635(5-II-3)
160	11	-4.17(1)	-3.55(1)	-2.70(1)	5620(1)	2684(1)	844(5-II-2)
160	12	-6.06(1)	-3.23(1)	-3.16(2)	4956(1)	2573(1)	711(4-II-3)
160	13	-6.16(1)	-2.91(1)	-2.42(3)	3807(2)	2587(1)	926(5-II-2)
160	14	-5.14(1)	-2.70(1)	-0.97(4-II-3)	3335(2)	1603(1)	1064(5-II-2)
160	15	-4.54(1)	-3.47(1)	-1.66(2)	4932(1)	2225(1)	955(5-II-2)
161	1	-3.28(1)	-5.80(2)	-0.37(5-II-2)	-311(4-I-1)	-4759(3)	1688(1)
161	2	-4.02(1)	-5.38(2)	-0.71(5-II-2)	683(4-II-1)	-4549(3)	1653(1)
161	3	-4.59(1)	-5.00(2)	-0.78(5-II-2)	936(3)	-4399(3)	1683(1)
161	4	-4.88(1)	-4.71(2)	0.82(5-I-2)	1097(5-II-1)	-4317(3)	1703(1)
161	5	-4.81(1)	-4.48(2)	1.20(5-I-2)	1064(5-II-1)	-4446(2)	1903(1)
161	6	-4.44(1)	-4.29(2)	1.72(5-I-2)	797(5-II-2)	-5068(2)	2376(1)
161	7	-3.59(5-II-2)	-4.09(2)	2.37(5-I-2)	-1764(5-I-2)	-6140(2)	3084(1)
161	8	-4.28(5-II-2)	-4.91(2)	3.10(4-II-1)	-4053(5-I-2)	-7330(2)	3431(1)
161	9	-3.48(5-II-2)	-4.50(2)	1.92(5-I-2)	-1083(5-I-2)	-5920(2)	2016(1)
161	10	-3.93(1)	-4.53(2)	1.42(5-I-2)	1209(5-II-2)	-4251(2)	1358(1)
161	11	-4.24(1)	-4.71(2)	1.10(5-I-2)	1666(3)	-2955(2)	948(1)
161	12	-4.17(1)	-4.88(2)	0.92(5-I-2)	1948(3)	-1820(4-I-3)	558(1)
161	13	-4.01(1)	-4.94(2)	0.81(5-I-2)	1968(3)	-1098(4-I-3)	-413(4-II-1)
161	14	-3.93(1)	-5.14(1)	0.80(5-I-2)	1499(3)	1326(4-II-2)	-661(4-II-1)
161	15	-3.97(1)	-5.40(1)	1.08(3)	706(4-II-1)	2265(4-II-4)	-1049(3)
161	16	-4.17(1)	-6.13(1)	1.21(3)	-1080(4-I-1)	4053(1)	-2053(3)
161	17	-3.78(1)	-7.60(1)	0.86(5-I-1)	-1797(4-I-1)	7597(1)	-2447(3)
161	18	-3.35(1)	-6.41(1)	0.57(5-I-1)	-1661(4-I-1)	3681(1)	-980(3)
161	19	-2.96(1)	-5.13(1)	0.53(3)	-2441(4-I-1)	-1467(4-I-2)	940(1)
161	20	2.12(5-II-2)	-4.40(4-II-1)	2.23(5-II-2)	-3119(3)	-6906(2)	2255(1)
161	21	-2.30(1)	-5.92(1)	0.49(4-I-1)	-1413(4-I-1)	-5304(3)	2023(1)
161	22	-4.31(1)	-5.02(2)	0.65(5-I-2)	1222(3)	-2910(3)	1205(1)
161	23	-4.41(1)	-4.92(2)	0.81(5-I-2)	1602(3)	-2642(3)	1044(1)
161	24	-4.17(1)	-4.95(2)	0.76(5-I-2)	1559(3)	-1814(4-I-2)	711(1)
161	25	-3.53(1)	-5.48(1)	0.88(3)	-566(4-I-1)	-1275(4-I-2)	612(1)
161	26	-3.20(1)	-5.60(1)	0.99(3)	-1111(4-I-1)	-1969(4-I-2)	1231(1)
161	27	-3.49(1)	-5.49(1)	0.60(5-I-1)	435(4-II-1)	-2628(4-I-2)	1380(1)
161	28	-3.96(1)	-5.13(1)	0.75(5-I-2)	1083(4-II-1)	-1522(4-I-2)	524(1)
161	29	-3.92(1)	-5.24(2)	0.59(5-I-2)	878(4-II-1)	-2614(3)	1210(1)
162	1	-5.38(1)	-2.18(1)	-0.50(4-II-1)	6650(2)	2089(3)	290(4-II-1)
162	2	-5.22(1)	-2.41(1)	-0.46(4-II-1)	6614(2)	1947(3)	478(4-II-1)
162	3	-5.05(1)	-2.62(1)	-0.44(4-II-1)	5907(2)	1684(3)	662(3)
162	4	-4.86(1)	-2.73(1)	0.47(4-I-1)	4239(3)	1114(3)	870(3)
162	5	-4.66(1)	-2.70(1)	0.60(4-I-1)	2324(4-II-2)	619(5-II-2)	979(3)
162	6	-4.28(1)	-2.53(3)	0.81(4-I-4)	-2393(4-I-2)	-1219(1)	927(3)
162	7	-4.59(4-II-1)	-2.00(5-II-2)	1.44(5-I-2)	-8980(2)	-2973(1)	1379(5-II-2)
162	8	-4.18(1)	-2.65(3)	0.55(4-I-4)	-2428(4-I-2)	-1375(1)	754(3)
162	9	-4.59(1)	-2.69(1)	0.46(4-I-1)	2356(4-II-2)	459(5-II-2)	749(3)
162	10	-4.83(1)	-2.73(1)	-0.46(4-II-1)	4304(3)	983(3)	701(3)
162	11	-5.02(1)	-2.65(1)	-0.50(4-II-1)	6031(3)	1502(3)	575(3)
162	12	-5.17(1)	-2.48(1)	-0.56(4-II-1)	6849(2)	1735(3)	443(4-II-4)
162	13	-5.30(1)	-2.34(1)	-0.65(4-II-1)	7000(2)	1779(3)	327(4-II-4)
162	14	-5.42(1)	-2.17(1)	-0.78(4-II-1)	6467(2)	1663(3)	-210(4-I-1)
162	15	-5.55(1)	-2.04(1)	-0.95(4-II-4)	5393(1)	1415(3)	-308(4-I-1)
162	16	-5.67(1)	-1.93(1)	-1.13(4-II-4)	3586(1)	988(3)	-492(4-I-1)
162	17	-5.72(1)	-1.84(1)	-1.01(4-II-4)	3413(1)	1049(3)	-570(4-I-1)

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
162	18	-5.68(1)	-1.75(1)	-0.96(3)	3272(1)	1178(3)	-640(4-I-1)
162	19	-5.58(1)	-1.62(1)	-1.00(3)	3235(1)	1357(3)	-723(3)
162	20	-5.60(1)	-1.69(1)	-0.71(4-II-1)	5054(1)	1805(3)	-534(4-I-1)
162	21	-5.49(1)	-1.90(1)	-0.58(4-II-1)	6116(1)	2026(3)	-368(4-I-1)
162	22	-5.35(1)	-2.19(1)	-0.56(4-II-1)	6723(2)	1944(3)	268(4-II-1)
162	23	-5.24(1)	-2.34(1)	-0.53(4-II-1)	6857(2)	1878(3)	396(4-II-1)
162	24	-5.35(1)	-2.22(1)	-0.62(4-II-1)	6832(2)	1844(3)	297(4-II-1)
162	25	-5.59(1)	-1.92(1)	-0.87(4-II-4)	5208(1)	1459(3)	-364(4-I-1)
162	26	-5.60(1)	-1.81(1)	-0.78(4-II-1)	5106(1)	1582(3)	-441(4-I-1)
162	27	-5.47(1)	-2.06(1)	-0.73(4-II-1)	6284(1)	1721(3)	-264(4-I-1)
162	28	-5.48(1)	-1.98(1)	-0.66(4-II-1)	6175(1)	1836(3)	-320(4-I-1)
163	1	-2.05(1)	-4.06(1)	1.14(1)	1462(1)	-2046(4-II-2)	1583(3)
163	2	-6.92(1)	-4.07(3)	-0.61(4-I-1)	1665(1)	-4129(4-II-2)	2475(3)
163	3	-5.15(1)	-2.86(1)	1.55(1)	437(1)	-4237(4-II-2)	2675(3)
163	4	-4.40(1)	-2.44(1)	2.23(1)	1157(1)	-4013(4-II-2)	1961(3)
163	5	-4.31(1)	-3.49(1)	3.37(1)	-730(5-I-4)	-5010(4-II-2)	1808(3)
163	6	-0.84(2)	-1.80(1)	0.79(1)	-910(3)	-1946(4-II-2)	1477(2)
163	7	0.24(4-II-2)	-1.60(1)	0.45(1)	-798(3)	-744(4-II-2)	1229(2)
163	8	0.35(4-II-2)	1.74(4-II-3)	1.02(4-II-4)	-926(3)	652(1)	972(2)
163	9	-0.42(4-I-2)	-2.77(1)	0.79(1)	596(1)	-708(4-II-2)	1502(2)
164	1	-4.46(2)	-1.81(1)	1.39(3)	-697(4-II-2)	4992(3)	1732(4-II-2)
164	2	-5.43(3)	-3.81(1)	1.47(3)	-2191(3)	3603(2)	1588(4-II-2)
164	3	-4.43(1)	-1.41(1)	1.62(3)	-928(4-II-3)	2911(2)	605(4-II-2)
164	4	-3.47(1)	0.64(4-II-2)	1.27(1)	-544(4-II-3)	2465(1)	-645(4-I-1)
164	5	-2.37(1)	1.53(4-II-2)	0.96(1)	-1221(3)	1161(1)	-717(2)
164	6	-3.89(1)	0.99(4-II-2)	1.64(2)	677(1)	2757(1)	386(4-II-1)
164	7	-4.63(1)	0.72(4-II-2)	2.18(3)	1519(1)	4154(2)	700(4-II-2)
164	8	-4.13(1)	-0.94(1)	2.68(3)	1456(1)	6267(3)	1214(4-II-2)
164	9	-4.10(1)	-1.38(1)	2.03(3)	1011(1)	5931(3)	1648(4-II-2)
164	10	-4.73(1)	-1.05(1)	2.06(3)	684(1)	4213(2)	937(4-II-2)
165	1	-3.83(1)	-2.73(1)	-2.44(1)	1054(1)	4044(1)	996(3)
165	2	-3.60(1)	-2.48(1)	-2.51(1)	1976(1)	3882(1)	413(1)
165	3	-3.44(1)	-2.25(1)	-2.67(2)	2942(1)	3487(1)	-371(4-II-3)
165	4	-3.21(1)	-2.47(1)	-2.99(3)	3773(2)	3136(1)	-748(3)
165	5	-3.12(1)	-2.48(1)	-3.51(3)	5565(2)	3072(3)	-1424(3)
165	6	-2.89(1)	-2.42(1)	-3.23(3)	3474(2)	2589(1)	-872(3)
165	7	-2.13(1)	-2.11(1)	-2.59(2)	1867(1)	1808(1)	-529(4-II-2)
165	8	1.33(4-II-2)	-2.55(1)	-1.76(1)	-866(5-I-3)	-322(5-I-4)	486(4-I-1)
165	9	-1.34(1)	-3.27(1)	-2.77(1)	-1086(5-I-3)	818(1)	1168(3)
165	10	-2.36(1)	-4.37(1)	-3.70(1)	-1910(3)	1212(1)	1709(3)
165	11	-9.59(1)	-6.38(1)	-3.97(1)	2271(1)	4037(1)	3896(3)
165	12	-5.49(1)	-3.90(1)	-3.00(1)	-1492(3)	4652(1)	2808(3)
165	13	-4.31(1)	-3.17(1)	-2.67(1)	-789(5-I-3)	4366(1)	1794(3)
165	14	-2.93(1)	-2.47(1)	-2.58(1)	1793(1)	3131(1)	142(4-I-2)
165	15	-2.94(1)	-2.61(1)	-2.62(1)	-531(5-I-1)	3104(1)	1019(3)
166	1	-5.23(1)	-2.21(1)	0.94(1)	5944(1)	2829(3)	-948(2)
166	2	-5.05(1)	-2.55(1)	0.87(2)	6183(2)	2370(3)	-693(2)
166	3	-4.92(1)	-2.79(1)	0.79(4-I-1)	5659(3)	1831(3)	-361(1)
166	4	-4.81(1)	-2.91(1)	0.83(4-I-1)	4372(3)	1125(5-II-2)	189(4-I-1)
166	5	-4.65(1)	-2.91(3)	0.87(4-I-4)	2641(4-II-2)	497(5-II-2)	751(3)
166	6	-4.39(1)	-2.65(5-II-2)	0.89(4-I-3)	-1783(4-I-2)	-1551(1)	1424(3)
166	7	-4.42(4-II-3)	-2.16(5-II-2)	2.25(5-I-2)	-7281(1)	-3363(2)	2204(3)
166	8	-4.32(1)	-3.02(3)	0.93(4-I-3)	-1808(4-I-3)	-1611(1)	985(3)
166	9	-4.60(1)	-2.99(3)	0.77(4-I-4)	2640(4-II-2)	338(5-II-2)	549(3)
166	10	-4.77(1)	-2.86(1)	0.77(4-I-1)	4402(3)	1034(5-II-2)	-136(4-I-1)
166	11	-4.91(1)	-2.78(1)	0.75(4-I-1)	5719(3)	1713(3)	-476(1)
166	12	-5.03(1)	-2.57(1)	0.80(2)	6309(2)	2240(3)	-806(2)
166	13	-5.23(1)	-2.25(1)	0.80(2)	6122(2)	2579(3)	-1101(2)
166	14	-5.41(1)	-1.89(1)	0.77(1)	5483(1)	2726(3)	-1233(2)
166	15	-5.60(1)	-1.59(1)	0.70(1)	4408(1)	2560(3)	-1220(2)
166	16	-5.66(1)	-1.26(1)	0.47(1)	2761(1)	2218(3)	-1029(2)
166	17	-5.71(1)	-1.04(1)	0.39(1)	2772(1)	2468(3)	-1188(2)
166	18	-5.83(1)	-0.96(1)	0.34(1)	2863(1)	2750(3)	-1437(2)
166	19	-6.17(1)	-0.71(1)	0.41(1)	2919(1)	3342(3)	-1709(2)
166	20	-5.67(1)	-1.14(1)	0.90(1)	4138(1)	3574(3)	-1182(2)
166	21	-5.43(1)	-1.72(1)	0.93(1)	5163(1)	3102(3)	-1155(2)
166	22	-5.62(1)	-1.37(1)	0.80(1)	3971(1)	3180(3)	-1247(2)
166	23	-5.48(1)	-1.55(1)	0.85(1)	4991(1)	2995(3)	-1260(2)
166	24	-5.61(1)	-1.40(1)	0.67(1)	4047(1)	2784(3)	-1192(2)
167	1	-4.63(1)	-3.16(1)	1.04(2)	4097(3)	1196(5-II-2)	-380(4-II-1)
167	2	-4.66(1)	-3.14(1)	1.14(2)	5217(3)	1975(3)	-698(1)
167	3	-4.69(1)	-3.00(1)	1.29(2)	5687(2)	2659(3)	-1023(1)
167	4	-4.75(1)	-2.71(1)	1.46(2)	5536(1)	3175(3)	-1116(1)
167	5	-4.88(1)	-2.22(1)	1.67(1)	4899(1)	3746(3)	-1006(1)
167	6	-5.25(1)	-1.54(1)	1.79(1)	3842(1)	4048(3)	-843(1)
167	7	-5.77(2)	-0.75(1)	1.96(1)	2798(1)	5418(3)	-941(1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
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167	8	-4.92(1)	-1.28(1)	1.89(1)	3708(1)	4462(3)	-322(1)
167	9	-4.66(1)	-1.75(1)	1.98(1)	4124(1)	3471(2)	193(4-II-1)
167	10	-4.61(1)	-2.10(1)	2.01(1)	4538(1)	2177(1)	369(3)
167	11	-4.69(1)	-2.64(1)	2.07(1)	5002(1)	1035(1)	444(3)
167	12	-4.97(1)	-3.68(1)	1.95(1)	5921(1)	-819(5-I-1)	280(1)
167	13	-5.67(1)	-5.21(1)	1.89(1)	7048(1)	-2141(3)	-409(4-II-3)
167	14	-7.33(1)	-6.01(1)	2.02(1)	8464(1)	-2989(3)	-2903(1)
167	15	-5.84(1)	-4.65(1)	1.09(1)	6017(1)	-1350(4-I-1)	-1599(1)
167	16	-5.23(1)	-4.08(1)	0.85(2)	4672(1)	635(1)	-809(1)
167	17	-5.13(1)	-3.79(1)	0.89(4-I-1)	3170(3)	1061(1)	506(4-I-3)
167	18	-5.10(1)	-3.67(1)	0.99(4-I-1)	2453(4-II-1)	1028(1)	888(4-I-3)
167	19	-5.14(1)	-3.52(1)	1.02(4-I-1)	1977(4-II-1)	944(5-II-2)	1298(3)
167	20	-5.15(1)	-3.34(2)	0.99(4-I-2)	1402(4-II-2)	781(5-II-2)	1679(3)
167	21	-5.18(1)	-3.13(3)	1.08(4-I-2)	-1277(4-I-2)	-810(5-I-2)	2071(3)
167	22	-5.11(1)	-2.93(5-II-2)	1.26(5-I-2)	-2695(1)	-1615(1)	2580(3)
167	23	-4.16(4-II-3)	-3.09(5-II-2)	2.45(5-I-2)	-6218(1)	-3300(1)	2522(3)
167	24	-4.40(1)	-2.93(3)	1.12(4-I-3)	-1425(4-I-3)	-1821(1)	1699(3)
167	25	-4.40(1)	-3.14(3)	1.00(2)	2406(4-II-2)	-463(5-I-2)	807(4-I-1)
167	26	-4.76(1)	-3.23(1)	1.06(2)	3609(3)	1209(5-II-2)	543(4-I-1)
167	27	-4.92(1)	-3.29(1)	1.05(4-I-2)	2660(4-II-1)	1056(5-II-2)	979(3)
167	28	-4.82(1)	-3.19(2)	1.08(4-I-3)	2209(4-II-2)	696(5-II-2)	1120(3)
167	29	-4.93(1)	-3.44(1)	1.03(4-I-1)	3111(3)	1231(5-II-2)	747(4-I-3)
167	30	-4.71(1)	-3.27(1)	1.14(2)	4736(3)	1804(3)	-402(4-II-2)
167	31	-4.88(1)	-3.75(1)	0.97(2)	4064(3)	1245(1)	407(4-I-3)
167	32	-4.96(1)	-3.58(1)	1.00(4-I-1)	3419(3)	1236(1)	630(4-I-3)
167	33	-4.84(1)	-3.58(1)	1.04(2)	4395(3)	1544(2)	401(4-I-3)
167	34	-4.78(1)	-3.43(1)	1.09(2)	4434(3)	1689(3)	349(4-I-3)
167	35	-4.60(1)	-3.43(1)	1.35(1)	5486(1)	1920(2)	-303(4-II-3)
167	36	-4.71(1)	-3.54(1)	1.16(2)	5036(2)	1741(2)	-347(4-II-3)
167	37	-4.68(1)	-3.70(1)	1.28(1)	5544(1)	1318(1)	-273(4-II-3)
167	38	-4.85(1)	-4.04(1)	1.09(2)	5353(1)	605(1)	-386(4-II-3)
167	39	-4.81(1)	-3.68(1)	1.02(2)	5023(1)	1337(1)	-418(4-II-3)
167	40	-4.59(1)	-3.53(1)	1.53(1)	5615(1)	1365(1)	-148(4-II-3)
167	41	-4.61(1)	-3.20(1)	1.78(1)	5519(1)	1235(1)	217(3)
167	42	-4.73(1)	-3.84(1)	1.51(1)	5854(1)	552(1)	-197(4-II-3)
167	43	-4.56(1)	-2.71(1)	1.86(1)	5149(1)	2180(2)	152(3)
167	44	-4.56(1)	-3.18(1)	1.62(1)	5509(1)	2060(2)	-169(4-II-3)
167	45	-4.67(1)	-3.16(1)	1.29(2)	5449(2)	2461(3)	-659(1)
167	46	-4.67(1)	-3.35(1)	1.25(2)	5229(2)	2139(3)	-422(4-II-3)
167	47	-4.67(1)	-2.57(1)	1.71(1)	5053(1)	3320(3)	-544(1)
167	48	-4.61(1)	-2.42(1)	1.87(1)	4961(1)	3205(2)	-280(1)
167	49	-4.59(1)	-2.87(1)	1.66(1)	5403(1)	2698(2)	-328(1)
167	50	-4.67(1)	-2.92(1)	1.49(2)	5516(1)	2969(3)	-744(1)
167	51	-4.60(1)	-3.17(1)	1.43(2)	5489(1)	2481(2)	-433(1)
168	1	-1.31(1)	0.98(3)	-0.52(4-II-3)	-3794(4-II-2)	1430(2)	3873(4-II-2)
168	2	1.13(4-II-3)	0.94(3)	-1.74(4-II-2)	-4771(4-II-2)	-3137(4-II-2)	4966(4-II-2)
168	3	1.35(3)	1.14(3)	-1.03(3)	-2828(4-II-2)	5438(3)	-4284(4-I-2)
168	4	0.81(4-II-3)	-0.79(4-II-2)	0.25(1)	-6484(4-II-2)	1252(1)	-1307(4-I-2)
168	5	-1.38(1)	0.20(3)	-0.45(4-II-3)	-5366(4-II-2)	840(3)	1424(4-II-2)
168	6	-0.92(1)	0.30(5-I-3)	-0.82(4-II-3)	-3718(4-II-2)	1472(3)	4025(4-II-2)
168	7	-0.73(1)	0.46(5-I-3)	-0.47(4-II-3)	-5703(4-II-2)	1159(1)	3371(4-II-2)
168	8	-2.28(2)	0.46(5-I-3)	-0.56(4-II-3)	-3547(4-II-2)	605(1)	1836(4-II-2)
169	1	-1.26(2)	-1.35(1)	-1.10(1)	5219(3)	-6970(3)	-3991(4-II-3)
169	2	0.63(4-II-3)	0.97(3)	-0.30(4-I-2)	3845(4-I-2)	-4090(3)	-2747(4-II-3)
169	3	0.80(4-II-3)	-3.18(1)	-2.31(3)	6541(3)	-5719(3)	-5825(3)
169	4	-2.78(1)	1.28(4-II-3)	-1.98(1)	5264(3)	-5319(3)	-6876(3)
169	5	-3.46(3)	-0.80(1)	-1.68(3)	2731(4-I-2)	-7860(3)	-4172(3)
169	6	-2.32(1)	-1.48(1)	-1.08(1)	4598(3)	-6309(3)	-4781(3)
170	1	-1.95(1)	-4.11(2)	0.19(4-II-3)	3940(3)	-2823(4-II-1)	-1225(4-II-2)
170	2	-3.37(3)	-3.68(2)	-0.30(4-I-3)	1678(3)	-2431(4-II-2)	540(4-I-1)
170	3	-1.11(1)	-5.21(2)	-0.61(2)	7116(3)	-3404(4-II-1)	-3443(4-II-2)
170	4	-1.69(1)	-4.50(2)	-0.72(3)	6271(3)	-3185(4-II-1)	-2433(4-II-2)
170	5	-1.60(1)	-4.28(2)	-0.53(3)	5518(3)	-3131(4-II-1)	-2088(4-II-2)
170	6	-1.63(1)	-4.51(2)	-0.49(3)	5783(3)	-3515(4-II-1)	-2157(4-II-2)
170	7	-1.93(1)	-4.69(2)	-0.55(2)	6826(3)	-3018(4-II-1)	-2856(4-II-2)
170	8	-1.30(1)	-4.54(2)	-0.75(3)	7118(3)	-2689(4-II-1)	-3091(2)
171	1	-5.42(3)	-2.70(3)	0.70(2)	2556(1)	1823(3)	1292(4-II-2)
171	2	-6.05(3)	-2.84(3)	0.18(2)	5096(2)	2295(3)	1130(3)
171	3	-5.66(3)	-2.50(3)	0.76(2)	3213(1)	1102(4-I-2)	1036(4-II-1)
171	4	-5.70(3)	-2.42(3)	1.05(2)	863(1)	1239(4-I-2)	1417(4-II-1)
171	5	-6.11(3)	-3.12(3)	2.15(2)	-3743(3)	-2224(4-II-1)	3663(3)
171	6	-4.08(3)	-3.01(3)	0.34(2)	2129(1)	1272(4-I-1)	1686(3)
171	7	-4.86(3)	-3.01(3)	0.97(2)	1416(1)	1367(4-I-1)	1734(3)
172	1	-8.66(1)	-1.85(3)	0.91(4-II-1)	3531(1)	93(5-I-2)	-323(4-II-1)
172	2	-8.39(1)	-1.87(3)	1.12(4-II-1)	3374(1)	189(5-I-2)	-346(4-II-1)
172	3	-7.85(1)	-1.89(2)	1.30(5-I-2)	3108(1)	303(5-I-2)	-343(4-II-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
172	4	-7.03(1)	-1.90(2)	1.44(5-I-2)	2726(1)	430(5-I-2)	-325(4-II-1)
172	5	-5.91(1)	-1.87(2)	1.54(5-I-2)	2230(1)	558(5-I-2)	-314(4-II-1)
172	6	-4.52(1)	-1.89(5-I-2)	1.57(5-I-2)	1683(4-II-3)	663(5-I-2)	-339(4-II-1)
172	7	-3.37(4-II-3)	-1.92(5-I-2)	1.65(4-II-1)	1282(4-II-3)	740(5-I-2)	-439(4-II-1)
172	8	-1.79(4-II-3)	-2.06(5-I-2)	1.63(4-II-1)	668(4-II-3)	849(5-I-2)	-664(4-II-1)
172	9	-3.28(4-II-3)	-2.10(5-I-2)	1.43(4-II-1)	1373(4-II-3)	919(5-I-2)	-835(4-II-1)
172	10	-4.50(1)	-1.99(5-I-2)	1.32(4-II-1)	1898(1)	936(5-I-2)	-839(5-I-2)
172	11	-5.83(1)	-1.96(2)	1.24(4-II-1)	2494(1)	1049(2)	-808(3)
172	12	-6.90(1)	-1.98(2)	1.21(4-II-1)	2983(1)	1187(2)	-735(5-I-2)
172	13	-7.69(1)	-1.97(2)	1.20(4-II-1)	3347(1)	1320(2)	-639(5-I-2)
172	14	-8.22(1)	-1.97(3)	1.16(4-II-1)	3595(1)	1454(2)	-531(5-I-2)
172	15	-8.50(1)	-2.00(3)	1.08(4-II-1)	3735(1)	1574(2)	-426(4-II-1)
172	16	-8.58(1)	-2.02(3)	0.90(4-II-1)	3770(1)	1655(2)	-316(4-II-1)
172	17	-8.50(1)	-2.33(3)	0.52(4-II-1)	3607(1)	1360(3)	-284(4-II-1)
172	18	-8.60(1)	-1.38(3)	-0.34(4-I-1)	3553(1)	172(3)	-254(4-II-1)
172	19	-8.69(1)	-1.79(3)	0.65(4-II-1)	3581(1)	-115(1)	-267(4-II-1)
173	1	-3.53(4-II-3)	-1.39(5-I-2)	1.37(4-II-1)	1748(1)	1524(5-I-2)	-1074(3)
173	2	-4.91(1)	-1.40(5-I-2)	1.57(4-II-1)	2275(1)	1419(2)	-1056(3)
173	3	-6.10(1)	-1.31(5-I-2)	1.73(4-II-1)	2713(1)	1269(2)	-1045(3)
173	4	-7.01(1)	-1.18(5-I-2)	1.81(3)	3049(1)	1103(3)	-1015(3)
173	5	-7.65(1)	-1.06(3)	1.93(3)	3279(1)	922(3)	-976(1)
173	6	-8.03(1)	-0.94(3)	1.98(1)	3405(1)	732(3)	-909(1)
173	7	-8.19(1)	-0.80(3)	1.91(1)	3441(1)	530(3)	-814(1)
173	8	-8.21(1)	-0.65(3)	1.73(1)	3418(1)	269(3)	-726(1)
173	9	-8.21(1)	-0.78(3)	1.92(1)	3402(1)	162(5-I-2)	-821(1)
173	10	-8.03(1)	-0.95(3)	2.05(1)	3346(1)	124(5-I-2)	-839(1)
173	11	-7.60(1)	-1.09(3)	2.11(1)	3205(1)	-93(5-II-2)	-806(3)
173	12	-6.89(1)	-1.23(3)	2.13(3)	2956(1)	-151(5-II-2)	-743(4-II-1)
173	13	-5.88(1)	-1.40(5-I-2)	2.13(3)	2599(1)	-214(5-II-2)	-700(4-II-1)
173	14	-4.57(1)	-1.57(5-I-2)	2.09(5-I-2)	2139(1)	-330(1)	-634(4-II-1)
173	15	-3.52(4-II-3)	-1.69(5-I-2)	2.09(4-II-1)	1690(4-II-3)	-598(1)	-550(4-II-1)
173	16	-2.83(4-II-3)	-1.62(5-I-2)	2.01(4-II-1)	1296(4-II-3)	-1329(1)	-532(4-II-1)
173	17	3.32(4-I-3)	4.43(5-II-2)	1.92(4-II-4)	-1993(4-I-3)	-2572(5-II-2)	1282(4-I-2)
173	18	-1.74(4-II-3)	2.24(5-II-2)	1.53(4-II-4)	-756(4-I-3)	1244(5-I-2)	-782(4-II-3)
173	19	-2.54(4-II-3)	-1.25(5-I-2)	1.22(4-II-1)	1253(4-II-3)	1721(5-I-2)	-1098(4-II-1)
174	1	-1.58(1)	-5.19(4-I-3)	1.67(4-II-3)	-540(4-II-3)	1826(4-I-3)	1162(1)
174	2	-2.71(1)	-5.01(2)	-1.50(4-I-3)	1201(1)	1688(4-I-3)	1083(1)
174	3	-3.92(1)	-5.36(2)	-1.61(1)	1734(1)	1803(2)	1097(1)
174	4	-4.99(1)	-5.54(2)	-2.11(1)	2108(1)	2049(2)	1131(1)
174	5	-5.58(1)	-5.50(1)	-2.43(1)	2436(1)	2293(1)	1032(1)
174	6	-4.98(1)	-5.18(1)	-2.23(1)	2084(1)	2605(1)	768(1)
174	7	-4.34(1)	-4.87(2)	-1.75(1)	1754(1)	2768(2)	484(4-I-3)
174	8	-3.53(1)	-4.38(4-I-3)	-1.26(4-I-3)	1416(1)	2947(2)	-600(4-II-3)
174	9	-2.58(1)	-4.52(4-I-3)	-1.02(4-I-3)	1131(1)	3183(2)	-1012(4-II-3)
174	10	-1.53(1)	-3.97(4-I-3)	-0.94(1)	1151(1)	3047(2)	-1309(4-II-3)
174	11	1.55(4-I-3)	-2.93(4-I-3)	-1.14(1)	1947(1)	2217(4-I-3)	-1516(3)
174	12	-2.99(4-II-3)	-3.00(4-I-3)	-0.53(1)	1841(1)	1238(2)	285(1)
174	13	5.97(4-I-3)	-4.50(4-I-3)	-1.08(1)	-2693(4-I-3)	-2390(4-II-3)	1008(1)
174	14	-0.87(1)	-6.97(4-I-3)	3.04(4-II-3)	-1484(3)	-3456(4-II-3)	1564(4-I-3)
175	1	-5.54(1)	-0.72(3)	-1.22(4-I-1)	2072(1)	991(3)	826(3)
175	2	-5.63(4-I-3)	0.29(5-II-1)	-1.72(4-I-3)	2222(4-I-3)	549(4-II-3)	901(4-I-4)
175	3	10.30(4-II-3)	1.24(4-I-3)	1.44(4-II-3)	-4594(4-II-3)	-530(4-I-3)	-647(4-II-3)
175	4	-5.86(4-I-3)	0.61(4-I-3)	-1.36(4-I-1)	2409(4-I-3)	-615(2)	-678(4-II-3)
175	5	-5.40(1)	-0.76(3)	-1.33(4-I-1)	2267(1)	-423(1)	-366(4-II-3)
175	6	-6.58(1)	-1.18(3)	-1.11(4-I-1)	2764(1)	-348(1)	247(4-I-1)
175	7	-7.42(1)	-1.42(3)	-0.85(4-I-1)	3161(1)	-296(1)	224(4-I-1)
175	8	-8.09(1)	-1.25(3)	-0.45(4-I-1)	3575(1)	140(5-I-2)	231(4-I-1)
175	9	-8.02(1)	-2.20(3)	0.47(4-II-1)	3601(1)	1344(3)	270(4-I-1)
175	10	-7.52(1)	-1.58(3)	-0.75(4-I-1)	3181(1)	1519(2)	378(4-I-1)
175	11	-6.70(1)	-1.19(3)	-0.98(4-I-1)	2673(1)	1293(3)	601(3)
176	1	-0.95(1)	-1.22(3)	-1.14(3)	546(4-II-1)	75(1)	-429(2)
176	2	1.98(4-II-4)	-0.93(3)	-0.74(3)	-390(1)	-353(4-I-4)	-422(3)
176	3	3.75(4-II-4)	-0.53(5-I-3)	0.17(1)	-511(1)	-304(4-I-1)	-351(3)
176	4	2.59(4-II-2)	-0.71(1)	0.51(1)	1362(1)	-327(1)	585(1)
176	5	1.02(4-II-4)	0.24(4-II-4)	0.60(1)	478(4-II-2)	-192(3)	130(4-II-1)
176	6	-1.16(1)	-1.43(3)	-1.34(2)	-532(1)	-1062(2)	-605(2)
176	7	1.73(4-II-4)	-1.10(3)	-0.59(3)	-415(1)	-500(3)	-364(3)
177	1	-9.07(2)	-5.12(2)	-1.78(2)	3899(2)	2021(1)	423(2)
177	2	-9.60(2)	-4.43(1)	-1.57(2)	4080(2)	1874(1)	543(2)
177	3	-8.85(2)	-4.19(1)	-1.97(2)	3727(2)	1896(1)	1161(3)
177	4	-6.35(1)	-4.26(1)	-2.03(2)	2810(1)	2810(1)	1491(3)
177	5	-5.51(1)	-3.29(1)	-3.14(2)	2175(1)	1899(1)	2279(3)
177	6	-5.46(1)	-2.57(1)	-2.92(2)	1076(1)	1342(1)	1400(3)
177	7	-5.26(1)	-2.37(1)	-3.02(2)	-1260(5-I-1)	499(1)	909(2)
177	8	-5.11(1)	-2.39(1)	-2.85(2)	1791(1)	370(1)	219(1)
177	9	-6.18(1)	-5.05(1)	-3.10(3)	2810(1)	1149(1)	780(2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
177	10	-5.86(1)	-3.58(1)	-2.88(2)	2525(1)	1717(1)	1398(2)
178	1	-0.21(5-I-2)	-2.09(2)	-1.21(3)	425(3)	79(3)	-77(3)
178	2	0.54(5-II-1)	-2.35(3)	-0.79(4-II-1)	60(5-I-3)	-21(5-II-3)	45(4-I-1)
178	3	0.50(4-II-1)	-2.42(3)	0.44(3)	-51(5-II-2)	-19(5-II-2)	30(4-I-4)
178	4	-0.96(1)	-1.65(3)	1.40(4-II-1)	365(3)	111(3)	83(3)
178	5	-0.28(4-II-1)	-1.15(2)	-1.04(4-II-2)	116(3)	93(3)	-79(3)
178	6	0.25(5-II-1)	-1.75(3)	-0.69(4-II-1)	48(5-I-3)	34(5-I-3)	28(4-I-4)
178	7	0.31(4-II-1)	-1.81(3)	0.40(3)	43(3)	-8(5-II-2)	56(4-I-4)
178	8	-0.41(1)	-0.98(4-II-1)	0.95(4-II-1)	86(3)	98(3)	101(3)
178	9	0.20(2)	-0.50(4-II-2)	-0.79(4-II-1)	13(4-I-2)	109(3)	-61(3)
178	10	-0.07(5-I-3)	-1.49(4-II-1)	-0.51(4-II-1)	32(3)	54(3)	22(4-I-4)
178	11	-0.14(4-I-1)	-1.77(4-II-1)	0.26(5-II-3)	35(3)	24(3)	65(3)
178	12	-0.16(1)	-0.89(4-II-1)	0.58(4-II-1)	-17(5-II-1)	68(4-II-1)	72(3)
178	13	0.39(2)	0.82(2)	-0.62(2)	-6(1)	155(3)	-71(3)
178	14	-0.13(4-II-1)	-1.66(4-II-1)	-0.15(4-II-1)	13(3)	69(3)	19(4-I-4)
178	15	-0.15(4-II-1)	-1.98(4-II-1)	0.10(5-II-3)	9(3)	37(3)	62(3)
178	16	-0.14(2)	-1.07(4-II-1)	0.17(4-II-1)	-20(3)	51(4-II-1)	46(3)
179	1	-1.40(3)	-0.14(1)	-1.42(3)	122(4-II-1)	44(4-II-1)	56(4-II-2)
179	2	-1.64(3)	0.20(5-I-3)	-1.87(3)	166(4-II-1)	79(4-II-1)	74(4-II-2)
179	3	-1.12(3)	0.73(3)	-2.14(3)	200(4-II-1)	58(4-II-1)	128(4-II-1)
179	4	2.52(3)	2.74(3)	-3.21(3)	-164(4-I-1)	-90(4-II-1)	129(4-II-1)
179	5	-0.98(3)	1.94(3)	-1.38(3)	69(4-II-1)	56(4-II-1)	91(4-II-2)
179	6	-1.09(3)	1.79(3)	-1.95(3)	67(4-II-1)	60(4-II-1)	112(4-II-2)
179	7	-0.58(3)	1.86(3)	-2.70(3)	-37(4-I-1)	56(3)	120(4-II-1)
179	8	1.71(3)	0.72(3)	-2.20(3)	-109(2)	76(4-I-1)	25(3)
179	9	-0.47(3)	3.70(3)	-1.10(3)	29(4-II-1)	67(4-II-1)	88(4-II-2)
179	10	-0.53(3)	3.02(3)	-1.64(3)	12(4-II-1)	62(4-II-1)	93(4-II-2)
179	11	-0.25(4-II-1)	1.97(3)	-2.00(3)	-36(4-II-1)	49(4-I-3)	75(4-II-2)
179	12	0.61(3)	0.59(3)	-1.36(3)	-65(4-II-1)	-121(4-II-2)	-9(5-II-3)
179	13	-0.07(3)	5.61(3)	-0.44(3)	6(4-II-1)	73(4-II-1)	73(4-II-2)
179	14	-0.06(2)	4.19(3)	-0.67(3)	-2(1)	56(4-II-1)	73(4-II-2)
179	15	-0.11(1)	2.31(3)	-0.76(3)	-16(4-II-1)	53(4-I-2)	49(4-II-2)
179	16	-0.17(3)	0.58(3)	-0.51(3)	-57(4-II-1)	-151(4-II-2)	-30(5-II-3)
180	1	0.77(3)	-2.52(3)	0.34(5-II-1)	108(2)	132(3)	-62(4-II-2)
180	2	1.30(3)	-1.82(3)	0.83(3)	136(2)	42(3)	-33(4-II-1)
180	3	1.49(3)	-1.39(3)	0.79(3)	135(2)	16(3)	18(4-I-1)
180	4	1.64(3)	-1.10(3)	0.38(3)	132(2)	4(3)	16(4-I-1)
180	5	-0.51(1)	-2.08(3)	-0.28(5-I-1)	56(2)	107(3)	44(4-I-1)
180	6	0.61(3)	-1.64(3)	-0.14(5-I-1)	87(2)	89(2)	41(4-I-1)
180	7	1.61(3)	-1.25(3)	0.18(5-II-1)	112(2)	44(3)	42(4-I-1)
180	8	2.77(3)	-1.06(3)	0.07(5-II-1)	128(2)	8(3)	38(4-I-1)
180	9	-0.95(3)	-1.75(3)	-0.63(3)	87(2)	208(2)	167(3)
180	10	0.24(5-II-1)	-1.40(3)	-0.36(3)	147(2)	64(2)	102(3)
180	11	1.34(3)	-1.16(1)	-0.23(3)	138(2)	23(2)	75(3)
180	12	2.68(3)	-1.02(1)	-0.05(3)	132(2)	6(2)	62(3)
180	13	-2.06(3)	-1.13(1)	-0.13(3)	11(4-II-4)	-47(3)	129(3)
180	14	-0.45(5-I-1)	-1.23(1)	-0.30(3)	-12(3)	-20(4-I-1)	38(4-I-1)
180	15	1.11(5-II-1)	-1.13(1)	-0.26(3)	-24(3)	-11(4-I-1)	44(3)
180	16	2.11(3)	-1.07(3)	-0.11(3)	-27(3)	-3(4-I-1)	42(3)
181	1	1.79(3)	2.28(3)	1.71(3)	153(2)	-235(5-II-3)	213(3)
181	2	0.62(3)	1.12(3)	1.64(3)	145(5-II-3)	55(3)	84(3)
181	3	0.25(1)	0.18(1)	1.35(3)	61(5-II-3)	-124(2)	66(3)
181	4	-0.13(5-II-2)	-0.67(2)	1.10(2)	-189(2)	-291(2)	-78(2)
181	5	0.51(5-I-3)	-0.87(2)	1.44(3)	-143(2)	-349(2)	176(3)
181	6	0.92(3)	-0.41(2)	2.15(3)	-152(2)	-73(2)	85(3)
181	7	0.64(3)	-0.43(2)	1.89(3)	-94(2)	-199(2)	-54(2)
181	8	0.48(1)	-0.33(2)	1.20(2)	-85(2)	-461(2)	92(3)
181	9	-0.70(5-II-3)	-1.30(2)	1.19(3)	-163(2)	-342(2)	107(3)
181	10	0.60(3)	-1.27(2)	1.98(3)	-179(2)	-167(2)	164(3)
181	11	1.01(3)	-0.74(2)	1.81(3)	-103(2)	-273(2)	108(3)
181	12	1.26(3)	-0.45(2)	1.21(2)	-75(2)	-451(2)	122(3)
181	13	-1.65(2)	-1.89(2)	1.80(3)	89(1)	-127(2)	114(3)
181	14	0.46(3)	-1.32(2)	1.59(3)	-51(4-II-2)	-214(2)	180(3)
181	15	1.28(3)	-0.92(2)	1.47(3)	-58(2)	-323(2)	138(3)
181	16	1.91(3)	-0.49(2)	1.06(2)	-66(2)	-473(2)	143(3)
182	1	0.18(5-I-3)	-1.07(3)	0.88(3)	36(4-II-1)	76(4-II-2)	-38(4-II-2)
182	2	2.25(3)	-0.67(3)	0.80(3)	44(4-II-2)	54(4-II-2)	-60(4-II-2)
182	3	4.45(3)	-0.30(3)	0.58(3)	56(4-II-2)	30(4-II-2)	-63(4-II-2)
182	4	6.84(3)	0.03(3)	0.21(3)	64(4-II-2)	8(4-II-2)	-57(4-II-2)
182	5	0.14(5-I-3)	-0.76(3)	0.32(3)	57(3)	72(2)	37(4-I-4)
182	6	2.55(3)	-0.49(3)	0.27(5-II-1)	56(3)	42(2)	34(4-I-4)
182	7	5.00(3)	-0.21(3)	0.18(5-II-1)	63(2)	22(4-II-2)	35(4-I-4)
182	8	7.53(3)	0.09(3)	0.06(5-II-1)	67(2)	5(4-II-2)	31(4-I-4)
182	9	0.29(3)	-0.61(3)	0.08(4-I-2)	58(3)	72(3)	53(4-I-1)
182	10	2.71(3)	-0.41(3)	-0.11(4-II-2)	57(3)	32(2)	45(4-I-1)
182	11	5.13(3)	-0.18(2)	-0.10(4-II-2)	58(3)	13(5-I-4)	43(4-I-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
182	12	7.60(3)	0.05(3)	-0.04(4-II-2)	58(3)	3(5-I-1)	38(4-I-1)
182	13	0.53(3)	-0.44(3)	-0.21(2)	16(5-I-4)	25(5-I-1)	69(4-I-1)
182	14	2.73(3)	-0.31(3)	-0.23(2)	20(5-I-4)	-28(5-II-1)	52(4-I-1)
182	15	5.00(3)	-0.15(3)	-0.18(4-II-3)	23(5-I-1)	-18(5-II-1)	43(4-I-1)
182	16	7.36(3)	-0.03(1)	-0.06(4-II-3)	24(5-I-1)	-5(5-II-1)	37(4-I-1)
183	1	0.66(5-I-3)	5.85(5-I-3)	0.69(5-I-3)	471(4-II-1)	-7760(4-I-1)	192(4-II-2)
183	2	0.29(5-I-3)	-5.61(5-II-3)	-0.07(4-II-1)	58(4-I-1)	-7092(4-I-1)	240(4-I-1)
183	3	-0.06(4-I-1)	4.17(5-I-3)	0.76(5-I-3)	19(4-I-1)	-5316(4-I-1)	-126(4-I-3)
183	4	0.31(5-I-3)	0.89(5-I-3)	0.53(5-I-3)	62(4-I-1)	-1562(4-I-1)	-320(4-I-1)
183	5	0.65(5-I-3)	-4.76(5-II-3)	0.27(5-II-1)	-671(4-I-1)	-7734(4-I-1)	176(4-I-1)
183	6	0.25(5-II-1)	-4.71(5-II-3)	0.18(4-I-1)	-128(4-I-1)	-7149(4-I-1)	379(4-I-1)
183	7	-1.07(5-I-3)	-4.45(5-II-3)	-1.78(5-II-3)	-101(4-II-1)	-5783(4-I-1)	-288(4-I-3)
183	8	1.70(5-I-3)	-1.45(5-II-3)	2.01(5-I-3)	511(4-I-1)	-1906(4-I-1)	-1020(4-I-1)
183	9	-0.19(5-II-3)	-3.89(5-II-3)	-0.82(5-I-1)	-865(4-I-1)	-7668(4-I-1)	307(4-I-1)
183	10	0.60(5-II-1)	-3.73(5-II-3)	-0.44(5-I-1)	-404(4-I-1)	-7164(4-I-1)	564(4-I-1)
183	11	-2.32(5-I-3)	-5.07(5-II-3)	-1.70(5-II-3)	-124(4-II-1)	-6697(4-I-1)	-315(4-I-3)
183	12	-3.09(5-II-3)	3.80(5-I-3)	4.28(5-I-3)	1417(4-I-1)	-3371(4-I-1)	-2023(4-I-1)
183	13	-0.62(2)	-2.54(5-II-3)	-1.30(2)	-980(4-I-1)	-7580(4-I-1)	317(4-I-1)
183	14	1.24(5-II-1)	-2.96(5-II-3)	-0.82(5-I-1)	-892(4-I-1)	-7163(4-I-1)	676(4-I-1)
183	15	-4.98(5-I-3)	-4.89(5-II-3)	-0.60(5-I-1)	-624(4-II-1)	-7902(4-I-1)	-223(5-II-4)
183	16	-0.56(5-I-1)	-9.69(5-II-3)	-5.56(5-I-3)	2216(4-I-1)	-8817(4-I-1)	-4704(4-I-1)
184	1	3.10(3)	5.75(3)	3.84(3)	-476(2)	-507(2)	-238(2)
184	2	1.18(3)	1.07(3)	0.16(3)	98(2)	-45(4-II-2)	68(3)
184	3	0.25(3)	0.19(3)	0.07(3)	-11(2)	17(4-I-2)	34(3)
184	4	-0.05(3)	-0.02(5-I-1)	-0.02(3)	11(3)	7(4-I-2)	10(3)
184	5	3.94(3)	1.18(3)	2.50(3)	50(3)	-176(4-II-2)	-93(4-II-2)
184	6	0.59(3)	1.60(3)	1.55(3)	82(2)	-46(4-II-2)	101(3)
184	7	0.27(3)	0.37(3)	0.48(3)	39(3)	-13(4-I-2)	39(3)
184	8	0.17(3)	-0.02(5-I-1)	0.11(3)	33(3)	6(4-I-2)	19(3)
184	9	3.29(3)	-0.62(1)	1.57(3)	229(2)	65(4-I-2)	-94(4-II-2)
184	10	1.04(3)	0.53(3)	1.75(3)	157(2)	-63(4-II-2)	56(3)
184	11	0.37(3)	0.26(3)	0.87(3)	79(2)	-12(4-II-2)	37(3)
184	12	0.12(3)	0.02(5-II-2)	0.19(3)	61(3)	-4(4-II-2)	17(3)
184	13	2.49(3)	-1.27(3)	0.93(3)	322(2)	152(3)	-106(2)
184	14	1.41(3)	-0.54(1)	1.60(3)	182(2)	-33(4-II-2)	-15(4-II-2)
184	15	0.97(3)	-0.35(1)	1.06(3)	111(2)	-17(4-II-2)	26(3)
184	16	0.57(3)	-0.43(3)	0.27(3)	84(3)	-5(4-II-2)	14(3)
185	1	-0.43(5-II-3)	-1.89(2)	1.68(3)	114(1)	170(1)	34(5-II-2)
185	2	0.75(3)	-1.59(2)	1.24(3)	95(1)	-232(2)	149(3)
185	3	1.40(3)	-0.97(2)	1.19(3)	-30(4-II-2)	-351(2)	130(3)
185	4	2.21(3)	-0.49(2)	0.90(2)	-57(2)	-489(2)	154(3)
185	5	-0.19(2)	-1.81(2)	1.44(5-II-1)	81(1)	157(1)	44(5-II-2)
185	6	0.65(3)	-1.38(2)	1.13(3)	81(1)	-232(2)	97(3)
185	7	1.52(3)	-0.94(2)	1.01(3)	22(4-I-2)	-358(2)	121(3)
185	8	2.47(3)	-0.51(2)	0.78(3)	-45(2)	-494(2)	146(3)
185	9	-0.09(2)	-1.78(2)	1.24(5-II-1)	49(1)	127(1)	62(3)
185	10	0.70(3)	-1.28(2)	1.00(5-II-1)	56(1)	-218(2)	81(3)
185	11	1.60(3)	-0.87(2)	0.86(3)	24(4-I-2)	-361(2)	107(3)
185	12	2.61(3)	-0.49(2)	0.68(3)	-34(2)	-494(2)	138(3)
185	13	-0.09(2)	-1.67(2)	1.02(5-II-1)	30(1)	105(1)	69(3)
185	14	0.76(3)	-1.21(2)	0.90(5-II-1)	36(3)	-214(2)	77(3)
185	15	1.68(3)	-0.83(2)	0.72(5-II-1)	20(4-I-2)	-358(2)	97(3)
185	16	2.72(3)	-0.48(2)	0.60(3)	-27(2)	-492(2)	128(3)
186	1	2.03(5-I-3)	-4.01(5-I-3)	1.49(3)	-753(4-I-1)	-6243(4-I-1)	415(4-I-1)
186	2	1.69(5-I-3)	-4.46(5-I-3)	1.55(3)	-541(4-I-1)	-5684(4-I-1)	1135(4-I-1)
186	3	0.97(3)	-8.25(5-I-3)	1.45(3)	208(4-II-1)	-5475(4-I-1)	2245(4-I-1)
186	4	-6.64(5-I-3)	-12.01(5-I-3)	4.51(5-I-3)	290(5-II-4)	-6182(4-I-1)	3514(4-I-1)
186	5	-0.66(1)	-2.32(3)	-1.08(5-II-3)	608(4-II-1)	-4290(4-I-1)	362(4-I-1)
186	6	0.73(5-II-1)	-1.76(3)	1.58(5-I-3)	785(4-II-1)	-3495(4-I-1)	845(4-I-1)
186	7	2.31(5-II-1)	-1.00(5-II-1)	1.46(5-I-3)	1253(4-II-1)	-2078(4-I-1)	1280(4-I-1)
186	8	3.04(5-II-1)	-0.76(1)	-0.21(5-I-1)	1675(4-II-1)	-590(3)	1020(4-I-1)
186	9	-1.01(1)	-2.01(3)	-1.46(5-II-3)	-562(4-I-1)	-4096(4-I-1)	309(4-II-3)
186	10	0.13(4-I-1)	-1.63(3)	-1.66(5-II-3)	740(4-II-1)	-3274(4-I-1)	558(4-II-3)
186	11	1.11(3)	-1.00(1)	-1.38(5-II-3)	1141(4-II-1)	-1939(4-I-1)	842(4-II-2)
186	12	2.51(3)	-0.78(5-II-3)	-0.31(5-I-3)	1492(4-II-1)	-601(1)	643(4-II-2)
186	13	-0.94(5-I-3)	-2.99(5-II-1)	-1.68(3)	-550(4-I-1)	-5103(4-I-1)	288(4-II-3)
186	14	-1.13(5-I-1)	-3.82(5-II-3)	-1.52(3)	-294(4-I-4)	-4792(4-I-1)	578(4-II-3)
186	15	1.48(5-II-1)	-7.25(5-II-3)	-1.31(3)	-225(4-II-1)	-4872(4-I-1)	1473(4-II-2)
186	16	4.37(5-I-3)	-10.55(5-II-3)	-3.90(5-II-3)	-597(4-II-1)	-5604(4-I-1)	2717(4-II-2)
187	1	-0.65(4-I-2)	-2.18(4-II-1)	1.70(2)	-708(4-I-1)	-5585(4-I-1)	282(3)
187	2	-1.11(5-II-3)	-2.91(5-I-3)	1.12(2)	-436(4-I-1)	-5510(4-I-1)	311(4-I-1)
187	3	3.01(5-I-3)	-5.59(5-I-3)	0.92(2)	-819(4-II-2)	-6080(4-I-1)	1401(4-I-1)
187	4	-5.09(5-I-1)	-11.17(5-I-3)	5.45(5-I-3)	2135(4-I-3)	-6428(4-I-1)	4312(4-I-1)
187	5	-0.58(4-I-2)	-2.89(5-I-3)	1.03(5-I-1)	382(4-II-1)	-5349(4-I-1)	323(4-I-1)
187	6	0.57(5-I-3)	-2.95(5-I-3)	1.47(5-I-1)	-79(5-I-4)	-4784(4-I-1)	658(4-I-1)
187	7	0.66(5-II-1)	-3.10(5-I-3)	2.82(5-I-1)	-237(4-II-3)	-3684(4-I-1)	1735(4-I-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
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R.37.12

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
187	8	3.11 (5-II-1)	-0.19 (5-I-3)	1.76 (5-I-3)	-506 (4-II-3)	-888 (4-I-1)	2044 (4-I-1)
187	9	0.54 (5-II-1)	-2.60 (5-I-3)	1.12 (5-I-1)	324 (4-II-1)	-5006 (4-I-1)	513 (4-I-1)
187	10	0.69 (5-II-1)	-2.35 (5-I-3)	-1.79 (5-II-1)	-77 (5-I-4)	-4135 (4-I-1)	827 (4-I-1)
187	11	0.61 (5-II-1)	-1.41 (5-I-3)	-1.53 (5-II-1)	-134 (4-I-1)	-2634 (4-I-1)	1319 (4-I-1)
187	12	1.20 (5-II-1)	-0.11 (5-I-3)	-0.65 (5-II-1)	-344 (4-I-1)	-688 (4-I-1)	1239 (4-I-1)
187	13	1.99 (5-II-1)	3.35 (5-II-1)	-1.97 (5-II-1)	315 (4-II-1)	-4868 (4-I-1)	648 (4-I-1)
187	14	0.10 (5-II-1)	2.05 (5-II-1)	-0.97 (5-II-1)	-38 (4-II-4)	-3806 (4-I-1)	613 (4-I-1)
187	15	-0.06 (5-I-1)	0.88 (5-II-1)	-0.61 (5-II-1)	-77 (4-I-1)	-2294 (4-I-1)	699 (4-I-1)
187	16	0.17 (5-II-1)	-0.13 (5-I-1)	-0.18 (5-II-1)	-213 (4-I-1)	-584 (4-I-1)	466 (4-I-1)
188	1	0.17 (3)	-1.45 (2)	0.67 (5-II-1)	18 (3)	-116 (2)	85 (3)
188	2	0.91 (3)	-1.06 (2)	0.58 (5-II-1)	16 (3)	-220 (2)	94 (3)
188	3	1.75 (3)	-0.72 (2)	0.48 (5-II-1)	13 (3)	-352 (2)	107 (3)
188	4	2.73 (3)	-0.46 (2)	0.39 (5-II-1)	-18 (2)	-484 (2)	121 (3)
188	5	0.24 (5-II-1)	-0.94 (2)	-0.30 (5-I-1)	27 (3)	175 (3)	102 (3)
188	6	0.93 (3)	-0.80 (2)	-0.27 (5-I-1)	29 (3)	-206 (2)	132 (3)
188	7	1.66 (3)	-0.60 (2)	0.22 (5-II-1)	38 (3)	-325 (2)	151 (3)
188	8	2.43 (3)	-0.48 (2)	0.22 (5-II-1)	37 (3)	-458 (2)	157 (3)
188	9	0.25 (5-II-1)	-0.75 (2)	-0.27 (5-I-1)	32 (3)	335 (3)	109 (3)
188	10	0.93 (5-II-1)	-0.67 (2)	-0.22 (5-I-1)	36 (3)	232 (3)	196 (3)
188	11	1.63 (5-II-1)	-0.52 (2)	-0.14 (5-I-1)	62 (3)	-259 (2)	246 (3)
188	12	2.35 (5-II-1)	-0.43 (2)	0.11 (5-II-1)	67 (3)	-454 (2)	233 (3)
188	13	-0.15 (5-I-1)	-1.09 (2)	-0.51 (1)	245 (3)	878 (3)	319 (3)
188	14	0.75 (5-II-1)	-0.86 (2)	0.12 (4-II-3)	293 (3)	386 (3)	266 (2)
188	15	1.67 (5-II-1)	-0.65 (2)	-0.09 (1)	207 (3)	-208 (2)	266 (2)
188	16	2.53 (5-II-1)	-0.35 (2)	-0.15 (1)	121 (3)	-482 (2)	226 (2)
189	1	-2.84 (1)	-0.97 (2)	-0.78 (1)	474 (3)	935 (3)	201 (3)
189	2	0.59 (4-II-2)	-0.83 (2)	-0.34 (1)	337 (3)	413 (3)	103 (2)
189	3	1.76 (5-II-1)	-0.71 (2)	-0.28 (1)	178 (3)	-202 (2)	167 (2)
189	4	2.80 (5-II-1)	-0.44 (2)	-0.41 (3)	83 (3)	-487 (2)	132 (2)
189	5	-1.24 (1)	-0.62 (5-II-1)	0.59 (2)	-73 (2)	417 (3)	429 (3)
189	6	0.66 (4-II-2)	-0.85 (2)	-0.38 (5-II-1)	-67 (2)	374 (3)	142 (2)
189	7	1.83 (5-II-1)	-0.67 (2)	-0.48 (5-II-1)	58 (3)	-188 (2)	169 (2)
189	8	2.92 (5-II-1)	-0.44 (2)	-0.62 (3)	23 (5-I-1)	-468 (2)	108 (2)
189	9	-0.46 (1)	-1.13 (5-II-1)	0.59 (2)	-47 (5-I-1)	422 (5-II-1)	359 (2)
189	10	1.06 (5-II-1)	-0.87 (2)	-0.39 (5-II-1)	-77 (2)	294 (3)	291 (2)
189	11	1.99 (5-II-1)	-0.70 (2)	-0.70 (5-II-1)	-41 (2)	-220 (2)	227 (2)
189	12	2.95 (5-II-1)	-0.44 (2)	-0.80 (3)	-47 (2)	-474 (2)	110 (2)
189	13	0.66 (4-II-3)	-1.46 (2)	0.50 (5-I-1)	52 (5-II-1)	544 (3)	337 (2)
189	14	1.49 (3)	-1.01 (2)	-0.69 (5-II-1)	-45 (2)	202 (5-II-1)	338 (2)
189	15	2.27 (3)	-0.68 (2)	-0.93 (5-II-1)	-58 (2)	-310 (2)	268 (2)
189	16	3.05 (3)	-0.45 (2)	-0.94 (3)	-83 (2)	-496 (2)	108 (2)
190	1	1.06 (3)	-1.50 (2)	-0.59 (5-II-1)	77 (5-II-1)	686 (3)	323 (2)
190	2	1.82 (3)	-0.89 (2)	-1.03 (5-II-1)	-92 (2)	148 (5-II-1)	347 (2)
190	3	2.43 (3)	-0.52 (2)	-1.11 (5-II-1)	-138 (2)	-413 (2)	280 (2)
190	4	3.20 (3)	-0.42 (2)	-1.03 (5-II-1)	-155 (2)	-526 (2)	78 (2)
190	5	1.58 (3)	-1.18 (2)	-0.89 (5-II-1)	-25 (5-I-1)	786 (3)	285 (3)
190	6	1.98 (3)	-0.51 (2)	-1.31 (5-II-1)	-240 (2)	93 (5-II-1)	314 (2)
190	7	2.42 (3)	-0.25 (2)	-1.15 (5-II-1)	-344 (2)	-497 (2)	284 (2)
190	8	3.32 (3)	-0.36 (2)	-0.98 (5-II-1)	-330 (2)	-565 (2)	95 (2)
190	9	2.20 (3)	-0.42 (4-I-4)	-1.19 (5-II-1)	-206 (2)	823 (3)	209 (3)
190	10	1.96 (3)	0.48 (5-II-1)	-1.46 (5-II-1)	-547 (2)	-121 (2)	198 (2)
190	11	2.29 (3)	0.30 (3)	-0.96 (5-II-1)	-801 (2)	-529 (2)	272 (2)
190	12	3.59 (2)	-0.31 (2)	-0.77 (5-II-1)	-747 (2)	-636 (2)	178 (2)
190	13	2.99 (3)	2.43 (5-II-1)	-1.28 (5-II-1)	-542 (3)	778 (3)	84 (5-I-4)
190	14	1.66 (3)	1.10 (5-II-1)	-0.93 (5-II-1)	-1081 (3)	-185 (2)	-62 (1)
190	15	1.94 (3)	0.29 (4-II-3)	-0.67 (5-II-1)	-1601 (3)	-559 (2)	73 (2)
190	16	4.35 (2)	-0.18 (4-I-3)	-0.36 (5-II-1)	-1707 (2)	-666 (2)	312 (2)
191	1	2.77 (3)	1.20 (4-II-2)	0.63 (2)	-351 (3)	647 (5-II-1)	-376 (3)
191	2	1.91 (3)	0.89 (4-II-2)	0.58 (4-II-3)	-899 (3)	-120 (2)	-446 (1)
191	3	2.03 (3)	0.33 (4-II-2)	-0.31 (4-I-3)	-1368 (2)	-333 (2)	-459 (1)
191	4	3.58 (2)	0.23 (2)	-0.27 (4-I-3)	-1860 (2)	-203 (2)	-299 (1)
191	5	1.67 (3)	-1.83 (4-I-2)	-0.40 (5-II-3)	-192 (1)	353 (5-II-3)	-643 (3)
191	6	2.31 (3)	-1.18 (4-I-2)	0.70 (4-II-3)	-355 (1)	-133 (1)	-786 (1)
191	7	2.54 (3)	-0.49 (4-I-2)	-0.70 (4-I-3)	-513 (2)	-155 (2)	-764 (1)
191	8	3.55 (2)	-0.13 (2)	-0.37 (4-I-3)	-617 (2)	-66 (2)	-642 (1)
191	9	1.68 (4-I-2)	-2.15 (3)	-1.01 (5-II-3)	-144 (1)	-614 (1)	-700 (3)
191	10	2.15 (3)	-1.26 (4-I-2)	-1.28 (4-I-3)	322 (4-II-3)	-170 (1)	-770 (1)
191	11	2.42 (3)	-0.74 (4-I-2)	-1.27 (4-I-3)	611 (4-II-3)	116 (4-II-3)	-775 (1)
191	12	4.05 (4-II-3)	-0.08 (1)	-0.61 (4-I-3)	772 (4-II-3)	68 (4-II-3)	-661 (1)
191	13	3.40 (4-I-2)	-1.99 (5-II-3)	-2.05 (3)	331 (3)	-746 (1)	-425 (4-I-3)
191	14	1.91 (4-I-2)	-1.52 (5-II-3)	-1.52 (4-I-2)	812 (4-II-3)	146 (4-II-3)	-668 (4-I-3)
191	15	1.94 (2)	-0.74 (5-II-3)	-1.47 (4-I-2)	1595 (4-II-3)	294 (4-II-3)	-810 (4-I-3)
191	16	4.82 (4-II-3)	-0.36 (4-I-3)	-0.99 (4-I-3)	2420 (4-II-3)	185 (4-II-3)	-793 (4-I-3)
192	1	-3.89 (3)	2.59 (5-II-3)	1.97 (1)	-371 (4-I-3)	-3441 (4-I-3)	219 (3)
192	2	-4.09 (5-II-3)	-3.68 (5-I-3)	1.65 (1)	-184 (1)	-3148 (4-I-3)	369 (4-I-1)
192	3	-4.40 (3)	-7.99 (5-I-3)	1.41 (1)	-473 (4-II-3)	-3117 (4-I-3)	992 (4-I-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
192	4	-9.15(5-I-1)	-10.84(5-I-3)	4.55(5-I-3)	-796(4-II-3)	-3455(4-I-3)	1825(4-I-2)
192	5	-2.26(3)	-0.83(1)	3.22(5-I-3)	-481(4-I-3)	-2589(4-I-3)	174(4-I-2)
192	6	-2.69(3)	-0.48(1)	2.98(5-I-3)	-611(4-I-3)	-1842(4-I-3)	500(4-I-3)
192	7	-3.31(4-II-3)	-0.40(5-II-3)	2.07(5-I-3)	-838(4-I-3)	-931(4-I-3)	745(4-I-3)
192	8	-4.14(4-II-3)	-0.50(5-I-1)	0.57(5-II-3)	-1092(4-I-3)	-87(4-II-1)	710(4-I-3)
192	9	-2.03(3)	-2.14(1)	2.80(5-I-1)	-277(4-I-3)	-1874(4-I-3)	-292(3)
192	10	-2.72(5-II-3)	-1.27(1)	2.61(5-I-1)	-352(4-I-3)	-1420(4-I-3)	-216(4-I-3)
192	11	-3.70(5-II-3)	-0.65(5-I-3)	1.89(5-I-1)	-538(4-I-3)	-711(4-I-3)	-316(4-I-3)
192	12	5.46(1)	0.40(5-I-1)	0.68(5-II-3)	-766(4-I-3)	-213(4-II-3)	-268(4-I-3)
192	13	-1.05(5-I-1)	-4.41(1)	-2.31(1)	148(4-II-3)	-1296(4-I-3)	-476(4-II-3)
192	14	1.65(1)	-5.20(5-II-1)	-2.49(1)	229(4-I-3)	-1878(4-I-3)	-516(4-II-3)
192	15	2.15(1)	-9.25(5-II-1)	-2.26(1)	564(4-I-3)	-2755(4-I-3)	-314(4-I-3)
192	16	-9.12(5-II-3)	-11.88(5-II-1)	-4.86(5-II-1)	822(4-I-3)	-4013(4-I-3)	-1500(4-I-3)
193	1	-5.17(4-II-2)	-2.07(4-II-1)	-3.55(3)	1379(4-I-2)	-528(4-II-3)	298(4-I-3)
193	2	-3.66(5-II-1)	-1.96(1)	-3.90(3)	2283(4-I-2)	-277(4-II-2)	-429(4-II-3)
193	3	-3.81(5-II-1)	-1.78(1)	-4.49(3)	2958(4-I-3)	335(4-I-3)	-410(4-II-3)
193	4	-3.19(5-II-1)	-1.82(1)	-4.94(3)	3384(4-I-3)	-472(4-II-3)	-420(4-II-3)
193	5	-3.28(4-II-2)	1.27(1)	-2.47(5-I-3)	902(4-I-3)	-872(4-I-3)	919(4-I-3)
193	6	-3.22(5-II-1)	-1.01(4-II-2)	-4.09(5-II-3)	1689(4-I-3)	-391(4-II-3)	-1187(4-II-3)
193	7	-4.03(5-II-1)	-1.55(5-I-1)	-4.36(3)	2679(4-I-3)	-129(4-I-1)	-1111(4-II-3)
193	8	-4.08(5-II-1)	-2.88(5-I-1)	-4.50(3)	3563(4-I-3)	-358(4-II-3)	-652(4-II-3)
193	9	-1.61(4-II-3)	1.52(1)	-1.74(5-II-3)	-696(4-II-3)	-1609(4-II-3)	1389(4-I-3)
193	10	-1.72(5-II-1)	1.30(1)	-3.15(5-I-3)	-1115(4-II-3)	-642(4-II-3)	-1812(4-II-3)
193	11	-3.79(5-II-1)	-2.36(5-II-3)	-5.36(5-I-3)	2151(4-I-3)	-453(4-I-1)	-1995(4-II-3)
193	12	-7.45(5-II-1)	-5.07(5-I-1)	-3.84(3)	3991(4-I-3)	-911(4-I-4)	-1330(4-II-3)
193	13	0.35(4-I-3)	3.43(4-II-3)	-0.65(5-II-3)	-258(4-II-3)	-2133(4-II-3)	1447(4-I-3)
193	14	-0.07(1)	2.25(1)	-1.24(5-II-3)	-363(4-II-3)	-903(4-II-3)	-1820(4-II-3)
193	15	-0.24(4-I-3)	-5.26(5-II-3)	-2.70(5-II-3)	522(4-I-3)	-558(4-I-1)	-2395(4-II-3)
193	16	-13.20(5-II-3)	-10.48(5-II-3)	-7.83(5-II-3)	4025(4-I-3)	-2633(4-I-2)	-2962(4-II-3)
194	1	-2.97(5-I-1)	-0.55(5-I-3)	3.10(5-I-3)	546(4-I-3)	-410(4-II-3)	594(4-II-3)
194	2	-4.01(5-I-1)	0.65(1)	2.66(5-II-3)	287(4-I-3)	-257(4-I-3)	414(4-II-3)
194	3	-4.75(5-I-1)	1.19(1)	1.93(5-II-3)	161(5-I-2)	-100(2)	284(4-II-3)
194	4	-4.96(5-I-1)	1.66(1)	0.92(5-II-3)	-190(1)	-342(4-I-3)	103(4-II-2)
194	5	-3.26(5-I-1)	-2.31(5-II-3)	2.27(5-II-3)	2097(4-I-3)	-1066(4-II-3)	1064(4-II-3)
194	6	-3.98(5-I-1)	-0.97(5-II-3)	1.97(5-II-3)	1652(4-I-3)	-606(4-II-3)	918(4-II-3)
194	7	-5.07(5-I-1)	-0.72(5-II-3)	1.22(5-II-3)	1244(4-I-3)	-269(3)	769(4-II-3)
194	8	-6.12(5-I-1)	0.47(1)	1.20(4-II-3)	961(4-I-3)	-737(4-I-3)	-279(4-I-3)
194	9	-5.31(5-I-3)	-6.39(5-II-3)	1.16(4-II-3)	4371(4-I-3)	-749(4-I-3)	2109(4-II-3)
194	10	-6.04(5-I-1)	-3.26(5-II-3)	2.37(5-I-1)	3517(4-I-3)	-396(4-II-1)	2222(4-II-3)
194	11	-5.69(5-I-1)	-2.02(5-II-3)	2.82(5-I-1)	2726(4-I-3)	-898(4-II-3)	2170(4-II-3)
194	12	-5.44(5-I-1)	-0.83(5-II-3)	2.22(5-I-1)	1991(4-I-3)	-1358(4-II-3)	-1173(4-I-3)
194	13	-10.18(5-I-3)	-1.04(5-II-3)	7.20(5-I-1)	6287(4-I-3)	-4255(4-I-3)	-5368(4-I-3)
194	14	-5.66(5-I-1)	-3.17(5-I-1)	6.48(5-I-1)	2942(4-I-3)	-1680(4-I-3)	-3974(4-I-3)
194	15	-2.26(5-I-1)	-2.80(5-I-1)	4.07(5-I-1)	1758(4-I-3)	-1872(4-II-3)	-3194(4-I-3)
194	16	-1.00(4-I-3)	-2.00(5-I-1)	2.48(5-I-1)	1376(4-I-3)	-5446(4-II-3)	-1780(4-I-3)
195	1	-0.90(4-II-3)	-1.84(4-II-3)	-2.14(4-II-3)	-75(1)	-639(1)	183(4-II-3)
195	2	0.59(4-I-3)	-1.51(4-II-3)	-1.66(4-II-3)	-148(4-II-3)	-144(1)	280(4-II-3)
195	3	-0.87(4-II-3)	-0.61(4-II-3)	-1.04(4-II-3)	-228(4-II-3)	35(5-I-3)	262(4-II-3)
195	4	-1.58(4-II-3)	-0.35(4-I-3)	-0.39(4-II-3)	-256(4-II-3)	27(5-I-2)	181(4-II-3)
195	5	-0.44(4-II-3)	-0.58(1)	-1.76(4-II-3)	-50(1)	-320(4-I-3)	124(3)
195	6	-1.34(4-II-3)	-0.54(4-II-3)	-1.95(4-II-3)	-76(1)	-185(1)	193(5-I-1)
195	7	-2.18(4-II-3)	-0.46(4-II-3)	1.62(4-I-3)	-106(4-II-3)	-70(1)	199(5-I-1)
195	8	-3.41(4-II-3)	-0.36(4-I-3)	0.68(4-I-3)	-154(4-II-3)	-13(1)	171(5-I-1)
195	9	-0.40(4-I-3)	-0.63(4-II-3)	0.86(4-I-3)	-53(1)	350(4-II-3)	123(4-I-2)
195	10	-0.57(4-II-3)	-1.07(4-II-3)	1.75(4-I-3)	-146(4-II-3)	-190(1)	139(4-I-3)
195	11	-2.85(4-II-3)	-1.05(4-II-3)	2.53(4-I-3)	-273(4-II-3)	-88(5-II-1)	178(5-I-1)
195	12	-6.12(4-II-3)	-0.07(4-I-3)	1.22(4-I-3)	-372(4-II-3)	-40(4-II-3)	187(5-I-1)
195	13	-0.87(4-I-3)	-3.54(4-I-3)	0.53(4-II-2)	-136(4-II-3)	-538(1)	262(4-I-3)
195	14	-2.34(4-I-3)	-2.43(5-I-2)	-0.36(5-I-4)	-557(4-II-3)	-284(5-II-1)	409(4-I-3)
195	15	-0.32(5-I-4)	-1.70(5-I-1)	-1.93(4-II-3)	-1131(4-II-3)	-275(5-II-3)	449(4-I-3)
195	16	-10.83(4-II-3)	-1.32(4-II-3)	-2.41(4-II-3)	-1335(4-II-3)	-73(4-I-3)	174(5-I-1)
196	1	-1.40(4-II-2)	0.07(5-II-3)	1.26(5-II-3)	805(4-II-2)	60(1)	-237(4-II-2)
196	2	-1.78(1)	0.31(1)	1.02(5-II-3)	634(4-II-2)	93(4-II-1)	-374(4-II-3)
196	3	-1.79(4-II-3)	0.71(1)	-0.96(1)	292(1)	64(1)	-346(4-II-3)
196	4	1.70(1)	1.74(1)	-1.28(1)	461(4-I-3)	22(1)	-301(4-II-3)
196	5	-0.95(1)	0.48(1)	1.11(5-II-3)	128(4-II-1)	-392(4-II-3)	-160(4-II-3)
196	6	-1.07(4-II-3)	0.87(1)	0.96(5-I-3)	108(3)	138(1)	-509(4-II-3)
196	7	-1.06(4-II-3)	1.07(1)	-1.27(1)	104(3)	80(1)	-536(4-II-3)
196	8	0.95(1)	0.59(1)	-0.98(1)	59(1)	185(4-II-3)	-444(4-II-3)
196	9	-0.47(1)	1.10(1)	0.79(5-II-3)	65(4-I-3)	-695(4-II-3)	-245(4-II-3)
196	10	-0.46(4-II-3)	1.13(1)	-0.78(1)	-42(4-II-3)	-176(4-II-3)	-472(4-II-3)
196	11	-0.52(4-II-3)	0.87(1)	-0.96(1)	60(4-II-3)	102(4-II-2)	-501(4-II-3)
196	12	-0.56(4-II-3)	0.37(1)	-0.66(1)	157(4-II-3)	362(4-II-3)	-427(4-II-3)
196	13	-0.12(3)	2.18(1)	0.34(5-II-3)	-70(4-II-3)	-782(4-II-3)	-261(4-II-3)
196	14	-0.08(3)	1.63(1)	-0.38(1)	-34(4-II-3)	-254(4-II-3)	-371(4-II-3)
196	15	-0.08(4-II-3)	0.94(1)	-0.39(1)	20(4-II-3)	121(4-II-2)	-389(4-II-3)

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
196	16	-0.31(4-II-3)	0.43(5-I-3)	-0.31(1)	93(4-II-3)	528(4-II-3)	-294(4-II-3)
197	1	0.13(2)	0.01(2)	-0.09(2)	-9(3)	9(2)	6(3)
197	2	0.19(2)	0.32(2)	-0.32(2)	-9(3)	60(2)	13(3)
197	3	0.27(2)	0.72(2)	-0.65(2)	-9(3)	166(2)	16(3)
197	4	0.69(3)	1.21(2)	-1.06(2)	-67(3)	353(2)	-37(2)
197	5	0.72(2)	-0.03(2)	-0.21(2)	-20(3)	8(2)	9(3)
197	6	0.83(2)	-0.01(5-II-2)	-0.57(2)	-19(3)	55(2)	12(3)
197	7	0.94(3)	-0.05(5-II-2)	-0.85(2)	-16(3)	143(2)	-12(2)
197	8	0.93(3)	-0.05(5-II-2)	-1.03(2)	-17(3)	261(2)	-62(2)
197	9	1.41(2)	0.01(2)	-0.18(2)	-12(2)	7(2)	13(3)
197	10	1.38(2)	-0.03(2)	-0.51(2)	-5(2)	49(2)	15(3)
197	11	1.34(2)	-0.05(2)	-0.79(2)	10(2)	135(2)	16(3)
197	12	1.38(3)	-0.09(2)	-1.06(2)	32(2)	267(2)	-53(2)
197	13	2.02(2)	0.02(2)	-0.16(2)	9(1)	6(2)	18(3)
197	14	1.92(2)	-0.01(2)	-0.46(2)	13(1)	49(2)	23(3)
197	15	1.83(2)	-0.04(2)	-0.74(2)	26(2)	138(2)	24(3)
197	16	1.85(3)	-0.07(2)	-1.00(2)	52(2)	274(2)	-42(2)
198	1	2.45(2)	0.02(2)	-0.16(2)	19(1)	6(2)	20(3)
198	2	2.31(2)	0.01(4-II-3)	-0.44(2)	22(1)	50(2)	27(3)
198	3	2.19(2)	-0.04(2)	-0.69(2)	35(2)	141(2)	29(3)
198	4	2.20(3)	-0.10(2)	-0.91(2)	62(2)	280(2)	-38(2)
198	5	2.76(2)	0.00(3)	-0.15(2)	24(1)	7(2)	22(3)
198	6	2.56(2)	-0.01(2)	-0.42(2)	27(1)	51(2)	29(3)
198	7	2.41(2)	-0.05(2)	-0.64(2)	39(2)	143(2)	31(3)
198	8	2.40(3)	-0.10(2)	-0.85(2)	64(2)	284(2)	-32(2)
198	9	3.06(2)	0.01(3)	-0.15(2)	27(1)	7(2)	23(3)
198	10	2.80(2)	-0.04(2)	-0.38(2)	30(1)	52(2)	31(3)
198	11	2.62(2)	-0.07(2)	-0.61(2)	41(2)	145(2)	33(3)
198	12	2.58(3)	-0.12(2)	-0.79(2)	67(2)	286(2)	-27(2)
198	13	3.38(2)	-0.20(3)	-0.10(2)	29(1)	7(2)	23(3)
198	14	3.01(2)	-0.04(2)	-0.36(2)	32(1)	52(2)	32(3)
198	15	2.80(2)	-0.05(2)	-0.57(2)	42(2)	146(2)	32(3)
198	16	2.76(3)	-0.18(2)	-0.74(2)	66(2)	287(2)	-22(2)
199	1	4.10(2)	0.07(2)	-0.11(3)	18(1)	7(2)	31(3)
199	2	3.69(2)	0.03(3)	-0.32(3)	22(1)	49(2)	39(3)
199	3	3.32(2)	0.00(3)	-0.48(3)	33(2)	140(2)	38(3)
199	4	3.09(3)	0.02(3)	-0.59(3)	54(2)	278(2)	9(3)
199	5	5.24(2)	0.19(3)	-0.08(3)	-7(5-I-1)	6(2)	41(3)
199	6	4.51(2)	0.03(2)	-0.24(3)	9(5-II-1)	46(2)	52(3)
199	7	3.79(2)	-0.01(1)	-0.33(3)	18(2)	131(2)	51(3)
199	8	3.22(3)	0.09(2)	-0.36(3)	42(2)	262(2)	30(3)
199	9	6.02(2)	0.27(3)	-0.05(3)	9(5-II-1)	6(2)	51(3)
199	10	4.99(2)	0.05(2)	-0.13(3)	11(5-II-1)	48(2)	64(3)
199	11	3.99(2)	-0.00(4-II-2)	-0.17(3)	18(2)	136(2)	66(3)
199	12	3.15(3)	0.11(2)	-0.19(3)	41(2)	268(2)	57(3)
199	13	5.97(2)	0.26(3)	0.08(3)	27(5-II-1)	8(2)	53(2)
199	14	4.90(2)	0.01(5-II-1)	0.20(3)	29(5-II-1)	57(2)	67(2)
199	15	3.93(2)	-0.12(3)	0.29(3)	38(2)	154(2)	69(2)
199	16	3.16(5-II-1)	-0.18(3)	0.36(3)	58(2)	299(2)	70(2)
200	1	4.97(2)	0.16(3)	0.17(3)	46(3)	9(2)	49(2)
200	2	4.23(2)	-0.02(3)	0.53(3)	47(3)	61(2)	64(2)
200	3	3.51(2)	-0.17(2)	0.75(3)	54(2)	163(2)	65(2)
200	4	2.96(5-II-1)	-0.37(2)	0.87(3)	84(2)	312(2)	75(2)
200	5	4.04(2)	0.06(2)	0.25(2)	41(5-II-1)	9(2)	46(2)
200	6	3.55(2)	-0.00(2)	0.69(3)	42(5-II-1)	60(2)	60(2)
200	7	3.11(2)	-0.10(2)	0.97(3)	47(2)	160(2)	60(2)
200	8	2.89(3)	-0.24(2)	1.07(3)	69(2)	301(2)	84(2)
200	9	2.87(2)	0.01(5-II-1)	0.29(2)	35(5-II-1)	9(2)	43(2)
200	10	2.74(2)	-0.02(2)	0.80(2)	36(5-II-1)	60(2)	55(2)
200	11	2.66(2)	-0.09(2)	1.12(2)	42(2)	157(2)	56(2)
200	12	2.72(3)	-0.17(2)	1.28(3)	64(2)	296(2)	90(2)
200	13	1.54(2)	-0.06(3)	0.32(2)	27(5-II-1)	9(2)	39(2)
200	14	1.81(2)	0.01(1)	0.86(2)	29(5-II-1)	61(2)	50(2)
200	15	2.10(2)	0.04(1)	1.23(2)	38(2)	160(2)	53(2)
200	16	2.49(3)	-0.05(5-II-1)	1.45(2)	59(2)	301(2)	97(2)
201	1	0.53(2)	-0.07(3)	0.27(2)	21(3)	10(2)	33(2)
201	2	1.02(2)	0.12(3)	0.75(2)	24(2)	65(2)	46(2)
201	3	1.50(2)	0.28(3)	1.19(2)	33(2)	166(2)	51(2)
201	4	2.11(3)	0.32(3)	1.52(2)	54(2)	309(2)	106(2)
201	5	-0.31(1)	-0.01(3)	0.14(2)	18(2)	12(2)	28(2)
201	6	0.45(5-II-1)	0.27(3)	0.45(2)	20(2)	71(2)	39(2)
201	7	0.88(5-II-1)	0.63(3)	0.94(2)	28(2)	176(2)	46(2)
201	8	1.60(2)	0.88(3)	1.49(2)	44(2)	323(2)	109(2)
201	9	-0.34(1)	0.02(3)	-0.08(1)	14(2)	14(2)	20(2)
201	10	-0.12(5-I-1)	0.29(2)	-0.11(1)	16(2)	80(2)	30(2)
201	11	-0.25(5-I-1)	0.78(3)	0.30(5-II-1)	21(2)	194(2)	40(2)

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201	12	0.69(5-II-1)	1.43(3)	1.15(2)	26(2)	359(2)	107(2)
201	13	-0.08(1)	-0.05(3)	-0.08(1)	6(2)	15(2)	8(2)
201	14	-0.04(1)	-0.23(1)	-0.19(1)	6(2)	87(2)	15(2)
201	15	-0.04(5-I-1)	-0.38(1)	-0.26(1)	16(2)	216(2)	27(2)
201	16	-1.94(2)	0.69(2)	-0.60(1)	-62(5-II-1)	434(2)	62(2)
202	1	3.40(1)	-2.18(1)	0.49(1)	-83(1)	-1554(1)	-72(1)
202	2	4.01(1)	-1.39(1)	-0.33(4-II-4)	45(5-I-2)	-593(1)	-383(1)
202	3	3.27(1)	-0.59(1)	-0.47(1)	122(4-II-1)	-142(1)	-348(1)
202	4	2.88(1)	-0.09(3)	-0.37(1)	177(3)	-13(5-II-3)	-241(1)
202	5	3.68(1)	-2.20(1)	-0.49(5-II-3)	-200(1)	-1838(1)	-118(1)
202	6	4.32(1)	-1.11(3)	-0.75(4-II-4)	-62(1)	-615(1)	-365(1)
202	7	3.30(1)	-0.35(3)	-0.75(1)	123(1)	-90(1)	-307(1)
202	8	2.57(1)	-0.06(5-II-3)	-0.40(1)	249(1)	15(1)	-219(1)
202	9	4.47(1)	-1.52(4-II-4)	-0.69(4-II-4)	-273(1)	-2102(1)	-161(1)
202	10	4.49(1)	-0.54(5-II-3)	-1.18(4-II-4)	48(5-I-2)	-581(1)	-302(1)
202	11	3.24(1)	-0.28(5-II-3)	-0.82(4-II-4)	261(1)	-41(2)	-224(1)
202	12	2.28(1)	-0.08(5-II-3)	-0.34(1)	398(1)	42(1)	-171(1)
202	13	6.10(1)	2.07(1)	-1.35(4-II-4)	-293(1)	-2251(1)	-89(1)
202	14	4.33(1)	1.49(1)	-1.05(4-II-4)	309(1)	-513(1)	-121(1)
202	15	2.82(1)	0.52(1)	-0.76(4-II-4)	556(1)	-31(5-II-3)	-96(1)
202	16	1.98(1)	-0.10(5-II-3)	-0.37(4-II-4)	650(1)	57(1)	-90(1)
203	1	1.55(1)	6.51(3)	2.49(1)	30(3)	175(1)	188(1)
203	2	0.14(4-II-4)	2.26(4-II-4)	0.89(1)	22(1)	26(4-II-3)	126(3)
203	3	-0.15(1)	0.47(4-II-3)	0.30(4-II-3)	19(3)	-97(1)	62(3)
203	4	-0.16(1)	0.06(4-II-2)	0.10(3)	14(3)	-42(1)	3(5-I-3)
203	5	0.51(1)	2.02(4-II-4)	3.08(1)	144(3)	163(1)	237(1)
203	6	1.18(1)	1.05(4-II-4)	2.63(1)	91(3)	-18(2)	165(3)
203	7	0.85(1)	-0.92(1)	0.76(4-II-3)	60(3)	-137(1)	85(3)
203	8	-0.15(1)	-0.33(1)	-0.15(1)	66(3)	-73(1)	-23(1)
203	9	-0.68(4-I-4)	-0.67(1)	4.06(1)	283(3)	164(1)	225(1)
203	10	2.50(1)	-1.77(1)	3.14(1)	153(3)	-77(1)	125(1)
203	11	1.90(1)	-2.09(1)	1.21(4-II-3)	46(3)	-169(1)	90(3)
203	12	-0.54(1)	-2.05(1)	-1.06(1)	135(3)	-226(1)	-63(1)
203	13	0.97(1)	-3.98(1)	5.38(1)	471(3)	-131(1)	204(1)
203	14	3.89(1)	-2.76(1)	2.99(1)	176(3)	-113(1)	-65(3)
203	15	2.60(1)	-2.92(1)	1.77(3)	84(3)	-131(1)	-57(3)
203	16	4.61(3)	-7.88(1)	-1.67(1)	48(1)	-1106(3)	-578(3)
204	1	2.26(1)	-5.54(1)	1.45(1)	205(1)	-587(1)	71(4-II-3)
204	2	3.10(1)	-4.02(1)	1.31(1)	190(3)	-287(1)	-42(1)
204	3	4.13(1)	-3.83(1)	0.84(1)	-245(1)	-222(1)	-82(1)
204	4	1.48(1)	-7.28(1)	2.82(1)	-1021(1)	-1637(1)	786(3)
204	5	2.53(1)	-4.41(1)	1.28(1)	181(3)	-666(1)	31(4-II-3)
204	6	3.51(1)	-3.77(1)	0.80(1)	98(5-II-3)	-364(1)	-175(1)
204	7	3.34(1)	-3.23(1)	1.32(1)	-284(1)	-291(1)	-294(1)
204	8	1.38(4-II-4)	-0.76(1)	0.99(1)	-444(1)	-358(1)	-75(1)
204	9	2.75(1)	-3.50(1)	0.98(1)	75(3)	-903(1)	-53(5-I-2)
204	10	3.62(1)	-2.97(1)	0.57(1)	56(5-II-3)	-462(1)	-317(1)
204	11	3.12(1)	-1.89(1)	0.55(3)	-126(1)	-263(1)	-355(1)
204	12	2.76(1)	-0.37(1)	0.15(4-I-4)	-182(1)	-116(1)	-212(1)
204	13	3.25(1)	-2.50(1)	0.96(1)	-34(1)	-1216(1)	-70(1)
204	14	3.93(1)	-1.87(1)	0.21(4-II-3)	72(4-II-1)	-525(1)	-373(1)
204	15	3.17(1)	-0.98(1)	0.17(4-I-4)	89(4-II-1)	-190(1)	-361(1)
204	16	2.83(1)	-0.17(1)	-0.24(1)	104(4-II-2)	-46(1)	-249(1)
205	1	4.53(1)	2.04(1)	-1.49(4-II-4)	-196(1)	-2234(1)	122(4-II-1)
205	2	4.39(1)	1.52(1)	-0.75(4-II-3)	294(1)	-499(1)	-37(1)
205	3	2.95(1)	0.61(1)	-0.58(4-II-3)	568(1)	31(1)	-50(1)
205	4	2.12(1)	0.12(1)	-0.33(4-II-3)	674(1)	58(1)	-55(1)
205	5	2.99(1)	-1.70(4-II-3)	-2.09(4-II-4)	-239(1)	-2031(1)	81(4-II-1)
205	6	4.04(1)	-0.59(4-II-3)	-1.01(4-II-3)	44(4-I-4)	-573(1)	71(4-II-2)
205	7	3.07(1)	0.21(1)	-0.58(4-II-3)	291(1)	-29(4-II-3)	28(4-II-3)
205	8	2.16(1)	-0.03(5-II-3)	-0.21(4-II-3)	459(1)	38(1)	-27(1)
205	9	2.41(1)	-2.04(3)	-2.31(4-II-4)	-249(1)	-1787(1)	73(5-I-3)
205	10	3.86(1)	-1.14(3)	-1.48(4-II-3)	-56(4-II-4)	-629(1)	116(1)
205	11	3.05(1)	-0.41(4-II-3)	-0.73(4-II-3)	160(1)	-70(1)	70(4-II-2)
205	12	2.23(1)	-0.08(4-II-3)	-0.21(4-II-3)	312(1)	32(1)	42(4-II-2)
205	13	1.77(1)	-1.85(3)	-2.83(4-II-4)	-142(1)	-1545(1)	93(5-I-3)
205	14	3.10(1)	-0.99(3)	-1.72(4-II-3)	71(4-I-4)	-632(1)	148(1)
205	15	2.76(1)	-0.40(3)	-0.92(4-II-3)	158(1)	-101(1)	138(1)
205	16	2.30(1)	-0.06(3)	-0.28(4-II-3)	265(1)	24(1)	88(1)
206	1	-1.45(5-II-3)	-1.12(1)	-3.15(4-II-4)	71(4-I-4)	-1312(1)	105(5-I-3)
206	2	2.68(1)	-0.83(1)	-1.94(4-II-3)	77(4-I-2)	-590(1)	158(1)
206	3	2.66(1)	-0.43(1)	-1.07(4-II-3)	140(1)	-112(1)	178(1)
206	4	2.34(1)	-0.12(3)	-0.34(4-II-3)	231(1)	-17(5-II-3)	135(1)
206	5	-1.43(5-II-3)	-1.34(1)	-2.94(4-II-4)	60(4-I-2)	-1127(1)	84(5-I-3)
206	6	2.00(1)	-1.15(1)	-2.24(4-II-3)	-114(4-II-2)	-552(1)	148(1)
206	7	2.31(1)	-0.51(1)	-1.22(4-II-3)	-169(4-II-2)	-129(1)	201(1)

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
206	8	2.34(1)	-0.11(1)	-0.37(4-II-3)	-194(4-II-3)	-26(5-II-3)	171(1)
206	9	-1.24(5-II-3)	-1.35(1)	-2.81(4-II-4)	-103(4-II-2)	-977(1)	79(5-I-2)
206	10	1.54(1)	-0.96(1)	-2.28(4-II-3)	-165(4-II-2)	-483(1)	140(1)
206	11	1.96(1)	-0.53(1)	-1.29(4-II-3)	-245(4-II-2)	-132(4-II-4)	236(1)
206	12	2.27(1)	-0.11(1)	-0.43(4-II-3)	-294(4-II-3)	-24(4-II-3)	204(1)
206	13	-1.19(5-II-3)	-0.55(4-I-3)	-3.05(4-II-4)	-259(4-II-2)	-835(1)	115(1)
206	14	-1.52(5-II-3)	0.35(4-II-2)	-1.86(4-II-3)	-258(4-II-2)	-411(1)	190(1)
206	15	1.35(1)	-0.29(1)	-1.21(4-II-3)	-306(4-II-3)	-147(4-II-4)	281(1)
206	16	1.96(1)	-0.13(4-II-3)	-0.55(4-II-3)	-360(4-II-3)	-50(4-II-3)	219(1)
207	1	-5.05(3)	0.96(3)	-1.34(1)	269(4-II-3)	1515(4-II-3)	-203(3)
207	2	-3.88(4-II-3)	0.38(4-II-3)	-0.98(1)	181(4-II-3)	485(4-II-3)	-144(1)
207	3	-2.07(5-II-3)	-0.32(1)	-0.88(1)	143(1)	-208(1)	-221(1)
207	4	-1.49(5-II-3)	-0.12(1)	-0.48(1)	158(1)	-106(3)	-304(1)
207	5	-5.15(3)	1.50(4-II-3)	0.97(5-II-3)	314(4-II-3)	1612(4-II-3)	-186(3)
207	6	-4.08(4-II-3)	-0.19(4-I-3)	1.22(5-II-3)	224(4-II-3)	513(4-II-3)	-142(1)
207	7	-1.72(5-II-3)	-0.82(3)	-0.80(1)	159(1)	-317(1)	-222(1)
207	8	-1.35(5-II-3)	-0.33(3)	-0.70(1)	223(1)	-180(3)	-383(1)
207	9	-5.86(3)	0.70(1)	1.42(5-II-3)	323(4-II-3)	1693(4-II-3)	-164(1)
207	10	-4.08(4-II-3)	-0.84(4-II-2)	1.80(5-II-3)	127(4-II-3)	499(4-II-3)	-137(1)
207	11	-1.45(4-II-3)	-1.27(3)	0.87(5-II-3)	59(1)	-404(1)	-134(1)
207	12	-1.19(5-II-3)	-1.17(3)	-1.35(1)	336(1)	-491(3)	-448(1)
207	13	-7.50(3)	-3.20(4-II-3)	2.00(5-II-3)	205(4-II-4)	1715(4-II-3)	-193(3)
207	14	-3.58(4-II-3)	-2.70(4-II-2)	1.52(5-II-3)	-172(4-II-3)	451(4-II-3)	-140(3)
207	15	0.96(1)	-1.86(4-II-2)	0.97(5-II-3)	-225(4-II-3)	-377(1)	-97(5-II-3)
207	16	2.06(4-II-2)	-2.81(3)	-1.46(1)	364(1)	-2275(3)	-980(3)
208	1	1.28(4-II-2)	5.77(3)	-0.26(4-I-4)	1001(3)	836(3)	311(3)
208	2	-2.04(3)	2.83(3)	0.44(1)	1238(3)	529(3)	-62(1)
208	3	-3.05(3)	1.16(3)	0.40(1)	959(3)	230(3)	-60(1)
208	4	-4.48(3)	0.49(4-II-2)	0.28(1)	748(3)	79(3)	-74(1)
208	5	1.95(4-II-2)	4.81(3)	1.81(3)	621(3)	325(1)	350(3)
208	6	-1.75(3)	2.77(3)	1.36(3)	734(3)	409(3)	56(5-I-1)
208	7	-2.91(3)	1.19(3)	0.96(3)	715(3)	198(3)	-90(1)
208	8	-4.21(3)	0.15(3)	0.44(3)	638(3)	41(3)	-77(1)
208	9	1.39(4-II-2)	2.76(3)	2.19(3)	410(3)	129(1)	325(3)
208	10	-1.44(3)	2.05(3)	2.37(3)	419(3)	248(3)	92(5-I-1)
208	11	-2.45(3)	0.85(3)	1.71(3)	452(3)	152(3)	-97(1)
208	12	-3.63(3)	0.10(3)	0.75(3)	463(3)	28(3)	-77(1)
208	13	0.53(4-II-2)	1.18(3)	2.31(3)	244(3)	-145(4-I-1)	223(3)
208	14	-1.11(3)	0.75(3)	2.82(3)	195(3)	131(1)	60(5-I-1)
208	15	-1.82(3)	0.21(3)	2.20(3)	212(1)	105(1)	-111(1)
208	16	-2.61(3)	-0.08(1)	1.00(3)	252(1)	30(3)	-76(1)
209	1	-4.38(3)	-0.51(4-I-2)	-3.31(4-II-4)	-183(4-II-2)	-679(1)	250(1)
209	2	-1.39(5-II-3)	0.78(4-II-4)	-1.65(4-II-3)	-252(4-II-2)	-248(1)	296(1)
209	3	1.58(1)	0.53(4-II-4)	-0.94(4-II-3)	-224(4-II-3)	-51(5-II-3)	345(1)
209	4	1.63(1)	0.17(4-II-3)	-0.44(4-II-3)	248(1)	43(1)	275(1)
209	5	-4.42(3)	1.28(4-II-2)	-3.19(4-II-4)	-54(5-I-3)	-434(1)	206(1)
209	6	-2.10(5-II-3)	0.74(4-II-3)	-1.82(4-II-3)	-99(1)	-223(1)	321(1)
209	7	-1.49(5-II-3)	0.48(4-II-3)	-0.67(4-II-3)	-100(4-I-3)	-65(1)	370(1)
209	8	-1.51(4-II-3)	0.08(4-II-3)	-0.15(4-II-3)	119(4-II-3)	-13(5-II-3)	315(1)
209	9	-4.67(4-II-4)	2.49(4-II-3)	-2.56(4-II-3)	137(4-II-3)	-230(1)	149(1)
209	10	-2.75(4-II-3)	1.10(4-II-3)	-1.42(4-II-3)	239(4-II-3)	-171(1)	268(1)
209	11	-1.79(4-II-3)	-0.54(1)	-0.47(1)	362(4-II-3)	-91(1)	339(1)
209	12	-1.67(4-II-3)	-0.13(1)	-0.10(1)	454(4-II-3)	-31(1)	298(1)
209	13	-5.65(4-II-2)	3.91(4-II-3)	-1.51(4-II-3)	373(4-II-3)	137(5-II-3)	90(1)
209	14	-3.23(4-II-3)	1.18(4-II-3)	-1.14(1)	487(4-II-3)	-121(1)	187(1)
209	15	-1.97(5-II-3)	-0.73(1)	-0.64(1)	646(4-II-3)	-106(1)	249(1)
209	16	-1.80(4-II-3)	-0.30(1)	-0.26(1)	852(4-II-3)	69(4-II-3)	249(1)
210	1	-5.32(4-II-3)	-2.63(4-II-3)	1.64(5-II-3)	190(4-II-2)	1947(4-II-3)	-334(3)
210	2	-3.43(4-II-3)	-2.67(4-II-3)	1.01(5-II-3)	-183(4-II-3)	477(4-II-2)	-89(4-II-3)
210	3	0.67(1)	-1.83(4-II-3)	0.53(5-II-3)	-211(4-II-3)	-329(1)	-64(5-II-3)
210	4	2.33(4-II-2)	-2.84(3)	1.43(1)	-730(3)	-2346(3)	1280(3)
210	5	-4.50(4-II-3)	-0.68(5-II-3)	2.52(4-II-3)	340(4-II-3)	1915(4-II-3)	-379(3)
210	6	-2.61(4-II-3)	-1.79(3)	1.22(5-II-3)	97(3)	593(4-II-2)	-194(3)
210	7	0.53(1)	-1.98(3)	0.56(4-I-2)	-121(4-II-2)	-358(1)	-66(4-II-3)
210	8	-0.75(1)	-1.55(3)	1.36(1)	-231(3)	-531(3)	354(3)
210	9	-4.02(3)	-1.50(5-II-3)	3.44(4-II-3)	301(3)	1762(4-II-3)	-370(3)
210	10	-1.50(4-II-3)	-2.09(3)	1.48(3)	124(3)	720(4-II-2)	-253(3)
210	11	0.23(1)	-1.47(1)	0.60(1)	19(1)	-261(1)	-76(4-II-3)
210	12	-0.54(1)	-0.43(1)	0.57(1)	-72(3)	-183(1)	147(2)
210	13	-3.52(3)	-6.05(3)	4.14(3)	227(3)	1647(4-II-2)	-380(3)
210	14	-0.41(3)	-2.09(1)	0.32(5-II-3)	17(3)	786(4-II-2)	-173(3)
210	15	0.17(3)	-1.27(1)	-0.24(4-II-2)	24(3)	-180(1)	-54(4-II-3)
210	16	0.12(4-II-3)	-0.31(1)	-0.17(4-II-3)	-11(3)	-115(1)	47(2)
211	1	-0.67(1)	-0.48(1)	2.55(3)	123(3)	-191(3)	153(3)
211	2	-1.19(3)	-0.56(1)	3.06(3)	72(3)	60(1)	-49(1)
211	3	-1.79(3)	-0.39(1)	2.32(3)	92(1)	68(1)	-95(1)

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
211	4	-2.21(3)	-0.08(1)	1.01(3)	98(1)	14(1)	-67(1)
211	5	-1.17(1)	-2.20(3)	2.79(3)	-55(1)	-310(3)	164(3)
211	6	-0.82(3)	-1.91(3)	3.04(3)	6(5-II-1)	-72(4-I-4)	55(5-I-1)
211	7	-1.02(3)	-1.07(3)	2.11(3)	37(1)	55(1)	-41(1)
211	8	-1.18(3)	-0.23(3)	0.80(3)	54(1)	22(1)	-41(1)
211	9	-1.56(3)	-4.78(3)	2.85(3)	-182(3)	-444(3)	186(3)
211	10	-0.43(3)	-3.51(3)	2.47(3)	-30(3)	-101(4-I-4)	57(5-I-1)
211	11	-0.41(3)	-1.55(3)	1.50(3)	9(1)	41(1)	-26(1)
211	12	-0.54(3)	-0.30(3)	0.48(3)	26(1)	20(1)	-28(1)
211	13	-0.52(3)	-9.48(3)	2.48(3)	-368(3)	-453(3)	206(3)
211	14	0.13(2)	-4.66(3)	0.87(3)	51(3)	-124(3)	37(5-I-1)
211	15	0.14(3)	-1.76(3)	0.58(3)	-17(3)	34(1)	-14(1)
211	16	0.10(3)	-0.28(3)	0.16(3)	8(1)	20(1)	-14(1)
212	1	-4.66(3)	-1.63(1)	-1.64(1)	-147(4-I-2)	1141(4-II-3)	-172(4-II-2)
212	2	-2.78(5-II-3)	-0.59(1)	-1.13(1)	-346(3)	199(4-II-3)	109(5-II-3)
212	3	-2.02(5-II-3)	0.14(5-II-3)	-0.83(1)	-458(5-II-3)	-107(5-II-3)	-131(1)
212	4	-1.89(5-II-3)	0.09(1)	-0.48(1)	-515(5-II-3)	-49(5-II-3)	-158(1)
212	5	-4.29(3)	0.98(5-II-3)	-1.75(1)	185(4-II-3)	1294(4-II-3)	-246(3)
212	6	-3.12(5-II-3)	-0.52(1)	-1.46(1)	-115(4-I-2)	286(4-II-3)	-226(1)
212	7	-2.19(5-II-3)	-0.19(1)	-0.93(1)	-249(5-II-3)	-108(4-I-2)	-247(1)
212	8	-1.85(5-II-3)	-0.03(1)	-0.39(1)	-357(5-II-3)	-56(3)	-233(1)
212	9	-4.09(3)	1.28(5-II-3)	-1.56(1)	234(4-II-3)	1346(4-II-3)	-230(3)
212	10	-3.29(5-II-2)	0.49(5-II-3)	-1.41(1)	161(4-II-2)	384(4-II-3)	-231(1)
212	11	-2.23(5-II-3)	-0.28(1)	-0.98(1)	-123(5-II-3)	-122(4-I-2)	-257(1)
212	12	-1.78(5-II-3)	-0.09(1)	-0.40(1)	-243(5-II-3)	-58(5-II-3)	-252(1)
212	13	-4.29(3)	0.81(5-II-3)	-1.41(1)	253(4-II-3)	1412(4-II-3)	-195(3)
212	14	-3.64(4-II-3)	0.37(5-II-3)	-1.18(1)	154(4-II-2)	437(4-II-3)	-184(1)
212	15	-2.11(5-II-3)	-0.19(1)	-0.93(1)	110(5-I-3)	-148(1)	-227(1)
212	16	-1.57(5-II-3)	-0.08(1)	-0.45(1)	-179(5-II-3)	-70(3)	-259(1)
213	1	-3.45(3)	3.15(4-II-3)	-0.89(5-II-2)	-366(1)	250(4-II-3)	66(5-II-3)
213	2	-2.88(5-II-3)	1.33(4-II-3)	-1.09(3)	-679(1)	-129(1)	153(4-II-3)
213	3	-2.04(5-II-3)	-0.52(1)	-0.58(3)	-1083(1)	-166(1)	155(4-II-3)
213	4	1.68(1)	0.09(4-II-3)	-0.27(5-II-3)	-1531(1)	-144(1)	151(4-II-3)
213	5	-3.69(3)	1.26(5-II-3)	-0.87(3)	-261(1)	457(4-II-3)	-98(1)
213	6	-2.93(5-II-3)	0.92(4-II-3)	-0.73(1)	-510(1)	-112(1)	172(5-II-3)
213	7	-2.09(5-II-3)	-0.54(1)	-0.62(1)	-789(1)	-143(1)	162(5-II-3)
213	8	1.67(1)	-0.14(1)	-0.26(1)	-1023(1)	-76(1)	-144(1)
213	9	-4.06(3)	-1.17(1)	-0.89(3)	-183(1)	629(4-II-3)	-178(1)
213	10	-2.98(5-II-3)	-0.83(1)	-0.79(1)	-347(1)	-108(1)	-219(1)
213	11	-2.10(5-II-3)	-0.52(1)	-0.72(1)	-503(1)	-118(1)	-247(1)
213	12	-1.57(5-II-3)	-0.15(1)	-0.36(1)	-633(1)	-38(3)	-218(1)
213	13	-4.58(5-II-3)	-2.09(4-II-2)	-0.89(1)	-173(1)	829(4-II-3)	-159(1)
213	14	-3.08(5-II-3)	-1.01(4-II-2)	-0.91(1)	-398(3)	-99(4-I-3)	-139(1)
213	15	-1.97(5-II-3)	-0.35(1)	-0.78(1)	-455(3)	-143(3)	-154(1)
213	16	-1.63(5-II-3)	-0.21(1)	-0.49(1)	-491(5-II-3)	-53(5-II-3)	-176(1)
214	1	-2.97(5-I-1)	-7.34(4-II-2)	-3.39(4-II-2)	-177(1)	-340(4-II-2)	207(4-II-3)
214	2	-0.86(4-I-2)	-1.76(4-II-1)	-0.91(5-I-3)	-667(3)	-289(3)	290(1)
214	3	-0.90(1)	1.30(3)	-1.02(5-I-3)	-1152(3)	-385(3)	209(1)
214	4	2.37(3)	5.24(3)	-3.52(3)	-1829(3)	-829(3)	-131(5-I-1)
214	5	-2.42(4-II-3)	-1.58(4-II-2)	-2.02(4-II-2)	47(4-I-1)	399(4-I-2)	-169(3)
214	6	-0.73(1)	-2.66(4-II-2)	-2.64(4-II-2)	-333(3)	-285(4-II-2)	-102(5-I-1)
214	7	0.39(4-II-2)	-1.00(4-II-2)	-2.72(3)	-663(3)	-457(3)	-199(4-II-2)
214	8	1.79(3)	-1.26(4-II-2)	-2.25(3)	-810(3)	-679(3)	-259(4-II-2)
214	9	-1.02(4-II-3)	-1.04(4-II-2)	-1.37(4-II-2)	53(4-I-1)	494(4-I-2)	-267(3)
214	10	-0.38(2)	-2.19(4-II-2)	-2.34(3)	-129(3)	-318(4-II-2)	-214(5-I-1)
214	11	-0.19(1)	-3.17(4-II-2)	-2.46(3)	-251(3)	-510(3)	-255(5-I-1)
214	12	0.67(3)	-3.93(4-II-2)	-1.44(3)	-287(3)	-558(3)	-247(4-II-2)
214	13	0.21(3)	-0.66(4-II-2)	-0.70(3)	64(2)	607(4-I-2)	-270(3)
214	14	-0.07(1)	-2.64(4-II-2)	-0.96(3)	-26(4-II-2)	-342(4-II-2)	-201(3)
214	15	-0.12(3)	-4.98(4-II-2)	-1.00(3)	-33(3)	-508(3)	-227(5-I-1)
214	16	-0.30(3)	-6.78(4-II-2)	-0.64(3)	-51(3)	-477(2)	-225(5-I-1)
215	1	3.41(1)	-2.80(1)	-1.51(4-II-2)	471(1)	-676(4-I-1)	539(3)
215	2	2.83(1)	1.21(1)	-0.84(5-I-3)	418(3)	-198(5-I-4)	341(3)
215	3	1.73(1)	0.92(1)	-0.54(5-I-3)	374(3)	-49(4-II-3)	246(3)
215	4	1.08(1)	0.48(3)	-0.38(4-II-3)	385(3)	29(4-I-4)	173(3)
215	5	-0.86(5-I-4)	-1.53(2)	-2.30(4-II-4)	-463(3)	-1471(3)	555(3)
215	6	1.40(1)	-1.59(1)	-1.79(4-II-2)	-506(3)	-636(3)	414(3)
215	7	1.70(1)	-0.86(1)	-1.01(4-II-2)	-437(3)	-227(3)	277(3)
215	8	1.57(1)	-0.05(1)	-0.28(5-I-3)	-406(3)	-29(3)	224(3)
215	9	-0.35(5-I-1)	-0.68(1)	-1.58(4-II-2)	-439(3)	-1678(3)	178(3)
215	10	0.77(1)	-0.85(1)	-1.88(4-II-2)	-535(3)	-915(3)	228(3)
215	11	-1.27(5-I-3)	-0.42(1)	-1.57(3)	-587(3)	-347(3)	211(3)
215	12	-2.16(5-I-3)	-0.12(5-I-3)	-0.64(3)	-595(3)	-60(3)	181(3)
215	13	0.60(1)	3.07(3)	-1.22(4-II-2)	-338(3)	-1942(3)	-41(1)
215	14	-0.76(4-II-2)	1.70(3)	-1.06(4-II-2)	-86(4-I-1)	-805(3)	134(3)
215	15	-2.12(4-II-2)	0.70(3)	-0.77(4-II-2)	92(4-II-2)	-246(3)	173(3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
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Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
215	16	-3.91(4-II-2)	-0.25(3)	-0.32(4-II-2)	147(4-II-2)	-11(4-I-1)	163(3)
216	1	5.30(1)	-2.79(3)	0.79(1)	587(1)	3513(1)	-670(1)
216	2	1.77(1)	0.37(1)	0.58(4-II-4)	42(5-II-1)	926(1)	-168(3)
216	3	1.22(1)	0.42(1)	0.34(4-II-4)	-218(1)	191(1)	92(1)
216	4	0.99(1)	-0.07(4-II-2)	0.15(4-II-2)	-213(1)	-5(5-I-3)	93(1)
216	5	1.06(1)	-2.43(1)	-2.02(3)	458(1)	2974(1)	-284(3)
216	6	1.95(1)	-1.71(1)	-0.77(3)	642(1)	1459(1)	-211(3)
216	7	1.32(1)	-0.67(1)	-0.19(5-I-4)	723(1)	466(1)	44(1)
216	8	1.14(1)	-0.07(1)	0.04(5-II-1)	699(2)	65(3)	83(1)
216	9	-1.01(4-I-3)	-1.32(1)	-2.33(3)	489(1)	2997(1)	242(1)
216	10	-1.04(4-I-4)	-1.28(1)	-1.45(1)	741(1)	1523(1)	389(1)
216	11	0.69(1)	-0.62(1)	-0.86(1)	892(2)	484(1)	187(1)
216	12	0.74(1)	-0.05(1)	-0.26(1)	916(3)	57(3)	99(1)
216	13	-2.38(4-I-4)	-2.26(3)	-1.75(1)	923(1)	3514(1)	828(1)
216	14	-1.23(4-I-4)	-1.05(5-I-4)	-1.71(1)	675(3)	1046(1)	453(3)
216	15	-0.74(4-I-4)	-0.70(3)	-1.17(3)	585(3)	293(3)	180(3)
216	16	-0.69(3)	-0.45(3)	-0.67(3)	574(3)	33(5-I-3)	80(3)
217	1	6.89(1)	10.95(1)	2.68(1)	2310(1)	770(1)	122(4-I-4)
217	2	-3.48(3)	6.74(1)	-2.16(3)	1757(1)	508(1)	-109(1)
217	3	-3.71(1)	3.98(1)	-4.02(3)	1101(1)	231(1)	80(4-I-4)
217	4	-2.67(1)	1.65(1)	-3.99(3)	609(1)	214(1)	-168(1)
217	5	3.91(1)	3.03(1)	-0.36(4-II-3)	198(1)	-371(1)	115(4-I-1)
217	6	1.68(1)	3.29(1)	1.23(1)	310(1)	182(1)	-188(1)
217	7	-1.42(3)	2.91(1)	-0.72(3)	386(1)	396(1)	-229(1)
217	8	-3.73(1)	2.28(1)	-1.28(3)	478(1)	574(1)	-429(1)
217	9	2.11(1)	1.07(1)	0.69(1)	-59(1)	-623(1)	98(4-I-4)
217	10	1.53(1)	1.41(1)	1.33(1)	90(4-I-3)	-56(1)	99(4-I-4)
217	11	0.69(1)	0.99(1)	0.98(1)	170(1)	407(1)	-198(1)
217	12	-1.56(1)	0.80(1)	-1.10(3)	200(1)	656(1)	-407(1)
217	13	0.37(2)	0.94(1)	0.51(1)	-47(1)	-665(1)	92(4-I-4)
217	14	0.40(1)	1.74(1)	1.17(1)	46(4-I-4)	-173(1)	114(4-I-4)
217	15	2.25(1)	2.08(1)	2.19(1)	227(1)	247(1)	119(4-I-4)
217	16	5.15(1)	-3.12(3)	1.33(1)	1248(1)	655(1)	183(2)
218	1	0.73(3)	-0.81(3)	-0.30(3)	-16(1)	-114(5-II-1)	76(4-I-1)
218	2	2.68(3)	-0.52(3)	-0.34(3)	-29(5-II-1)	-80(5-II-1)	52(4-I-1)
218	3	4.78(3)	-0.26(3)	-0.26(3)	-37(5-II-1)	-41(5-II-1)	38(4-I-1)
218	4	7.09(3)	-0.09(2)	-0.09(3)	-44(5-II-1)	-9(5-II-1)	29(4-I-1)
218	5	0.82(3)	-1.21(3)	-0.51(3)	-17(5-II-1)	-204(3)	68(4-I-1)
218	6	2.67(3)	-0.80(3)	-0.56(3)	-42(5-II-1)	-123(3)	46(4-I-1)
218	7	4.63(3)	-0.39(3)	-0.45(3)	-45(5-II-1)	-54(3)	-32(4-II-1)
218	8	6.81(3)	-0.07(3)	-0.18(3)	-49(5-II-1)	-10(5-II-1)	-29(4-II-1)
218	9	0.94(3)	-1.76(3)	-0.90(3)	18(5-I-1)	-319(3)	52(4-I-1)
218	10	2.66(3)	-1.14(3)	-0.97(3)	-42(5-II-1)	-165(3)	43(4-I-1)
218	11	4.37(3)	-0.54(3)	-0.81(3)	-31(5-II-1)	-63(3)	-34(5-II-4)
218	12	6.30(3)	-0.08(3)	-0.34(3)	29(5-I-1)	-9(5-II-1)	-31(5-II-4)
218	13	1.09(3)	-2.20(3)	-1.51(3)	42(5-I-1)	-425(3)	32(5-I-4)
218	14	2.63(3)	-1.39(3)	-1.60(3)	37(5-I-1)	-199(3)	58(5-I-4)
218	15	3.95(3)	-0.64(3)	-1.32(3)	64(4-II-3)	-65(3)	39(5-I-4)
218	16	5.47(3)	-0.11(3)	-0.55(3)	88(3)	-5(3)	27(5-I-4)
219	1	-0.21(5-I-1)	-1.50(3)	0.37(5-I-1)	-202(2)	-345(2)	213(3)
219	2	0.32(5-II-1)	-1.05(3)	-0.41(5-II-1)	-267(2)	-93(3)	108(3)
219	3	0.89(5-II-1)	-0.65(3)	-0.43(5-II-1)	-170(2)	-18(4-I-1)	69(3)
219	4	1.69(3)	-0.27(1)	-0.21(5-II-1)	-137(3)	-3(4-I-1)	49(3)
219	5	0.17(5-II-1)	-1.38(3)	-0.48(5-II-1)	-63(3)	-196(3)	89(3)
219	6	0.52(5-II-1)	-0.79(3)	-0.69(5-II-1)	-118(2)	-116(3)	122(3)
219	7	0.79(5-II-1)	-0.36(3)	-0.72(3)	-136(2)	-42(3)	94(3)
219	8	1.20(3)	-0.03(5-I-1)	-0.36(3)	-131(3)	-6(3)	63(3)
219	9	0.36(5-II-1)	-0.76(3)	-0.92(5-II-1)	-22(3)	-108(3)	56(3)
219	10	0.61(5-II-1)	-0.23(5-I-1)	-1.08(3)	-45(3)	-107(3)	81(3)
219	11	0.49(5-II-1)	-0.10(5-I-1)	-0.79(3)	-68(3)	-62(3)	76(3)
219	12	0.61(3)	-0.06(3)	-0.33(3)	-83(3)	-15(3)	53(3)
219	13	0.93(3)	1.97(5-II-1)	-1.29(3)	-5(4-I-1)	-71(4-I-1)	48(3)
219	14	0.08(3)	1.16(5-II-1)	-0.68(3)	-7(3)	-95(3)	56(3)
219	15	0.04(3)	0.45(5-II-1)	-0.39(3)	-16(3)	-70(3)	49(3)
219	16	0.11(3)	0.04(5-II-1)	-0.13(3)	-24(3)	-22(3)	27(3)
220	1	3.50(3)	1.81(3)	4.31(3)	-723(3)	236(4-II-2)	59(3)
220	2	-0.54(4-II-2)	1.76(3)	3.50(3)	-481(3)	213(3)	32(5-II-1)
220	3	-1.80(3)	1.48(3)	2.75(3)	-498(3)	149(3)	69(5-II-1)
220	4	-2.29(3)	1.24(3)	2.17(3)	-484(3)	112(3)	66(5-II-1)
220	5	1.37(3)	1.22(3)	2.55(3)	-193(3)	488(3)	-36(1)
220	6	0.42(3)	1.85(3)	3.18(3)	-252(3)	345(3)	-166(3)
220	7	-0.74(3)	2.28(3)	2.79(3)	-235(3)	211(3)	-109(3)
220	8	-1.25(3)	2.49(3)	2.24(3)	-220(3)	96(3)	-81(5-I-4)
220	9	0.35(3)	1.38(3)	1.56(3)	63(3)	756(3)	-100(1)
220	10	0.21(3)	2.14(3)	1.92(3)	-29(5-I-4)	543(3)	-143(3)
220	11	-0.17(4-II-2)	2.83(3)	1.99(3)	-52(3)	341(3)	-67(5-I-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
220	12	-0.49(3)	3.38(3)	1.76(3)	-61(3)	190(3)	-51(5-I-4)
220	13	-0.02(5-I-1)	2.11(3)	0.41(3)	65(3)	1111(3)	-136(3)
220	14	-0.01(5-I-1)	2.74(3)	0.64(3)	16(1)	728(3)	-99(3)
220	15	-0.04(2)	3.61(3)	0.75(3)	13(1)	431(3)	-46(5-I-4)
220	16	-0.10(3)	4.49(3)	0.73(3)	3(1)	238(3)	-34(5-I-4)
221	1	-1.42(4-II-2)	0.61(3)	-3.08(3)	-77(4-I-1)	-470(3)	277(3)
221	2	-0.41(5-I-1)	1.00(3)	-1.57(3)	202(1)	-37(3)	393(3)
221	3	0.31(5-II-1)	0.52(3)	-0.80(3)	404(1)	108(3)	421(3)
221	4	0.46(1)	0.03(4-I-1)	-0.15(3)	438(1)	58(3)	387(3)
221	5	-2.66(3)	0.88(4-II-3)	-2.29(3)	-82(3)	-252(5-II-1)	352(3)
221	6	-1.53(4-II-3)	0.45(4-II-3)	-1.10(3)	50(1)	38(1)	640(3)
221	7	-0.68(5-I-4)	0.12(4-II-3)	-0.19(3)	111(1)	79(1)	601(3)
221	8	0.30(1)	-0.06(1)	0.05(4-II-4)	164(1)	41(3)	489(3)
221	9	-4.60(3)	1.36(4-II-3)	-1.30(3)	37(1)	341(1)	411(3)
221	10	-2.77(3)	0.38(4-II-3)	0.19(5-I-1)	56(1)	97(1)	616(3)
221	11	-0.87(5-I-4)	-0.24(1)	0.20(4-II-2)	-87(4-II-1)	-21(4-II-1)	621(3)
221	12	0.32(1)	-0.06(1)	0.11(4-II-2)	-114(4-II-1)	-18(4-II-1)	518(3)
221	13	-8.43(3)	-0.20(4-II-1)	1.57(3)	-203(4-II-2)	470(1)	429(3)
221	14	-1.90(3)	-0.93(4-II-2)	0.52(4-II-3)	-110(4-II-1)	150(1)	487(3)
221	15	-0.53(5-I-4)	-0.56(3)	0.15(4-II-2)	-270(4-II-1)	-45(4-II-1)	481(3)
221	16	0.50(4-II-1)	-0.22(3)	-0.15(1)	-442(4-II-1)	-48(3)	394(3)
222	1	-1.37(3)	0.24(1)	1.21(3)	-340(3)	-1377(4-II-3)	738(3)
222	2	-0.77(4-II-3)	0.33(2)	0.47(1)	-267(4-II-1)	-204(4-II-2)	318(2)
222	3	0.26(1)	0.15(2)	0.16(1)	-411(4-II-1)	57(4-I-1)	261(4-I-2)
222	4	1.21(1)	0.10(3)	-0.16(3)	-562(4-II-1)	26(4-I-1)	201(4-I-2)
222	5	-1.27(1)	-1.70(1)	0.90(3)	-500(4-II-2)	-1433(4-II-3)	487(3)
222	6	0.16(1)	-1.09(1)	0.37(2)	-619(4-II-2)	-482(4-II-2)	428(2)
222	7	0.69(1)	-0.43(1)	-0.14(4-II-2)	-633(4-II-2)	-85(4-I-2)	320(4-I-1)
222	8	1.24(1)	-0.08(1)	-0.10(4-II-4)	-597(4-II-2)	13(4-I-1)	250(4-I-1)
222	9	-1.06(1)	-2.06(3)	0.37(4-I-1)	-512(4-II-2)	-1518(4-II-2)	285(4-I-1)
222	10	0.53(3)	-1.19(1)	-0.52(4-II-1)	-662(4-II-2)	-581(4-II-2)	330(4-I-1)
222	11	0.78(1)	-0.56(1)	-0.44(1)	-665(3)	-107(3)	321(4-I-1)
222	12	1.06(1)	-0.10(1)	-0.19(1)	-612(3)	-14(4-I-2)	256(4-I-1)
222	13	1.31(4-II-3)	-0.44(5-I-2)	-1.11(4-II-2)	-761(4-II-2)	-1905(4-II-2)	-319(4-II-1)
222	14	0.65(1)	-0.76(5-I-1)	-0.81(1)	-698(3)	-425(4-II-3)	204(4-I-1)
222	15	0.56(1)	-0.58(5-I-3)	-0.63(3)	-566(2)	-76(4-I-1)	281(3)
222	16	0.62(1)	-0.32(3)	-0.38(3)	-475(2)	45(4-II-2)	259(3)

Risultati Analisi Dinamica - Sollecitazioni massime per combinazione - Sigma terreno platea - S.L.E
Scenario di calcolo: ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO

Combinazione	Muro	Nodi	SigmaMax daN/cm ²	SigmaMin daN/cm ²
6	11	2016-2095-2094-2091	0.58	0.44
7	11	2016-2095-2094-2091	0.54	0.41
8	11	2016-2095-2094-2091	0.53	0.39
9-I-1	11	2016-2095-2094-2091	0.51	0.38
9-II-1	11	2016-2095-2094-2091	0.53	0.37
9-I-2	11	2016-2095-2094-2091	0.51	0.38
9-II-2	11	2016-2095-2094-2091	0.53	0.37
9-I-3	11	2016-2095-2094-2091	0.51	0.38
9-II-3	11	2016-2095-2094-2091	0.53	0.37
9-I-4	11	2016-2095-2094-2091	0.51	0.38
9-II-4	11	2016-2095-2094-2091	0.53	0.37
10-I-1	11	2016-2095-2094-2091	0.55	0.40
10-II-1	5	2020-2001-2025-2019	0.54	0.39
10-I-2	11	2016-2095-2094-2091	0.55	0.40
10-II-2	5	2020-2001-2025-2019	0.54	0.39
10-I-3	11	2016-2095-2094-2091	0.55	0.40
10-II-3	5	2020-2001-2025-2019	0.54	0.39
10-I-4	11	2016-2095-2094-2091	0.55	0.40
10-II-4	5	2020-2001-2025-2019	0.54	0.39
Assoluti				
6	11	2016-2095-2094-2091	0.58	
9-II-2	11	2016-2095-2094-2091		0.37

Risultati Analisi Dinamica - Spostamenti massimi - Nodi - S.L.E.
Scenario di calcolo: ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	mrad	mrad	mrad

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
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Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
1	0.00(6)	0.00(6)	-9.59(6)	0.02(9-II-4)	-0.02(10-II-2)	0.00(6)
2	0.03(9-II-4)	-0.02(10-I-3)	-9.50(6)	-0.01(10-II-3)	0.08(9-II-4)	0.01(10-II-2)
3	0.03(9-II-3)	-0.01(10-I-3)	-9.49(6)	0.04(9-II-2)	-0.01(9-II-3)	0.01(9-II-4)
4	0.03(9-II-4)	-0.01(10-I-3)	-9.51(6)	0.05(9-II-2)	0.01(10-I-3)	0.02(9-II-4)
5	0.04(9-II-4)	-0.03(10-I-3)	-9.52(6)	-0.02(10-II-3)	0.04(9-II-4)	0.01(10-II-3)
6	0.03(9-II-4)	-0.00(10-I-3)	-9.53(6)	0.04(9-II-4)	0.03(9-II-2)	0.01(10-II-3)
7	0.04(9-II-4)	-0.03(10-I-3)	-9.53(6)	-0.03(10-II-3)	0.04(10-II-3)	0.02(6)
8	0.03(9-II-4)	-0.01(10-I-3)	-9.54(6)	0.03(9-II-1)	0.05(9-II-4)	0.01(10-II-3)
9	0.07(9-II-4)	-0.03(10-I-3)	-9.54(6)	-0.01(10-II-3)	0.01(9-II-4)	0.02(9-II-4)
10	0.03(9-II-4)	-0.01(10-I-3)	-9.54(6)	0.01(10-II-3)	0.06(9-II-4)	-0.00(10-I-3)
11	0.07(9-II-4)	-0.02(10-I-3)	-9.56(6)	0.01(6)	-0.04(9-II-4)	-0.01(9-II-1)
12	0.03(9-II-4)	-0.01(10-I-3)	-9.55(6)	-0.01(9-II-3)	0.04(9-II-4)	-0.02(9-II-3)
13	0.04(9-II-4)	-0.02(10-I-3)	-9.55(6)	-0.01(9-II-3)	-0.05(9-II-4)	-0.02(9-II-4)
14	0.03(9-II-4)	-0.01(9-II-3)	-9.54(6)	-0.02(9-II-3)	0.01(10-II-4)	-0.02(9-II-4)
15	0.02(9-II-4)	-0.02(9-II-4)	-9.54(6)	-0.01(9-I-1)	-0.05(9-II-4)	0.01(9-II-3)
16	0.04(9-II-4)	-0.01(10-I-3)	-9.51(6)	-0.03(9-I-1)	-0.01(9-II-3)	-0.02(9-II-3)
17	0.02(9-II-4)	-0.01(10-I-3)	-9.51(6)	0.01(10-I-1)	-0.05(9-II-4)	0.03(9-II-4)
18	0.04(9-II-4)	0.00(10-II-3)	-9.49(6)	-0.03(10-II-3)	-0.02(9-II-3)	-0.01(9-II-4)
19	0.02(9-II-4)	0.01(10-II-3)	-9.48(6)	0.01(10-I-1)	0.02(9-II-3)	0.01(10-I-4)
20	0.03(9-II-4)	0.01(10-II-3)	-9.46(6)	-0.03(9-I-4)	-0.03(9-I-1)	-0.01(9-II-4)
21	0.01(9-II-4)	0.02(10-II-3)	-9.47(6)	0.01(10-I-2)	0.02(9-II-4)	-0.00(9-II-1)
22	0.02(9-II-4)	0.01(10-II-3)	-9.45(6)	-0.01(9-I-4)	-0.03(9-I-2)	-0.01(9-II-4)
23	0.01(9-II-4)	0.01(10-II-3)	-9.45(6)	-0.02(9-II-4)	0.04(9-II-4)	0.00(6)
24	0.01(9-II-4)	0.01(10-II-3)	-9.44(6)	-0.01(9-I-1)	-0.04(9-I-2)	-0.00(10-II-3)
25	-0.01(9-I-2)	0.01(10-II-3)	-9.44(6)	-0.01(10-II-3)	0.02(9-II-2)	0.00(6)
26	0.01(9-II-4)	-0.01(10-I-3)	-9.44(6)	-0.00(10-I-4)	-0.03(9-I-2)	0.00(10-I-3)
27	0.01(9-II-2)	-0.01(10-I-3)	-9.44(6)	0.01(10-I-3)	0.01(9-II-2)	-0.00(10-II-2)
28	0.01(9-II-3)	-0.01(10-I-3)	-9.44(6)	0.01(9-I-3)	-0.04(9-I-2)	0.01(10-I-3)
29	0.00(9-II-3)	-0.02(10-I-3)	-9.44(6)	0.01(10-I-3)	0.02(9-II-3)	-0.01(10-II-3)
30	0.02(9-II-3)	-0.02(10-I-3)	-9.46(6)	0.01(9-I-3)	-0.03(9-I-4)	0.01(9-II-3)
31	0.02(9-II-4)	-0.02(10-I-3)	-9.46(6)	0.03(9-II-3)	0.05(9-II-3)	-0.01(6)
32	0.03(9-II-3)	-0.02(10-I-3)	-9.48(6)	0.03(9-I-3)	-0.03(9-II-3)	0.02(9-II-3)
33	0.02(9-II-4)	-0.02(10-I-3)	-9.48(6)	0.01(9-II-4)	0.05(9-II-4)	-0.00(6)
34	0.00(6)	0.00(6)	-9.56(6)	-0.01(10-I-3)	-0.04(9-II-4)	0.00(6)
35	0.00(6)	0.00(6)	-9.56(6)	-0.01(10-I-3)	-0.04(9-II-4)	0.00(6)
36	0.00(6)	0.00(6)	-9.56(6)	0.01(10-II-3)	-0.05(9-II-4)	0.00(6)
37	0.00(6)	0.00(6)	-9.55(6)	0.01(10-II-3)	-0.05(9-II-4)	0.00(6)
38	0.00(6)	0.00(6)	-9.50(6)	-0.01(10-I-3)	-0.06(9-II-4)	0.00(6)
39	0.00(6)	0.00(6)	-9.51(6)	-0.02(10-I-3)	-0.06(9-II-4)	0.00(6)
40	0.00(6)	0.00(6)	-9.54(6)	0.01(10-II-3)	-0.06(9-II-4)	0.00(6)
41	0.00(6)	0.00(6)	-9.52(6)	0.01(10-II-3)	-0.06(9-II-3)	0.00(6)
42	0.00(6)	0.00(6)	-9.55(6)	-0.02(10-I-3)	-0.05(9-II-4)	0.00(6)
43	0.00(6)	0.00(6)	-9.53(6)	-0.02(10-I-3)	-0.06(9-II-4)	0.00(6)
44	0.00(6)	0.00(6)	-9.54(6)	-0.02(10-I-3)	-0.06(9-II-4)	0.00(6)
45	0.00(6)	0.00(6)	-9.51(6)	0.00(10-II-3)	-0.06(9-II-3)	0.00(6)
46	0.00(6)	0.00(6)	-9.50(6)	-0.01(10-I-3)	-0.06(9-II-3)	0.00(6)
47	0.00(6)	0.00(6)	-9.49(6)	-0.01(10-I-3)	-0.06(9-II-4)	0.00(6)
48	0.00(6)	0.00(6)	-9.48(6)	-0.01(10-I-3)	-0.06(9-II-4)	0.00(6)
49	0.00(6)	0.00(6)	-9.48(6)	-0.01(10-I-3)	-0.06(9-II-4)	0.00(6)
50	0.00(6)	0.00(6)	-9.48(6)	-0.01(10-I-3)	-0.06(9-II-3)	0.00(6)
51	0.00(6)	0.00(6)	-9.49(6)	-0.01(10-I-3)	-0.06(9-II-3)	0.00(6)
52	0.00(6)	0.00(6)	-9.52(6)	-0.01(10-I-3)	-0.05(9-II-4)	0.00(6)
53	0.07(9-II-4)	0.01(10-II-3)	-9.60(6)	0.01(9-II-1)	-0.03(9-II-4)	-0.02(9-II-4)
2001	0.00(6)	0.00(6)	-11.17(6)	0.23(10-II-2)	-0.37(9-II-4)	0.00(6)
2002	0.00(6)	0.00(6)	-9.94(6)	0.20(10-II-1)	0.07(9-I-1)	0.00(6)
2003	0.00(6)	0.00(6)	-10.97(6)	0.23(10-II-1)	0.29(9-I-1)	0.00(6)
2004	0.00(6)	0.00(6)	-10.39(6)	0.14(10-II-1)	-0.33(9-II-1)	0.00(6)
2005	0.00(6)	0.00(6)	-9.28(6)	0.09(10-II-1)	-0.04(9-II-2)	0.00(6)
2006	0.00(6)	0.00(6)	-10.12(6)	0.17(10-II-1)	0.28(9-I-1)	0.00(6)
2007	0.00(6)	0.00(6)	-10.10(6)	0.06(10-II-1)	-0.28(9-II-4)	0.00(6)
2008	-0.01(9-II-1)	-0.00(10-II-1)	-9.09(6)	0.06(10-II-1)	-0.08(9-II-2)	0.00(10-I-3)
2009	0.00(6)	0.00(6)	-9.74(6)	0.11(10-II-1)	0.26(9-I-2)	0.00(6)
2010	0.00(6)	0.00(6)	-10.11(6)	-0.06(10-I-2)	-0.24(9-II-4)	0.00(6)
2011	-0.03(10-I-3)	0.02(9-II-3)	-9.12(6)	-0.08(10-I-3)	-0.15(9-II-2)	0.01(9-II-3)
2012	0.00(6)	0.00(6)	-9.66(6)	-0.06(10-I-3)	0.25(9-I-2)	0.00(6)
2013	0.00(6)	0.00(6)	-10.50(6)	-0.17(10-I-2)	-0.30(9-II-3)	0.00(6)
2014	0.00(6)	0.00(6)	-9.34(6)	-0.07(10-I-3)	-0.10(9-II-3)	0.00(6)
2015	0.00(6)	0.00(6)	-10.09(6)	-0.17(10-I-3)	0.26(9-I-3)	0.00(6)
2016	0.00(6)	0.00(6)	-11.29(6)	-0.23(10-I-2)	-0.35(9-II-3)	0.00(6)
2017	0.00(6)	0.00(6)	-9.99(6)	-0.22(10-I-3)	-0.07(9-II-3)	0.00(6)
2018	0.00(6)	0.00(6)	-10.93(6)	-0.25(10-I-3)	0.28(9-I-3)	0.00(6)
2019	0.00(6)	0.00(6)	-11.42(6)	0.23(10-II-1)	-0.37(9-II-4)	0.00(6)
2020	0.00(6)	0.00(6)	-11.25(6)	0.23(10-II-2)	-0.37(9-II-4)	0.00(6)
2021	0.00(6)	0.00(6)	-9.99(6)	0.23(10-II-1)	-0.11(9-II-4)	0.00(6)
2022	0.00(6)	0.00(6)	-10.01(6)	0.20(10-II-1)	0.06(9-I-1)	0.00(6)
2023	0.00(6)	0.00(6)	-11.05(6)	0.23(10-II-1)	0.29(9-I-2)	0.00(6)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
2024	0.00(6)	0.00(6)	-11.18(6)	0.24(10-II-1)	0.29(9-I-2)	0.00(6)
2025	0.00(6)	0.00(6)	-11.32(6)	0.24(10-II-1)	-0.37(9-II-4)	0.00(6)
2026	0.00(6)	0.00(6)	-9.89(6)	0.23(10-II-1)	-0.11(9-II-4)	0.00(6)
2027	0.00(6)	0.00(6)	-11.09(6)	0.24(10-II-1)	0.29(9-I-1)	0.00(6)
2028	0.02(10-II-1)	0.02(10-II-2)	-9.37(6)	0.10(10-II-1)	-0.03(9-II-4)	-0.01(9-I-1)
2029	-0.01(9-I-2)	0.00(10-II-3)	-9.43(6)	0.12(10-II-1)	0.03(9-I-2)	-0.01(10-II-1)
2031	0.00(6)	0.00(6)	-9.29(6)	0.10(10-II-1)	-0.04(9-II-2)	0.00(6)
2032	0.00(6)	0.00(6)	-9.32(6)	0.09(10-II-1)	-0.03(9-II-2)	0.00(6)
2033	0.00(6)	0.00(6)	-9.32(6)	0.10(10-II-1)	0.02(9-I-2)	0.00(6)
2035	0.00(6)	0.00(6)	-10.53(6)	0.14(10-II-1)	-0.33(9-II-4)	0.00(6)
2036	0.03(10-II-1)	0.02(10-II-2)	-9.23(6)	0.07(10-II-1)	0.03(9-I-4)	-0.01(10-II-1)
2037	0.02(10-II-1)	0.01(10-II-2)	-9.26(6)	0.07(10-II-1)	0.02(9-I-2)	-0.01(9-II-2)
2038	0.00(6)	0.00(6)	-9.27(6)	0.09(10-II-1)	-0.03(9-II-2)	0.00(6)
2040	0.00(6)	0.00(6)	-10.24(6)	0.17(10-II-1)	0.28(9-I-1)	0.00(6)
2041	0.00(6)	0.00(6)	-10.22(6)	0.06(10-II-1)	-0.28(9-II-4)	0.00(6)
2042	0.03(9-II-2)	0.01(10-II-2)	-9.10(6)	0.02(10-II-1)	0.02(10-II-2)	0.01(10-I-4)
2043	0.00(6)	0.00(6)	-9.11(6)	0.05(10-II-1)	-0.05(9-II-2)	0.00(6)
2044	0.00(6)	0.00(6)	-9.02(6)	0.07(10-II-1)	-0.05(9-II-2)	0.00(6)
2046	0.00(6)	0.00(6)	-9.86(6)	0.10(10-II-2)	0.26(9-I-2)	0.00(6)
2047	0.02(9-II-2)	0.01(10-II-2)	-9.10(6)	-0.04(10-I-1)	-0.02(9-II-2)	0.02(10-II-1)
2048	0.00(6)	0.00(6)	-9.08(6)	0.03(10-II-1)	-0.05(9-II-2)	0.00(6)
2049	-0.02(10-I-3)	0.00(9-II-3)	-9.03(6)	0.04(10-II-1)	-0.09(9-II-2)	0.01(10-II-1)
2050	-0.04(10-I-3)	-0.00(6)	-8.93(6)	0.06(10-II-1)	-0.11(9-II-2)	0.01(10-II-1)
2052	0.00(6)	0.00(6)	-9.06(6)	0.05(10-II-2)	0.21(9-I-2)	0.00(6)
2053	0.01(9-II-2)	0.02(10-II-2)	-9.12(6)	-0.06(10-I-1)	-0.04(9-II-2)	0.04(9-II-3)
2054	-0.05(10-I-3)	-0.00(6)	-8.89(6)	0.05(10-II-1)	-0.12(9-II-2)	-0.00(10-I-3)
2056	-0.03(9-I-1)	0.03(10-II-1)	-9.13(6)	-0.08(10-I-1)	-0.10(9-II-2)	0.01(10-II-1)
2057	-0.04(10-I-4)	0.03(10-II-1)	-9.03(6)	-0.06(10-I-1)	-0.12(9-II-2)	-0.01(10-I-3)
2058	-0.01(9-I-2)	-0.01(10-I-1)	-9.62(6)	-0.02(10-I-4)	-0.19(9-II-4)	0.02(9-II-4)
2059	-0.02(9-I-2)	0.06(10-II-1)	-9.44(6)	-0.18(10-I-4)	-0.09(9-II-4)	0.02(9-II-4)
2060	-0.02(9-I-2)	0.02(10-II-2)	-9.28(6)	-0.10(10-I-3)	-0.15(9-II-2)	-0.02(9-II-2)
2061	0.00(6)	0.00(6)	-10.22(6)	-0.05(10-I-4)	-0.24(9-II-4)	0.00(6)
2062	0.00(6)	0.00(6)	-8.91(6)	-0.06(10-I-2)	0.12(9-I-2)	0.00(6)
2063	0.00(6)	0.00(6)	-9.77(6)	-0.06(10-I-2)	0.25(9-I-2)	0.00(6)
2064	-0.03(9-I-2)	0.02(10-II-1)	-9.50(6)	-0.08(10-I-4)	-0.09(9-II-4)	0.08(9-II-4)
2065	-0.03(9-I-2)	0.02(9-I-1)	-9.45(6)	-0.08(10-I-3)	-0.14(9-II-4)	-0.03(6)
2066	-0.06(9-I-1)	-0.04(10-I-3)	-9.55(6)	-0.09(10-I-4)	-0.14(9-II-3)	0.06(9-II-4)
2067	-0.04(9-I-2)	0.02(10-II-2)	-9.41(6)	-0.10(10-I-3)	-0.18(9-II-2)	0.01(9-II-2)
2068	-0.04(9-I-2)	-0.03(10-I-2)	-9.55(6)	-0.03(9-II-3)	-0.07(9-II-4)	-0.06(10-I-3)
2069	-0.05(10-I-3)	0.01(10-II-2)	-9.41(6)	-0.07(10-I-3)	-0.20(9-II-2)	0.01(9-II-2)
2070	0.01(9-II-4)	-0.01(10-I-3)	-9.65(6)	-0.09(9-II-3)	-0.21(9-II-4)	-0.01(10-II-3)
2071	0.01(9-II-4)	-0.02(10-I-3)	-9.57(6)	-0.05(9-II-3)	-0.12(9-II-4)	-0.03(10-II-3)
2072	-0.04(9-II-3)	-0.01(10-I-2)	-9.39(6)	-0.03(10-I-3)	-0.19(9-II-2)	-0.01(10-I-3)
2073	0.02(9-II-4)	-0.02(10-I-3)	-9.56(6)	-0.05(9-II-3)	-0.14(9-II-4)	-0.01(10-II-3)
2074	-0.02(9-II-3)	-0.01(10-I-2)	-9.42(6)	-0.01(10-I-3)	-0.15(9-II-3)	-0.02(10-I-3)
2075	0.02(9-II-4)	-0.02(10-I-3)	-9.56(6)	-0.07(10-I-3)	-0.14(9-II-4)	-0.01(10-II-3)
2076	-0.01(10-II-3)	-0.01(9-II-2)	-9.44(6)	-0.02(10-I-3)	-0.11(9-II-3)	-0.02(9-II-4)
2077	0.02(9-II-4)	-0.02(10-I-3)	-9.52(6)	-0.05(10-I-3)	-0.09(9-II-4)	-0.01(10-II-3)
2078	0.00(6)	0.00(6)	-9.47(6)	-0.04(10-I-3)	-0.09(9-II-3)	0.00(6)
2079	0.01(9-II-4)	-0.01(9-I-3)	-9.50(6)	-0.05(10-I-3)	-0.07(9-II-4)	-0.01(9-II-3)
2080	0.00(6)	0.00(6)	-10.63(6)	-0.16(10-I-3)	-0.30(9-II-4)	0.00(6)
2081	0.00(6)	0.00(6)	-10.21(6)	-0.17(10-I-3)	0.26(9-I-3)	0.00(6)
2082	0.00(6)	0.00(6)	-9.74(6)	-0.14(10-I-3)	-0.20(9-II-4)	0.00(6)
2083	0.00(6)	0.00(6)	-9.59(6)	-0.11(10-I-3)	-0.13(9-II-4)	0.00(6)
2084	0.00(6)	0.00(6)	-9.51(6)	-0.06(10-I-3)	-0.09(9-II-4)	0.00(6)
2085	0.00(6)	0.00(6)	-9.37(6)	-0.07(10-I-3)	-0.10(9-II-3)	0.00(6)
2086	0.00(6)	0.00(6)	-9.40(6)	-0.16(10-I-3)	0.10(6)	0.00(6)
2087	0.00(6)	0.00(6)	-11.01(6)	-0.24(10-I-3)	-0.34(9-II-4)	0.00(6)
2088	0.00(6)	0.00(6)	-9.88(6)	-0.19(10-I-3)	-0.13(9-II-4)	0.00(6)
2089	0.00(6)	0.00(6)	-9.78(6)	-0.23(10-I-3)	-0.04(9-II-2)	0.00(6)
2090	0.00(6)	0.00(6)	-10.14(6)	-0.25(10-I-3)	0.21(9-I-2)	0.00(6)
2091	0.00(6)	0.00(6)	-11.44(6)	-0.24(10-I-2)	-0.35(9-II-4)	0.00(6)
2092	0.00(6)	0.00(6)	-10.06(6)	-0.20(10-I-3)	-0.13(9-II-1)	0.00(6)
2093	0.00(6)	0.00(6)	-11.06(6)	-0.25(10-I-3)	0.28(9-I-3)	0.00(6)
2094	0.00(6)	0.00(6)	-11.54(6)	-0.23(10-I-2)	-0.35(9-II-4)	0.00(6)
2095	0.00(6)	0.00(6)	-11.38(6)	-0.23(10-I-2)	-0.35(9-II-4)	0.00(6)
2096	0.00(6)	0.00(6)	-10.15(6)	-0.20(10-I-3)	-0.13(9-II-1)	0.00(6)
2097	0.00(6)	0.00(6)	-10.08(6)	-0.22(10-I-3)	-0.05(9-II-3)	0.00(6)
2098	0.00(6)	0.00(6)	-11.03(6)	-0.25(10-I-3)	0.28(9-I-2)	0.00(6)
2099	0.00(6)	0.00(6)	-11.16(6)	-0.25(10-I-3)	0.28(9-I-2)	0.00(6)
3005	-0.14(9-II-1)	-0.11(10-II-1)	-9.29(6)	0.12(10-II-1)	0.21(9-I-1)	0.02(9-I-1)
3008	-0.17(9-II-2)	-0.10(10-II-1)	-9.10(6)	0.12(10-II-1)	-0.18(9-II-1)	0.02(10-I-4)
3011	-0.33(9-II-2)	0.13(10-I-3)	-9.14(6)	-0.12(10-I-3)	-0.31(9-II-3)	0.05(9-II-3)
3014	-0.21(9-II-3)	0.10(10-I-3)	-9.35(6)	-0.13(10-I-3)	-0.27(9-II-3)	-0.06(9-II-2)
3028	0.05(9-I-2)	-0.11(10-II-1)	-9.36(6)	0.09(10-II-1)	0.03(9-I-4)	-0.02(9-II-1)
3029	0.05(9-I-2)	-0.13(10-II-1)	-9.43(6)	0.09(10-II-1)	0.04(9-I-2)	0.02(9-II-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
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Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
3030	0.05(9-I-2)	-0.12(10-II-1)	-9.48(6)	0.10(10-II-1)	0.07(6)	0.01(9-II-2)
3031	0.04(9-I-2)	-0.08(10-II-1)	-9.29(6)	0.08(10-II-1)	0.02(9-I-2)	-0.02(9-II-2)
3032	-0.14(9-II-1)	-0.11(10-II-1)	-9.32(6)	0.09(10-II-1)	0.13(9-I-1)	0.00(10-I-4)
3033	0.04(9-I-2)	-0.13(10-II-1)	-9.33(6)	0.11(10-II-1)	0.05(6)	0.02(9-II-2)
3034	0.04(9-I-2)	-0.12(10-II-1)	-9.38(6)	0.11(10-II-1)	0.07(6)	0.01(9-II-2)
3036	0.07(10-II-2)	-0.09(10-II-1)	-9.23(6)	0.08(10-II-1)	0.03(9-I-4)	-0.01(9-II-2)
3037	0.05(9-I-2)	-0.08(10-II-1)	-9.26(6)	0.06(10-II-1)	0.02(9-I-2)	-0.01(9-II-2)
3038	-0.04(9-II-2)	-0.13(10-II-1)	-9.28(6)	0.10(10-II-1)	0.04(6)	0.02(10-II-1)
3039	-0.04(9-II-2)	-0.12(10-II-1)	-9.33(6)	0.10(10-II-1)	0.07(6)	0.01(9-I-1)
3042	0.06(10-II-2)	0.04(10-I-1)	-9.10(6)	-0.02(10-I-1)	0.03(10-II-2)	0.01(10-I-4)
3043	-0.05(9-II-2)	-0.06(10-II-1)	-9.11(6)	0.04(10-II-1)	-0.04(9-II-2)	0.02(10-II-2)
3044	-0.15(9-II-2)	-0.10(10-II-1)	-9.02(6)	0.08(10-II-1)	-0.10(9-II-2)	0.04(10-I-4)
3045	-0.15(9-II-2)	-0.07(10-II-1)	-9.02(6)	0.09(10-II-1)	-0.08(9-II-2)	0.04(10-I-4)
3047	0.05(10-II-1)	0.06(10-I-1)	-9.10(6)	-0.05(10-I-1)	0.03(10-II-1)	0.01(10-I-4)
3048	-0.07(9-II-2)	-0.06(10-II-1)	-9.08(6)	0.04(10-II-1)	-0.04(9-II-2)	0.01(10-II-2)
3049	-0.17(9-II-2)	-0.09(10-II-1)	-9.03(6)	0.06(10-II-1)	-0.11(9-II-2)	0.03(9-I-1)
3050	-0.22(9-II-2)	-0.09(10-II-1)	-8.94(6)	0.05(10-II-1)	-0.12(9-II-2)	0.04(6)
3051	-0.22(9-II-2)	-0.06(10-II-1)	-8.91(6)	0.07(10-II-1)	-0.11(9-II-2)	0.06(6)
3053	0.02(10-II-1)	0.08(10-I-1)	-9.12(6)	-0.06(10-I-1)	0.03(10-II-1)	0.07(10-II-1)
3054	-0.26(9-II-2)	-0.09(10-II-1)	-8.89(6)	0.07(10-II-1)	-0.14(9-II-2)	-0.01(10-II-1)
3055	-0.26(9-II-2)	-0.06(10-II-1)	-8.86(6)	0.07(10-II-1)	-0.11(9-II-2)	0.04(6)
3056	-0.10(9-II-2)	0.21(10-I-4)	-9.13(6)	-0.12(10-I-3)	-0.06(9-II-2)	0.07(10-II-1)
3057	-0.19(9-II-2)	0.11(10-I-3)	-9.03(6)	-0.07(10-I-1)	-0.11(9-II-2)	-0.08(9-I-3)
3058	-0.10(9-II-3)	0.01(9-I-1)	-9.61(6)	-0.01(10-I-4)	-0.07(9-II-4)	0.07(10-I-4)
3059	-0.12(9-II-3)	0.19(10-I-4)	-9.44(6)	-0.08(10-I-4)	-0.08(9-II-4)	0.04(9-II-2)
3060	-0.14(9-II-4)	0.20(10-I-4)	-9.28(6)	-0.13(10-I-3)	-0.08(9-II-4)	-0.01(9-II-2)
3064	-0.12(9-II-3)	0.13(10-I-4)	-9.50(6)	-0.09(10-I-4)	-0.10(9-II-4)	0.10(10-I-3)
3066	-0.15(9-II-3)	0.06(9-I-1)	-9.56(6)	-0.10(10-I-4)	-0.11(9-II-4)	0.10(10-I-3)
3068	-0.14(9-II-3)	0.00(9-II-3)	-9.54(6)	-0.04(9-II-3)	-0.08(9-II-4)	-0.03(10-I-3)
3069	-0.19(9-II-4)	-0.01(10-II-3)	-9.43(6)	-0.02(10-I-3)	-0.06(6)	-0.05(9-II-4)
3070	-0.12(9-II-3)	0.02(9-II-3)	-9.63(6)	-0.01(10-I-4)	-0.08(9-II-4)	-0.03(9-I-2)
3071	-0.11(9-II-3)	0.01(9-II-3)	-9.56(6)	0.04(10-II-4)	0.07(9-I-4)	-0.02(10-II-2)
3072	-0.16(9-II-3)	-0.02(10-II-3)	-9.38(6)	0.02(10-II-3)	-0.29(9-II-4)	-0.01(9-II-3)
3073	-0.08(9-II-3)	0.00(9-II-3)	-9.56(6)	0.01(10-II-4)	-0.06(9-II-3)	-0.05(10-I-3)
3074	-0.10(9-II-4)	-0.02(10-II-3)	-9.42(6)	-0.03(10-I-3)	-0.06(9-II-4)	-0.07(10-I-3)
3075	-0.06(10-II-2)	-0.02(10-I-2)	-9.54(6)	0.02(6)	-0.05(10-II-3)	-0.01(6)
3076	-0.06(9-II-3)	0.02(10-I-3)	-9.44(6)	-0.03(10-I-3)	-0.05(9-II-4)	-0.05(10-I-3)
3077	-0.06(9-II-3)	-0.01(9-I-3)	-9.52(6)	0.01(6)	-0.06(10-II-3)	0.03(10-I-3)
3078	-0.07(9-II-3)	0.04(10-I-3)	-9.47(6)	-0.03(10-I-3)	-0.05(9-II-3)	0.03(9-II-3)
3079	-0.07(9-II-3)	0.02(10-I-3)	-9.49(6)	-0.01(10-I-3)	-0.06(9-II-3)	0.03(10-I-3)
3084	-0.13(9-II-3)	0.05(10-I-3)	-9.50(6)	-0.03(10-I-3)	-0.09(9-II-3)	0.03(9-II-3)
3085	-0.14(9-II-3)	0.10(10-I-3)	-9.37(6)	-0.08(10-I-3)	-0.13(9-II-3)	-0.04(9-II-3)
4001	-3.42(9-II-1)	1.90(10-I-2)	-11.04(6)	0.24(10-II-2)	0.58(9-I-1)	0.08(10-I-4)
4002	-3.42(9-II-1)	1.77(10-I-3)	-9.95(6)	0.16(10-II-1)	-0.45(9-II-1)	0.08(10-I-4)
4003	-3.42(9-II-1)	1.95(10-I-4)	-10.89(6)	-0.25(10-I-4)	-0.29(9-II-1)	0.08(10-I-4)
4004	-3.20(9-II-1)	1.90(10-I-2)	-10.43(6)	0.29(10-II-2)	-0.85(9-II-1)	0.08(10-I-4)
4005	-3.20(9-II-1)	1.77(10-I-3)	-9.29(6)	0.33(10-II-1)	-0.50(9-II-1)	0.08(10-I-4)
4006	-3.20(9-II-1)	1.95(10-I-4)	-10.19(6)	0.31(10-II-4)	0.92(9-I-1)	0.08(10-I-4)
4007	-3.01(9-II-1)	1.90(10-I-2)	-10.18(6)	-0.27(10-I-2)	-1.02(9-II-1)	0.08(10-I-4)
4008	-3.01(9-II-1)	1.77(10-I-3)	-9.11(6)	-0.36(10-I-1)	-0.47(9-II-1)	0.08(10-I-4)
4009	-3.01(9-II-1)	1.95(10-I-4)	-9.83(6)	-0.25(10-I-4)	1.03(9-I-1)	0.08(10-I-4)
4010	-3.02(9-II-3)	1.90(10-I-2)	-10.21(6)	-0.19(10-I-2)	-1.10(9-II-3)	0.08(10-I-4)
4011	-3.02(9-II-3)	1.77(10-I-3)	-9.15(6)	-0.21(10-I-3)	-0.43(9-II-3)	0.08(10-I-4)
4012	-3.02(9-II-3)	1.95(10-I-4)	-9.75(6)	-0.17(10-I-4)	1.08(9-I-3)	0.08(10-I-4)
4013	-3.23(9-II-3)	1.90(10-I-2)	-10.55(6)	-0.24(10-I-2)	-0.90(9-II-3)	0.08(10-I-4)
4014	-3.23(9-II-3)	1.77(10-I-3)	-9.36(6)	-0.27(10-I-3)	-0.48(9-II-3)	0.08(10-I-4)
4015	-3.23(9-II-3)	1.95(10-I-4)	-10.16(6)	-0.25(10-I-4)	0.93(9-I-3)	0.08(10-I-4)
4016	-3.45(9-II-3)	1.90(10-I-2)	-11.19(6)	-0.33(10-I-2)	0.57(9-I-3)	0.08(10-I-4)
4017	-3.45(9-II-3)	1.77(10-I-3)	-10.01(6)	-0.29(10-I-3)	-0.46(9-II-3)	0.08(10-I-4)
4018	-3.45(9-II-3)	1.95(10-I-4)	-10.87(6)	-0.32(10-I-4)	-0.32(9-II-3)	0.08(10-I-4)

Risultati Analisi Dinamica - Reazioni massime - Nodi - S.I.E
Scenario di calcolo: ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO

Nodo	Rx	Ry	Rz	Mx	My	Mz
	kg	kg	kg	kg*m	kg*m	kg*m
1	-22170(9-II-4)	-2656(10-II-3)	0	0	0	3255(9-II-4)
34	-2373(9-II-4)	571(10-I-3)	0	0	0	70(9-II-4)
35	-2006(9-II-4)	599(10-I-3)	0	0	0	-6(9-I-3)
36	-1921(9-II-4)	760(10-I-3)	0	0	0	-13(10-II-3)
37	-1940(9-II-4)	768(10-I-3)	0	0	0	-27(10-II-3)
38	-1432(9-II-4)	-788(10-II-3)	0	0	0	20(9-II-4)
39	-1807(9-II-4)	-648(10-II-3)	0	0	0	-3(10-II-3)
40	-1368(9-II-3)	633(10-I-3)	0	0	0	-20(10-II-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
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Nodo	Rx	Ry	Rz	Mx	My	Mz
41	-1307 (9-II-3)	766 (10-I-3)	0	0	0	-10 (10-II-2)
42	-2046 (9-II-4)	423 (10-I-3)	0	0	0	3 (9-I-4)
43	-1520 (9-II-4)	-270 (10-II-3)	0	0	0	24 (10-I-3)
44	-1621 (9-II-4)	156 (10-I-3)	0	0	0	21 (9-II-3)
45	-979 (9-II-3)	813 (10-I-3)	0	0	0	-15 (9-II-3)
46	-717 (9-II-3)	846 (10-I-3)	0	0	0	-5 (9-II-2)
47	-1069 (9-II-4)	-908 (10-II-3)	0	0	0	-41 (9-II-4)
48	-202 (9-II-4)	-162 (10-II-3)	0	0	0	19 (9-II-2)
49	-316 (9-II-4)	-526 (10-II-3)	0	0	0	47 (9-II-4)
50	-210 (9-II-4)	439 (10-I-3)	0	0	0	7 (10-II-3)
51	-359 (9-II-3)	666 (10-I-3)	0	0	0	-3 (10-I-3)
52	486 (9-II-4)	-155 (10-I-3)	0	0	0	-10 (9-II-4)
2001	-9354 (9-I-1)	-19088 (10-I-2)	0	0	0	-729 (9-II-1)
2002	-16991 (9-I-1)	4660 (10-II-3)	0	0	0	751 (9-I-1)
2003	10448 (9-II-1)	-18846 (10-I-4)	0	0	0	621 (9-I-1)
2004	6633 (9-II-1)	-14470 (10-I-2)	0	0	0	-657 (10-I-2)
2005	-4032 (9-I-1)	-8592 (10-I-3)	0	0	0	2053 (9-I-1)
2006	11266 (9-II-1)	-15130 (10-I-4)	0	0	0	603 (10-I-4)
2007	6017 (9-II-1)	-9237 (10-I-2)	0	0	0	-565 (10-I-2)
2009	11267 (9-II-1)	-10725 (10-I-4)	0	0	0	-546 (10-II-4)
2010	-5411 (9-I-3)	10201 (10-II-2)	0	0	0	480 (10-II-2)
2012	11451 (9-II-3)	-9445 (10-I-4)	0	0	0	620 (10-I-4)
2013	-10801 (9-I-3)	12428 (10-II-2)	0	0	0	598 (10-II-2)
2014	14609 (9-I-3)	2451 (6)	0	0	0	3291 (9-II-3)
2015	-6254 (9-I-3)	12687 (10-II-4)	0	0	0	-1221 (10-II-4)
2016	-10150 (9-I-3)	19607 (10-II-2)	0	0	0	647 (9-II-3)
2017	-16592 (9-I-3)	7504 (10-II-1)	0	0	0	738 (9-II-3)
2018	7685 (9-II-3)	16550 (10-II-4)	0	0	0	-1716 (10-II-4)
2019	-87 (10-II-2)	-95 (9-II-1)	0	0	0	0
2020	877 (10-II-2)	105 (10-I-2)	0	0	0	18 (10-I-2)
2021	-300 (9-II-1)	-94 (10-I-3)	0	0	0	8 (9-II-1)
2022	-465 (9-I-4)	147 (10-I-3)	0	0	0	-15 (9-II-1)
2023	-874 (10-II-4)	88 (10-I-4)	0	0	0	-15 (10-I-4)
2024	77 (10-II-4)	-92 (9-I-1)	0	0	0	0
2025	-106 (9-II-1)	944 (9-II-1)	0	0	0	-11 (10-I-2)
2026	-2773 (9-II-1)	5180 (9-II-1)	0	0	0	379 (9-II-1)
2027	94 (9-I-1)	776 (9-I-1)	0	0	0	15 (10-I-3)
2031	-21190 (10-II-1)	-17588 (10-II-2)	0	0	0	611 (10-II-1)
2032	-1686 (10-I-4)	-5523 (10-II-3)	0	0	0	98 (9-I-1)
2033	6509 (9-I-2)	-4203 (10-II-1)	0	0	0	438 (10-II-1)
2035	140 (9-I-1)	383 (9-II-1)	0	0	0	-8 (10-I-2)
2038	9773 (10-II-1)	-1492 (10-II-1)	0	0	0	-1296 (10-I-3)
2040	68 (9-I-1)	224 (9-I-2)	0	0	0	-5 (10-II-4)
2041	136 (9-I-1)	815 (9-II-1)	0	0	0	6 (10-II-2)
2043	-18189 (10-II-1)	-8215 (10-I-4)	0	0	0	-1087 (10-II-1)
2044	30066 (10-I-3)	5835 (6)	0	0	0	1015 (10-I-1)
2046	-103 (9-II-1)	278 (10-II-2)	0	0	0	-13 (10-II-4)
2048	1889 (9-I-2)	-11397 (9-II-3)	0	0	0	-300 (10-II-1)
2052	-779 (9-II-4)	1967 (10-I-3)	0	0	0	46 (10-I-3)
2061	221 (9-I-3)	-511 (10-II-2)	0	0	0	18 (10-II-2)
2062	10165 (10-I-4)	-2041 (10-II-1)	0	0	0	-791 (10-I-4)
2063	-103 (9-II-3)	344 (10-II-2)	0	0	0	12 (10-I-4)
2078	-4954 (9-II-2)	2365 (10-I-2)	0	0	0	495 (9-II-3)
2080	88 (9-I-3)	-475 (10-I-4)	0	0	0	-10 (10-I-2)
2081	63 (9-I-3)	161 (10-II-3)	0	0	0	6 (10-I-4)
2082	-2529 (9-II-2)	3654 (10-I-2)	0	0	0	133 (9-II-4)
2083	-7553 (9-II-4)	4936 (10-I-2)	0	0	0	-37 (10-I-2)
2084	-4105 (10-I-2)	10058 (10-I-3)	0	0	0	490 (9-II-3)
2085	4344 (9-I-2)	9645 (10-I-3)	0	0	0	-118 (10-II-1)
2086	-733 (6)	-782 (6)	0	0	0	34 (10-I-1)
2087	3439 (9-II-3)	-3396 (10-II-2)	0	0	0	-117 (9-II-3)
2088	-970 (9-II-3)	-2330 (10-I-3)	0	0	0	-21 (9-II-2)
2089	3392 (10-II-1)	-6598 (9-I-3)	0	0	0	299 (9-I-4)
2090	-5859 (10-I-2)	-5850 (9-I-3)	0	0	0	-1315 (10-I-4)
2091	-117 (9-II-3)	-836 (9-II-3)	0	0	0	-11 (9-II-3)
2092	-766 (9-II-3)	-1473 (10-I-3)	0	0	0	-38 (9-II-1)
2093	127 (9-I-3)	-653 (9-I-3)	0	0	0	11 (9-I-4)
2094	-67 (10-I-2)	98 (9-II-3)	0	0	0	0
2095	870 (10-I-2)	-70 (10-II-2)	0	0	0	10 (10-I-2)
2096	-476 (9-II-3)	51 (10-II-2)	0	0	0	-9 (9-II-3)
2097	-835 (9-I-3)	-53 (10-II-1)	0	0	0	13 (9-II-3)
2098	-596 (10-I-3)	-56 (10-II-4)	0	0	0	-7 (10-I-4)
2099	59 (10-I-4)	83 (9-I-3)	0	0	0	0

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Travi - S.L.E



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
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Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Asta	N.in. N.fin.	N kg	Ty kg	Tz kg	Mt kg*m	My kg*m	Mz kg*m
301	3071	-1293 (9-II-2)	139 (10-I-3)	-3093 (6)	-32 (9-I-3)	2051 (6)	314 (9-I-2)
	3072	-1293 (9-II-2)	139 (10-I-3)	2808 (9-I-4)	-32 (9-I-3)	1466 (9-I-4)	-259 (10-I-3)
401	4001	0	5 (10-I-2)	-5394 (9-II-1)	4019 (10-I-2)	6356 (9-II-1)	19 (10-I-2)
	4002	0	5 (10-I-2)	6392 (9-I-1)	-3958 (10-II-2)	10401 (9-I-1)	-19 (10-I-2)
401	4002	0	-8 (10-I-4)	-5944 (9-II-1)	3432 (10-II-4)	9871 (9-II-1)	-28 (10-I-4)
	4003	0	-8 (10-I-4)	4647 (9-I-1)	-3533 (10-I-4)	5233 (9-I-1)	28 (10-I-4)
402	4003	0	85 (9-I-2)	-8310 (10-II-4)	3012 (9-I-2)	6900 (10-II-4)	197 (9-I-2)
	4006	0	85 (9-I-2)	9539 (10-I-4)	-1909 (9-II-2)	8460 (10-I-4)	-197 (9-I-2)
402	4006	0	27 (9-I-3)	-7487 (10-II-4)	2165 (9-I-3)	6215 (10-II-4)	55 (9-I-3)
	4009	0	27 (9-I-3)	8367 (10-I-4)	-1920 (9-II-3)	8027 (10-I-4)	-55 (9-I-3)
402	4009	0	7 (10-II-4)	-9515 (10-II-4)	2700 (10-II-4)	8228 (10-II-4)	19 (10-II-4)
	4012	0	7 (10-II-4)	9843 (10-I-4)	-2624 (10-I-4)	10546 (10-I-4)	-19 (10-II-4)
402	4012	0	-20 (9-I-1)	-8833 (10-II-4)	2339 (9-II-1)	8364 (10-II-4)	-48 (9-I-1)
	4015	0	-20 (9-I-1)	8301 (10-I-4)	-2598 (9-I-1)	8169 (10-I-4)	48 (9-I-1)
402	4015	0	-110 (9-I-3)	-8633 (10-II-4)	1678 (9-II-3)	7721 (10-II-4)	-240 (9-I-3)
	4018	0	-110 (9-I-3)	7507 (10-I-4)	-2959 (9-I-3)	6403 (10-I-4)	240 (9-I-3)
403	4011	0	5 (10-II-4)	-1505 (9-I-3)	65 (10-II-4)	2370 (9-I-3)	19 (10-II-4)
	4010	0	5 (10-II-4)	1914 (9-II-3)	65 (10-II-4)	3996 (9-II-3)	-19 (10-II-4)
403	4012	0	-4 (10-II-2)	-1826 (9-I-3)	-46 (10-II-2)	3796 (9-I-3)	-15 (10-II-2)
	4011	0	-4 (10-II-2)	1354 (9-II-3)	-46 (10-II-2)	2146 (9-II-3)	15 (10-II-2)
404	4004	0	-106 (9-II-4)	-9684 (10-I-2)	1731 (9-I-4)	8467 (10-I-2)	-246 (9-II-4)
	4001	0	-106 (9-II-4)	8671 (10-II-2)	-3184 (9-II-4)	7448 (10-II-2)	246 (9-II-4)
404	4007	0	-37 (9-II-3)	-8508 (10-I-2)	1866 (9-I-3)	8002 (10-I-2)	-73 (9-II-3)
	4004	0	-37 (9-II-3)	7791 (10-II-2)	-2221 (9-II-3)	6523 (10-II-2)	73 (9-II-3)
404	4010	0	-10 (10-I-4)	-10070 (10-I-2)	2600 (10-II-4)	10681 (10-I-2)	-27 (10-I-4)
	4007	0	-10 (10-I-4)	9870 (10-II-2)	-2731 (10-I-4)	8641 (10-II-2)	27 (10-I-4)
404	4013	0	25 (9-II-1)	-9056 (10-I-2)	2641 (9-II-1)	8851 (10-I-2)	59 (9-II-1)
	4010	0	25 (9-II-1)	9564 (10-II-2)	-2296 (9-I-1)	8805 (10-II-2)	-59 (9-II-1)
404	4016	0	135 (9-II-4)	-8194 (10-I-2)	3134 (9-II-4)	7058 (10-I-2)	294 (9-II-4)
	4013	0	135 (9-II-4)	9263 (10-II-2)	-1496 (9-I-4)	8137 (10-II-2)	-294 (9-II-4)
405	4005	0	-4 (10-I-4)	-1605 (9-I-1)	-56 (10-I-4)	2632 (9-I-1)	-16 (10-I-4)
	4004	0	-4 (10-I-4)	1831 (9-II-1)	-56 (10-I-4)	3523 (9-II-1)	16 (10-I-4)
405	4005	0	7 (10-I-2)	-1523 (9-II-1)	71 (10-I-2)	2669 (9-II-1)	23 (10-I-2)
	4006	0	7 (10-I-2)	1692 (9-I-1)	71 (10-I-2)	3246 (9-I-1)	-23 (10-I-2)
406	4008	0	-5 (10-I-4)	-1532 (9-I-1)	-68 (10-I-4)	2435 (9-I-1)	-20 (10-I-4)
	4007	0	-5 (10-I-4)	1894 (9-II-1)	-68 (10-I-4)	3858 (9-II-1)	20 (10-I-4)
406	4008	0	8 (10-I-2)	-1424 (9-II-1)	85 (10-I-2)	2382 (9-II-1)	28 (10-I-2)
	4009	0	8 (10-I-2)	1776 (9-I-1)	85 (10-I-2)	3599 (9-I-1)	-28 (10-I-2)
407	4002	0	11 (9-I-3)	-11273 (10-II-3)	88 (9-I-3)	9560 (10-II-3)	25 (9-I-3)
	4005	0	11 (9-I-3)	12214 (10-I-3)	88 (9-I-3)	10588 (10-I-3)	-25 (9-I-3)
407	4005	0	8 (10-II-4)	-10510 (10-II-3)	47 (10-II-4)	8834 (10-II-3)	15 (10-II-4)
	4008	0	8 (10-II-4)	11445 (10-I-3)	47 (10-II-4)	10661 (10-I-3)	-15 (10-II-4)
407	4008	0	6 (9-II-1)	-13227 (10-II-3)	60 (9-II-1)	11650 (10-II-3)	15 (9-II-1)
	4011	0	6 (9-II-1)	12966 (10-I-3)	60 (9-II-1)	13907 (10-I-3)	-15 (9-II-1)
407	4011	0	-6 (9-II-3)	-12305 (10-II-1)	-52 (9-II-3)	11398 (10-II-1)	-14 (9-II-3)
	4014	0	-6 (9-II-3)	11316 (10-I-1)	-52 (9-II-3)	11513 (10-I-1)	14 (9-II-3)
407	4014	0	-16 (9-I-1)	-10954 (10-II-1)	-117 (9-I-1)	9470 (10-II-1)	-36 (9-I-1)
	4017	0	-16 (9-I-1)	10421 (10-I-1)	-117 (9-I-1)	9149 (10-I-3)	36 (9-I-1)
408	4014	0	6 (10-II-4)	-1601 (9-I-3)	73 (10-II-4)	2652 (9-I-3)	21 (10-II-4)
	4013	0	6 (10-II-4)	1844 (9-II-3)	73 (10-II-4)	3605 (9-II-3)	-21 (10-II-4)
408	4015	0	-8 (10-II-2)	-1739 (9-I-3)	-82 (10-II-2)	3402 (9-I-3)	-27 (10-II-2)
	4014	0	-8 (10-II-2)	1477 (9-II-3)	-82 (10-II-2)	2511 (9-II-3)	27 (10-II-2)
409	4017	0	-6 (10-II-2)	-6403 (9-I-3)	3932 (10-I-2)	10447 (9-I-3)	-24 (10-II-2)
	4016	0	-6 (10-II-2)	5392 (9-II-3)	-4048 (10-II-2)	6347 (9-II-3)	24 (10-II-2)
409	4018	0	10 (10-II-4)	-4669 (9-I-3)	3559 (10-II-4)	5263 (9-I-3)	33 (10-II-4)
	4017	0	10 (10-II-4)	5922 (9-II-3)	-3411 (10-I-4)	9746 (9-II-3)	-33 (10-II-4)

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Pilastri - S.L.E
Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
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Asta	N.in. N.fin.	N kg	Ty kg	Tz kg	Mt kg*m	My kg*m	Mz kg*m
2001	2001	-15723 (10-II-1)	-740 (9-II-1)	1242 (10-I-2)	59 (10-I-4)	-4044 (10-I-2)	2342 (9-I-1)
	4001	-13680 (10-II-1)	-740 (9-II-1)	1242 (10-I-2)	59 (10-I-4)	2725 (10-I-2)	2332 (9-II-1)
2002	2002	-24794 (10-II-1)	1900 (9-I-1)	576 (10-I-3)	59 (10-I-4)	-1675 (10-I-3)	5355 (9-I-1)
	4002	-22750 (10-II-1)	1900 (9-I-1)	576 (10-I-3)	59 (10-I-4)	1462 (10-I-3)	-5000 (9-I-1)
2003	2003	-14494 (10-II-1)	-886 (9-II-1)	1246 (10-I-4)	59 (10-I-4)	-4117 (10-I-4)	-2751 (9-II-1)
	4003	-12451 (10-II-1)	-886 (9-II-1)	1246 (10-I-4)	59 (10-I-4)	2673 (10-I-4)	2080 (9-II-1)
2004	2004	-19783 (10-II-4)	1049 (9-I-1)	1734 (10-I-2)	59 (10-I-4)	-4710 (10-I-2)	2986 (9-I-1)
	4004	-17739 (10-II-4)	1049 (9-I-1)	1734 (10-I-2)	59 (10-I-4)	4739 (10-I-2)	-2730 (9-I-1)
2005	2005	-16508 (10-II-2)	161 (9-I-1)	1440 (9-II-3)	20 (9-I-1)	-673 (10-I-3)	487 (9-I-1)
	3005	-23778 (10-II-2)	-876 (9-I-1)	-2861 (10-I-3)	73 (10-I-4)	-2203 (10-I-3)	919 (9-I-1)
2005	3005	-25641 (10-II-1)	1293 (9-I-1)	3102 (10-I-3)	-73 (10-II-4)	-6069 (10-I-3)	-2689 (9-II-1)
	4005	-24141 (10-II-1)	1293 (9-I-1)	3102 (10-I-3)	-73 (10-II-4)	6341 (10-I-3)	-2557 (9-I-1)
2006	2006	-19125 (10-II-2)	-1186 (9-II-1)	1864 (10-I-4)	59 (10-I-4)	-5080 (10-I-4)	-3254 (9-II-1)
	4006	-17081 (10-II-2)	-1186 (9-II-1)	1864 (10-I-4)	59 (10-I-4)	5078 (10-I-4)	3208 (9-II-1)
2007	2007	-21027 (10-I-2)	1099 (9-I-1)	-1250 (10-II-2)	59 (10-I-4)	3238 (10-II-2)	2982 (9-I-1)
	4007	-18984 (10-I-2)	1099 (9-I-1)	-1250 (10-II-2)	59 (10-I-4)	-3576 (10-II-2)	-3010 (9-I-1)
2008	2008	-17339 (10-I-4)	113 (9-II-1)	-87 (10-I-3)	70 (10-I-4)	-38 (10-I-1)	403 (9-I-1)
	3008	-26359 (10-I-3)	-850 (9-I-1)	-2319 (10-I-3)	61 (10-I-4)	-1653 (10-I-3)	861 (9-I-1)
2008	3008	-27103 (10-I-3)	1289 (9-I-1)	-2479 (10-II-3)	-90 (10-II-4)	4558 (10-II-3)	2651 (9-I-1)
	4008	-25603 (10-I-3)	1289 (9-I-1)	-2479 (10-II-3)	-90 (10-II-4)	-5356 (10-II-3)	-2503 (9-I-1)
2009	2009	-20343 (10-I-4)	-1210 (9-II-1)	-1109 (10-II-4)	59 (10-I-4)	-3520 (10-I-4)	-3224 (9-II-1)
	4009	-18299 (10-I-4)	-1210 (9-II-1)	-1109 (10-II-4)	59 (10-I-4)	-3223 (10-II-4)	3369 (9-II-1)
2010	2010	-22298 (10-II-4)	1126 (9-I-3)	-1198 (10-II-2)	59 (10-I-4)	3447 (10-II-2)	2968 (9-I-3)
	4010	-20255 (10-II-4)	1126 (9-I-3)	-1198 (10-II-2)	59 (10-I-4)	-3084 (10-II-2)	-3168 (9-I-3)
2011	2011	-14744 (10-II-1)	-495 (9-I-3)	-2024 (9-II-3)	210 (9-II-3)	861 (9-II-3)	449 (9-I-3)
	3011	-25924 (10-II-1)	-1284 (9-I-3)	2576 (10-II-1)	76 (9-I-1)	1870 (10-II-3)	1356 (9-I-3)
2011	3011	-27617 (10-II-1)	1310 (9-I-3)	-2315 (10-II-3)	-114 (10-II-4)	4969 (10-II-3)	2674 (9-I-3)
	4011	-26117 (10-II-1)	1310 (9-I-3)	-2315 (10-II-3)	-114 (10-II-4)	-4292 (10-II-3)	-2565 (9-I-3)
2012	2012	-21213 (10-II-2)	-1241 (9-II-3)	-1109 (10-II-4)	59 (10-I-4)	3265 (10-II-4)	-3275 (9-II-3)
	4012	-19169 (10-II-2)	-1241 (9-II-3)	-1109 (10-II-4)	59 (10-I-4)	-2780 (10-II-4)	3489 (9-II-3)
2013	2013	-20711 (10-II-2)	1082 (9-I-3)	-1545 (10-II-2)	59 (10-I-4)	4406 (10-II-2)	3035 (9-I-3)
	4013	-18668 (10-II-2)	1082 (9-I-3)	-1545 (10-II-2)	59 (10-I-4)	-4015 (10-II-2)	-2860 (9-I-3)
2014	2014	-16536 (10-I-3)	-721 (9-I-3)	401 (10-II-3)	-252 (9-II-3)	102 (6)	-51 (10-II-1)
	3014	-24797 (10-I-3)	-1616 (9-I-3)	-2340 (10-I-1)	-75 (9-II-1)	1763 (10-II-1)	1554 (9-I-3)
2014	3014	-24935 (10-I-3)	1441 (9-I-3)	-2442 (10-II-1)	123 (9-II-3)	5051 (10-II-1)	2978 (9-I-3)
	4014	-23435 (10-I-3)	1441 (9-I-3)	-2442 (10-II-1)	123 (9-II-3)	-4719 (10-II-1)	-2785 (9-I-3)
2015	2015	-19221 (10-II-4)	-1195 (9-II-3)	-1544 (10-II-4)	59 (10-I-4)	4388 (10-II-4)	-3259 (9-II-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
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Asta	N.in.	N	Ty	Tz	Mt	My	Mz
	4015	-17177 (10-II-4)	-1195 (9-II-3)	-1544 (10-II-4)	59 (10-I-4)	-4026 (10-II-4)	3254 (9-II-3)
2016	2016	-15190 (10-I-3)	-759 (9-II-3)	-1347 (10-II-2)	59 (10-I-4)	4154 (10-II-2)	2304 (9-I-3)
	4016	-13146 (10-I-3)	-759 (9-II-3)	-1347 (10-II-2)	59 (10-I-4)	-3188 (10-II-2)	2365 (9-II-3)
2017	2017	-23889 (10-I-3)	1971 (9-I-3)	-653 (10-II-1)	59 (10-I-4)	1793 (10-II-1)	5614 (9-I-3)
	4017	-21846 (10-I-3)	1971 (9-I-3)	-653 (10-II-1)	59 (10-I-4)	-1765 (10-II-1)	-5128 (9-I-3)
2018	2018	-13685 (10-I-3)	-864 (9-II-3)	-1347 (10-II-4)	59 (10-I-4)	4215 (10-II-4)	-2715 (9-II-3)
	4018	-11641 (10-I-3)	-864 (9-II-3)	-1347 (10-II-4)	59 (10-I-4)	-3125 (10-II-4)	1994 (9-II-3)

Risultati Analisi Dinamica - Sollecitazioni Massime - Muri discretizzati - S.L.E
Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Muro	Pann.	Sxx daN/cm ²	Syy daN/cm ²	Sxy daN/cm ²	Mxx kg*m/m	Myy kg*m/m	Mxy kg*m/m
1	1	0.52 (10-I-4)	0.40 (9-II-1)	-0.41 (10-I-3)	-102 (10-I-4)	-83 (9-II-4)	236 (10-I-3)
1	2	-0.15 (10-I-4)	1.49 (10-I-3)	-0.83 (10-I-4)	92 (10-I-4)	-677 (9-II-1)	350 (10-I-4)
1	3	1.65 (10-I-4)	0.20 (9-I-1)	-0.73 (10-I-3)	-783 (10-I-4)	68 (9-II-1)	317 (9-II-1)
1	4	0.44 (10-II-4)	0.56 (9-I-1)	-2.32 (10-I-3)	-316 (10-II-4)	-381 (9-I-1)	901 (10-I-3)
2	1	-0.34 (10-I-4)	1.80 (9-II-1)	-0.50 (10-II-4)	98 (10-I-4)	-1200 (9-II-1)	-399 (10-I-4)
2	2	0.44 (10-I-4)	-0.83 (9-I-1)	-0.88 (10-II-4)	107 (10-II-4)	332 (9-I-1)	-579 (10-II-1)
2	3	0.10 (10-I-4)	-2.20 (9-I-1)	-0.84 (10-II-4)	66 (10-I-4)	951 (9-I-1)	-521 (10-II-4)
2	4	0.06 (10-I-4)	-3.41 (9-I-1)	-0.76 (10-II-4)	38 (10-I-4)	1478 (9-I-1)	-450 (10-II-4)
2	5	0.04 (10-I-4)	-4.39 (10-II-2)	-0.67 (10-II-4)	28 (10-I-4)	1913 (10-II-2)	-361 (9-II-1)
2	6	0.03 (10-I-4)	-5.17 (10-II-2)	-0.57 (10-II-4)	24 (10-I-4)	2244 (10-II-1)	-274 (9-II-1)
2	7	0.03 (10-I-4)	-5.63 (10-II-1)	-0.47 (10-II-4)	22 (10-I-4)	2437 (10-II-1)	-183 (9-II-1)
2	8	0.02 (10-I-1)	-5.75 (10-II-1)	-0.37 (10-II-4)	20 (10-I-1)	2491 (10-II-1)	-93 (9-II-1)
2	9	0.01 (10-I-1)	-5.57 (10-II-1)	-0.25 (9-II-1)	17 (10-I-1)	2414 (10-II-1)	65 (9-I-1)
2	10	-0.01 (10-II-1)	-5.07 (10-II-4)	-0.15 (9-II-1)	14 (9-II-1)	2211 (10-II-4)	164 (9-I-1)
2	11	-0.02 (10-II-1)	-4.27 (10-II-4)	0.05 (10-I-4)	21 (9-II-1)	1876 (10-II-4)	269 (9-I-1)
2	12	0.03 (10-I-3)	-3.38 (9-II-1)	0.16 (10-II-2)	9 (10-I-2)	1489 (9-II-1)	386 (9-I-1)
2	13	0.24 (10-I-3)	-1.99 (9-II-1)	0.19 (9-I-1)	68 (9-I-1)	918 (9-II-1)	581 (9-I-1)
2	14	0.07 (10-II-3)	1.51 (9-I-1)	-0.55 (9-II-1)	47 (9-I-1)	-1030 (9-I-1)	513 (10-I-2)
2	15	-0.38 (10-I-4)	2.56 (9-II-1)	0.89 (10-I-4)	-315 (10-II-4)	-1575 (9-II-1)	704 (10-II-4)
2	16	0.35 (10-I-4)	-0.72 (9-I-1)	0.48 (10-I-4)	-413 (10-I-4)	-297 (9-II-1)	826 (10-II-4)
2	17	0.11 (10-I-4)	-2.15 (9-I-1)	0.31 (10-I-4)	-146 (10-I-4)	917 (9-I-1)	836 (10-II-4)
2	18	0.09 (10-I-4)	-3.37 (9-I-1)	0.15 (10-I-4)	-88 (10-I-4)	1450 (9-I-1)	777 (10-II-4)
2	19	0.06 (10-I-4)	-4.34 (10-II-2)	-0.18 (10-II-4)	-52 (10-I-4)	1890 (10-II-2)	690 (10-II-4)
2	20	0.04 (10-I-4)	-5.10 (10-II-2)	-0.25 (10-II-4)	-38 (10-I-4)	2214 (10-II-1)	591 (10-II-4)
2	21	0.03 (10-I-4)	-5.54 (10-II-1)	-0.32 (10-II-4)	-29 (10-I-1)	2400 (10-II-1)	487 (10-II-4)
2	22	0.02 (10-I-1)	-5.67 (10-II-1)	-0.37 (10-II-4)	-17 (10-I-1)	2454 (10-II-1)	373 (10-II-4)
2	23	-0.02 (10-II-1)	-5.49 (10-II-1)	-0.41 (10-II-4)	24 (10-II-1)	2383 (10-II-1)	258 (9-II-1)
2	24	-0.03 (10-II-1)	-5.02 (10-II-4)	-0.46 (9-I-3)	34 (10-II-1)	2188 (10-II-4)	156 (9-II-1)
2	25	0.03 (10-I-1)	-4.24 (10-II-4)	-0.54 (9-I-2)	29 (10-II-1)	1858 (10-II-4)	59 (9-II-1)
2	26	0.10 (9-II-1)	-3.31 (9-II-1)	-0.71 (9-I-2)	-36 (10-I-2)	1453 (9-II-1)	-141 (10-II-2)
2	27	0.36 (9-II-1)	-2.04 (9-II-1)	-1.01 (9-I-3)	-235 (10-I-2)	944 (9-II-1)	-141 (10-II-2)
2	28	0.29 (10-II-2)	2.37 (9-I-1)	-1.86 (9-II-1)	-284 (10-II-2)	-1440 (9-I-1)	524 (9-II-1)
3	1	-0.15 (10-I-3)	1.59 (9-II-1)	0.24 (9-I-1)	16 (9-II-1)	-1249 (9-II-1)	-538 (10-I-4)
3	2	0.25 (10-I-3)	-2.24 (9-I-1)	-0.59 (9-II-1)	54 (9-II-1)	1017 (9-I-1)	-714 (9-II-1)
3	3	-0.02 (10-II-1)	-3.64 (9-I-1)	-0.51 (10-II-4)	10 (10-I-1)	1602 (9-I-1)	-536 (9-II-1)
3	4	-0.05 (10-II-2)	-4.65 (9-I-1)	-0.35 (10-II-4)	19 (9-I-1)	2022 (9-I-1)	-440 (9-II-1)
3	5	-0.05 (10-II-2)	-5.60 (10-II-2)	-0.20 (10-II-4)	18 (10-I-1)	2433 (10-II-2)	-346 (9-II-1)
3	6	0.09 (9-II-3)	-6.40 (10-II-2)	0.04 (9-I-1)	32 (9-II-1)	2839 (10-II-2)	-184 (9-II-4)
3	7	0.32 (10-II-4)	2.29 (9-II-1)	1.38 (9-I-1)	-280 (10-II-4)	-1595 (9-II-1)	504 (9-II-1)
3	8	0.29 (9-I-1)	-2.26 (9-I-1)	0.61 (9-II-3)	-201 (10-I-3)	1037 (9-I-1)	578 (10-II-4)
3	9	-0.05 (9-II-1)	-3.55 (9-I-1)	0.41 (9-II-4)	56 (10-II-4)	1561 (9-I-1)	537 (10-II-4)
3	10	-0.06 (10-II-1)	-4.60 (9-I-1)	0.36 (9-II-3)	62 (10-II-1)	1981 (9-I-1)	380 (10-II-4)
3	11	-0.02 (10-II-1)	-5.56 (10-II-2)	0.39 (9-II-3)	40 (10-II-1)	2411 (10-II-2)	219 (10-II-4)
3	12	-0.11 (10-II-2)	-6.23 (10-II-2)	0.31 (10-II-2)	29 (10-II-1)	2780 (10-II-2)	74 (10-II-4)
4	1	-0.07 (9-II-3)	-7.01 (10-II-2)	0.16 (10-II-2)	8 (9-I-1)	2924 (10-II-2)	-98 (9-II-2)
4	2	0.05 (10-I-1)	-7.33 (10-II-1)	0.23 (10-II-2)	19 (10-I-1)	3148 (10-II-1)	-65 (9-II-1)
4	3	0.04 (10-I-2)	-7.38 (10-II-1)	0.32 (10-II-2)	25 (10-I-2)	3164 (10-II-1)	106 (9-I-1)
4	4	0.05 (10-I-2)	-7.07 (10-II-1)	0.40 (10-II-2)	25 (10-I-2)	3034 (10-II-1)	218 (9-I-1)
4	5	0.04 (10-I-2)	-6.39 (10-II-1)	0.47 (10-II-2)	27 (10-I-2)	2752 (10-II-1)	327 (9-I-1)
4	6	0.04 (10-I-2)	-5.34 (10-II-4)	0.55 (10-II-2)	29 (10-I-2)	2312 (10-II-1)	428 (9-I-1)
4	7	0.05 (10-I-2)	-4.11 (9-II-1)	0.64 (10-II-2)	36 (10-I-2)	1776 (9-II-1)	519 (10-II-2)
4	8	0.08 (10-I-2)	-2.65 (9-II-1)	0.74 (10-II-2)	63 (10-I-2)	1143 (9-II-1)	586 (10-II-2)
4	9	0.43 (10-I-2)	-1.04 (9-II-1)	0.82 (10-II-2)	102 (10-II-2)	430 (9-II-1)	637 (10-II-1)
4	10	-0.38 (10-I-2)	1.85 (9-I-1)	0.46 (10-II-2)	97 (10-I-2)	-1249 (9-I-1)	434 (10-I-2)
4	11	0.05 (10-I-4)	-6.94 (10-II-2)	0.35 (10-II-2)	13 (10-II-2)	2882 (10-II-2)	-143 (9-I-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
4	12	0.02 (10-I-2)	-7.20 (10-II-1)	0.33 (10-II-2)	-28 (10-I-2)	3093 (10-II-1)	-221 (10-II-2)
4	13	0.04 (10-I-2)	-7.23 (10-II-1)	0.25 (10-II-2)	-43 (10-I-2)	3105 (10-II-1)	-319 (10-II-2)
4	14	0.06 (10-I-2)	-6.93 (10-II-1)	0.15 (10-II-2)	-53 (10-I-2)	2976 (10-II-1)	-409 (10-II-2)
4	15	0.06 (10-I-2)	-6.28 (10-II-1)	-0.16 (10-I-2)	-54 (10-I-2)	2704 (10-II-1)	-492 (10-II-2)
4	16	0.06 (10-I-2)	-5.27 (10-II-4)	-0.28 (10-I-2)	-54 (10-I-2)	2280 (10-II-1)	-581 (10-II-2)
4	17	0.07 (10-I-2)	-4.06 (9-II-1)	-0.39 (10-I-2)	-77 (10-I-2)	1743 (9-II-1)	-673 (10-II-2)
4	18	0.07 (10-I-2)	-2.60 (9-II-1)	-0.51 (10-I-2)	-116 (10-I-2)	1113 (9-II-1)	-752 (10-II-2)
4	19	0.30 (10-I-2)	-0.93 (9-II-1)	-0.62 (10-I-2)	-385 (10-I-2)	368 (9-II-1)	-777 (10-II-2)
4	20	-0.41 (10-I-2)	2.53 (9-I-1)	-0.99 (10-I-2)	-276 (10-II-2)	-1596 (9-I-1)	-654 (10-II-2)
5	1	-0.15 (10-I-2)	1.57 (9-I-2)	0.85 (10-I-2)	88 (10-I-2)	-738 (9-I-1)	-371 (10-I-2)
5	2	0.53 (10-I-2)	0.44 (9-I-1)	0.41 (10-I-2)	-106 (10-I-2)	-75 (9-I-2)	-247 (10-I-3)
5	3	-0.44 (10-I-2)	0.67 (9-II-1)	2.37 (10-I-2)	-304 (10-II-2)	-445 (9-II-1)	-914 (10-I-2)
5	4	1.67 (10-I-2)	0.22 (9-II-1)	0.77 (9-I-2)	-786 (10-I-2)	80 (9-I-1)	-328 (9-I-1)
6	1	4.13 (10-I-2)	0.42 (9-II-1)	1.29 (9-II-1)	-2335 (10-I-2)	-474 (9-II-1)	-1097 (9-II-1)
6	2	2.46 (10-I-2)	0.23 (9-II-1)	0.81 (9-II-1)	-1589 (10-I-2)	75 (9-I-1)	267 (9-I-1)
6	3	1.74 (10-I-2)	0.18 (9-I-1)	-0.15 (9-I-1)	-708 (10-I-2)	-262 (9-I-1)	-926 (9-II-1)
6	4	1.55 (10-I-2)	0.26 (9-I-1)	1.09 (9-II-1)	-583 (10-I-2)	112 (9-II-1)	527 (10-I-2)
6	5	-1.30 (10-II-2)	-0.11 (9-II-1)	-0.15 (10-I-1)	640 (10-II-2)	101 (9-II-1)	-815 (9-II-1)
6	6	-1.32 (10-II-2)	-0.05 (9-II-1)	0.86 (9-II-1)	650 (10-II-2)	29 (9-I-1)	447 (10-I-2)
6	7	-2.42 (10-II-2)	-0.10 (9-II-1)	-0.10 (10-I-2)	1127 (10-II-2)	97 (9-II-1)	-636 (9-II-1)
6	8	-2.44 (10-II-2)	-0.04 (9-II-1)	0.65 (9-II-1)	1135 (10-II-2)	11 (9-I-1)	350 (10-I-2)
6	9	-3.16 (10-II-2)	-0.08 (9-II-1)	0.11 (10-II-2)	1447 (10-II-2)	86 (9-II-1)	-455 (9-II-1)
6	10	-3.22 (10-II-2)	-0.04 (9-II-1)	0.46 (9-II-1)	1467 (10-II-2)	-7 (9-II-1)	236 (10-I-2)
6	11	-3.51 (10-II-2)	-0.05 (9-II-1)	0.18 (10-II-2)	1595 (10-II-2)	69 (9-II-1)	-283 (9-II-1)
6	12	-3.60 (10-II-2)	-0.03 (9-II-1)	0.29 (9-II-1)	1627 (10-II-2)	7 (9-I-1)	114 (10-I-2)
6	13	-3.45 (10-II-1)	0.03 (9-I-1)	0.28 (10-II-2)	1568 (10-II-1)	49 (9-II-1)	-134 (9-II-1)
6	14	-3.54 (10-II-1)	-0.02 (9-II-1)	0.14 (9-II-1)	1605 (10-II-1)	13 (9-I-4)	-94 (10-II-2)
6	15	-2.97 (9-II-1)	0.09 (9-I-3)	0.48 (10-II-2)	1376 (9-II-1)	-38 (9-I-1)	-48 (9-I-2)
6	16	-3.08 (9-II-1)	0.04 (9-I-1)	0.05 (9-I-2)	1413 (9-II-1)	14 (9-I-1)	-247 (10-II-2)
6	17	-2.16 (10-I-2)	0.37 (10-I-2)	0.80 (10-II-2)	1028 (10-I-2)	-253 (9-I-1)	-66 (9-I-2)
6	18	-2.22 (10-I-2)	0.33 (9-I-1)	0.16 (9-I-3)	1037 (10-I-2)	28 (10-II-2)	-496 (10-II-2)
6	19	-1.50 (10-I-2)	0.31 (9-II-1)	1.76 (10-I-2)	-365 (10-II-2)	-214 (9-II-1)	-507 (10-I-2)
6	20	-0.39 (9-II-1)	-0.23 (9-I-1)	0.60 (9-I-3)	-321 (10-II-2)	32 (9-I-1)	-503 (9-I-1)
7	1	1.49 (10-I-2)	0.25 (9-II-1)	-0.95 (10-II-2)	-1084 (10-I-2)	-274 (9-II-1)	-367 (9-II-1)
7	2	0.76 (10-I-2)	-0.14 (9-I-1)	-0.27 (9-I-1)	-742 (10-I-2)	36 (9-I-3)	411 (9-I-1)
7	3	-2.14 (10-II-2)	0.32 (9-I-1)	-0.40 (9-I-4)	1008 (10-II-2)	-251 (9-I-1)	-511 (9-II-1)
7	4	-2.25 (10-II-2)	0.29 (9-I-1)	0.57 (9-II-1)	1058 (10-II-2)	50 (10-I-2)	450 (10-I-2)
7	5	-3.00 (10-II-2)	0.09 (9-I-1)	0.11 (9-II-4)	1359 (10-II-2)	-40 (9-I-1)	-465 (9-II-1)
7	6	-3.10 (10-II-2)	0.02 (9-I-4)	0.50 (9-II-1)	1404 (10-II-2)	19 (9-I-1)	225 (10-I-2)
7	7	-3.27 (10-II-2)	0.07 (9-I-1)	0.29 (9-II-4)	1460 (10-II-2)	-26 (9-I-1)	-352 (9-II-1)
7	8	-3.33 (10-II-2)	-0.02 (9-II-4)	0.38 (9-II-1)	1493 (10-II-2)	17 (9-I-1)	80 (10-I-2)
7	9	-3.02 (10-II-1)	0.07 (9-I-4)	0.41 (9-II-4)	1362 (10-II-1)	-30 (9-I-4)	-240 (10-I-2)
7	10	-3.09 (10-II-1)	0.02 (9-I-1)	0.26 (9-II-1)	1391 (10-II-1)	18 (9-I-4)	-147 (10-II-2)
7	11	-2.29 (10-II-4)	0.10 (9-I-3)	0.61 (10-II-4)	1065 (10-II-4)	-66 (9-I-4)	-168 (10-I-2)
7	12	-2.41 (10-II-4)	0.07 (9-I-1)	0.18 (10-I-2)	1102 (10-II-4)	20 (9-I-4)	-289 (10-II-2)
7	13	-1.25 (10-I-2)	0.29 (10-I-2)	1.01 (9-I-1)	641 (10-I-2)	-236 (9-I-2)	-203 (10-I-2)
7	14	-1.30 (10-I-2)	0.30 (9-I-2)	0.27 (10-I-2)	655 (10-I-2)	48 (10-II-2)	-516 (10-II-2)
7	15	1.41 (10-I-2)	0.35 (9-II-4)	1.77 (10-I-2)	-931 (10-II-2)	-224 (9-II-2)	-539 (10-I-2)
7	16	1.01 (10-II-2)	-0.22 (9-I-2)	0.64 (10-I-2)	-711 (10-II-2)	37 (9-I-1)	-510 (9-I-3)
8	1	1.59 (10-I-2)	0.21 (9-II-1)	-0.91 (10-II-2)	-1192 (10-I-2)	-267 (9-II-1)	-433 (9-II-1)
8	2	1.29 (10-I-2)	0.12 (9-II-1)	0.27 (9-II-1)	-1037 (10-I-2)	19 (9-I-3)	394 (9-I-1)
8	3	-1.80 (10-II-2)	0.35 (9-I-1)	-0.24 (9-I-1)	849 (10-II-2)	-246 (9-I-1)	-712 (9-II-1)
8	4	-1.86 (10-II-2)	0.26 (9-I-1)	0.74 (9-II-1)	871 (10-II-2)	43 (10-I-2)	482 (10-I-2)
8	5	-2.61 (10-II-2)	0.10 (9-I-1)	0.31 (9-II-1)	1187 (10-II-2)	-53 (9-I-1)	-694 (9-II-1)
8	6	-2.75 (10-II-2)	0.04 (9-I-4)	0.73 (9-II-1)	1251 (10-II-2)	20 (9-I-1)	266 (10-I-2)
8	7	-3.01 (10-II-2)	0.04 (9-I-1)	0.42 (9-II-1)	1346 (10-II-2)	31 (9-II-1)	-566 (9-II-1)
8	8	-3.10 (10-II-2)	-0.02 (9-II-4)	0.60 (9-II-1)	1391 (10-II-2)	18 (9-I-1)	127 (10-I-2)
8	9	-3.03 (10-II-1)	-0.05 (9-II-4)	0.48 (9-II-1)	1363 (10-II-1)	56 (9-II-4)	-436 (10-I-2)
8	10	-3.09 (10-II-1)	-0.02 (9-II-4)	0.47 (10-I-2)	1389 (10-II-1)	10 (9-I-1)	-74 (10-II-2)
8	11	-2.69 (10-II-1)	-0.09 (9-II-4)	0.47 (9-II-1)	1227 (10-II-1)	83 (9-II-4)	-278 (10-I-2)
8	12	-2.73 (10-II-1)	-0.04 (9-II-4)	0.31 (10-I-2)	1243 (10-II-1)	6 (9-I-3)	-175 (10-II-2)
8	13	-2.09 (10-II-4)	-0.12 (9-II-3)	0.44 (9-I-3)	980 (10-II-4)	113 (9-II-3)	104 (10-II-2)
8	14	-2.10 (10-II-4)	-0.07 (9-II-4)	0.12 (10-I-2)	980 (10-II-4)	6 (9-I-3)	-269 (10-II-2)
8	15	-1.23 (9-II-1)	-0.15 (9-II-3)	0.42 (9-I-3)	642 (9-II-1)	156 (9-II-3)	313 (10-II-2)
8	16	-1.25 (10-I-2)	-0.10 (9-II-4)	-0.32 (10-II-2)	634 (10-I-2)	-21 (9-II-3)	-355 (10-II-2)
8	17	0.73 (10-II-2)	0.19 (10-I-2)	0.50 (9-I-3)	185 (10-I-2)	-145 (9-I-3)	474 (10-II-2)
8	18	0.61 (10-II-2)	0.24 (9-I-3)	-0.50 (10-II-2)	187 (10-I-2)	22 (10-II-2)	-532 (10-II-2)
8	19	2.66 (10-II-2)	-0.25 (9-I-3)	1.05 (10-I-2)	-1623 (10-II-2)	-154 (9-II-3)	393 (10-II-2)
8	20	2.39 (9-I-1)	-0.21 (9-I-3)	0.25 (9-I-3)	-1452 (10-II-2)	27 (9-I-1)	-440 (9-I-3)
9	1	2.28 (10-I-2)	0.27 (9-II-4)	-2.26 (10-II-2)	-1462 (10-I-2)	-183 (9-II-2)	668 (10-II-2)
9	2	2.17 (10-I-2)	-0.31 (9-I-2)	-0.80 (9-I-1)	-1346 (10-I-2)	30 (9-I-3)	666 (9-I-1)
9	3	-1.23 (10-II-2)	0.37 (10-II-2)	-1.38 (10-I-4)	654 (10-II-2)	-263 (9-I-2)	228 (9-I-1)
9	4	-1.29 (10-II-2)	0.36 (9-I-2)	-0.34 (9-I-1)	658 (10-II-2)	29 (10-I-2)	749 (10-I-2)
9	5	-2.73 (9-II-3)	0.14 (9-I-1)	-0.95 (10-I-4)	1283 (9-II-3)	-64 (9-I-4)	167 (9-I-1)
9	6	-2.82 (9-II-3)	0.06 (9-I-3)	-0.20 (9-I-1)	1299 (9-II-3)	-14 (9-II-4)	488 (10-I-2)
9	7	-3.67 (9-II-3)	0.10 (9-I-2)	-0.58 (10-I-4)	1659 (9-II-4)	-44 (9-I-4)	189 (10-II-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

Pagina 100 di
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
9	8	-3.75 (9-II-3)	0.04 (9-I-3)	-0.22 (10-II-2)	1686 (9-II-3)	11 (9-I-1)	311 (10-I-2)
9	9	-4.02 (9-II-4)	0.06 (9-I-4)	-0.34 (10-I-4)	1799 (9-II-4)	27 (9-II-4)	252 (10-II-2)
9	10	-4.09 (9-II-4)	0.02 (9-I-4)	-0.28 (10-II-2)	1828 (9-II-4)	10 (9-I-4)	148 (10-I-2)
9	11	-3.97 (10-I-3)	0.03 (9-I-4)	-0.18 (10-I-4)	1760 (10-I-3)	43 (9-II-3)	345 (10-II-2)
9	12	-4.05 (10-I-3)	-0.02 (9-II-4)	-0.38 (10-II-2)	1796 (10-I-3)	16 (9-I-3)	-119 (10-II-2)
9	13	-3.65 (10-I-2)	0.04 (9-I-3)	-0.12 (10-I-3)	1604 (10-I-2)	37 (9-II-3)	459 (10-II-2)
9	14	-3.72 (10-I-2)	-0.02 (9-II-4)	-0.49 (10-II-2)	1647 (10-I-2)	25 (9-I-3)	-223 (10-II-2)
9	15	-2.99 (10-I-2)	-0.09 (9-I-3)	0.11 (10-II-3)	1331 (10-I-2)	-60 (9-I-3)	553 (10-II-2)
9	16	-3.09 (10-I-2)	0.03 (9-I-3)	-0.61 (10-II-2)	1384 (10-I-2)	29 (9-I-3)	-324 (10-II-2)
9	17	-2.02 (10-I-2)	0.32 (9-I-3)	0.25 (9-I-3)	902 (10-I-2)	-267 (9-I-3)	598 (9-II-3)
9	18	-2.09 (10-I-2)	0.25 (9-I-3)	-0.68 (9-II-3)	949 (10-I-2)	80 (10-II-2)	-465 (10-II-2)
9	19	1.95 (10-II-2)	0.34 (9-II-3)	0.61 (10-I-2)	-1329 (10-II-2)	-362 (9-II-3)	487 (10-II-2)
9	20	1.19 (10-II-2)	0.19 (9-II-3)	-0.29 (9-II-3)	-975 (10-II-2)	34 (10-II-2)	-325 (9-I-3)
10	1	-0.97 (10-II-2)	0.43 (9-II-3)	-1.48 (10-II-2)	-228 (10-I-2)	-245 (9-II-3)	422 (10-II-2)
10	2	0.21 (10-II-3)	-0.19 (9-I-3)	-0.49 (9-I-1)	-282 (10-II-4)	19 (9-I-3)	434 (9-I-3)
10	3	-1.50 (9-II-3)	0.22 (10-II-2)	-0.51 (10-I-2)	760 (9-II-3)	-206 (9-I-3)	-85 (9-II-3)
10	4	-1.64 (9-I-1)	0.30 (9-I-3)	0.07 (10-I-2)	810 (10-I-4)	39 (10-I-2)	362 (10-I-2)
10	5	-2.32 (10-I-3)	-0.07 (9-II-4)	-0.36 (10-I-2)	1086 (10-I-3)	73 (9-II-3)	75 (9-I-3)
10	6	-2.41 (10-I-3)	-0.05 (9-II-3)	-0.08 (9-II-3)	1114 (10-I-3)	28 (9-I-3)	161 (10-I-2)
10	7	-2.72 (10-I-2)	-0.05 (9-II-3)	-0.33 (10-I-2)	1236 (10-I-2)	59 (9-II-3)	274 (9-II-3)
10	8	-2.73 (10-I-2)	-0.04 (9-II-3)	-0.30 (9-II-3)	1240 (10-I-2)	20 (9-I-3)	55 (10-I-2)
10	9	-2.62 (10-I-2)	-0.04 (9-II-3)	-0.26 (9-II-1)	1184 (10-I-2)	45 (9-II-3)	437 (9-II-3)
10	10	-2.61 (10-I-2)	-0.03 (9-II-3)	-0.48 (9-II-3)	1189 (10-I-2)	22 (9-I-3)	-92 (10-II-2)
10	11	-1.99 (10-I-2)	0.05 (9-I-3)	-0.18 (9-II-1)	920 (10-I-2)	-49 (9-I-3)	597 (9-II-3)
10	12	-2.03 (10-I-2)	0.03 (9-I-3)	-0.65 (9-I-3)	944 (10-I-2)	32 (9-I-3)	-209 (10-II-2)
10	13	-0.75 (10-I-2)	0.24 (9-I-3)	0.34 (9-I-1)	420 (10-I-2)	-247 (9-I-3)	674 (9-II-3)
10	14	-0.90 (10-I-2)	0.26 (9-I-3)	-0.82 (9-II-3)	502 (10-I-2)	78 (10-II-2)	-391 (10-II-2)
10	15	3.63 (10-II-2)	0.35 (9-II-3)	-0.71 (9-II-3)	-1954 (10-II-2)	-391 (9-II-3)	771 (9-II-3)
10	16	2.03 (10-II-2)	0.24 (9-II-3)	-0.56 (9-II-3)	-1257 (10-II-2)	55 (9-I-3)	-331 (9-I-3)
11	1	-0.53 (10-II-2)	0.43 (9-II-3)	-1.86 (10-II-2)	-272 (10-I-2)	-317 (9-II-3)	716 (10-II-2)
11	2	1.42 (10-II-2)	0.15 (9-II-3)	-0.60 (9-I-3)	-694 (10-II-2)	71 (9-I-3)	266 (9-I-3)
11	3	-0.19 (10-II-2)	1.23 (9-I-2)	-0.67 (10-II-2)	107 (10-II-2)	-563 (9-I-3)	278 (10-II-2)
11	4	0.48 (10-II-2)	0.34 (9-I-3)	-0.35 (10-II-2)	-81 (10-II-2)	-68 (9-I-2)	207 (10-II-1)
12	1	-0.12 (10-I-4)	-5.55 (10-I-3)	0.08 (9-I-1)	55 (10-I-2)	2321 (10-I-2)	-39 (10-II-2)
12	2	-0.08 (10-I-2)	-5.65 (10-I-3)	-0.20 (9-II-1)	41 (10-I-2)	2412 (10-I-3)	149 (10-I-2)
12	3	-0.05 (10-I-2)	-5.64 (10-I-3)	-0.26 (9-II-1)	18 (10-I-2)	2414 (10-I-3)	278 (10-I-2)
12	4	-0.03 (10-I-2)	-5.47 (10-I-3)	-0.28 (10-I-2)	-25 (10-II-2)	2340 (10-I-3)	392 (10-I-2)
12	5	-0.02 (10-I-2)	-5.08 (10-I-3)	-0.28 (10-I-2)	-37 (10-II-2)	2181 (10-I-3)	500 (10-I-2)
12	6	0.04 (10-II-2)	-4.48 (10-I-3)	-0.28 (10-I-2)	-54 (10-II-2)	1929 (10-I-3)	606 (10-I-2)
12	7	0.09 (10-II-2)	-3.71 (9-II-3)	-0.26 (10-I-2)	-92 (10-II-2)	1585 (9-II-3)	705 (10-I-2)
12	8	0.16 (10-II-2)	-2.77 (9-II-3)	0.15 (10-II-2)	-170 (10-II-2)	1192 (9-II-3)	770 (10-I-2)
12	9	0.47 (10-II-2)	-1.49 (9-II-3)	0.49 (10-II-2)	-461 (10-II-2)	640 (9-II-3)	731 (10-I-2)
12	10	-0.32 (10-II-2)	1.83 (9-I-3)	1.24 (10-II-2)	-316 (10-I-2)	-1232 (9-I-3)	495 (10-I-2)
12	11	-0.03 (10-I-2)	-5.54 (10-I-3)	0.04 (10-II-2)	9 (9-I-3)	2318 (10-I-2)	-19 (9-I-1)
12	12	-0.02 (10-I-3)	-5.62 (10-I-3)	-0.15 (10-I-2)	22 (10-II-3)	2404 (10-I-3)	22 (9-II-3)
12	13	0.01 (10-II-3)	-5.62 (10-I-3)	-0.30 (10-I-2)	26 (10-II-2)	2407 (10-I-3)	-36 (9-I-3)
12	14	0.02 (10-II-2)	-5.45 (10-I-3)	-0.42 (10-I-2)	27 (10-II-2)	2337 (10-I-3)	-76 (9-I-3)
12	15	0.02 (10-II-2)	-5.07 (10-I-3)	-0.53 (10-I-2)	31 (10-II-2)	2183 (10-I-3)	-122 (9-I-3)
12	16	0.03 (10-II-2)	-4.48 (10-I-3)	-0.65 (10-I-2)	36 (10-II-2)	1939 (10-I-3)	-176 (10-I-2)
12	17	0.05 (10-II-2)	-3.74 (9-II-3)	-0.75 (10-I-2)	45 (10-II-2)	1618 (9-II-3)	-243 (10-I-2)
12	18	0.11 (10-II-2)	-2.90 (9-II-3)	-0.83 (10-I-2)	69 (10-II-2)	1260 (9-II-3)	-330 (10-I-2)
12	19	0.49 (10-II-2)	-1.74 (9-II-3)	-0.80 (10-I-2)	90 (10-I-2)	761 (9-I-3)	-477 (10-I-2)
12	20	-0.30 (10-II-2)	1.10 (9-I-3)	0.36 (10-II-2)	89 (10-II-2)	-876 (9-I-3)	-431 (10-II-2)
13	1	0.36 (10-I-4)	-1.97 (9-I-3)	-0.83 (9-I-3)	-350 (10-I-4)	-1295 (9-II-3)	-579 (9-II-3)
13	2	0.37 (9-I-3)	-2.58 (9-I-3)	-0.13 (9-II-4)	-239 (10-II-1)	1172 (9-I-3)	-793 (10-I-4)
13	3	0.04 (10-II-4)	-3.39 (9-I-3)	0.37 (9-I-4)	37 (10-I-3)	1482 (9-I-3)	-756 (10-I-4)
13	4	-0.09 (10-I-3)	-4.00 (9-I-3)	0.33 (9-I-1)	60 (10-I-3)	1723 (10-I-2)	-608 (10-I-4)
13	5	-0.13 (10-I-3)	-4.62 (10-I-2)	0.20 (9-I-1)	87 (10-I-3)	2016 (10-I-2)	-422 (10-I-4)
13	6	-0.09 (10-I-2)	-5.15 (10-I-2)	0.13 (9-I-1)	90 (10-I-3)	2318 (10-I-3)	-196 (10-I-4)
13	7	0.14 (10-I-1)	-0.78 (9-I-3)	0.28 (9-II-3)	22 (9-II-3)	-855 (9-II-3)	390 (10-II-4)
13	8	0.25 (10-II-1)	-2.64 (9-I-3)	0.83 (10-I-4)	61 (9-II-3)	1195 (9-I-3)	490 (9-II-3)
13	9	-0.03 (10-I-2)	-3.47 (9-I-3)	0.81 (10-I-4)	17 (10-II-3)	1529 (9-I-3)	294 (9-II-3)
13	10	-0.05 (10-I-2)	-3.99 (9-I-3)	0.65 (10-I-4)	25 (9-I-3)	1730 (9-I-3)	221 (9-II-3)
13	11	-0.04 (10-I-2)	-4.61 (10-I-2)	0.45 (10-I-4)	15 (10-II-3)	2011 (10-I-2)	172 (9-II-3)
13	12	-0.06 (10-I-4)	-5.12 (10-I-2)	0.19 (9-I-1)	19 (10-II-2)	2308 (10-I-3)	73 (9-II-1)
14	1	0.91 (10-II-4)	0.15 (9-I-3)	0.37 (9-II-3)	-472 (10-II-4)	44 (9-II-3)	-166 (9-II-3)
14	2	0.35 (10-I-4)	0.50 (9-I-3)	1.12 (10-II-1)	-245 (10-I-4)	-321 (9-I-3)	-415 (10-II-1)
14	3	0.34 (10-II-4)	0.22 (9-II-3)	0.20 (10-II-1)	-38 (10-II-1)	-31 (9-II-4)	-136 (10-II-1)
14	4	-0.09 (10-II-4)	0.75 (9-II-4)	0.44 (10-II-4)	69 (10-II-4)	-358 (9-II-3)	-182 (10-II-4)
15	1	-0.38 (10-II-4)	0.89 (9-II-3)	-0.86 (10-II-4)	-248 (10-I-4)	-696 (9-II-3)	-344 (10-I-4)
15	2	0.22 (9-I-3)	-1.68 (9-I-3)	-0.85 (10-II-4)	-237 (10-II-4)	709 (9-I-3)	-434 (10-I-4)
15	3	0.22 (10-II-4)	-2.94 (9-I-3)	-0.53 (10-I-4)	-219 (10-II-4)	1248 (9-I-3)	-499 (10-I-4)
15	4	0.16 (10-II-4)	-3.91 (9-I-3)	-0.27 (10-II-4)	-160 (10-II-4)	1642 (9-I-3)	-487 (10-I-4)
15	5	0.11 (10-II-4)	-4.62 (9-I-3)	0.12 (10-I-4)	-108 (10-II-4)	1949 (9-I-3)	-464 (10-I-4)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
15	6	0.07(10-II-4)	-5.08(10-I-2)	0.21(10-I-4)	-74(10-II-4)	2168(10-I-3)	-418(10-I-4)
15	7	0.04(10-II-3)	-5.39(10-I-3)	0.26(10-I-4)	-49(10-II-4)	2305(10-I-3)	-350(10-I-4)
15	8	0.02(10-II-3)	-5.47(10-I-3)	0.28(10-I-4)	-32(10-II-3)	2339(10-I-3)	-264(10-I-4)
15	9	-0.03(10-I-3)	-5.31(10-I-3)	0.30(9-I-1)	-22(10-II-3)	2277(10-I-3)	-166(10-I-4)
15	10	-0.02(10-I-3)	-4.94(10-I-4)	0.32(9-I-1)	-19(10-II-3)	2122(10-I-4)	-68(9-II-3)
15	11	0.04(10-II-3)	-4.34(10-I-4)	0.38(9-I-1)	-35(10-II-3)	1875(10-I-4)	89(10-II-4)
15	12	0.10(10-II-2)	-3.53(9-II-3)	0.54(9-I-3)	-66(10-II-3)	1522(9-II-3)	150(10-I-2)
15	13	0.42(9-II-3)	-2.53(9-II-3)	0.86(9-I-2)	-302(10-II-1)	1152(9-II-3)	139(10-I-2)
15	14	0.49(10-I-2)	-1.51(9-II-3)	1.84(9-II-3)	-372(10-I-2)	-982(9-I-3)	-542(9-II-3)
15	15	-0.27(10-II-4)	0.66(9-II-3)	-0.24(10-II-4)	61(10-II-1)	-556(9-II-3)	292(10-II-4)
15	16	0.25(10-II-4)	-1.76(9-I-3)	0.48(10-I-4)	92(10-I-4)	761(9-I-3)	430(10-II-2)
15	17	0.18(10-II-4)	-3.04(9-I-3)	0.54(10-I-4)	60(10-II-4)	1303(9-I-3)	329(10-I-4)
15	18	0.10(10-II-4)	-3.95(9-I-3)	0.52(10-I-4)	56(10-II-4)	1677(9-I-3)	252(10-I-4)
15	19	0.06(10-II-4)	-4.62(9-I-3)	0.49(10-I-4)	44(10-II-4)	1967(9-I-3)	193(10-I-4)
15	20	0.04(10-II-4)	-5.07(10-I-2)	0.44(10-I-4)	35(10-II-4)	2171(10-I-2)	137(9-II-3)
15	21	0.03(10-II-4)	-5.38(10-I-3)	0.36(10-I-4)	30(10-II-4)	2305(10-I-3)	85(9-II-3)
15	22	0.02(10-II-3)	-5.45(10-I-3)	0.27(10-I-4)	26(10-II-3)	2338(10-I-3)	36(9-II-3)
15	23	0.01(10-II-3)	-5.29(10-I-3)	0.16(10-I-4)	24(10-II-3)	2275(10-I-3)	-53(9-I-3)
15	24	-0.01(10-I-3)	-4.92(10-I-4)	0.05(9-II-3)	22(10-II-3)	2121(10-I-4)	-109(9-I-3)
15	25	-0.01(10-I-4)	-4.32(10-I-4)	-0.12(10-II-4)	29(9-II-3)	1878(10-I-4)	-179(9-I-3)
15	26	0.03(10-II-4)	-3.59(9-II-3)	-0.20(10-I-2)	25(10-II-3)	1560(9-II-3)	-268(9-I-3)
15	27	0.30(10-II-1)	-2.56(9-II-3)	-0.18(10-I-2)	81(9-I-3)	1161(9-II-3)	-466(9-I-3)
15	28	0.11(10-I-1)	0.48(9-I-3)	0.55(9-II-3)	54(9-I-3)	-526(9-I-3)	-486(10-II-2)
16	1	2.56(10-I-4)	0.18(9-I-1)	-0.72(9-I-1)	-1564(10-I-4)	79(9-II-1)	-246(9-II-1)
16	2	4.14(10-I-4)	0.37(9-I-1)	-1.19(9-I-1)	-2274(10-I-4)	-416(9-I-1)	994(9-I-1)
16	3	1.82(10-I-4)	0.28(9-II-1)	-0.96(9-I-1)	-703(10-I-4)	108(9-I-1)	-485(10-I-4)
16	4	2.00(10-I-4)	0.17(9-II-1)	0.18(9-II-1)	-824(10-I-4)	-264(9-II-1)	819(9-I-1)
16	5	-0.87(10-II-4)	-0.04(9-I-1)	-0.76(9-I-1)	448(10-II-4)	32(9-II-1)	-415(10-I-4)
16	6	-0.86(10-II-4)	-0.11(9-I-1)	0.16(10-I-1)	443(10-II-4)	89(9-I-1)	730(9-I-1)
16	7	-1.81(10-II-4)	-0.05(9-I-1)	-0.55(9-I-1)	858(10-II-4)	12(9-II-1)	-340(10-I-4)
16	8	-1.82(10-II-4)	-0.11(9-I-1)	0.14(10-I-1)	865(10-II-4)	104(9-I-1)	555(9-I-1)
16	9	-2.47(10-II-4)	-0.04(9-I-1)	-0.36(9-I-1)	1142(10-II-4)	-8(9-I-1)	-247(10-I-4)
16	10	-2.44(10-II-4)	-0.10(9-I-1)	0.13(10-I-1)	1136(10-II-4)	95(9-I-1)	374(9-I-1)
16	11	-2.78(10-II-1)	-0.04(9-I-1)	-0.18(9-I-1)	1278(10-II-1)	-6(9-I-1)	-148(10-I-4)
16	12	-2.75(10-II-1)	-0.09(9-I-1)	0.11(10-I-1)	1270(10-II-1)	92(9-I-1)	198(9-I-1)
16	13	-2.77(10-II-1)	-0.06(9-I-1)	0.10(10-I-2)	1269(10-II-1)	15(9-II-2)	-60(10-I-4)
16	14	-2.73(10-II-1)	-0.10(9-I-1)	0.14(10-I-1)	1251(10-II-1)	89(9-I-1)	-68(10-I-2)
16	15	-2.59(9-I-1)	-0.05(9-I-1)	0.27(10-I-2)	1188(9-I-1)	24(9-II-1)	107(10-II-4)
16	16	-2.52(9-I-1)	-0.04(9-I-2)	0.16(10-I-1)	1152(9-I-1)	65(9-I-1)	-225(10-I-2)
16	17	-2.24(10-I-4)	0.28(9-II-1)	0.29(10-II-4)	1029(10-I-4)	46(10-II-4)	283(10-II-4)
16	18	-2.19(10-I-4)	0.37(10-I-3)	-0.16(10-II-4)	1008(10-I-4)	-260(9-II-1)	-286(10-I-2)
16	19	-1.15(9-I-1)	0.14(9-I-1)	-0.33(9-II-3)	239(9-I-1)	33(10-II-4)	309(9-II-1)
16	20	-2.06(10-I-4)	0.40(9-I-1)	-1.14(10-I-4)	627(10-I-4)	-302(9-I-1)	277(10-I-4)
17	1	-1.19(10-II-4)	0.17(9-I-1)	0.21(9-II-1)	-358(10-I-4)	26(10-I-1)	-340(9-II-1)
17	2	-1.60(10-II-4)	0.51(9-I-1)	0.76(10-II-4)	-750(10-I-4)	-387(9-I-1)	378(9-I-1)
17	3	-2.43(10-II-4)	0.33(9-II-1)	-0.69(9-I-1)	1123(10-II-4)	62(10-I-4)	-299(10-I-4)
17	4	-2.28(10-II-4)	0.37(10-II-4)	-0.27(9-I-1)	1058(10-II-4)	-298(9-II-1)	623(9-I-1)
17	5	-2.64(10-II-4)	0.03(9-I-1)	-0.64(9-I-1)	1187(10-II-4)	28(9-II-1)	-104(10-I-4)
17	6	-2.54(10-II-4)	0.05(9-II-1)	-0.53(10-II-2)	1142(10-II-4)	40(9-I-1)	590(9-I-1)
17	7	-2.39(10-II-1)	-0.07(9-I-2)	-0.45(9-I-1)	1095(10-II-1)	11(9-II-1)	65(10-II-4)
17	8	-2.41(10-II-1)	-0.10(9-I-1)	-0.54(10-II-2)	1095(10-II-1)	98(9-I-1)	426(9-I-1)
17	9	-1.91(10-II-1)	-0.10(9-I-1)	-0.23(10-I-4)	901(10-II-1)	-6(9-I-2)	132(10-II-4)
17	10	-1.96(10-II-1)	-0.15(9-I-1)	-0.46(10-II-2)	920(10-II-1)	136(9-I-1)	230(10-I-4)
17	11	-1.35(9-I-1)	-0.10(9-I-1)	0.12(10-II-4)	665(9-I-1)	14(9-II-2)	185(10-II-4)
17	12	-1.36(9-I-1)	-0.13(9-I-3)	-0.34(10-II-2)	668(9-I-1)	129(9-I-2)	-81(10-II-4)
17	13	-0.71(10-I-4)	0.23(9-II-4)	0.26(10-II-4)	397(10-I-4)	42(10-II-4)	322(10-II-4)
17	14	-0.64(10-I-4)	0.22(10-I-4)	-0.36(10-II-2)	373(10-I-4)	-178(9-II-4)	-218(10-II-4)
17	15	0.97(10-II-4)	0.10(9-I-4)	-0.33(9-II-3)	-687(10-II-4)	35(9-II-1)	316(10-I-4)
17	16	1.34(10-II-4)	0.24(9-I-2)	-1.08(10-I-4)	-868(10-II-4)	-223(9-I-2)	266(10-I-4)
18	1	1.01(10-I-4)	-0.14(9-II-1)	0.37(9-II-1)	-849(10-I-4)	10(9-II-3)	-450(9-II-1)
18	2	1.47(10-I-4)	0.43(9-I-1)	1.24(10-II-4)	-1078(10-I-4)	-306(9-I-1)	-211(10-II-4)
18	3	-1.93(10-II-4)	0.34(9-II-4)	-0.56(10-I-4)	906(10-II-4)	44(10-I-4)	-438(10-I-4)
18	4	-1.79(10-II-4)	0.36(10-II-4)	0.28(9-II-1)	859(10-II-4)	-282(9-II-4)	514(10-I-4)
18	5	-2.61(10-II-4)	0.02(9-II-2)	-0.56(10-I-4)	1161(10-II-4)	31(9-II-1)	-244(10-I-4)
18	6	-2.51(10-II-4)	0.05(9-II-1)	-0.16(10-II-2)	1114(10-II-4)	-49(9-II-1)	525(10-I-4)
18	7	-2.91(10-II-1)	-0.05(9-I-2)	-0.42(10-I-4)	1290(10-II-1)	20(9-II-1)	-175(10-I-4)
18	8	-2.90(10-II-1)	-0.06(9-I-2)	-0.18(10-II-2)	1275(10-II-1)	56(9-I-2)	412(10-I-4)
18	9	-3.07(10-II-1)	-0.04(9-I-2)	-0.26(10-I-4)	1359(10-II-1)	13(9-II-2)	-117(10-I-4)
18	10	-3.06(10-II-1)	-0.08(9-I-2)	-0.11(10-II-2)	1352(10-II-1)	68(9-I-2)	262(10-I-4)
18	11	-3.12(6)	-0.04(9-I-2)	-0.10(10-I-4)	1378(6)	13(9-II-2)	-57(10-I-4)
18	12	-3.11(6)	-0.07(9-I-2)	0.06(6)	1369(6)	60(9-I-2)	112(10-I-4)
18	13	-3.08(10-I-3)	-0.03(9-I-2)	0.20(10-I-3)	1364(10-I-3)	22(9-II-3)	85(10-II-4)
18	14	-3.06(10-I-3)	-0.04(9-I-2)	0.08(6)	1342(10-I-3)	36(9-I-2)	-178(10-II-4)
18	15	-2.93(10-I-4)	0.04(9-II-2)	0.30(10-II-4)	1293(10-I-4)	30(9-II-3)	170(10-II-4)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
18	16	-2.80(10-I-4)	0.09(9-II-3)	-0.12(10-II-2)	1234(10-I-4)	-72(9-II-3)	-268(9-I-3)
18	17	-2.30(10-I-4)	0.35(9-II-4)	0.28(9-I-3)	1073(10-I-4)	45(10-II-4)	390(10-II-4)
18	18	-2.17(10-I-4)	0.38(10-I-4)	-0.52(9-II-3)	1025(10-I-4)	-294(9-II-4)	-264(9-I-3)
18	19	-0.44(10-I-4)	-0.15(9-II-3)	-0.55(9-II-3)	-496(10-II-4)	25(10-II-4)	464(9-II-3)
18	20	-1.30(10-I-4)	0.43(9-I-3)	-1.60(10-I-4)	-700(10-II-4)	-293(9-I-3)	449(10-I-4)
19	1	0.48(10-I-4)	0.11(9-I-4)	0.16(9-II-1)	-643(10-I-4)	30(9-II-3)	-333(9-II-1)
19	2	0.90(10-I-4)	0.29(9-I-2)	0.81(10-I-4)	-853(10-I-4)	-283(9-I-2)	386(10-I-4)
19	3	-1.37(10-II-4)	0.26(9-II-4)	-0.60(10-I-4)	644(10-II-4)	52(10-I-4)	-423(10-I-4)
19	4	-1.33(10-II-4)	0.30(10-II-4)	0.12(9-II-4)	629(10-II-4)	-237(9-II-4)	561(10-I-4)
19	5	-2.07(6)	-0.07(9-I-3)	-0.52(10-I-4)	950(6)	18(9-II-2)	-296(10-I-4)
19	6	-2.04(6)	-0.08(9-I-1)	-0.07(10-II-2)	938(6)	91(9-I-2)	488(10-I-4)
19	7	-2.68(6)	-0.06(9-I-3)	-0.35(10-I-4)	1210(6)	10(9-II-1)	-232(10-I-4)
19	8	-2.70(6)	-0.10(9-I-2)	0.07(6)	1214(6)	91(9-I-2)	349(10-I-4)
19	9	-3.16(10-I-3)	-0.04(9-I-3)	-0.19(10-I-4)	1414(10-I-3)	-6(9-I-2)	-153(10-I-4)
19	10	-3.15(10-I-3)	-0.09(9-I-3)	0.08(6)	1415(10-I-3)	85(9-I-3)	203(10-I-4)
19	11	-3.43(10-I-3)	-0.02(9-I-3)	0.08(9-I-3)	1521(10-I-3)	6(9-II-3)	-67(10-I-4)
19	12	-3.42(10-I-3)	-0.06(9-I-3)	0.06(9-I-3)	1520(10-I-3)	63(9-I-3)	70(10-I-4)
19	13	-3.37(10-I-4)	-0.05(9-I-2)	0.22(9-I-3)	1494(10-I-4)	15(9-II-3)	89(10-II-4)
19	14	-3.40(10-I-4)	-0.07(9-I-3)	-0.13(10-II-2)	1498(10-I-4)	69(9-I-3)	-177(9-I-3)
19	15	-3.06(10-I-4)	0.04(9-II-3)	0.38(9-I-3)	1378(10-I-4)	-11(9-I-3)	174(10-II-4)
19	16	-3.01(10-I-4)	0.08(9-II-3)	-0.19(10-II-2)	1353(10-I-4)	48(9-I-3)	-339(9-I-3)
19	17	-2.29(10-I-4)	0.15(9-II-4)	0.42(9-I-3)	1046(10-I-4)	70(10-II-4)	350(10-II-4)
19	18	-2.27(10-I-4)	0.19(9-II-3)	-0.50(9-II-3)	1026(10-I-4)	-160(9-II-1)	-323(9-I-3)
19	19	-1.08(10-I-4)	0.18(9-I-3)	0.20(9-I-3)	-420(10-II-4)	37(10-II-4)	240(9-II-3)
19	20	-1.30(10-I-4)	0.36(9-I-3)	-0.45(10-I-4)	-727(10-II-4)	-336(9-I-3)	-350(9-I-3)
20	1	-0.86(9-I-3)	0.09(9-I-3)	0.17(9-II-4)	127(9-I-3)	17(10-I-4)	-276(9-II-4)
20	2	-1.39(10-II-4)	0.36(9-I-3)	0.70(10-II-4)	357(10-II-4)	-245(9-I-3)	107(10-I-4)
20	3	-2.10(9-I-3)	0.17(9-II-3)	-0.18(9-I-4)	980(9-I-3)	47(10-I-4)	-312(10-I-4)
20	4	-2.04(9-I-3)	0.18(10-II-3)	0.40(10-I-3)	949(9-I-3)	-153(9-II-3)	187(10-II-2)
20	5	-2.78(10-I-3)	0.06(9-II-3)	-0.21(10-II-2)	1259(10-I-3)	18(9-II-3)	-113(10-I-4)
20	6	-2.71(10-I-3)	0.08(9-II-2)	-0.17(10-II-3)	1240(10-I-3)	-56(9-II-3)	208(10-II-2)
20	7	-2.89(10-I-3)	-0.07(9-I-3)	-0.06(10-II-2)	1313(10-I-3)	15(9-II-3)	61(10-II-4)
20	8	-2.83(10-I-3)	-0.08(9-I-3)	-0.21(10-II-3)	1292(10-I-3)	90(9-I-3)	54(10-II-2)
20	9	-2.57(10-I-4)	0.03(9-II-3)	0.24(9-I-3)	1174(10-I-4)	10(9-II-3)	178(10-II-4)
20	10	-2.54(10-I-4)	-0.05(9-I-3)	-0.23(10-II-3)	1159(10-I-4)	58(9-I-3)	-236(9-I-3)
20	11	-1.76(10-I-4)	-0.08(9-I-3)	0.41(9-I-3)	817(10-I-4)	26(9-II-3)	286(10-II-4)
20	12	-1.83(10-I-4)	-0.09(9-I-3)	-0.37(10-II-3)	838(10-I-4)	90(9-I-3)	-374(9-I-3)
20	13	-0.69(10-I-4)	0.12(9-II-3)	0.71(9-I-3)	358(10-I-4)	84(10-II-4)	308(10-II-4)
20	14	0.74(10-II-4)	0.07(9-II-3)	-0.24(9-II-3)	313(10-I-4)	-133(9-II-3)	-590(9-I-3)
20	15	1.47(10-II-4)	0.27(9-I-3)	0.53(9-I-3)	-907(10-II-4)	47(9-II-3)	184(9-II-3)
20	16	2.44(10-II-4)	0.39(9-I-3)	0.72(9-I-3)	-1336(10-II-4)	-393(9-I-3)	-666(9-I-3)
21	1	-1.97(9-I-3)	0.45(10-II-4)	0.94(10-II-4)	528(9-I-3)	175(10-I-4)	180(10-I-4)
21	2	-4.06(9-I-3)	-0.74(10-I-4)	-0.63(10-I-4)	1477(9-I-3)	1030(10-I-3)	666(10-I-4)
21	3	-2.78(9-I-3)	0.25(10-II-4)	-0.48(10-I-4)	1031(9-I-3)	-240(10-II-4)	-348(10-II-4)
21	4	-4.74(9-I-3)	-0.63(10-I-3)	-0.28(10-I-4)	1887(9-I-3)	978(10-I-4)	566(10-I-4)
21	5	-3.71(9-I-3)	-0.51(10-I-4)	-0.65(10-I-4)	1516(9-I-3)	-417(10-II-4)	-365(10-II-4)
21	6	-5.00(9-I-3)	-0.69(10-I-3)	-0.33(10-I-4)	2182(9-I-3)	980(10-I-4)	457(10-I-4)
21	7	-4.42(9-I-3)	-0.64(10-I-4)	-0.71(10-I-4)	1839(9-I-3)	-428(10-II-4)	-282(10-II-4)
21	8	-5.17(10-I-2)	-0.77(10-I-3)	-0.37(10-I-4)	2342(10-I-3)	1016(10-I-4)	385(10-I-4)
21	9	-4.92(9-I-3)	-0.72(10-I-4)	-0.69(10-I-4)	2058(9-I-3)	-392(10-II-1)	-193(10-II-4)
21	10	-5.30(10-I-3)	-0.86(10-I-3)	-0.40(10-I-4)	2427(10-I-3)	1056(10-I-3)	320(10-I-4)
21	11	-5.27(10-I-3)	-0.80(10-I-3)	-0.60(10-I-4)	2205(10-I-3)	-359(10-II-1)	-117(10-II-4)
21	12	-5.35(10-I-3)	-0.94(10-I-3)	-0.40(10-I-4)	2457(10-I-3)	1091(10-I-3)	253(10-I-4)
21	13	-5.45(10-I-3)	-0.86(10-I-3)	-0.47(10-I-4)	2281(10-I-3)	-340(10-II-2)	-56(10-II-4)
21	14	-5.33(10-I-3)	-0.99(10-I-3)	-0.40(10-I-4)	2441(10-I-3)	1110(10-I-3)	185(10-I-4)
21	15	-5.44(10-I-3)	-0.91(10-I-3)	-0.32(10-I-4)	2277(10-I-3)	-330(10-II-2)	88(9-I-1)
21	16	-5.22(10-I-3)	-1.03(10-I-3)	-0.41(9-I-1)	2384(10-I-3)	1123(10-I-3)	119(10-I-4)
21	17	-5.25(10-I-3)	-0.96(10-I-3)	-0.14(10-I-4)	2195(10-I-3)	-326(10-II-1)	116(9-I-1)
21	18	-5.02(10-I-3)	-1.06(10-I-3)	-0.43(9-I-1)	2286(10-I-3)	1130(10-I-3)	56(10-I-4)
21	19	-4.88(10-I-4)	-1.00(10-I-3)	0.20(10-II-4)	2039(10-I-4)	-345(9-I-3)	132(9-I-1)
21	20	-4.72(10-I-4)	-1.08(10-I-3)	-0.45(9-I-1)	2150(10-I-4)	1146(10-I-3)	-81(10-II-4)
21	21	-4.34(10-I-4)	-1.01(10-I-3)	0.33(10-II-4)	1817(10-I-4)	-430(9-I-3)	149(9-I-1)
21	22	-4.33(10-I-4)	-1.07(10-I-3)	-0.49(9-I-1)	2004(10-I-4)	1185(10-I-3)	-138(10-II-4)
21	23	-3.64(9-II-3)	-0.93(10-I-3)	0.40(9-II-1)	1511(9-II-3)	-602(9-I-3)	234(9-I-2)
21	24	-3.84(10-I-4)	-0.97(10-I-4)	-0.56(9-I-2)	1852(10-I-4)	1200(10-I-3)	-197(10-II-4)
21	25	-2.95(9-II-3)	-0.68(10-I-2)	0.39(9-II-2)	1139(9-II-3)	-878(9-I-3)	383(9-I-3)
21	26	-3.27(10-I-4)	-0.86(10-I-3)	-0.66(9-I-3)	1529(10-I-4)	1240(10-I-2)	-211(9-II-1)
21	27	-2.42(9-II-3)	0.94(10-II-1)	-0.99(9-I-3)	-696(9-I-3)	-457(10-II-1)	642(9-I-3)
21	28	-2.90(9-II-3)	-0.74(10-I-4)	-0.56(9-I-3)	797(9-II-3)	1208(10-I-2)	-91(9-II-2)
22	1	-2.24(10-I-4)	-2.16(9-I-3)	0.77(10-I-3)	380(10-I-3)	-508(10-II-4)	-1043(10-I-3)
22	2	-1.52(10-I-4)	-2.65(9-I-3)	0.70(10-I-4)	345(10-I-4)	-1075(10-II-4)	-1146(10-I-3)
22	3	-1.09(10-I-4)	-2.81(9-I-2)	0.52(10-I-4)	187(10-I-4)	-2033(10-II-4)	-871(10-I-4)
22	4	-0.85(10-I-4)	-2.36(10-I-3)	-0.42(10-II-4)	-330(10-II-4)	-1220(10-II-1)	-467(10-I-4)
22	5	0.42(9-I-3)	-1.24(10-I-3)	-0.80(10-II-4)	-265(10-II-4)	-796(10-II-1)	617(10-II-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
22	6	-1.89(10-II-2)	-2.94(10-I-3)	-0.54(10-II-4)	796(10-II-4)	1840(10-I-3)	457(10-II-4)
22	7	-2.42(10-I-4)	-1.90(10-I-3)	-0.26(10-II-4)	1400(10-I-4)	2101(9-I-2)	103(10-II-4)
22	8	-2.28(9-I-3)	-1.83(10-I-3)	1.11(10-I-4)	1097(9-I-3)	1971(9-I-3)	514(10-II-2)
22	9	-1.37(10-II-4)	-1.01(10-I-3)	0.90(9-II-1)	348(10-II-4)	435(9-II-1)	-172(10-II-4)
22	10	-1.99(10-II-4)	-1.31(9-I-2)	0.78(9-II-4)	629(10-II-4)	398(10-I-3)	-876(10-I-3)
22	11	-2.23(10-I-4)	-1.72(10-I-3)	0.68(10-I-3)	640(9-I-3)	403(10-I-3)	-823(10-I-3)
22	12	-1.90(10-I-4)	-2.10(10-I-3)	0.51(10-I-4)	881(10-I-4)	524(10-I-3)	-726(10-I-3)
22	13	-1.62(10-I-4)	-2.37(10-I-3)	0.36(10-I-4)	782(10-I-4)	759(9-I-3)	-691(10-I-3)
23	1	-3.85(6)	-2.94(10-II-1)	0.89(10-I-4)	4046(10-I-3)	1418(10-I-3)	492(6)
23	2	-3.50(6)	-2.55(6)	0.57(10-I-4)	4466(10-I-3)	1613(6)	287(6)
23	3	-3.29(6)	-2.32(6)	0.37(10-II-2)	4409(10-I-3)	1616(6)	189(6)
23	4	-3.11(6)	-2.13(6)	0.24(10-II-2)	4137(10-I-2)	1635(6)	-51(10-II-2)
23	5	-2.92(6)	-1.90(6)	0.10(10-II-2)	3506(10-I-2)	1629(10-II-1)	-140(10-II-2)
23	6	-2.65(6)	-1.69(6)	-0.32(6)	3232(9-II-4)	1717(10-II-1)	-70(10-I-4)
23	7	-2.88(6)	-1.97(6)	-0.16(6)	3699(10-I-2)	1655(10-II-1)	-129(9-II-3)
23	8	-3.09(6)	-2.23(6)	0.12(10-II-2)	4187(10-I-3)	1712(10-II-1)	71(6)
23	9	-3.27(6)	-2.48(6)	0.21(10-II-2)	4346(10-I-3)	1738(6)	168(6)
23	10	-3.45(6)	-2.74(6)	0.32(10-II-2)	4150(10-I-3)	1755(6)	215(6)
23	11	-3.63(9-I-2)	-2.88(6)	0.45(10-II-2)	3716(10-I-3)	1684(6)	174(6)
23	12	-3.85(9-I-2)	-2.85(6)	0.48(10-II-2)	3161(10-I-3)	1475(6)	92(6)
23	13	-4.03(9-I-2)	-2.65(6)	0.41(10-II-2)	2638(9-I-2)	1213(10-I-3)	-56(10-II-2)
23	14	-3.85(9-I-2)	-2.39(6)	0.12(10-II-2)	1995(9-I-2)	777(10-I-3)	104(6)
23	15	-3.37(9-I-2)	-2.03(6)	-0.40(6)	1418(9-I-2)	523(10-I-3)	115(6)
23	16	-1.97(9-I-2)	-1.86(10-I-3)	-0.54(6)	289(9-I-4)	116(9-I-1)	102(10-I-3)
23	17	1.80(9-II-4)	-1.41(10-I-4)	-0.84(10-I-4)	-1137(9-II-4)	-733(10-II-4)	-1309(10-II-4)
23	18	-2.01(9-I-3)	-1.82(10-I-3)	-1.22(6)	921(9-I-3)	-162(10-II-3)	-1260(10-II-3)
23	19	-3.64(9-I-2)	-2.08(6)	-1.03(6)	1894(9-I-2)	532(9-I-4)	-787(10-II-2)
23	20	-4.79(9-I-2)	-2.21(6)	-0.44(6)	2348(9-I-2)	673(6)	-606(10-II-2)
23	21	-5.35(9-I-2)	-2.41(6)	0.52(10-II-2)	2700(10-I-3)	796(6)	-409(10-II-2)
23	22	-5.27(10-I-2)	-2.72(10-II-1)	1.25(10-II-2)	2878(10-I-3)	964(6)	106(6)
23	23	-3.51(6)	-2.69(10-II-1)	0.47(10-II-2)	4261(10-I-3)	1653(6)	283(6)
23	24	-3.36(6)	-2.52(6)	0.34(10-II-2)	4371(10-I-3)	1692(6)	224(6)
23	25	-3.48(6)	-2.75(6)	0.41(10-II-2)	4170(10-I-3)	1711(6)	239(6)
23	26	-4.23(9-I-2)	-2.54(6)	0.29(10-II-2)	2649(9-I-2)	924(6)	-180(10-II-2)
23	27	-4.23(9-I-2)	-2.82(6)	0.69(10-II-2)	3503(10-I-3)	1300(6)	81(6)
23	28	-3.97(9-I-2)	-2.86(6)	0.60(10-II-2)	3341(10-I-3)	1430(6)	83(6)
23	29	-4.53(9-I-2)	-2.68(6)	0.59(10-II-2)	3052(10-I-3)	1101(6)	-165(10-II-2)
23	30	-3.68(9-I-2)	-2.91(6)	0.55(10-II-2)	3812(10-I-3)	1626(6)	192(6)
23	31	-3.78(9-I-2)	-2.91(6)	0.69(10-II-2)	3855(10-I-3)	1510(6)	203(6)
24	1	-2.15(10-II-2)	-2.33(6)	-0.48(10-II-4)	1383(10-I-3)	2456(10-I-2)	1143(10-II-2)
24	2	-2.64(10-II-2)	-2.17(6)	-0.34(10-II-4)	2012(10-I-3)	3690(10-I-2)	1388(10-II-3)
24	3	-3.14(10-II-2)	-2.04(6)	-0.22(10-II-1)	2242(10-I-3)	4280(10-I-3)	1422(10-II-3)
24	4	-3.75(10-II-2)	-2.02(6)	-0.23(10-I-1)	2277(10-I-3)	4507(10-I-3)	1618(10-II-3)
24	5	-3.41(10-I-2)	-1.64(6)	0.31(9-II-2)	1844(10-I-3)	4696(10-I-3)	1560(10-II-3)
24	6	-2.66(10-II-2)	-1.12(6)	0.98(9-I-3)	1721(10-I-3)	4765(10-I-3)	1376(10-II-3)
24	7	-1.73(10-II-2)	-0.28(6)	1.59(10-I-3)	1130(10-II-2)	4453(10-I-3)	1061(10-II-3)
24	8	-0.64(6)	0.46(9-II-3)	1.69(10-I-3)	701(10-II-2)	3891(10-I-3)	948(10-II-3)
24	9	0.43(9-II-2)	0.37(9-II-2)	1.30(10-I-3)	-570(9-II-2)	2778(6)	285(10-II-3)
24	10	-0.88(6)	0.50(10-II-2)	1.12(10-I-3)	-786(10-II-2)	1432(9-II-3)	-529(10-I-3)
24	11	-1.21(10-II-2)	-0.43(6)	0.99(10-I-3)	115(10-II-2)	529(9-II-3)	-141(6)
24	12	-1.55(10-II-2)	-2.66(10-I-2)	0.12(9-II-3)	-70(10-I-2)	-1990(10-II-2)	-136(6)
24	13	-1.75(10-II-1)	-2.57(6)	-0.46(10-I-1)	565(9-I-1)	951(6)	646(9-II-3)
24	14	-1.68(10-II-2)	-1.21(6)	0.69(9-II-3)	1026(10-II-2)	2606(10-I-2)	609(9-II-3)
24	15	-2.26(10-II-2)	-1.88(6)	0.29(9-II-2)	1635(10-I-3)	3702(10-I-2)	1090(10-II-2)
25	1	-3.20(6)	-2.73(9-I-2)	0.49(9-I-3)	1652(6)	3100(10-I-4)	-534(9-I-3)
25	2	-3.03(6)	-3.98(9-I-2)	0.96(9-I-3)	1505(6)	3227(10-I-4)	-770(10-II-2)
25	3	-2.83(6)	-5.18(10-II-2)	1.47(10-I-2)	1309(6)	2436(10-I-3)	-801(10-I-2)
25	4	-2.36(6)	-5.16(10-II-2)	1.15(10-II-2)	1355(6)	2332(10-I-3)	-849(10-I-2)
25	5	-1.88(6)	-4.68(9-I-2)	0.57(9-I-3)	1391(6)	2003(10-II-2)	-992(10-I-1)
25	6	-1.19(6)	-4.60(9-I-2)	-0.15(9-II-3)	1335(6)	861(9-I-3)	-895(10-I-1)
25	7	-0.58(6)	-3.59(9-I-2)	-0.52(9-II-3)	475(9-I-3)	-595(9-II-3)	-440(10-I-1)
25	8	0.61(10-I-4)	-1.53(9-I-3)	-1.19(10-II-4)	-457(10-I-4)	-2186(10-I-4)	512(10-II-4)
25	9	-0.83(6)	-2.98(9-I-2)	-0.28(10-II-4)	-755(10-I-4)	-1719(10-I-4)	1053(10-II-4)
25	10	-1.51(6)	-3.30(10-I-4)	-0.22(10-II-1)	-101(10-II-2)	-1550(10-I-4)	1149(10-II-1)
25	11	-2.14(6)	-3.23(10-I-4)	-0.33(10-I-2)	257(6)	-1250(10-I-1)	1245(10-I-3)
25	12	-2.67(6)	-2.90(10-I-4)	-0.53(10-I-4)	422(10-I-3)	-947(10-I-2)	1291(10-I-3)
25	13	-3.02(6)	-2.41(10-I-4)	-0.68(10-I-4)	500(10-I-3)	-686(9-I-3)	1287(10-I-3)
25	14	-3.17(10-I-3)	-1.91(10-I-4)	-0.79(10-I-4)	474(10-I-3)	-505(9-I-3)	1245(10-I-3)
25	15	-3.10(10-I-3)	-1.68(10-I-4)	-0.78(10-I-4)	561(10-I-3)	-170(10-II-4)	965(10-I-4)
25	16	-2.72(10-I-3)	-1.01(10-I-4)	-0.63(10-I-4)	535(10-I-3)	318(10-I-4)	858(10-I-4)
25	17	-1.75(10-I-4)	-0.63(10-I-4)	-0.73(10-I-4)	486(10-I-4)	315(10-I-4)	-310(10-II-4)
25	18	-2.84(10-I-3)	-1.56(10-I-4)	-0.73(10-I-4)	1449(10-I-3)	1727(10-I-4)	-271(10-II-4)
25	19	-3.08(10-I-3)	-2.06(10-I-2)	-0.17(6)	1609(10-I-3)	2501(10-I-4)	-250(10-II-4)
25	20	-1.70(6)	-3.48(9-I-2)	0.20(9-I-3)	645(9-I-3)	1326(9-I-2)	-422(10-I-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
25	21	-1.43(6)	-2.97(9-I-3)	-0.23(9-II-3)	150(9-I-3)	699(9-I-3)	-57(10-I-1)
25	22	-1.91(6)	-3.10(9-I-3)	0.23(10-I-2)	539(9-I-3)	1079(9-I-2)	-44(10-I-1)
25	23	-1.87(6)	-2.89(9-I-2)	0.27(10-I-1)	408(6)	581(9-I-4)	414(10-II-1)
25	24	-1.28(6)	-2.86(9-I-3)	0.36(10-I-1)	-280(10-I-4)	124(9-I-3)	589(10-II-1)
25	25	-1.70(6)	-2.96(9-I-2)	0.19(10-I-1)	134(6)	-298(9-II-3)	856(10-II-1)
25	26	-3.02(10-I-3)	-1.90(10-I-4)	-0.51(10-I-4)	968(10-I-3)	498(10-I-4)	887(10-I-4)
25	27	-2.88(10-I-3)	-2.39(10-I-4)	-0.14(10-I-4)	1229(10-I-3)	1536(10-I-4)	538(10-I-4)
25	28	-2.82(6)	-2.44(10-I-4)	-0.38(10-I-4)	832(10-I-3)	442(10-I-4)	931(10-I-4)
25	29	-2.58(6)	-2.77(10-I-4)	-0.11(10-I-4)	727(6)	305(10-I-4)	892(10-I-4)
25	30	-2.16(6)	-2.91(10-I-4)	0.08(10-I-2)	466(6)	95(10-II-2)	860(10-I-3)
25	31	-2.24(6)	-2.85(9-I-2)	0.28(10-I-2)	740(6)	946(9-I-1)	362(6)
25	32	-2.63(6)	-2.60(9-I-1)	0.21(10-II-2)	1133(6)	1387(10-I-4)	339(10-I-4)
25	33	-2.22(6)	-2.98(9-I-2)	0.32(10-II-2)	885(6)	1531(9-I-1)	-106(9-I-4)
25	34	-2.74(6)	-2.93(9-I-2)	0.46(10-II-2)	1346(6)	2321(10-I-4)	-262(9-I-3)
25	35	-2.21(6)	-3.65(9-I-2)	0.39(9-I-3)	1131(6)	1967(9-I-2)	-524(10-I-1)
26	1	-2.55(10-I-2)	-0.33(9-II-3)	-0.93(9-II-4)	1073(10-I-2)	-45(9-I-3)	333(10-I-2)
26	2	-2.70(10-I-2)	-0.51(9-II-3)	-0.85(9-II-1)	1103(10-I-2)	35(9-II-3)	358(10-I-2)
26	3	-2.35(10-I-3)	-0.73(10-I-3)	-0.62(9-II-1)	967(10-I-3)	81(9-II-4)	409(10-I-2)
26	4	-1.60(9-II-3)	-0.70(9-I-3)	-0.84(10-I-2)	587(9-II-3)	-375(9-I-3)	406(10-I-2)
26	5	-1.46(10-II-2)	0.43(10-II-2)	-1.60(9-I-3)	607(10-II-2)	-462(9-I-2)	639(9-I-3)
26	6	-1.47(9-II-3)	1.68(9-I-3)	-0.63(9-I-2)	640(9-II-3)	136(10-I-2)	164(9-I-2)
26	7	-2.27(10-I-3)	0.37(9-I-3)	-0.80(10-I-2)	1003(10-I-3)	221(9-II-3)	214(9-I-1)
26	8	-2.67(10-I-2)	-0.21(9-II-3)	-0.87(9-II-1)	1131(10-I-2)	284(9-II-3)	379(9-II-4)
26	9	-2.53(10-I-2)	-0.36(9-II-3)	-0.87(9-II-1)	1088(10-I-2)	310(9-II-3)	452(9-II-4)
26	10	-1.76(10-I-2)	-0.46(9-II-3)	-0.76(10-I-2)	780(10-I-2)	384(9-II-3)	546(9-II-4)
26	11	0.89(10-II-2)	-0.30(9-II-3)	-0.39(10-I-2)	-481(10-II-2)	202(9-II-3)	434(9-II-4)
26	12	4.84(10-II-2)	1.26(9-I-3)	1.17(9-I-2)	-2108(10-II-2)	-593(9-I-3)	-544(9-I-2)
26	13	0.77(10-II-2)	0.43(9-I-3)	-0.86(9-II-4)	323(10-I-2)	-264(9-I-3)	-129(10-II-2)
26	14	-1.85(10-I-2)	-0.22(9-II-3)	-0.98(9-II-4)	800(10-I-2)	-133(9-I-3)	234(10-I-2)
27	1	-3.57(10-II-1)	-2.12(10-II-1)	-0.18(9-II-3)	5234(10-II-1)	1391(10-II-1)	405(9-II-3)
27	2	-3.57(10-II-1)	-2.11(10-II-1)	-0.19(9-II-4)	5203(10-II-1)	1432(10-II-1)	430(9-II-3)
27	3	-3.59(10-II-4)	-2.09(10-II-1)	-0.20(9-II-4)	4809(10-II-1)	1449(10-II-1)	439(9-II-3)
27	4	-3.62(10-II-4)	-2.07(10-II-1)	-0.20(9-II-4)	4056(9-II-4)	1436(10-II-1)	411(9-II-4)
27	5	-3.64(10-II-4)	-2.07(10-II-1)	-0.20(9-II-4)	3014(9-II-2)	1356(10-II-1)	333(9-II-4)
27	6	-3.63(10-I-2)	-2.07(10-II-1)	-0.18(9-II-4)	1642(9-II-2)	1158(10-II-1)	222(9-II-1)
27	7	-3.56(10-I-2)	-2.00(10-II-1)	-0.09(9-II-1)	-788(9-I-2)	719(9-II-1)	73(9-II-1)
27	8	-3.42(10-I-2)	-1.70(9-II-1)	0.07(10-I-4)	-2865(9-I-2)	204(9-II-1)	-102(10-I-2)
27	9	-3.38(10-II-2)	-1.19(10-I-2)	-0.37(9-I-1)	-5778(9-I-2)	-1339(10-II-2)	947(10-II-2)
27	10	-3.67(10-II-2)	-1.90(10-I-2)	0.54(10-II-2)	-4561(9-I-1)	373(9-II-1)	620(10-II-2)
27	11	-3.65(10-II-1)	-2.62(10-II-1)	0.62(10-II-2)	-3799(9-I-2)	649(9-II-1)	466(10-II-2)
27	12	-3.64(6)	-3.16(10-II-1)	0.42(10-II-2)	-3674(9-I-2)	937(10-II-1)	425(10-II-2)
27	13	-3.72(10-I-2)	-3.33(10-II-2)	-0.22(10-I-2)	-3794(10-I-1)	1029(10-II-2)	321(10-II-2)
27	14	-3.95(10-I-2)	-3.14(10-II-2)	-0.47(9-II-1)	-4082(10-I-2)	886(10-II-2)	207(9-II-3)
27	15	-4.04(10-I-2)	-2.68(10-II-2)	-0.47(9-II-1)	-4754(10-I-2)	370(10-II-2)	239(9-II-3)
27	16	-3.66(9-II-1)	-1.76(10-II-2)	0.84(10-I-2)	-6038(9-I-1)	-1569(10-I-2)	-377(10-I-2)
27	17	-3.48(9-II-1)	-2.31(10-II-2)	0.34(9-I-3)	-1606(9-I-1)	-412(10-I-2)	708(10-II-2)
27	18	-3.63(9-II-1)	-2.37(10-II-2)	0.18(10-I-4)	1476(9-II-1)	670(10-II-2)	587(10-II-2)
27	19	-3.74(10-II-4)	-2.31(10-II-2)	0.11(10-I-4)	3326(9-II-2)	1174(10-II-1)	502(10-II-2)
27	20	-3.81(10-II-4)	-2.25(10-II-1)	-0.09(9-II-3)	4501(10-II-1)	1477(10-II-1)	503(9-II-3)
27	21	-3.85(10-II-1)	-2.22(10-II-1)	-0.10(9-II-3)	5198(10-II-1)	1624(10-II-1)	529(9-II-3)
27	22	-3.87(10-II-1)	-2.18(10-II-1)	-0.11(9-II-3)	5442(10-II-1)	1619(10-II-1)	546(9-II-3)
27	23	-3.85(10-II-1)	-2.15(10-II-1)	-0.11(9-II-3)	5208(10-II-1)	1468(10-II-1)	500(9-II-3)
27	24	-3.87(10-II-1)	-2.08(10-II-1)	-0.10(9-II-3)	4536(10-II-4)	1234(10-II-1)	407(9-II-3)
27	25	-3.88(10-II-1)	-2.02(10-II-1)	0.11(9-I-3)	3185(6)	1893(10-II-1)	357(9-II-3)
27	26	-3.72(10-II-1)	-2.06(10-II-1)	0.09(9-I-3)	4293(10-II-4)	1198(10-II-1)	300(9-II-3)
27	27	-3.66(10-II-1)	-2.12(10-II-1)	-0.15(9-II-3)	4926(10-II-1)	1303(10-II-1)	378(9-II-3)
27	28	-3.75(10-II-1)	-2.15(10-II-1)	-0.12(9-II-3)	5281(10-II-1)	1437(10-II-1)	464(9-II-3)
27	29	-3.68(10-II-1)	-2.15(10-II-1)	-0.13(9-II-3)	5332(10-II-1)	1459(10-II-1)	469(9-II-3)
27	30	-3.79(10-II-1)	-2.19(10-II-1)	-0.10(9-II-3)	5206(10-II-1)	1556(10-II-1)	530(9-II-3)
27	31	-3.79(10-II-1)	-2.17(10-II-1)	-0.11(9-II-3)	5404(10-II-1)	1552(10-II-1)	516(9-II-3)
27	32	-3.74(10-II-1)	-2.17(10-II-1)	-0.10(9-II-3)	5277(10-II-1)	1508(10-II-1)	516(9-II-3)
27	33	-3.65(10-II-1)	-2.15(10-II-1)	-0.13(9-II-4)	5102(10-II-1)	1461(10-II-1)	496(9-II-3)
27	34	-3.71(10-II-1)	-2.18(10-II-1)	0.10(9-I-4)	4901(10-II-1)	1463(10-II-1)	541(9-II-3)
27	35	-3.77(10-II-4)	-2.22(10-II-1)	0.11(9-I-3)	4688(10-II-1)	1456(10-II-1)	546(9-II-3)
27	36	-3.73(10-II-4)	-2.25(10-II-1)	0.16(9-I-4)	3699(9-II-2)	1274(10-II-2)	598(10-II-1)
27	37	-3.87(10-II-4)	-2.63(10-II-2)	-0.14(9-II-1)	-2211(9-I-2)	1202(10-II-2)	582(9-II-1)
27	38	-3.85(10-II-4)	-2.33(10-II-2)	0.28(9-I-3)	-2004(9-I-2)	829(10-II-2)	751(10-II-1)
27	39	-3.82(10-II-4)	-2.35(10-II-2)	0.25(9-I-4)	-327(9-I-2)	1173(10-II-2)	720(9-II-4)
27	40	-3.72(10-II-4)	-2.27(10-II-2)	0.26(9-I-4)	2030(9-II-1)	1044(10-II-2)	703(10-II-1)
27	41	-3.71(10-II-4)	-2.13(10-II-1)	-0.12(9-II-4)	3513(9-II-2)	1451(10-II-1)	514(9-II-4)
27	42	-3.66(10-II-1)	-2.14(10-II-1)	-0.12(9-II-4)	4494(10-II-1)	1454(10-II-1)	522(9-II-3)
27	43	-3.71(10-II-1)	-2.19(10-II-1)	0.14(9-I-4)	4092(9-II-4)	1394(10-II-2)	590(9-II-3)
27	44	-3.75(10-II-1)	-2.20(10-II-1)	0.17(9-I-4)	2835(9-II-2)	1357(10-II-2)	629(9-II-3)
27	45	-3.75(10-II-4)	-2.15(10-II-1)	-0.12(9-II-4)	2207(9-II-2)	1438(10-II-1)	443(9-II-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
27	46	-3.83 (10-II-4)	-2.25 (10-II-2)	0.16 (9-I-4)	1170 (9-II-2)	1381 (10-II-2)	583 (9-II-1)
27	47	-3.79 (6)	-2.69 (10-II-1)	0.18 (9-I-1)	-2154 (9-I-2)	1276 (10-II-1)	382 (9-II-1)
27	48	-3.83 (10-I-4)	-2.76 (10-II-2)	-0.12 (9-II-1)	-2152 (9-I-2)	1348 (10-II-2)	471 (9-II-1)
27	49	-3.84 (10-II-4)	-2.39 (10-II-2)	0.11 (9-I-1)	-751 (9-I-2)	1471 (10-II-2)	470 (9-II-1)
27	50	-3.77 (6)	-2.19 (10-II-1)	-0.11 (9-II-1)	672 (9-II-2)	1350 (10-II-1)	327 (9-II-1)
27	51	-3.73 (6)	-2.24 (10-II-1)	0.12 (9-I-1)	-1685 (9-I-2)	1120 (10-II-1)	236 (9-II-1)
28	1	-4.99 (10-II-2)	-2.83 (10-II-1)	-0.52 (10-II-2)	3465 (10-II-2)	1690 (10-II-2)	535 (10-II-2)
28	2	-4.61 (10-II-1)	-2.88 (10-II-1)	-0.78 (10-II-2)	3727 (10-II-2)	2849 (10-II-1)	730 (10-II-2)
28	3	-4.52 (10-II-2)	-2.83 (10-II-1)	-1.01 (10-II-2)	3798 (10-II-2)	3667 (10-II-1)	1027 (10-II-2)
28	4	-4.70 (10-II-1)	-2.87 (10-II-1)	-1.53 (10-II-2)	4749 (10-II-2)	5205 (10-II-1)	1973 (10-II-2)
28	5	-4.75 (10-II-1)	-2.68 (10-II-1)	-1.06 (10-II-2)	4307 (10-II-2)	3562 (10-II-1)	1034 (10-II-2)
28	6	-4.76 (10-II-1)	-2.67 (10-II-1)	-0.82 (10-II-2)	4308 (10-II-1)	3104 (10-II-1)	703 (10-II-2)
28	7	-4.83 (10-II-1)	-2.62 (10-II-1)	-0.71 (10-II-2)	4218 (10-II-1)	2551 (10-II-2)	433 (10-II-2)
28	8	-4.86 (10-II-1)	-2.55 (10-II-1)	-0.69 (10-II-2)	3990 (10-II-1)	2051 (10-II-2)	200 (10-II-2)
28	9	-4.77 (10-II-1)	-2.45 (10-II-1)	-0.75 (10-II-2)	3560 (10-II-1)	1518 (10-II-2)	-163 (10-I-2)
28	10	-4.60 (10-II-1)	-2.34 (10-II-2)	-0.88 (10-II-2)	3024 (10-II-4)	939 (10-II-2)	-342 (10-I-2)
28	11	-4.24 (10-II-1)	-2.22 (10-II-2)	-1.11 (10-II-2)	2364 (9-II-1)	336 (10-II-2)	-478 (10-I-2)
28	12	-3.67 (9-II-1)	-2.04 (10-II-2)	-1.47 (10-II-2)	1596 (9-II-1)	-618 (10-I-2)	-553 (10-I-2)
28	13	-2.82 (9-II-1)	-1.75 (10-II-2)	-1.79 (10-II-2)	834 (9-II-1)	-1224 (10-I-2)	-636 (10-I-2)
28	14	-1.56 (9-II-1)	-1.65 (10-II-2)	-1.90 (10-II-2)	-724 (9-I-1)	-1862 (10-I-2)	-666 (10-I-2)
28	15	2.33 (9-I-1)	-0.82 (10-II-2)	-1.74 (10-II-2)	-1645 (9-I-1)	-2987 (10-I-2)	-1643 (10-I-2)
28	16	-1.39 (9-II-1)	-1.50 (10-II-2)	-2.52 (10-II-2)	297 (9-II-1)	-2407 (10-I-3)	-1604 (10-I-2)
28	17	-2.82 (9-II-1)	-1.94 (10-II-2)	-2.63 (10-II-2)	1146 (9-II-1)	-1981 (9-I-1)	-1303 (10-I-2)
28	18	-4.24 (9-II-1)	-1.98 (10-II-2)	-2.47 (10-II-2)	1478 (9-II-1)	-1998 (9-I-1)	-1148 (10-I-2)
28	19	-5.31 (10-II-1)	-2.11 (10-II-2)	-2.23 (10-II-2)	2120 (10-II-4)	-2047 (9-I-1)	-1017 (10-I-2)
28	20	-6.11 (10-II-1)	-2.14 (10-II-2)	-1.88 (10-II-2)	2601 (10-II-1)	-1986 (10-I-4)	-717 (9-I-3)
28	21	-6.67 (10-II-1)	-2.14 (10-II-1)	-1.46 (10-II-2)	2852 (10-II-1)	-1929 (10-I-4)	-421 (9-I-3)
28	22	-6.95 (10-II-1)	-2.18 (10-II-1)	-1.01 (9-I-1)	2991 (10-II-1)	-1874 (9-II-1)	-143 (9-I-3)
28	23	-6.91 (10-II-1)	-2.20 (10-II-1)	-0.57 (9-I-1)	3019 (10-II-2)	-1737 (9-II-1)	260 (9-II-3)
28	24	-6.64 (10-II-2)	-2.18 (10-II-1)	0.18 (9-II-1)	2848 (10-II-2)	-1706 (9-II-1)	468 (9-II-3)
28	25	-5.60 (10-II-2)	-2.70 (10-II-1)	-0.35 (9-I-1)	3239 (10-II-2)	169 (10-II-2)	413 (10-II-2)
28	26	-4.54 (10-II-1)	-2.25 (10-II-2)	-1.35 (10-II-2)	2509 (9-II-1)	-402 (10-I-2)	-450 (10-I-2)
28	27	-4.09 (9-II-1)	-2.15 (10-II-2)	-1.71 (10-II-2)	1959 (9-II-1)	-1083 (10-I-3)	-594 (10-I-2)
28	28	-4.89 (10-II-1)	-2.25 (10-II-2)	-1.70 (10-II-2)	2449 (10-II-4)	-1131 (10-I-3)	-496 (10-I-2)
28	29	-4.94 (10-II-1)	-2.38 (10-II-2)	-1.11 (10-II-2)	3071 (10-II-1)	271 (10-II-2)	-316 (10-I-2)
28	30	-5.43 (10-II-1)	-2.30 (10-II-2)	-1.43 (10-II-2)	2950 (10-II-1)	-789 (10-I-3)	-316 (10-I-2)
28	31	-5.85 (10-II-1)	-2.40 (10-II-1)	-1.16 (10-II-2)	3273 (10-II-1)	-634 (10-I-2)	-145 (10-I-2)
28	32	-5.08 (10-II-1)	-2.57 (10-II-1)	-0.79 (10-II-2)	3839 (10-II-1)	1469 (10-II-2)	157 (10-II-2)
28	33	-5.04 (10-II-1)	-2.52 (10-II-1)	-0.91 (10-II-2)	3479 (10-II-1)	882 (10-II-2)	-170 (10-I-2)
28	34	-5.35 (10-II-1)	-2.54 (10-II-1)	-0.91 (10-II-2)	3546 (10-II-1)	525 (10-II-2)	-96 (10-I-2)
28	35	-5.58 (10-II-1)	-2.62 (10-II-1)	-0.73 (10-II-2)	3670 (10-II-1)	713 (10-II-2)	305 (10-II-2)
28	36	-5.98 (10-II-1)	-2.51 (10-II-1)	-0.68 (9-I-1)	3421 (10-II-1)	-413 (10-I-2)	293 (10-II-2)
28	37	-5.61 (10-II-2)	-2.61 (10-II-1)	-0.55 (10-II-2)	3494 (10-II-1)	483 (10-II-2)	394 (10-II-2)
28	38	-6.08 (10-II-1)	-2.45 (10-II-1)	-0.90 (10-II-2)	3402 (10-II-1)	-609 (10-I-2)	157 (10-II-2)
28	39	-5.55 (10-II-1)	-2.56 (10-II-1)	-0.85 (10-II-2)	3655 (10-II-1)	594 (10-II-2)	209 (10-II-2)
28	40	-5.22 (10-II-1)	-2.73 (10-II-1)	-0.72 (10-II-2)	3853 (10-II-1)	1482 (10-II-2)	372 (10-II-2)
28	41	-4.98 (10-II-1)	-2.71 (10-II-1)	-0.73 (10-II-2)	4070 (10-II-1)	2102 (10-II-2)	397 (10-II-2)
28	42	-5.18 (10-II-1)	-2.63 (10-II-1)	-0.76 (10-II-2)	3896 (10-II-1)	1471 (10-II-2)	274 (10-II-2)
28	43	-5.14 (10-II-2)	-2.76 (10-II-1)	-0.64 (10-II-2)	3749 (10-II-1)	1641 (10-II-2)	455 (10-II-2)
28	44	-4.84 (10-II-1)	-2.81 (10-II-1)	-0.78 (10-II-2)	4062 (10-II-1)	2591 (10-II-1)	577 (10-II-2)
29	1	-6.36 (9-I-2)	-1.15 (10-II-1)	0.46 (10-II-2)	2796 (10-I-1)	645 (10-II-1)	-265 (9-I-1)
29	2	-5.87 (9-I-2)	-1.43 (10-II-1)	0.81 (10-II-2)	3116 (10-II-1)	921 (10-II-1)	-154 (9-I-1)
29	3	-5.22 (9-I-2)	-1.67 (10-II-1)	1.21 (10-II-2)	3341 (10-II-1)	1152 (10-II-1)	55 (9-II-1)
29	4	-4.46 (9-I-2)	-1.87 (10-II-1)	1.53 (10-II-2)	3400 (10-II-1)	1281 (10-II-1)	178 (9-II-1)
29	5	-3.67 (9-I-2)	-2.07 (10-II-1)	1.63 (10-II-2)	3226 (10-II-2)	1305 (10-II-1)	242 (10-I-2)
29	6	-2.82 (9-I-2)	-2.23 (10-II-1)	1.60 (10-II-2)	2717 (9-I-1)	1221 (10-II-4)	263 (10-I-2)
29	7	-1.83 (9-I-2)	-2.41 (10-II-1)	1.44 (10-II-2)	1753 (9-I-1)	1016 (10-II-4)	134 (10-I-2)
29	8	-0.67 (9-I-4)	-2.50 (10-II-4)	1.11 (10-II-1)	981 (9-I-1)	837 (10-II-4)	-228 (10-II-2)
29	9	1.26 (9-II-1)	-1.96 (10-II-4)	0.45 (9-I-3)	-821 (9-II-1)	-762 (10-I-4)	462 (10-I-1)
29	10	-1.25 (9-I-1)	-2.32 (10-II-4)	1.20 (9-I-1)	-1293 (10-I-4)	1107 (10-II-4)	-75 (9-I-2)
29	11	-1.99 (9-I-1)	-2.44 (10-II-4)	1.09 (9-I-1)	-1290 (10-I-4)	1030 (10-II-4)	-208 (9-I-1)
29	12	-2.46 (9-I-1)	-2.34 (10-II-1)	0.66 (9-I-1)	-1618 (10-I-4)	871 (10-II-1)	-242 (10-II-2)
29	13	-2.71 (9-I-2)	-2.00 (10-II-1)	0.16 (10-I-4)	-1878 (10-II-1)	630 (10-II-1)	-271 (10-II-2)
29	14	-2.78 (10-II-1)	-1.53 (9-I-1)	-0.47 (10-II-4)	-1891 (10-II-4)	350 (9-I-1)	-236 (10-II-2)
29	15	-2.52 (9-I-2)	-0.87 (9-I-1)	-0.83 (10-I-2)	-1960 (10-II-4)	-182 (10-II-4)	-107 (10-II-3)
29	16	0.66 (9-II-1)	-0.52 (10-I-4)	-1.17 (10-I-4)	-1735 (9-II-1)	-1013 (10-II-4)	-769 (10-II-4)
29	17	-2.44 (9-I-1)	-1.08 (10-II-1)	-1.48 (10-I-2)	562 (9-I-1)	-591 (10-I-1)	-717 (10-II-3)
29	18	-3.94 (9-I-1)	-1.41 (10-II-1)	-1.60 (10-I-2)	1679 (9-I-2)	-237 (10-I-1)	-799 (10-II-2)
29	19	-5.14 (9-I-2)	-1.37 (10-II-1)	-1.41 (10-I-2)	2396 (9-I-2)	82 (9-I-3)	-639 (10-II-2)
29	20	-5.99 (9-I-2)	-1.21 (10-II-1)	-1.04 (10-I-2)	2827 (9-I-2)	198 (9-I-3)	-372 (10-II-2)
29	21	-6.42 (9-I-2)	-1.13 (10-II-1)	-0.61 (9-II-1)	3050 (10-II-1)	284 (9-I-3)	-72 (10-I-2)
29	22	-6.55 (10-II-1)	-1.02 (10-II-1)	-0.22 (9-I-1)	3053 (10-I-1)	310 (10-II-1)	233 (6)
29	23	-6.36 (10-I-3)	-0.93 (10-II-1)	0.22 (9-I-1)	2754 (10-I-3)	265 (10-II-1)	313 (6)
29	24	-5.77 (10-I-3)	-0.93 (10-II-1)	0.29 (9-I-1)	2632 (10-I-3)	189 (10-II-1)	438 (6)

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
29	25	-5.28(10-I-3)	-0.91(10-II-1)	0.17(10-I-4)	1607(10-I-1)	219(10-II-1)	-55(10-I-4)
29	26	-6.21(10-I-3)	-0.78(10-II-1)	-0.08(6)	1921(10-I-1)	244(10-II-1)	-553(9-I-1)
29	27	-6.57(10-II-1)	-0.89(10-II-1)	0.20(10-I-4)	2398(10-I-1)	318(10-II-1)	-372(9-I-1)
29	28	-6.16(10-II-1)	-1.21(10-II-1)	-0.19(6)	3321(10-II-1)	399(10-II-1)	-33(9-I-1)
29	29	-6.32(10-II-1)	-1.06(10-II-1)	0.08(9-I-1)	3045(10-I-1)	312(10-II-1)	-135(9-I-1)
29	30	-6.11(9-I-2)	-1.25(10-II-1)	0.17(9-I-1)	3249(10-II-1)	525(10-II-1)	-107(9-I-1)
29	31	-5.51(9-I-2)	-1.39(10-II-1)	-0.61(6)	3203(10-II-1)	374(9-I-3)	-42(10-II-2)
29	32	-5.93(9-I-2)	-1.32(10-II-1)	-0.37(6)	3365(10-II-1)	412(10-II-1)	37(6)
29	33	-5.38(9-I-2)	-1.54(10-II-1)	-0.18(6)	3368(10-II-1)	645(10-II-1)	45(6)
29	34	-5.51(9-I-2)	-1.50(10-II-1)	0.37(10-II-2)	3377(10-II-1)	801(10-II-1)	-73(9-I-1)
29	35	-4.77(9-I-2)	-1.52(10-II-1)	-0.69(10-I-2)	2846(9-I-2)	370(9-I-3)	-82(10-II-2)
29	36	-4.60(9-I-1)	-1.56(10-II-1)	-0.08(6)	3042(10-II-1)	715(10-II-1)	35(6)
29	37	-4.33(9-I-2)	-1.76(10-II-1)	1.04(10-II-2)	3139(10-II-1)	1279(10-II-1)	37(9-II-1)
29	38	-4.48(9-I-1)	-1.61(10-II-1)	0.59(10-II-2)	3077(10-II-1)	1019(10-II-1)	-44(9-I-1)
29	39	-4.95(9-I-2)	-1.65(10-II-1)	0.76(10-II-2)	3341(10-II-1)	1091(10-II-1)	-53(9-I-1)
29	40	-3.86(9-I-1)	-1.51(10-II-1)	0.15(10-II-2)	2273(9-I-2)	643(9-I-1)	-65(9-I-1)
29	41	-3.81(9-I-1)	-1.43(10-II-1)	-0.58(10-I-2)	2053(9-I-2)	296(9-I-1)	-93(10-II-2)
29	42	-3.37(9-I-2)	-1.33(9-I-3)	0.25(10-II-2)	713(9-I-1)	708(10-II-1)	-76(9-I-1)
29	43	-3.22(9-I-1)	-1.28(9-I-3)	0.10(10-II-2)	556(9-I-1)	519(9-I-1)	-121(9-I-1)
29	44	-3.18(9-I-2)	-1.20(9-I-1)	0.09(10-II-2)	-384(9-II-1)	568(9-I-1)	-106(10-II-2)
29	45	-3.53(9-I-1)	-1.22(9-I-3)	0.23(10-II-2)	1403(9-I-2)	687(9-I-1)	-40(9-I-1)
29	46	-2.96(9-I-1)	-1.05(9-I-2)	-0.46(10-I-2)	609(9-I-1)	209(9-I-1)	85(10-I-2)
29	47	-3.61(9-I-1)	-1.45(10-II-1)	0.51(10-II-2)	1772(9-I-2)	907(10-II-1)	-51(9-I-1)
29	48	-3.93(9-I-1)	-1.57(10-II-1)	0.55(10-II-2)	2516(9-I-2)	967(10-II-1)	-46(9-I-1)
29	49	-3.77(9-I-1)	-1.61(10-II-1)	0.80(10-II-2)	2276(9-I-2)	1160(10-II-1)	36(6)
29	50	-3.76(9-I-2)	-1.80(10-II-1)	1.12(10-II-2)	2684(10-II-1)	1368(10-II-1)	40(9-II-1)
29	51	-3.34(9-I-1)	-1.45(10-II-1)	0.44(10-II-2)	943(9-I-1)	905(10-II-1)	-76(9-I-1)
29	52	-3.08(9-I-2)	-1.57(10-II-1)	0.32(9-I-1)	-401(9-II-1)	847(10-II-1)	-128(9-I-1)
29	53	-2.50(9-I-1)	-2.01(10-II-1)	1.01(10-II-2)	656(9-I-1)	1346(10-II-4)	-176(9-I-1)
29	54	-2.91(9-I-1)	-1.83(10-II-1)	0.68(9-I-1)	76(9-I-4)	1106(10-II-1)	-163(9-I-1)
29	55	-3.13(9-I-2)	-1.89(10-II-1)	1.12(10-II-2)	1912(9-I-1)	1391(10-II-1)	-48(9-I-1)
29	56	-3.33(9-I-1)	-1.64(10-II-1)	0.76(10-II-2)	1383(9-I-1)	1163(10-II-1)	-81(9-I-1)
30	1	-4.15(10-II-1)	-1.09(10-I-4)	0.51(10-II-4)	800(10-II-1)	-110(9-II-1)	1053(10-I-4)
30	2	-4.37(10-II-1)	-1.66(10-I-4)	0.24(10-II-4)	1539(10-II-1)	646(10-II-2)	978(10-I-4)
30	3	-4.46(10-II-1)	-2.04(10-I-4)	0.12(10-II-4)	2142(10-II-1)	1136(10-II-2)	860(10-I-4)
30	4	-4.50(10-II-1)	-2.32(10-II-4)	-0.11(10-I-4)	2614(10-II-1)	1561(10-II-3)	681(10-I-4)
30	5	-4.54(10-II-1)	-2.50(10-II-4)	0.11(10-II-1)	2956(10-II-1)	1929(10-II-1)	468(10-I-4)
30	6	-4.56(10-II-1)	-2.56(10-II-4)	0.18(10-II-1)	3150(10-II-1)	2214(10-II-1)	197(10-I-4)
30	7	-4.64(10-II-1)	-2.53(10-II-4)	0.25(9-I-3)	3278(10-II-1)	2492(10-II-1)	-240(10-II-1)
30	8	-4.73(10-II-1)	-2.41(10-II-4)	0.39(10-II-1)	3352(10-II-1)	2663(10-II-1)	-569(10-II-1)
30	9	-4.84(10-II-1)	-2.50(10-II-1)	0.75(10-II-1)	3767(9-I-3)	3131(10-II-1)	-1440(10-II-1)
30	10	-4.22(10-II-1)	-2.52(10-II-1)	0.53(9-I-3)	2561(10-II-1)	2915(10-II-1)	-885(10-II-2)
30	11	-3.85(10-II-1)	-2.54(10-II-4)	0.45(9-I-4)	1640(10-II-4)	2064(10-II-1)	-572(9-I-1)
30	12	-3.34(10-II-1)	-2.59(10-II-4)	0.38(9-I-1)	450(9-II-1)	790(10-II-4)	246(9-II-1)
30	13	-2.70(10-II-1)	-2.58(9-II-1)	0.66(9-I-1)	-803(10-I-4)	-1126(9-I-1)	976(9-II-1)
30	14	-2.20(9-II-1)	-2.55(9-II-1)	2.19(9-I-1)	-1862(9-I-1)	-4818(9-I-1)	1785(9-II-1)
30	15	-2.43(9-II-1)	-3.34(10-II-1)	0.67(9-I-1)	-415(9-I-1)	-3180(9-I-1)	1660(9-II-1)
30	16	-3.07(9-II-1)	-3.64(10-II-1)	-0.52(9-II-1)	418(9-II-1)	-2401(9-I-1)	1423(9-II-1)
30	17	-3.75(9-II-1)	-3.61(10-II-2)	-0.77(10-II-4)	923(10-II-4)	-2085(9-I-1)	1510(10-II-1)
30	18	-4.50(10-II-4)	-3.36(10-II-2)	-0.90(10-II-4)	1174(10-II-4)	-1834(9-I-1)	1663(10-II-1)
30	19	-5.14(10-II-4)	-3.03(9-I-1)	-0.89(10-I-4)	1257(10-II-4)	-1581(9-I-1)	1788(10-II-1)
30	20	-5.61(10-II-1)	-2.62(9-I-1)	-0.76(10-I-4)	1211(10-II-1)	-1345(9-I-4)	1883(10-II-1)
30	21	-5.88(10-II-1)	-2.15(9-I-1)	-0.53(10-I-4)	1052(10-II-1)	-1146(9-I-3)	1946(10-II-1)
30	22	-5.91(10-II-1)	-1.67(9-I-1)	-0.23(10-I-4)	775(10-II-1)	-972(9-I-3)	2007(10-II-1)
30	23	-5.71(10-II-1)	-1.15(9-I-1)	0.46(9-II-1)	306(10-II-2)	-862(10-II-4)	2004(10-I-4)
30	24	-5.14(10-II-1)	-0.59(10-I-4)	0.84(9-II-1)	-501(9-II-1)	-839(10-II-4)	1811(10-I-4)
30	25	-4.17(10-II-1)	0.12(10-II-4)	1.39(10-II-4)	-826(9-II-1)	-735(10-II-4)	1787(10-I-4)
30	26	-2.79(9-I-1)	0.73(10-II-1)	1.77(10-II-4)	-1839(9-II-1)	-873(10-II-4)	1818(10-I-4)
30	27	1.00(9-II-1)	1.17(10-II-4)	1.91(10-II-4)	-2905(9-II-1)	-1273(10-II-1)	1608(10-I-4)
30	28	-2.61(9-I-1)	0.19(9-I-1)	1.39(10-II-4)	-1278(9-II-4)	-1196(10-II-1)	937(10-I-4)
30	29	-3.59(10-II-1)	-0.42(10-I-2)	0.85(10-II-4)	-323(9-II-4)	-616(9-II-1)	1072(10-I-4)
30	30	-5.10(10-II-1)	-1.51(9-I-1)	0.38(9-II-1)	1213(10-II-1)	-473(9-II-1)	1485(10-I-4)
30	31	-4.59(10-II-1)	-1.20(10-I-4)	0.56(9-II-1)	869(10-II-1)	-434(9-II-1)	1353(10-I-4)
30	32	-4.66(10-II-1)	-1.65(10-I-4)	0.30(9-II-1)	1491(10-II-1)	218(10-I-4)	1206(10-I-4)
30	33	-5.25(10-II-1)	-2.31(9-I-1)	-0.26(10-I-4)	1874(10-II-1)	-197(9-II-1)	1391(10-I-4)
30	34	-5.22(10-II-1)	-1.91(9-I-1)	0.14(9-II-1)	1653(10-II-1)	-253(9-II-1)	1419(10-I-4)
30	35	-4.83(10-II-1)	-2.46(10-II-4)	-0.13(10-I-4)	2283(10-II-1)	751(10-II-2)	1036(10-I-4)
30	36	-4.70(10-II-1)	-2.35(10-II-4)	0.10(9-II-1)	2359(10-II-1)	1063(10-II-2)	906(10-I-4)
30	37	-4.63(10-II-1)	-2.51(10-II-4)	0.08(10-II-4)	2688(10-II-1)	1489(10-II-2)	698(10-I-4)
30	38	-4.76(10-II-1)	-2.03(10-I-4)	0.14(9-II-1)	1978(10-II-1)	601(10-II-2)	1103(10-I-4)
30	39	-5.13(10-II-1)	-2.63(9-I-1)	-0.38(10-I-4)	1913(10-II-1)	-291(9-I-3)	1380(10-I-4)
30	40	-4.84(10-II-1)	-2.89(10-II-2)	-0.42(10-I-4)	1867(10-II-4)	-345(9-I-4)	1318(10-I-4)
30	41	-4.58(10-II-1)	-2.71(10-II-1)	0.14(9-I-3)	2610(10-II-1)	1509(10-II-1)	566(10-I-4)
30	42	-4.63(10-II-1)	-2.62(10-II-4)	0.10(9-I-3)	2674(10-II-1)	1468(10-II-1)	649(10-I-4)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
30	43	-4.55(10-II-1)	-2.64(10-II-4)	0.19(9-I-3)	2905(10-II-1)	1954(10-II-1)	377(10-I-4)
30	44	-4.82(10-II-1)	-2.63(10-II-4)	-0.16(10-I-4)	2326(10-II-1)	726(10-II-2)	983(10-I-4)
30	45	-4.66(10-II-1)	-2.78(10-II-1)	-0.13(10-I-1)	2280(10-II-4)	784(10-II-3)	896(10-I-4)
30	46	-4.33(10-II-1)	-2.70(10-II-1)	0.37(9-I-4)	2480(10-II-4)	1940(10-II-1)	160(10-I-3)
30	47	-4.53(10-II-1)	-2.59(10-II-1)	0.44(9-I-3)	2916(10-II-1)	2519(10-II-1)	-309(10-I-1)
30	48	-4.22(10-II-1)	-2.69(10-II-1)	0.46(9-I-4)	2580(10-II-1)	2327(10-II-1)	-352(10-II-1)
30	49	-4.47(10-II-1)	-2.73(10-II-1)	0.25(9-I-3)	2570(10-II-4)	1729(10-II-1)	384(10-I-3)
30	50	-4.51(10-II-1)	-2.64(10-II-1)	0.31(9-I-3)	2948(10-II-1)	2250(10-II-1)	92(10-I-1)
30	51	-4.42(10-II-1)	-2.87(10-II-1)	0.08(9-I-4)	2187(10-II-4)	928(10-II-3)	748(10-I-3)
30	52	-4.43(10-II-4)	-3.09(10-II-1)	-0.37(10-I-2)	1733(10-II-4)	-345(9-I-4)	1208(10-I-4)
30	53	-3.51(10-II-4)	-2.93(10-II-1)	0.32(9-I-1)	1005(9-II-1)	151(10-II-3)	792(9-II-1)
30	54	-3.97(10-II-4)	-3.15(10-II-1)	-0.21(10-I-2)	1474(10-II-4)	-292(9-I-1)	1042(10-I-3)
30	55	-3.95(10-II-1)	-2.76(10-II-1)	0.40(9-I-1)	1811(10-II-4)	1575(10-II-1)	133(10-I-2)
30	56	-4.16(10-II-1)	-2.85(10-II-1)	0.26(9-I-1)	2022(10-II-4)	1157(10-II-1)	521(10-I-3)
31	1	-2.57(6)	-4.60(10-I-3)	-0.45(9-I-1)	795(6)	2555(10-I-3)	252(9-I-1)
31	2	-3.04(6)	-4.55(10-I-3)	-0.32(9-I-1)	1018(6)	2297(10-I-3)	107(9-I-1)
31	3	-3.60(10-I-2)	-4.35(10-I-3)	-0.26(9-I-1)	1329(6)	1944(10-I-3)	-108(9-I-1)
31	4	-4.11(10-I-2)	-3.90(10-I-3)	-0.21(9-I-1)	1643(10-I-2)	1551(10-I-3)	-140(9-II-1)
31	5	-4.66(10-I-2)	-3.22(10-I-3)	0.12(9-II-1)	1958(10-I-2)	1217(10-I-3)	-89(9-II-1)
31	6	-4.16(10-I-2)	-3.86(10-I-3)	0.32(9-II-1)	1896(10-I-2)	1711(10-I-3)	-101(9-II-1)
31	7	-3.56(6)	-4.42(10-I-3)	0.43(9-II-1)	1821(10-I-2)	2004(10-I-3)	-229(9-II-1)
31	8	-2.96(6)	-4.83(10-I-3)	0.49(9-II-1)	1676(10-I-2)	2155(10-I-3)	-390(9-II-1)
31	9	-2.22(6)	-5.02(10-I-3)	0.57(9-II-1)	1343(10-I-2)	2088(10-I-3)	-478(9-II-1)
31	10	-1.43(6)	-5.60(10-I-3)	0.78(10-I-3)	723(6)	1844(10-I-3)	-351(10-I-3)
31	11	-1.11(6)	-5.47(10-I-3)	-0.32(9-I-1)	310(6)	1443(10-I-3)	265(9-I-1)
31	12	-0.93(6)	-4.96(10-I-3)	-1.06(9-I-1)	337(6)	1121(10-I-3)	613(9-I-4)
31	13	-1.10(6)	-4.37(10-I-3)	-1.78(9-I-1)	308(6)	1499(6)	923(9-I-2)
31	14	-1.61(6)	-4.32(10-I-3)	-1.19(9-I-1)	471(6)	2277(10-I-3)	584(9-I-1)
31	15	-2.06(6)	-4.57(10-I-3)	-0.68(9-I-1)	594(6)	2505(10-I-3)	438(9-I-1)
31	16	-2.87(6)	-4.64(10-I-3)	-0.16(9-I-1)	1200(6)	2377(10-I-3)	-108(10-I-2)
31	17	-3.29(6)	-4.51(10-I-3)	-0.14(9-I-1)	1466(10-I-2)	2183(10-I-3)	-160(10-I-2)
31	18	-2.86(6)	-4.71(10-I-3)	0.26(9-II-1)	1360(10-I-2)	2392(10-I-3)	-214(10-I-2)
31	19	-2.28(6)	-5.03(10-I-3)	0.22(9-II-1)	1027(6)	2485(10-I-3)	-221(10-I-2)
31	20	-1.82(6)	-4.99(10-I-3)	-0.36(9-I-1)	643(6)	2276(10-I-3)	118(9-I-1)
31	21	-2.39(6)	-4.82(10-I-3)	-0.22(9-I-1)	969(6)	2476(10-I-3)	86(9-I-1)
32	1	-3.54(10-II-1)	-4.06(10-II-2)	-0.99(10-II-2)	1905(10-II-1)	2738(10-II-2)	779(10-I-4)
32	2	-4.22(10-II-1)	-3.77(10-II-2)	-1.31(10-II-2)	1210(10-II-2)	1735(10-II-2)	1461(10-II-1)
32	3	-4.85(10-II-1)	-3.58(10-II-2)	-1.82(10-II-2)	-158(9-II-1)	916(10-II-2)	2132(10-II-1)
32	4	-4.88(10-II-1)	-3.00(9-I-1)	-1.34(9-I-1)	-427(9-II-1)	700(10-II-2)	1972(10-II-1)
32	5	-4.81(10-II-1)	-2.40(9-I-1)	-1.01(9-I-1)	-789(9-II-1)	412(10-II-2)	1907(10-II-1)
32	6	-4.60(10-II-2)	-1.87(9-I-1)	-0.59(9-I-1)	-1550(9-II-1)	-553(9-II-1)	1810(10-II-1)
32	7	-4.00(9-I-1)	-1.52(9-I-1)	1.04(9-II-1)	-2442(9-II-1)	-1143(9-II-1)	2179(9-I-1)
32	8	-3.36(9-I-1)	-1.75(9-I-1)	2.24(9-II-1)	-4408(9-II-1)	-2421(9-II-1)	2391(9-I-1)
32	9	-3.62(9-I-1)	-1.87(9-I-1)	0.66(9-II-1)	-928(9-II-1)	-1657(9-II-1)	1170(9-I-1)
32	10	-3.56(9-I-1)	-2.36(10-II-4)	-0.33(9-I-1)	821(9-I-1)	-332(9-II-1)	541(9-I-1)
32	11	-3.36(10-II-2)	-3.01(10-II-1)	-0.42(9-I-1)	1600(10-II-2)	1193(10-II-2)	-169(9-II-1)
32	12	-3.12(10-II-2)	-3.54(10-II-2)	-0.43(9-I-1)	2038(10-II-1)	2213(10-II-2)	-508(9-II-1)
32	13	-2.80(10-II-1)	-4.08(10-II-1)	-0.42(9-I-1)	2278(10-II-1)	3224(10-II-2)	-687(9-II-1)
32	14	-2.45(10-II-1)	-4.53(10-II-1)	-0.38(10-I-4)	2312(10-II-1)	3965(10-II-2)	-798(9-II-1)
32	15	-1.90(10-II-1)	-4.92(10-II-1)	-0.82(10-II-2)	2411(10-II-1)	5794(10-II-1)	-1111(9-II-2)
32	16	-2.59(10-II-1)	-4.54(10-II-1)	-0.61(10-II-2)	2557(10-II-1)	4464(10-II-2)	-285(9-II-1)
32	17	-3.08(10-II-1)	-4.27(10-II-2)	-0.76(10-II-2)	2278(10-II-1)	3634(10-II-2)	208(9-I-1)
32	18	-4.10(10-II-1)	-2.85(9-I-1)	-0.80(9-I-1)	761(9-I-1)	724(9-I-1)	1122(9-I-1)
32	19	-3.85(10-II-2)	-2.45(9-I-1)	-0.53(9-I-1)	554(9-I-1)	185(9-I-1)	1038(9-I-1)
32	20	-3.64(10-II-2)	-2.97(10-II-2)	-0.59(9-I-1)	1282(10-II-2)	1085(10-II-2)	534(9-I-1)
32	21	-3.62(10-II-1)	-3.73(10-II-2)	-0.90(9-I-1)	1686(10-II-1)	2310(10-II-2)	694(9-I-1)
32	22	-4.12(10-II-1)	-3.42(10-II-2)	-1.17(9-I-1)	1037(10-II-2)	1473(10-II-2)	1320(10-II-4)
32	23	-3.94(10-II-1)	-3.27(10-II-2)	-0.84(9-I-1)	1209(10-II-2)	1522(10-II-2)	890(9-I-1)
32	24	-3.44(10-II-2)	-3.45(10-II-2)	-0.63(9-I-1)	1724(10-II-2)	1984(10-II-2)	242(9-I-1)
32	25	-3.22(10-II-1)	-3.92(10-II-2)	-0.68(9-I-1)	2077(10-II-1)	2934(10-II-2)	75(9-I-1)
33	1	-1.83(10-II-1)	-2.04(10-II-2)	0.14(9-II-3)	1483(9-I-1)	-1830(9-II-2)	-393(9-II-4)
33	2	-2.25(10-II-1)	-2.32(10-II-1)	0.26(9-II-3)	1741(10-II-1)	-840(9-II-2)	-356(9-II-4)
33	3	-2.02(10-II-1)	-1.77(10-II-1)	0.28(9-II-4)	1138(10-II-1)	-2211(9-II-2)	414(9-I-1)
33	4	-2.29(10-II-1)	-1.95(10-II-1)	0.33(9-II-4)	1687(10-II-1)	-973(9-II-2)	228(9-I-4)
33	5	-2.05(10-II-1)	-1.72(10-II-1)	0.47(9-II-4)	1038(10-II-1)	-2506(9-II-2)	1039(10-II-2)
33	6	-2.32(10-II-1)	-1.84(10-II-1)	0.56(9-II-4)	1562(10-II-1)	-1502(9-II-2)	733(10-II-2)
33	7	-2.30(10-II-1)	-2.13(10-II-1)	1.15(9-II-2)	247(9-I-2)	-4555(9-II-2)	2323(10-II-2)
33	8	-1.97(10-II-1)	-2.19(10-II-1)	0.75(9-II-4)	1154(9-I-1)	-2338(9-II-2)	1245(10-II-2)
34	1	-1.06(9-I-1)	-3.14(10-II-1)	0.40(9-I-3)	-595(10-II-3)	-523(10-II-3)	-1534(10-II-1)
34	2	-1.60(9-I-2)	-2.71(10-II-1)	0.72(9-I-3)	-472(10-II-3)	1330(10-I-3)	-1177(10-II-2)
34	3	-2.13(9-I-2)	-2.50(10-II-1)	0.79(9-I-3)	279(10-I-3)	1810(9-I-4)	-1310(10-II-2)
34	4	-2.68(9-I-2)	-2.35(10-II-1)	0.79(9-I-3)	914(9-I-2)	2201(9-I-1)	-1413(10-II-1)
34	5	-1.27(9-I-1)	-3.13(10-II-1)	-0.43(9-II-3)	-287(10-II-3)	-922(10-II-3)	-1678(10-II-2)
34	6	-1.63(9-I-1)	-2.67(10-II-1)	-0.15(9-II-3)	-616(10-II-3)	964(10-I-3)	-757(9-II-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

Pagina 108 di
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
34	7	-1.82 (9-I-2)	-2.49 (10-II-1)	0.19 (9-I-3)	-489 (10-II-3)	1536 (9-II-1)	-743 (9-I-1)
34	8	-1.91 (9-I-2)	-2.58 (10-II-1)	0.25 (9-I-3)	-278 (10-II-3)	1850 (9-II-1)	-730 (10-II-2)
34	9	-1.69 (9-I-1)	-3.19 (10-II-1)	-1.06 (10-II-4)	505 (9-I-1)	-1269 (10-II-3)	-2169 (10-II-2)
34	10	-2.05 (9-I-1)	-2.71 (10-II-1)	-0.77 (9-II-3)	-266 (9-II-1)	-277 (10-II-2)	-721 (9-I-1)
34	11	-2.14 (9-I-1)	-2.60 (10-II-1)	-0.54 (9-II-3)	-278 (9-II-1)	994 (9-II-1)	-470 (9-I-1)
34	12	-2.07 (9-I-1)	-2.71 (10-II-1)	-0.38 (9-II-3)	-162 (9-II-1)	1587 (9-II-1)	-399 (9-I-1)
34	13	-2.68 (10-II-2)	-3.21 (10-II-1)	-1.84 (10-II-1)	-522 (9-II-2)	-2746 (10-II-2)	-3417 (10-II-2)
34	14	-2.91 (10-II-2)	-3.02 (10-II-1)	-1.38 (10-II-2)	-912 (9-II-1)	-163 (10-II-2)	-626 (9-I-1)
34	15	-2.99 (10-II-2)	-2.62 (10-II-1)	-1.10 (9-II-3)	407 (9-I-1)	1333 (9-II-1)	424 (10-II-4)
34	16	-3.32 (10-II-2)	-2.22 (10-II-1)	-0.98 (9-II-3)	1437 (9-I-1)	1877 (9-II-1)	1043 (10-II-1)
35	1	-1.98 (10-II-1)	-1.28 (10-I-2)	-0.73 (10-II-2)	2386 (10-II-1)	1681 (10-II-4)	1123 (10-II-1)
35	2	-1.89 (10-II-1)	-1.13 (9-II-1)	-0.89 (10-II-2)	2548 (10-II-1)	1341 (9-II-1)	1745 (10-II-2)
35	3	-1.78 (9-I-3)	-0.93 (9-II-1)	-0.95 (10-II-2)	3069 (9-I-1)	1030 (9-II-1)	1830 (10-II-1)
35	4	-1.82 (9-II-1)	-0.64 (9-II-1)	-1.05 (10-II-2)	2804 (9-I-1)	582 (9-II-1)	1308 (10-II-1)
35	5	-1.88 (10-II-1)	-1.19 (9-II-1)	-0.71 (10-II-2)	2059 (10-II-1)	1926 (10-II-3)	869 (10-II-2)
35	6	-1.81 (10-II-1)	-1.13 (9-II-1)	-0.97 (10-II-2)	2096 (9-I-2)	1394 (9-II-1)	1348 (10-II-2)
35	7	-1.73 (9-I-3)	-0.96 (9-II-1)	-1.07 (10-II-2)	2307 (9-I-2)	922 (9-II-1)	1627 (10-II-2)
35	8	-1.69 (9-II-4)	-0.74 (9-II-1)	-1.22 (10-II-2)	2124 (9-I-2)	314 (9-II-1)	1098 (10-II-2)
35	9	-1.73 (10-II-1)	-1.21 (9-II-1)	-0.75 (10-II-2)	1807 (10-II-1)	1891 (10-II-3)	750 (10-II-2)
35	10	-1.72 (10-II-1)	-1.17 (9-II-1)	-1.04 (10-II-2)	1640 (10-II-1)	1402 (9-II-1)	1050 (10-II-2)
35	11	-1.70 (9-I-2)	-1.01 (9-II-1)	-1.20 (10-II-2)	1412 (9-II-1)	1015 (9-II-1)	1387 (10-I-4)
35	12	-1.51 (9-II-1)	-0.82 (9-II-1)	-1.34 (10-II-2)	1338 (9-II-1)	-383 (10-II-2)	1045 (10-I-4)
35	13	-1.56 (10-II-1)	-1.36 (10-I-2)	-0.73 (10-II-2)	1631 (10-II-1)	1678 (10-II-2)	540 (9-I-1)
35	14	-1.60 (10-II-1)	-1.24 (9-II-1)	-1.14 (10-II-2)	1310 (10-II-1)	1350 (9-II-1)	704 (9-II-1)
35	15	-1.59 (9-I-2)	-1.10 (9-II-1)	-1.31 (10-II-2)	506 (9-II-1)	1036 (9-II-1)	853 (10-I-3)
35	16	-1.45 (9-II-1)	-0.85 (9-II-1)	-1.32 (10-II-2)	503 (9-II-1)	496 (9-II-1)	870 (10-I-4)
36	1	-1.30 (9-II-1)	-2.85 (10-II-1)	1.27 (10-II-1)	568 (10-I-2)	579 (10-I-3)	-989 (10-II-2)
36	2	-0.96 (9-II-1)	-3.01 (10-II-1)	0.97 (10-II-1)	323 (10-I-3)	-437 (10-II-3)	-1157 (10-II-2)
36	3	-1.68 (9-I-2)	-2.65 (10-II-1)	1.08 (9-I-3)	304 (10-I-3)	1255 (10-I-3)	-1245 (10-II-2)
36	4	-2.23 (9-I-2)	-2.61 (10-II-1)	1.07 (9-I-3)	427 (9-I-3)	1838 (9-I-1)	-1321 (10-II-2)
36	5	-2.60 (10-II-2)	-3.19 (10-II-1)	1.00 (9-I-3)	756 (9-I-3)	3277 (9-I-2)	-1337 (10-II-2)
36	6	-2.30 (10-II-2)	-2.86 (10-II-1)	1.05 (9-I-3)	134 (9-II-1)	2428 (9-I-1)	-892 (10-II-2)
36	7	-2.08 (10-II-2)	-2.71 (10-II-1)	1.22 (10-II-1)	-173 (6)	1357 (9-I-1)	-390 (10-II-2)
36	8	-1.55 (10-II-2)	-2.81 (10-II-1)	1.42 (10-II-1)	734 (9-II-1)	662 (10-I-3)	587 (9-I-2)
36	9	-1.51 (10-I-2)	-2.70 (10-II-1)	1.36 (10-II-1)	663 (9-II-1)	989 (10-I-3)	-419 (9-II-1)
37	1	-1.70 (9-I-1)	-0.76 (9-I-1)	-0.94 (10-II-1)	3272 (10-I-3)	-739 (10-II-3)	-126 (10-II-3)
37	2	-1.22 (10-II-1)	-0.94 (9-I-1)	-1.22 (10-II-1)	4704 (9-II-3)	884 (9-I-1)	-2069 (10-II-3)
37	3	-1.01 (10-II-1)	-1.22 (9-I-1)	-1.36 (10-II-2)	5191 (9-II-3)	1496 (9-I-1)	-3120 (10-II-1)
37	4	-0.79 (10-II-1)	-1.58 (9-I-1)	-1.55 (10-II-2)	6592 (10-II-2)	1893 (9-I-1)	-3973 (10-II-1)
37	5	-1.56 (9-I-2)	-1.06 (9-I-1)	-0.83 (10-II-2)	2604 (9-I-1)	-2427 (10-II-3)	781 (10-I-4)
37	6	-1.08 (10-II-1)	-1.20 (9-I-1)	-1.09 (10-II-2)	3943 (9-II-3)	-370 (10-II-4)	-922 (10-II-4)
37	7	-0.82 (10-II-1)	-1.46 (9-I-1)	-1.20 (10-II-2)	4583 (9-II-3)	962 (9-I-1)	-1545 (10-II-4)
37	8	-0.40 (10-II-1)	-2.06 (10-II-2)	-1.08 (10-II-2)	5021 (10-II-2)	1079 (9-I-1)	-1997 (9-II-2)
37	9	-1.49 (9-I-2)	-1.22 (9-I-1)	-0.80 (10-II-2)	1807 (9-I-1)	-3654 (10-II-3)	1285 (10-I-4)
37	10	-0.95 (10-II-1)	-1.38 (9-I-1)	-0.98 (10-II-2)	3068 (9-II-3)	-888 (9-II-1)	-323 (6)
37	11	-0.77 (10-II-1)	-1.66 (9-I-1)	-1.01 (10-II-2)	3728 (9-II-3)	584 (9-I-1)	-700 (6)
37	12	-0.57 (10-II-1)	-2.16 (10-II-2)	-0.74 (10-II-4)	3848 (9-I-1)	506 (9-I-1)	-1139 (9-II-2)
37	13	-1.14 (9-I-2)	-1.27 (9-I-1)	-0.75 (10-II-2)	1015 (9-I-1)	-4616 (10-II-1)	1718 (10-I-4)
37	14	-0.96 (10-II-1)	-1.51 (9-I-1)	-0.84 (10-II-2)	2224 (9-II-3)	-1268 (9-II-1)	235 (9-I-1)
37	15	-0.81 (10-II-1)	-1.77 (9-I-1)	-0.85 (10-II-2)	2895 (9-I-1)	-303 (9-II-1)	-276 (6)
37	16	-0.70 (10-II-1)	-2.15 (10-II-2)	-0.57 (10-I-4)	3056 (9-I-1)	-490 (9-II-1)	-750 (9-II-2)
38	1	-1.23 (10-II-1)	-1.14 (10-I-1)	-0.58 (9-I-1)	1416 (9-II-1)	2210 (10-I-2)	822 (10-I-4)
38	2	-1.13 (10-II-1)	-1.15 (10-I-2)	-0.74 (9-I-1)	1475 (9-II-1)	1622 (9-II-1)	1249 (10-I-4)
38	3	-0.96 (10-II-1)	-1.14 (9-II-1)	-0.83 (9-I-1)	1515 (9-II-1)	932 (9-II-1)	1284 (10-I-4)
38	4	-0.76 (10-II-1)	-1.09 (9-II-1)	-0.86 (9-I-1)	1577 (9-II-1)	-816 (9-I-1)	1089 (10-I-3)
38	5	-0.86 (10-II-1)	-1.13 (10-I-4)	-0.63 (9-I-1)	1088 (10-II-1)	2922 (10-I-2)	848 (10-I-4)
38	6	-0.90 (10-II-1)	-1.21 (10-I-4)	-0.70 (9-I-1)	987 (10-II-1)	1816 (9-II-1)	1181 (9-I-1)
38	7	-0.97 (10-II-1)	-1.26 (10-I-4)	-0.70 (9-I-1)	885 (10-II-1)	487 (9-II-1)	1197 (9-I-1)
38	8	-1.07 (10-II-1)	-1.47 (10-II-2)	-0.64 (10-II-2)	616 (10-II-1)	-2063 (9-I-1)	1251 (10-I-4)
38	9	-0.76 (10-II-1)	-0.72 (9-I-1)	-0.65 (9-I-1)	1063 (10-II-1)	3346 (10-I-2)	921 (10-I-4)
38	10	-0.94 (10-II-1)	-0.80 (9-I-1)	-0.61 (9-I-1)	952 (10-II-1)	2130 (9-II-1)	1407 (10-I-4)
38	11	-1.12 (10-II-1)	-0.84 (10-I-4)	-0.54 (9-I-1)	826 (9-II-1)	424 (9-II-1)	1527 (10-I-4)
38	12	-1.29 (10-II-1)	-0.94 (10-I-1)	-0.50 (10-II-2)	543 (9-II-1)	-2226 (9-I-1)	1279 (10-I-4)
38	13	-0.97 (10-II-1)	0.14 (9-II-1)	-0.51 (9-I-1)	1416 (10-II-1)	5735 (10-I-2)	744 (10-I-4)
38	14	-1.37 (10-II-1)	0.16 (9-II-1)	-0.20 (9-I-1)	885 (9-II-1)	2728 (9-II-1)	1710 (10-I-4)
38	15	-1.41 (10-II-1)	-0.23 (9-I-1)	0.09 (9-II-1)	578 (9-II-1)	517 (9-II-1)	1816 (10-I-4)
38	16	-1.38 (10-II-1)	-0.51 (9-I-1)	0.10 (9-II-1)	421 (9-II-1)	-2868 (9-I-1)	1585 (10-I-4)
39	1	-1.74 (10-II-1)	0.57 (9-II-2)	1.18 (10-I-2)	646 (9-II-4)	4401 (10-I-3)	3325 (10-I-4)
39	2	-1.55 (10-II-1)	-0.22 (9-I-2)	0.71 (9-II-1)	829 (10-II-1)	2112 (9-II-1)	2065 (10-I-4)
39	3	-1.48 (10-II-1)	-0.54 (9-I-2)	0.58 (9-II-1)	476 (9-II-1)	-674 (9-I-1)	1336 (10-I-4)
39	4	-1.41 (10-II-1)	-0.64 (9-I-2)	0.46 (9-II-1)	-558 (10-I-1)	-3382 (9-I-1)	1292 (10-I-4)
39	5	-1.52 (10-II-1)	-1.39 (9-I-2)	0.73 (9-II-1)	1083 (10-II-1)	661 (10-I-1)	2116 (10-I-4)
39	6	-1.33 (10-II-1)	-1.09 (9-I-2)	0.80 (9-II-1)	1323 (10-II-1)	574 (9-II-1)	1911 (10-I-4)
39	7	-1.32 (10-II-1)	-1.08 (9-I-2)	0.66 (9-II-1)	1226 (10-II-1)	-1340 (9-I-1)	1268 (10-I-4)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
39	8	-1.34 (10-II-1)	-1.09 (9-I-2)	0.56 (6)	1052 (10-II-1)	-3353 (9-I-1)	1410 (10-I-4)
39	9	-1.61 (10-II-1)	-1.75 (9-I-2)	0.54 (9-II-1)	1580 (10-II-1)	-649 (10-II-1)	1829 (10-I-4)
39	10	-1.34 (10-II-1)	-1.62 (9-I-2)	0.60 (9-II-1)	1800 (10-II-1)	-874 (9-I-1)	1757 (10-I-4)
39	11	-1.23 (10-II-1)	-1.50 (9-I-2)	0.58 (6)	2023 (10-II-1)	-1781 (9-I-1)	1395 (9-I-1)
39	12	-1.24 (10-II-1)	-1.46 (9-I-2)	0.52 (6)	1956 (10-II-1)	-3093 (9-I-1)	1511 (10-I-4)
39	13	-1.69 (10-II-1)	-1.96 (9-I-2)	0.41 (9-II-1)	1930 (10-II-1)	-1288 (10-II-1)	1904 (10-II-2)
39	14	-1.36 (10-II-1)	-1.85 (9-I-2)	0.46 (6)	2404 (10-II-1)	-1387 (10-II-2)	1961 (9-I-1)
39	15	-1.19 (10-II-1)	-1.76 (9-I-2)	0.47 (6)	2896 (10-II-1)	-1977 (9-I-1)	1736 (9-I-1)
39	16	-1.07 (10-II-1)	-1.78 (9-I-2)	0.39 (6)	3107 (10-II-1)	-2881 (10-I-3)	1647 (9-I-1)
40	1	-0.83 (10-II-1)	-1.62 (10-I-4)	-0.66 (9-I-1)	988 (9-I-1)	-4186 (9-II-1)	1323 (9-II-1)
40	2	-0.97 (10-II-1)	-1.62 (9-I-1)	-0.61 (9-I-1)	996 (9-I-1)	-2077 (9-II-1)	1011 (10-II-2)
40	3	-1.08 (10-II-1)	-1.80 (10-II-2)	-0.49 (9-I-4)	1325 (9-I-1)	-1301 (9-II-1)	562 (9-I-1)
40	4	-1.28 (10-II-1)	-2.04 (10-II-2)	-0.27 (10-I-4)	1443 (9-I-1)	-1537 (9-II-1)	-143 (9-II-4)
40	5	-1.22 (10-II-1)	-1.31 (10-I-3)	-0.48 (9-I-1)	486 (9-I-1)	-3791 (9-II-1)	1296 (10-II-2)
40	6	-1.25 (10-II-1)	-1.47 (10-I-4)	-0.32 (9-I-1)	639 (9-I-1)	-2926 (9-II-1)	1154 (9-I-1)
40	7	-1.44 (10-II-1)	-1.60 (10-II-2)	-0.18 (9-I-1)	689 (9-I-1)	-2475 (9-II-1)	869 (9-I-1)
40	8	-1.69 (10-II-1)	-1.71 (10-II-2)	0.07 (9-II-4)	785 (9-I-1)	-2539 (9-II-2)	544 (9-I-1)
40	9	-1.39 (10-II-1)	-1.10 (10-II-2)	-0.19 (9-I-1)	408 (9-I-2)	-4070 (9-II-1)	1413 (10-II-2)
40	10	-1.50 (10-II-1)	-1.25 (10-II-2)	0.12 (10-II-4)	562 (9-I-1)	-3313 (9-II-1)	1042 (9-I-1)
40	11	-1.65 (10-II-1)	-1.34 (10-II-1)	0.19 (9-II-1)	576 (9-I-1)	-2874 (9-II-2)	984 (9-I-1)
40	12	-1.94 (10-II-1)	-1.28 (10-II-1)	0.23 (9-II-1)	633 (9-I-1)	-3142 (9-II-2)	904 (10-II-2)
40	13	-1.38 (10-II-1)	-0.83 (10-II-3)	0.32 (10-II-4)	-192 (10-I-1)	-5328 (9-II-1)	1362 (9-I-1)
40	14	-1.60 (10-II-1)	-0.80 (9-I-2)	0.37 (10-II-4)	160 (9-I-2)	-3308 (9-II-1)	1044 (9-I-1)
40	15	-1.80 (10-II-1)	-0.77 (9-I-2)	0.44 (10-II-4)	461 (9-I-2)	-2070 (9-II-2)	1307 (10-II-2)
40	16	-2.07 (10-II-1)	-0.78 (6)	0.57 (10-II-4)	414 (10-II-1)	-1031 (9-II-2)	1683 (10-II-2)
41	1	-3.41 (10-II-2)	-3.00 (10-II-1)	-0.35 (9-II-3)	1325 (9-I-1)	3187 (10-II-1)	-108 (10-I-2)
41	2	-3.33 (10-II-2)	-2.92 (10-II-1)	-0.17 (9-II-4)	991 (9-I-1)	2130 (10-II-1)	-385 (9-I-3)
41	3	-3.10 (9-I-1)	-2.72 (10-II-1)	0.29 (9-I-1)	516 (9-I-1)	992 (10-II-3)	-597 (9-I-4)
41	4	-2.68 (9-I-1)	-2.63 (10-II-1)	0.53 (9-I-1)	-836 (9-II-1)	-951 (10-I-2)	-696 (9-I-1)
41	5	-1.75 (9-I-1)	-2.21 (10-II-1)	1.22 (9-I-1)	-2050 (9-II-1)	-4321 (10-I-3)	-460 (9-I-1)
41	6	-2.58 (10-II-1)	-2.46 (10-II-1)	0.71 (9-I-1)	-888 (10-I-4)	-281 (10-I-3)	254 (9-II-1)
41	7	-2.92 (10-II-1)	-2.72 (10-II-1)	0.66 (9-I-1)	162 (9-II-1)	1895 (10-II-1)	218 (9-II-1)
41	8	-2.97 (10-II-1)	-2.81 (10-II-1)	0.64 (9-I-4)	501 (9-II-1)	3589 (10-II-1)	-263 (9-I-1)
41	9	-2.99 (10-II-1)	-3.10 (10-II-1)	0.87 (9-I-3)	718 (9-I-3)	4197 (10-II-1)	-487 (9-I-1)
41	10	-2.90 (10-II-1)	-3.34 (10-II-1)	1.36 (9-I-3)	958 (9-I-3)	4781 (10-II-1)	-576 (9-I-2)
41	11	-2.56 (10-II-1)	-3.11 (10-II-1)	0.50 (9-I-3)	502 (9-I-2)	4487 (10-II-1)	-353 (9-I-1)
41	12	-2.63 (10-II-2)	-3.34 (10-II-1)	-0.56 (9-II-3)	605 (9-I-1)	4299 (10-II-1)	-227 (9-I-4)
41	13	-3.19 (10-II-2)	-3.58 (10-II-1)	-1.49 (9-II-3)	1300 (10-II-1)	4594 (10-II-1)	669 (10-II-2)
41	14	-3.45 (10-II-2)	-3.29 (10-II-1)	-1.05 (9-II-3)	1757 (10-II-2)	4237 (10-II-1)	469 (10-II-2)
41	15	-3.45 (10-II-2)	-3.18 (10-II-1)	-0.68 (9-II-3)	1618 (9-I-1)	3969 (10-II-1)	353 (10-II-2)
41	16	-2.86 (9-I-1)	-2.45 (10-II-1)	0.36 (9-I-1)	-488 (9-II-1)	1513 (10-II-1)	-585 (9-I-1)
41	17	-2.99 (10-II-1)	-2.65 (10-II-1)	0.40 (9-I-3)	176 (9-I-1)	3261 (10-II-1)	-454 (9-I-1)
41	18	-3.11 (10-II-2)	-3.06 (10-II-1)	-0.24 (9-II-4)	737 (9-I-1)	3345 (10-II-1)	-440 (9-I-4)
41	19	-2.88 (10-II-2)	-3.02 (10-II-1)	-0.38 (9-II-3)	650 (9-I-1)	3874 (10-II-1)	-416 (9-I-4)
41	20	-3.02 (10-II-2)	-2.82 (10-II-1)	0.10 (9-I-3)	457 (9-I-1)	3502 (10-II-1)	-500 (9-I-1)
41	21	-3.09 (10-II-2)	-3.08 (10-II-1)	-0.54 (9-II-3)	935 (9-I-1)	3833 (10-II-1)	-198 (10-I-4)
41	22	-3.35 (10-II-2)	-3.26 (10-II-1)	-0.76 (9-II-3)	1309 (9-I-1)	4148 (10-II-1)	192 (9-II-3)
41	23	-3.03 (10-II-2)	-2.71 (10-II-1)	0.21 (9-I-4)	344 (9-I-1)	2299 (10-II-1)	-648 (9-I-1)
41	24	-3.19 (10-II-2)	-2.87 (10-II-1)	-0.18 (9-II-4)	825 (9-I-1)	2835 (10-II-1)	-419 (9-I-3)
41	25	-3.29 (10-II-2)	-3.11 (10-II-1)	-0.44 (9-II-3)	1065 (9-I-1)	3203 (10-II-1)	-269 (9-I-3)
42	1	-5.26 (10-II-1)	-2.29 (10-II-1)	1.19 (10-I-4)	5641 (10-II-2)	1166 (9-I-1)	-359 (9-I-2)
42	2	-4.70 (10-II-1)	-2.15 (10-II-1)	1.02 (10-I-4)	4138 (10-II-4)	1061 (9-I-2)	-585 (9-I-2)
42	3	-4.10 (10-II-1)	-2.36 (10-II-1)	1.10 (10-I-4)	3414 (10-II-4)	1160 (9-I-2)	-722 (9-I-2)
42	4	-3.66 (10-II-1)	-2.40 (10-II-1)	1.06 (10-I-4)	2959 (10-II-4)	1122 (9-I-2)	-776 (9-I-2)
42	5	-3.68 (10-II-1)	-2.45 (10-II-1)	0.93 (10-I-2)	4181 (10-II-1)	1638 (10-II-2)	-1103 (6)
42	6	-3.66 (10-II-1)	-2.50 (10-II-1)	0.87 (10-I-2)	4877 (10-II-1)	1941 (10-II-1)	-1251 (10-I-1)
42	7	-3.64 (10-II-1)	-2.53 (10-II-2)	0.86 (10-I-2)	5082 (10-II-1)	2109 (10-II-1)	-1284 (10-I-2)
42	8	-3.62 (10-II-1)	-2.55 (10-II-2)	0.84 (10-I-2)	4823 (10-II-1)	2101 (10-II-1)	-1216 (10-I-2)
42	9	-3.59 (10-II-1)	-2.57 (10-II-2)	0.82 (10-I-2)	4126 (10-II-1)	1880 (10-II-1)	-1033 (10-I-2)
42	10	-3.55 (10-II-1)	-2.58 (10-II-2)	0.77 (10-I-2)	3003 (9-II-2)	1412 (9-II-1)	-718 (10-I-2)
42	11	-3.48 (9-II-4)	-2.55 (10-II-2)	0.71 (10-I-2)	1448 (9-II-2)	701 (9-II-1)	-255 (10-I-2)
42	12	-3.39 (9-II-4)	-2.38 (10-II-1)	0.68 (10-I-2)	-1403 (9-I-2)	-537 (9-I-1)	548 (9-I-1)
42	13	-3.26 (10-II-1)	-2.67 (10-I-2)	0.77 (9-II-1)	-4401 (10-I-3)	-2533 (10-II-2)	2426 (9-I-1)
42	14	-3.60 (10-II-1)	-3.25 (10-I-2)	0.74 (10-II-2)	-3332 (9-I-1)	-1283 (10-II-2)	2264 (10-II-2)
42	15	-3.73 (10-II-4)	-3.51 (10-II-4)	0.54 (10-II-2)	-2815 (10-I-4)	-648 (10-II-2)	2334 (10-II-2)
42	16	-3.99 (10-II-4)	-3.50 (10-II-2)	0.19 (10-I-1)	-2673 (10-I-3)	-192 (9-I-1)	2215 (10-II-2)
42	17	-4.29 (10-II-4)	-3.09 (10-II-2)	-0.18 (9-II-3)	-2643 (10-I-2)	147 (9-II-1)	1999 (10-II-2)
42	18	-4.50 (10-II-4)	-2.40 (10-II-2)	-0.34 (10-II-2)	-2635 (10-I-2)	249 (10-II-2)	1721 (10-II-2)
42	19	-4.55 (10-II-1)	-1.48 (10-II-2)	-0.38 (10-II-2)	-2584 (10-I-2)	189 (10-II-2)	1382 (10-II-2)
42	20	-4.29 (10-II-1)	-0.40 (10-II-2)	-0.31 (10-II-2)	-2477 (10-I-2)	-371 (10-I-2)	999 (10-II-2)
42	21	-3.55 (10-II-1)	1.53 (10-I-2)	0.75 (10-I-2)	-2556 (10-I-2)	-624 (10-I-2)	866 (10-II-2)
42	22	-1.25 (9-II-2)	3.05 (10-I-2)	1.69 (10-I-2)	-3334 (9-I-2)	-1657 (10-I-2)	-577 (10-I-2)
42	23	-2.74 (10-II-3)	0.24 (9-II-1)	-0.49 (10-II-2)	-1474 (9-I-2)	-975 (10-I-2)	-200 (10-I-2)
42	24	-3.56 (10-II-1)	-0.80 (10-II-2)	0.30 (10-I-2)	-648 (9-I-2)	-165 (10-I-2)	-431 (10-I-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

Pagina 110 di
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
42	25	-4.00(10-II-1)	-1.44(10-II-4)	0.48(10-I-2)	707(9-II-2)	838(10-II-2)	-690(10-I-2)
42	26	-4.29(10-II-1)	-1.95(10-II-4)	0.61(10-I-2)	1600(10-II-1)	1465(10-II-3)	-810(10-I-2)
42	27	-4.45(10-II-1)	-2.26(10-II-4)	0.72(10-I-2)	2494(10-II-1)	2026(10-II-2)	-820(10-I-2)
42	28	-4.56(10-II-2)	-2.44(10-II-4)	0.76(10-I-2)	3255(10-II-1)	2396(10-II-2)	-768(10-I-2)
42	29	-4.65(10-II-2)	-2.51(10-II-4)	0.74(10-I-2)	3941(10-II-1)	2648(10-II-1)	-658(10-I-2)
42	30	-4.74(10-II-2)	-2.48(10-II-1)	0.69(10-I-2)	4480(10-II-1)	2804(10-II-1)	-469(10-I-2)
42	31	-4.85(10-II-2)	-2.40(10-II-1)	0.65(10-I-2)	4954(10-II-1)	2836(10-II-1)	-209(10-I-2)
42	32	-5.08(10-II-1)	-2.21(10-II-1)	0.63(10-I-2)	5361(10-II-2)	2839(10-II-1)	219(9-II-3)
42	33	-5.73(10-II-1)	-2.10(10-II-1)	0.90(10-I-4)	6500(10-II-2)	2103(9-I-1)	355(9-II-2)
42	34	-4.22(10-II-1)	-2.50(10-II-1)	0.92(10-I-2)	4612(10-II-1)	2766(10-II-1)	-638(10-I-2)
42	35	-4.33(10-II-1)	-2.48(10-II-1)	0.90(10-I-2)	5060(10-II-1)	2689(10-II-1)	-584(10-I-2)
42	36	-4.46(10-II-1)	-2.48(10-II-1)	0.84(10-I-2)	4877(10-II-1)	2815(10-II-1)	-486(10-I-2)
42	37	-4.58(10-II-1)	-2.49(10-II-1)	0.76(10-I-2)	4686(10-II-1)	2852(10-II-1)	-440(10-I-2)
42	38	-4.48(10-II-1)	-2.50(10-II-1)	0.80(10-I-2)	4196(10-II-1)	2810(10-II-1)	-575(10-I-2)
42	39	-4.35(10-II-1)	-2.50(10-II-1)	0.87(10-I-2)	4426(10-II-1)	2843(10-II-1)	-566(10-I-2)
42	40	-4.97(10-II-1)	-2.33(10-II-1)	1.02(10-I-4)	5380(10-II-2)	1906(9-I-1)	-204(10-I-1)
42	41	-4.57(10-II-1)	-2.42(10-II-1)	0.84(10-I-2)	5134(10-II-1)	2748(10-II-1)	-389(10-I-2)
42	42	-4.64(10-II-1)	-2.36(10-II-1)	0.82(10-I-2)	5298(10-II-1)	2642(10-II-1)	-325(10-I-2)
42	43	-4.70(10-II-1)	-2.44(10-II-1)	0.78(10-I-2)	5094(10-II-1)	2786(10-II-1)	-317(10-I-2)
42	44	-4.48(10-II-1)	-2.43(10-II-1)	0.91(10-I-2)	5319(10-II-1)	2592(10-II-1)	-457(10-I-2)
42	45	-4.80(10-II-1)	-2.36(10-II-1)	0.90(10-I-2)	5483(10-II-1)	2341(10-II-1)	-198(10-I-1)
42	46	-4.51(10-II-1)	-2.38(10-II-1)	1.02(10-I-2)	4890(10-II-1)	1631(9-I-2)	-605(10-I-1)
42	47	-4.43(10-II-1)	-2.43(10-II-1)	0.99(10-I-2)	5345(10-II-1)	2036(10-II-1)	-574(10-I-1)
42	48	-4.28(10-II-1)	-2.47(10-II-1)	0.94(10-I-2)	5376(10-II-1)	2331(10-II-1)	-654(10-I-1)
42	49	-4.04(10-II-1)	-2.51(10-II-1)	0.95(10-I-2)	5281(10-II-1)	2137(10-II-1)	-922(10-I-1)
42	50	-3.83(10-II-1)	-2.52(10-II-1)	0.93(10-I-2)	5098(10-II-1)	2016(10-II-1)	-1122(10-I-1)
42	51	-4.12(10-II-1)	-2.40(10-II-1)	1.03(10-I-2)	4448(10-II-1)	1559(9-I-2)	-880(6)
42	52	-3.92(10-II-1)	-2.46(10-II-1)	0.98(10-I-2)	4642(10-II-1)	1726(10-II-2)	-1055(6)
42	53	-4.12(10-II-1)	-2.46(10-II-1)	1.00(10-I-2)	5102(10-II-1)	1897(10-II-2)	-869(10-I-1)
42	54	-4.15(10-II-1)	-2.50(10-II-1)	0.94(10-I-2)	5176(10-II-1)	2524(10-II-1)	-758(10-I-2)
42	55	-4.07(10-II-1)	-2.51(10-II-1)	0.94(10-I-2)	4725(10-II-1)	2616(10-II-1)	-784(10-I-2)
42	56	-3.91(10-II-1)	-2.53(10-II-1)	0.93(10-I-2)	4788(10-II-1)	2428(10-II-1)	-950(10-I-2)
42	57	-3.76(10-II-1)	-2.54(10-II-1)	0.89(10-I-2)	4819(10-II-1)	2245(10-II-1)	-1107(10-I-2)
42	58	-3.79(10-II-1)	-2.54(10-II-1)	0.91(10-I-2)	5154(10-II-1)	2205(10-II-1)	-1152(10-I-2)
42	59	-3.96(10-II-1)	-2.52(10-II-1)	0.93(10-I-2)	5197(10-II-1)	2345(10-II-1)	-967(10-I-2)
42	60	-3.90(10-II-1)	-2.51(10-II-1)	0.92(10-I-2)	3957(10-II-1)	2336(10-II-1)	-817(10-I-2)
42	61	-3.74(10-II-1)	-2.54(10-II-2)	0.86(10-I-2)	4060(10-II-1)	2089(10-II-1)	-957(10-I-2)
42	62	-4.03(10-II-1)	-2.49(10-II-1)	0.96(10-I-2)	3954(10-II-1)	2570(10-II-1)	-686(10-I-2)
42	63	-4.12(10-II-1)	-2.59(10-II-2)	0.79(10-I-2)	-278(9-I-2)	1423(10-II-2)	823(10-II-1)
42	64	-4.09(10-II-1)	-2.93(10-II-2)	0.56(10-I-1)	-1497(9-I-1)	759(9-II-1)	1536(10-II-1)
42	65	-3.74(10-II-1)	-2.43(9-II-1)	0.77(10-I-2)	-867(9-I-2)	532(9-II-1)	573(9-I-1)
42	66	-3.83(10-II-1)	-2.68(9-II-1)	0.86(10-I-1)	-1827(9-I-1)	444(9-II-1)	1230(9-I-1)
42	67	-3.94(10-II-1)	-2.52(9-II-1)	0.83(10-I-2)	-356(9-I-2)	1100(9-II-1)	556(9-I-1)
42	68	-4.04(10-II-1)	-2.57(10-II-4)	0.81(10-I-2)	-372(9-I-2)	1269(9-II-1)	734(9-I-1)
42	69	-3.95(10-II-1)	-2.87(10-II-4)	0.69(10-I-1)	-1725(9-I-1)	622(9-II-1)	1493(10-II-1)
42	70	-3.72(10-II-1)	-2.45(10-II-1)	0.77(10-I-2)	1418(9-II-2)	1196(9-II-1)	-252(10-I-2)
42	71	-3.73(10-II-1)	-2.51(10-II-2)	0.83(10-I-2)	2918(9-II-2)	1720(10-II-4)	-675(10-I-2)
42	72	-4.10(10-II-1)	-2.46(10-II-2)	0.92(10-I-2)	1278(9-II-2)	1915(10-II-2)	280(9-I-1)
42	73	-3.92(10-II-1)	-2.44(10-II-1)	0.86(10-I-2)	1433(9-II-2)	1567(9-II-1)	-88(10-I-1)
42	74	-4.04(10-II-1)	-2.46(10-II-4)	0.90(10-I-2)	1322(9-II-2)	1772(10-II-1)	174(9-I-1)
42	75	-4.07(10-II-1)	-2.44(10-II-1)	0.97(10-I-2)	2259(9-II-2)	2273(10-II-2)	-199(10-I-2)
42	76	-4.04(10-II-1)	-2.47(10-II-1)	0.97(10-I-2)	3112(10-II-1)	2476(10-II-2)	-485(10-I-2)
42	77	-4.02(10-II-1)	-2.45(10-II-1)	0.95(10-I-2)	2563(9-II-2)	2195(10-II-1)	-319(10-I-2)
42	78	-3.90(10-II-1)	-2.47(10-II-1)	0.90(10-I-2)	2823(9-II-2)	2051(10-II-1)	-539(10-I-2)
42	79	-4.14(10-II-1)	-2.33(10-II-2)	0.93(10-I-2)	2249(10-II-1)	2333(10-II-2)	-404(10-I-2)
42	80	-4.24(10-II-1)	-2.30(10-II-4)	0.84(10-I-2)	2391(10-II-1)	2266(10-II-2)	-601(10-I-2)
42	81	-4.24(10-II-1)	-2.40(10-II-4)	0.89(10-I-2)	2929(10-II-1)	2560(10-II-2)	-558(10-I-2)
42	82	-4.36(10-II-1)	-2.47(10-II-4)	0.84(10-I-2)	3530(10-II-1)	2672(10-II-2)	-628(10-I-2)
42	83	-4.25(10-II-1)	-2.49(10-II-1)	0.91(10-I-2)	3818(10-II-1)	2795(10-II-2)	-572(10-I-2)
42	84	-4.15(10-II-1)	-2.49(10-II-1)	0.95(10-I-2)	3963(10-II-1)	2747(10-II-2)	-599(10-I-2)
42	85	-4.16(10-II-1)	-2.45(10-II-1)	0.95(10-I-2)	3118(10-II-1)	2661(10-II-2)	-485(10-I-2)
42	86	-4.12(10-II-1)	-2.38(10-II-2)	0.98(10-I-2)	2306(9-II-2)	2414(10-II-2)	-285(10-I-2)
42	87	-4.10(10-II-1)	-2.42(10-II-1)	0.99(10-I-2)	2304(9-II-2)	2391(10-II-2)	-220(10-I-2)
42	88	-4.11(10-II-1)	-2.46(10-II-1)	0.99(10-I-2)	3195(10-II-1)	2626(10-II-2)	-468(10-I-2)
42	89	-4.23(10-II-1)	-2.70(10-II-2)	0.49(10-I-1)	-1299(9-I-2)	900(10-II-2)	1434(10-II-2)
42	90	-4.17(10-II-1)	-2.49(10-II-2)	0.79(10-I-2)	217(9-II-2)	1544(10-II-2)	775(10-II-2)
42	91	-4.12(10-II-1)	-2.42(10-II-2)	0.94(10-I-2)	1339(9-II-2)	2038(10-II-2)	257(9-I-1)
42	92	-4.28(10-II-1)	-2.28(10-II-2)	0.50(10-I-2)	-1113(9-I-2)	950(10-II-2)	1215(10-II-2)
42	93	-4.15(10-II-1)	-2.28(10-II-2)	0.82(10-I-2)	384(9-II-2)	1586(10-II-2)	600(10-II-2)
42	94	-4.10(10-II-1)	-2.32(10-II-2)	0.95(10-I-2)	1425(9-II-2)	2074(10-II-2)	139(10-II-2)
42	95	-4.07(10-II-1)	-2.20(10-II-2)	0.92(10-I-2)	1485(9-II-2)	1998(10-II-2)	-194(10-I-2)
42	96	-4.09(10-II-1)	-2.08(10-II-2)	0.80(10-I-2)	1550(9-II-2)	1809(10-II-2)	-474(10-I-2)
42	97	-4.18(10-II-1)	-1.75(10-II-2)	0.58(10-I-2)	-969(9-I-2)	848(10-II-2)	907(10-II-2)
42	98	-3.80(10-II-1)	-1.16(10-II-2)	0.68(10-I-2)	-808(9-I-2)	518(10-II-2)	486(10-II-2)

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42	99	-4.04 (10-II-1)	-2.00 (10-II-2)	0.85 (10-I-2)	520 (9-II-2)	1501 (10-II-2)	331 (10-II-2)
42	100	-3.94 (10-II-1)	-1.74 (10-II-2)	0.74 (10-I-2)	629 (9-II-2)	1244 (10-II-2)	-229 (10-I-2)
43	1	-2.23 (10-II-1)	-4.11 (9-I-1)	0.45 (10-I-1)	1542 (9-I-2)	2467 (10-II-1)	528 (10-II-1)
43	2	-2.32 (10-II-1)	-4.55 (10-II-2)	0.17 (10-I-1)	1816 (10-II-1)	3039 (10-II-1)	558 (10-II-1)
43	3	-2.49 (10-II-1)	-4.72 (10-II-2)	-0.40 (10-II-1)	2071 (10-II-1)	3343 (10-II-1)	607 (10-II-1)
43	4	-2.69 (10-II-1)	-4.69 (10-II-1)	-0.66 (9-I-3)	2288 (10-II-1)	3407 (10-II-1)	666 (10-II-1)
43	5	-2.84 (10-II-1)	-4.53 (10-II-1)	-0.89 (9-I-3)	2531 (10-II-1)	3284 (10-II-1)	776 (10-II-1)
43	6	-2.98 (10-II-1)	-4.41 (10-II-1)	-1.09 (9-I-3)	2617 (9-I-2)	2967 (10-II-1)	833 (10-II-1)
43	7	-2.82 (10-II-1)	-4.76 (10-II-1)	-1.40 (10-II-1)	3276 (9-I-2)	3070 (9-I-3)	1459 (10-II-1)
43	8	-3.04 (10-II-1)	-4.30 (10-II-1)	-1.15 (9-I-3)	3170 (10-II-1)	2949 (10-II-1)	795 (10-II-1)
43	9	-3.06 (10-II-1)	-4.14 (10-II-1)	-0.98 (10-II-1)	2945 (10-II-1)	3072 (10-II-1)	607 (10-II-1)
43	10	-3.04 (10-II-1)	-4.03 (10-II-1)	-0.90 (10-II-1)	2622 (10-II-1)	3155 (10-II-1)	431 (10-II-1)
43	11	-2.95 (10-II-1)	-3.95 (10-II-1)	-0.86 (10-II-1)	2222 (10-II-1)	3094 (10-II-1)	287 (10-II-4)
43	12	-2.78 (10-II-1)	-3.88 (10-II-1)	-0.87 (10-II-1)	1777 (10-II-1)	2902 (10-II-2)	153 (10-II-4)
43	13	-2.56 (10-II-1)	-3.72 (10-II-1)	-0.93 (10-II-1)	1265 (10-II-4)	2515 (10-II-2)	-128 (10-I-4)
43	14	-2.32 (10-II-1)	-3.48 (10-II-2)	-1.01 (10-II-1)	742 (10-II-4)	1994 (9-I-1)	-255 (10-I-4)
43	15	-1.94 (10-II-4)	-3.10 (9-I-1)	-1.13 (10-II-1)	225 (10-II-4)	1236 (9-I-1)	-350 (10-I-1)
43	16	-1.50 (10-II-4)	-2.59 (9-I-1)	-1.31 (10-II-1)	-681 (10-I-4)	207 (9-I-1)	-328 (10-I-1)
43	17	-0.92 (10-II-4)	-1.77 (9-I-1)	-1.45 (10-II-1)	-1245 (10-I-4)	-1153 (9-II-1)	-259 (10-I-1)
43	18	3.73 (10-I-4)	-1.06 (9-I-1)	-1.12 (10-II-1)	-2454 (10-I-4)	-2509 (9-II-1)	-952 (10-I-3)
43	19	1.26 (10-I-4)	-2.47 (9-I-1)	-1.85 (10-II-1)	-683 (10-I-4)	-2331 (10-I-2)	-522 (10-I-1)
43	20	-1.29 (10-II-4)	-2.86 (9-I-1)	-1.81 (9-I-1)	-495 (10-I-4)	-2370 (10-I-3)	-540 (9-II-2)
43	21	-1.98 (10-II-4)	-3.08 (9-I-1)	-1.67 (9-I-1)	509 (10-II-4)	-2636 (10-I-4)	-575 (10-I-3)
43	22	-2.44 (10-II-4)	-3.19 (9-I-1)	-1.30 (9-I-1)	907 (10-II-4)	-2600 (10-II-2)	-443 (10-I-3)
43	23	-2.71 (10-II-1)	-3.21 (10-II-2)	-0.90 (9-I-1)	971 (10-II-1)	-2569 (10-II-1)	-313 (10-I-3)
43	24	-2.72 (10-II-1)	-3.11 (10-II-1)	-0.39 (9-I-1)	958 (10-II-1)	-2562 (10-II-1)	-203 (10-I-3)
43	25	-2.50 (9-I-1)	-2.87 (10-II-1)	0.28 (10-I-2)	885 (9-I-1)	-2413 (10-II-4)	-86 (10-I-4)
43	26	-2.20 (9-I-1)	-2.27 (9-I-2)	0.69 (10-I-1)	760 (9-I-1)	-2293 (10-II-4)	153 (10-II-4)
43	27	-2.23 (10-I-4)	-0.64 (9-I-1)	0.90 (10-I-4)	616 (10-I-4)	-1870 (9-II-1)	559 (10-II-4)
43	28	-2.02 (10-II-1)	-2.31 (9-I-1)	0.98 (10-I-1)	784 (9-I-1)	347 (9-I-1)	390 (10-II-1)
43	29	-2.21 (10-II-1)	-3.35 (9-I-1)	0.72 (10-I-1)	1230 (9-I-1)	1595 (9-I-1)	496 (10-II-1)
43	30	-1.59 (10-II-4)	-3.21 (9-I-1)	-1.08 (10-II-1)	813 (10-II-4)	-453 (9-II-1)	-248 (9-II-2)
43	31	-1.43 (10-II-4)	-2.91 (9-I-1)	-1.02 (10-II-1)	459 (10-II-4)	-339 (9-II-1)	-266 (10-I-1)
43	32	-1.65 (10-II-4)	-3.20 (9-I-1)	-0.97 (10-II-1)	831 (10-II-4)	508 (9-I-1)	-223 (10-I-1)
43	33	-1.20 (10-II-4)	-3.09 (9-I-1)	-1.31 (10-II-1)	486 (10-II-4)	-1106 (9-II-1)	-276 (9-II-1)
43	34	-1.72 (10-II-4)	-3.22 (9-I-1)	-1.24 (10-II-1)	818 (10-II-4)	-1485 (9-II-4)	-234 (9-II-1)
43	35	-1.99 (10-II-4)	-3.39 (10-II-2)	-1.02 (9-I-2)	1155 (10-II-4)	-1167 (9-II-1)	-148 (9-II-1)
43	36	-1.73 (10-II-4)	-3.33 (10-II-2)	-1.00 (10-II-1)	1067 (10-II-4)	-525 (9-II-1)	-189 (9-II-1)
43	37	-1.84 (10-II-4)	-3.48 (10-II-2)	-0.83 (10-II-1)	1338 (10-II-4)	678 (9-I-1)	-183 (10-I-1)
43	38	-2.00 (10-II-1)	-3.77 (10-II-2)	-0.65 (10-II-1)	1809 (10-II-4)	1414 (9-I-1)	101 (10-II-2)
43	39	-1.95 (10-II-1)	-3.64 (10-II-2)	-0.72 (10-II-1)	1560 (10-II-4)	631 (9-I-1)	-87 (10-I-2)
43	40	-1.99 (10-II-1)	-3.72 (10-II-2)	-0.63 (10-II-1)	1659 (10-II-1)	733 (9-I-1)	81 (9-I-1)
43	41	-2.06 (10-II-1)	-3.60 (10-II-2)	-0.62 (10-II-1)	1529 (10-II-1)	-183 (9-II-1)	-55 (10-I-2)
43	42	-2.00 (10-II-1)	-3.56 (10-II-2)	-0.80 (9-I-2)	1342 (10-II-4)	-631 (9-II-1)	-112 (10-I-2)
43	43	-2.23 (10-II-1)	-3.47 (10-II-2)	-0.70 (9-I-2)	1335 (10-II-1)	-1216 (9-II-1)	-100 (10-I-2)
43	44	-2.00 (10-II-1)	-3.74 (10-II-2)	-0.54 (10-II-1)	1707 (10-II-1)	1030 (9-I-1)	170 (9-I-1)
43	45	-2.05 (10-II-1)	-3.81 (10-II-2)	-0.42 (10-II-1)	1798 (10-II-1)	1569 (9-I-1)	288 (9-I-2)
43	46	-2.08 (10-II-1)	-3.84 (10-II-2)	-0.55 (10-II-1)	1922 (10-II-1)	1808 (9-I-1)	215 (9-I-2)
43	47	-2.14 (10-II-1)	-3.92 (9-I-1)	-0.23 (10-II-1)	1756 (10-II-1)	2105 (10-II-2)	387 (9-I-2)
43	48	-2.24 (10-II-1)	-3.42 (10-II-2)	-0.44 (9-I-2)	1324 (10-II-1)	-1121 (9-II-1)	51 (10-II-2)
43	49	-2.04 (10-II-1)	-3.61 (10-II-2)	-0.50 (10-II-1)	1542 (10-II-1)	206 (9-I-1)	122 (9-I-1)
43	50	-1.99 (10-II-1)	-3.57 (9-I-1)	-0.35 (10-II-1)	1516 (10-II-1)	646 (9-I-1)	202 (9-I-1)
43	51	-2.03 (10-II-1)	-3.48 (9-I-1)	0.24 (10-I-1)	1407 (9-I-1)	1160 (9-I-1)	296 (9-I-2)
43	52	-2.07 (9-I-1)	-3.24 (10-II-2)	-0.18 (10-II-1)	1254 (10-II-1)	-805 (9-II-1)	86 (10-II-2)
43	53	-1.93 (9-I-1)	-2.89 (9-I-1)	0.39 (10-I-1)	1151 (9-I-1)	-389 (9-II-1)	100 (10-II-1)
43	54	-1.92 (10-II-4)	-3.28 (10-II-2)	-0.89 (10-II-1)	863 (10-II-4)	1220 (9-I-1)	-255 (10-I-1)
43	55	-2.04 (10-II-1)	-3.56 (10-II-2)	-0.76 (10-II-1)	1508 (10-II-4)	1595 (9-I-1)	-126 (10-I-1)
43	56	-2.22 (10-II-1)	-3.53 (10-II-2)	-0.83 (10-II-1)	1305 (10-II-4)	1987 (9-I-1)	-167 (10-I-1)
43	57	-2.68 (10-II-1)	-3.85 (10-II-1)	-0.78 (10-II-1)	2083 (10-II-1)	2929 (10-II-2)	202 (10-II-1)
43	58	-2.46 (10-II-1)	-3.72 (10-II-2)	-0.80 (10-II-1)	1674 (10-II-4)	2489 (10-II-2)	-69 (10-I-1)
43	59	-2.46 (10-II-1)	-3.82 (10-II-1)	-0.70 (10-II-1)	2093 (10-II-1)	2673 (10-II-2)	202 (10-II-1)
43	60	-2.18 (10-II-1)	-3.77 (10-II-2)	-0.67 (10-II-1)	1895 (10-II-4)	2070 (10-II-2)	118 (10-II-1)
43	61	-2.32 (10-II-1)	-4.16 (10-II-2)	-0.39 (10-II-1)	2066 (10-II-1)	2780 (10-II-1)	453 (10-II-1)
43	62	-2.27 (10-II-1)	-3.95 (10-II-2)	-0.56 (10-II-1)	2134 (10-II-1)	2479 (10-II-2)	297 (10-II-1)
43	63	-2.55 (10-II-1)	-4.28 (10-II-2)	-0.54 (10-II-1)	2348 (10-II-1)	3217 (10-II-1)	523 (10-II-1)
43	64	-2.54 (10-II-1)	-4.01 (10-II-1)	-0.64 (10-II-1)	2353 (10-II-1)	3001 (10-II-2)	365 (10-II-1)
43	65	-2.83 (10-II-1)	-3.97 (10-II-1)	-0.78 (10-II-1)	2396 (10-II-1)	3131 (10-II-1)	333 (10-II-1)
43	66	-2.77 (10-II-1)	-4.06 (10-II-1)	-0.72 (10-II-1)	2537 (10-II-1)	3209 (10-II-1)	437 (10-II-1)
43	67	-2.92 (10-II-1)	-4.08 (10-II-1)	-0.81 (10-II-1)	2648 (10-II-1)	3246 (10-II-1)	471 (10-II-1)
43	68	-2.77 (10-II-1)	-4.29 (10-II-1)	-0.69 (10-II-1)	2557 (10-II-1)	3354 (10-II-1)	586 (10-II-1)
43	69	-2.92 (10-II-1)	-4.27 (10-II-1)	-0.84 (10-II-1)	2764 (10-II-1)	3262 (10-II-1)	638 (10-II-1)
44	1	-4.77 (9-I-1)	-1.86 (10-II-1)	-1.03 (10-I-2)	2350 (9-I-1)	1350 (9-I-2)	-1567 (10-II-1)
44	2	-5.60 (10-II-2)	-1.88 (10-II-1)	-0.47 (9-II-4)	2771 (10-II-1)	1383 (9-I-2)	-1283 (10-II-1)
44	3	-5.99 (10-II-1)	-2.07 (10-II-1)	0.50 (9-I-4)	2977 (10-II-1)	1355 (9-I-2)	-1046 (10-II-2)

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44	4	-6.20 (10-II-1)	-2.23 (10-II-1)	1.09 (9-I-4)	2854 (10-II-1)	1218 (9-I-2)	-853 (10-II-2)
44	5	-5.94 (10-II-1)	-2.48 (10-II-1)	1.65 (9-I-4)	2678 (10-II-1)	1012 (9-I-2)	-655 (9-II-1)
44	6	-5.23 (10-II-1)	-2.76 (10-II-1)	2.03 (9-I-2)	2376 (10-II-2)	835 (9-I-1)	-456 (9-II-1)
44	7	-4.33 (10-II-1)	-3.05 (10-II-1)	2.42 (9-I-2)	1882 (10-I-3)	549 (9-I-1)	-333 (10-II-2)
44	8	-3.95 (10-II-1)	-3.14 (10-II-1)	1.67 (9-I-2)	2108 (9-I-2)	1181 (9-I-2)	-758 (10-II-2)
44	9	-4.10 (10-II-1)	-3.00 (10-II-1)	1.39 (9-I-2)	2283 (9-I-2)	1779 (9-I-2)	-1042 (9-I-3)
44	10	-4.38 (10-II-1)	-2.74 (10-II-1)	1.42 (9-I-2)	2437 (9-I-3)	2039 (9-I-2)	-1380 (9-I-3)
44	11	-4.26 (10-II-1)	-3.09 (10-II-1)	1.28 (9-I-2)	2670 (10-II-2)	2498 (9-I-2)	-985 (10-II-1)
44	12	-4.56 (10-II-1)	-3.01 (10-II-1)	1.28 (9-I-2)	2928 (10-II-1)	2120 (9-I-2)	-877 (10-II-1)
44	13	-5.01 (10-II-1)	-2.74 (10-II-1)	1.05 (9-I-2)	3156 (10-II-1)	1967 (9-I-2)	-841 (10-II-1)
44	14	-5.27 (10-II-2)	-2.43 (10-II-1)	0.68 (9-I-4)	3151 (10-II-1)	1809 (9-I-2)	-820 (10-II-1)
44	15	-5.06 (10-II-2)	-2.18 (10-II-1)	0.17 (9-I-4)	2905 (10-II-1)	1679 (9-I-2)	-826 (10-II-1)
44	16	-4.51 (9-I-1)	-1.96 (10-II-1)	-0.58 (10-I-2)	2403 (10-II-2)	1511 (9-I-2)	-881 (10-II-1)
44	17	-3.53 (9-I-1)	-1.89 (10-II-1)	-1.09 (10-I-2)	1679 (9-I-1)	1248 (9-I-2)	-1010 (10-II-1)
44	18	-2.04 (9-I-1)	-2.11 (10-II-1)	-1.40 (10-I-1)	694 (9-I-1)	797 (9-I-1)	-1219 (10-II-1)
44	19	2.63 (9-II-1)	-1.77 (10-II-4)	-2.55 (10-I-4)	-1349 (9-II-1)	-222 (10-II-4)	-1734 (10-II-4)
44	20	-1.78 (9-I-1)	-1.86 (10-II-1)	-1.83 (10-I-1)	786 (9-I-1)	711 (9-I-1)	-2063 (10-II-4)
44	21	-3.58 (9-I-1)	-1.85 (10-II-1)	-1.49 (10-I-2)	1723 (9-I-1)	1196 (9-I-2)	-1866 (10-II-1)
44	22	-4.82 (10-II-1)	-2.91 (10-II-1)	1.61 (9-I-2)	2742 (10-II-1)	1516 (9-I-2)	-809 (9-I-3)
44	23	-5.46 (10-II-1)	-2.62 (10-II-1)	1.32 (9-I-4)	3030 (10-II-1)	1462 (9-I-2)	-828 (10-II-1)
45	1	-6.44 (10-II-1)	-1.74 (10-II-1)	0.88 (9-I-3)	2916 (10-II-1)	865 (10-II-1)	-594 (9-I-4)
45	2	-6.84 (10-II-1)	-1.67 (10-II-1)	0.84 (9-I-3)	2991 (10-II-1)	803 (10-II-1)	-363 (9-I-4)
45	3	-6.80 (10-II-1)	-1.66 (10-II-1)	0.81 (10-II-1)	2882 (10-II-1)	797 (10-II-1)	-137 (9-I-4)
45	4	-6.28 (10-II-2)	-1.73 (10-II-1)	0.80 (10-II-1)	2578 (10-II-2)	823 (10-II-1)	172 (10-I-1)
45	5	-5.30 (9-I-1)	-1.84 (10-II-1)	0.79 (10-II-1)	2099 (9-I-1)	854 (10-II-1)	293 (10-I-1)
45	6	-3.91 (9-I-1)	-1.94 (10-II-1)	0.76 (10-II-1)	1499 (9-I-1)	862 (10-II-1)	361 (10-I-1)
45	7	-1.95 (9-I-1)	-1.97 (9-I-1)	0.53 (10-II-1)	635 (9-I-1)	709 (10-II-4)	377 (10-I-1)
45	8	2.47 (9-II-1)	-1.39 (10-II-1)	-1.09 (10-I-4)	-1019 (9-II-1)	576 (10-II-1)	347 (10-I-4)
45	9	-1.86 (9-I-1)	-1.58 (10-II-4)	0.59 (10-II-1)	762 (9-I-1)	680 (9-I-3)	-686 (10-II-1)
45	10	-3.88 (9-I-1)	-1.79 (10-II-1)	0.40 (10-II-1)	1632 (9-I-1)	667 (10-II-1)	-742 (10-II-1)
45	11	-5.31 (9-I-1)	-1.80 (10-II-1)	0.49 (10-II-1)	2227 (9-I-1)	648 (10-II-1)	-734 (10-II-1)
45	12	-6.31 (10-II-2)	-1.72 (10-II-1)	0.55 (10-II-1)	2688 (10-II-1)	615 (10-II-1)	-649 (10-II-2)
45	13	-6.85 (10-II-1)	-1.64 (10-II-1)	0.70 (9-I-3)	2945 (10-II-1)	594 (10-II-1)	-522 (10-II-2)
45	14	-6.95 (10-II-1)	-1.61 (10-II-1)	0.90 (9-I-3)	3011 (10-II-1)	594 (10-II-1)	-392 (10-II-2)
45	15	-6.63 (10-II-1)	-1.64 (10-II-1)	1.13 (9-I-3)	2885 (10-II-1)	587 (10-II-1)	-290 (9-I-3)
45	16	-5.65 (10-II-2)	-1.64 (10-II-1)	1.40 (10-II-2)	2496 (10-II-2)	620 (10-II-1)	-147 (9-I-1)
45	17	-4.69 (10-I-2)	-1.64 (10-II-1)	1.26 (10-II-2)	1724 (10-I-3)	623 (10-II-1)	-186 (9-I-1)
45	18	-5.05 (10-II-2)	-1.59 (10-II-1)	1.15 (10-II-2)	1400 (10-I-3)	709 (10-II-1)	-343 (9-I-3)
45	19	-5.01 (10-II-2)	-1.79 (10-II-1)	1.08 (10-II-2)	688 (9-II-1)	562 (10-II-1)	-303 (10-II-2)
45	20	-4.86 (10-II-2)	-1.66 (10-II-1)	1.16 (10-II-2)	1820 (10-I-2)	576 (10-II-4)	-1133 (10-II-1)
45	21	-5.41 (10-II-2)	-1.76 (10-II-1)	0.78 (9-I-3)	2456 (10-II-1)	789 (10-II-1)	-636 (10-II-1)
45	22	-5.39 (10-II-2)	-1.54 (10-II-1)	1.09 (9-I-3)	2325 (10-II-2)	715 (10-II-1)	-548 (10-II-2)
46	1	-5.06 (10-II-2)	-2.83 (10-II-4)	-2.36 (10-I-4)	2666 (10-II-1)	974 (10-II-4)	1005 (10-I-1)
46	2	-5.46 (10-II-1)	-2.71 (10-II-4)	-2.40 (10-I-4)	2679 (10-II-1)	1222 (10-II-4)	1102 (10-I-4)
46	3	-5.79 (10-II-1)	-2.37 (10-II-4)	-2.25 (10-I-4)	2435 (10-II-1)	1416 (10-II-4)	1118 (10-I-4)
46	4	-5.87 (10-II-1)	-1.86 (10-II-4)	-1.94 (10-I-4)	2063 (10-II-1)	1429 (10-II-4)	1043 (10-I-4)
46	5	-5.66 (10-II-1)	-1.43 (9-I-4)	-1.44 (10-I-4)	1663 (10-II-1)	1316 (10-II-4)	934 (10-I-4)
46	6	-4.92 (10-II-1)	-1.00 (9-I-1)	-0.92 (10-I-4)	1119 (9-I-2)	904 (9-I-1)	678 (10-I-4)
46	7	-3.52 (10-II-1)	-0.60 (9-I-1)	0.35 (9-II-1)	526 (9-I-4)	649 (9-I-1)	589 (10-I-4)
46	8	0.81 (10-I-1)	-0.55 (9-I-1)	1.23 (9-II-1)	-990 (10-I-1)	-138 (10-II-4)	-777 (9-II-1)
46	9	-2.85 (10-II-1)	-1.44 (9-I-1)	-0.97 (10-I-4)	1256 (10-II-1)	-627 (10-I-4)	-617 (9-II-1)
46	10	-4.06 (10-II-1)	-2.01 (10-II-4)	-1.71 (10-I-4)	1552 (10-II-1)	-269 (10-I-4)	-141 (9-II-1)
46	11	-4.63 (10-II-1)	-2.51 (10-II-4)	-2.08 (10-I-4)	1995 (10-II-1)	212 (9-I-3)	232 (10-I-4)
46	12	-5.04 (10-II-1)	-2.63 (10-II-4)	-2.18 (10-I-4)	2242 (10-II-1)	530 (6)	504 (10-I-4)
46	13	-5.27 (10-II-1)	-2.63 (10-II-4)	-2.14 (10-I-4)	2370 (10-II-1)	818 (6)	721 (10-I-4)
46	14	-5.30 (10-II-2)	-2.53 (10-II-4)	-2.04 (10-I-1)	2447 (10-II-1)	1131 (6)	931 (10-I-4)
46	15	-5.15 (10-II-2)	-2.36 (10-II-4)	-1.94 (10-I-1)	2395 (10-II-2)	1381 (10-II-1)	1128 (10-I-4)
46	16	-4.92 (10-II-2)	-2.18 (10-II-4)	-1.90 (10-I-1)	2227 (10-II-2)	1527 (10-II-1)	1243 (10-I-1)
46	17	-4.74 (10-II-2)	-1.94 (10-II-4)	-1.97 (10-I-1)	1775 (10-I-2)	1364 (10-II-1)	1086 (10-I-1)
46	18	-4.21 (10-II-2)	-1.66 (10-II-4)	-1.77 (10-I-1)	1806 (10-I-4)	1238 (10-II-1)	1023 (10-I-1)
46	19	-3.94 (10-I-4)	-1.39 (10-II-4)	-1.58 (10-I-1)	1085 (10-I-4)	466 (10-II-4)	414 (10-I-1)
46	20	-4.76 (10-II-2)	-1.80 (10-II-4)	-2.03 (10-I-1)	1057 (10-I-4)	209 (9-II-4)	340 (10-I-1)
46	21	-4.95 (10-II-2)	-2.08 (10-II-4)	-2.07 (10-I-1)	1256 (10-I-4)	426 (9-II-4)	445 (10-I-1)
46	22	-4.60 (10-II-2)	-2.20 (10-II-4)	-1.91 (10-I-1)	1511 (10-II-2)	523 (9-II-4)	460 (10-I-1)
46	23	-4.80 (10-II-2)	-2.65 (10-II-4)	-2.19 (10-I-1)	2226 (10-II-1)	767 (9-II-4)	817 (10-I-1)
46	24	-5.11 (10-II-1)	-2.02 (10-II-4)	-1.63 (10-I-4)	2290 (10-II-1)	946 (10-II-4)	930 (10-I-4)
46	25	-4.46 (10-II-1)	-1.87 (10-II-4)	-1.39 (10-I-4)	1930 (10-II-1)	484 (9-I-4)	695 (10-I-4)
46	26	-4.82 (10-II-1)	-2.33 (10-II-4)	-1.82 (10-I-4)	2284 (10-II-1)	718 (10-II-4)	836 (10-I-4)
46	27	-5.42 (10-II-1)	-2.47 (10-II-4)	-2.04 (10-I-4)	2706 (10-II-1)	1352 (10-II-4)	1150 (10-I-4)
46	28	-5.36 (10-II-1)	-2.25 (10-II-4)	-1.89 (10-I-4)	2522 (10-II-1)	1211 (10-II-4)	1058 (10-I-4)
46	29	-5.14 (10-II-1)	-2.49 (10-II-4)	-1.91 (10-I-4)	2687 (10-II-1)	1282 (10-II-4)	1096 (10-I-4)
46	30	-5.02 (10-II-1)	-2.57 (10-II-4)	-1.96 (10-I-4)	2555 (10-II-1)	1040 (10-II-4)	991 (10-I-4)
46	31	-5.28 (10-II-1)	-2.58 (10-II-4)	-2.12 (10-I-4)	2805 (10-II-1)	1366 (10-II-4)	1182 (10-I-4)
46	32	-5.11 (10-II-1)	-2.56 (10-II-4)	-2.00 (10-I-1)	2802 (10-II-1)	1419 (10-II-4)	1170 (10-I-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

Pagina 113 di
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
46	33	-5.12 (10-II-2)	-2.57 (10-II-4)	-2.04 (10-I-1)	2686 (10-II-1)	1297 (10-II-4)	1120 (10-I-4)
46	34	-5.05 (10-II-1)	-2.58 (10-II-4)	-2.02 (10-I-1)	2769 (10-II-1)	1397 (10-II-4)	1161 (10-I-4)
46	35	-5.10 (10-II-1)	-2.64 (10-II-4)	-2.02 (10-I-1)	2673 (10-II-1)	1161 (10-II-4)	1062 (10-I-4)
46	36	-4.81 (10-II-2)	-2.22 (10-II-4)	-1.99 (10-I-1)	2292 (10-II-2)	1345 (10-II-4)	1122 (10-I-1)
46	37	-5.03 (10-II-2)	-2.42 (10-II-4)	-2.04 (10-I-1)	2609 (10-II-2)	1417 (10-II-4)	1174 (10-I-4)
46	38	-5.05 (10-II-2)	-2.51 (10-II-4)	-2.03 (10-I-1)	2764 (10-II-1)	1385 (10-II-4)	1167 (10-I-4)
46	39	-5.11 (10-II-2)	-2.56 (10-II-4)	-2.12 (10-I-1)	2758 (10-II-1)	1288 (10-II-4)	1155 (10-I-4)
46	40	-4.97 (10-II-2)	-2.24 (10-II-4)	-2.14 (10-I-1)	2238 (10-II-2)	1147 (10-II-4)	1040 (10-I-1)
46	41	-5.03 (10-II-2)	-2.48 (10-II-4)	-2.04 (10-I-1)	2679 (10-II-1)	1420 (10-II-4)	1182 (10-I-4)
46	42	-4.93 (10-II-2)	-2.45 (10-II-4)	-2.03 (10-I-1)	2513 (10-II-1)	1125 (10-II-4)	1058 (10-I-1)
47	1	-4.64 (9-I-2)	-1.68 (10-II-1)	-0.66 (10-I-2)	2300 (9-I-2)	464 (10-II-1)	725 (10-I-2)
47	2	-4.78 (9-I-2)	-2.22 (10-II-1)	-1.19 (10-I-2)	2863 (9-I-1)	688 (10-II-1)	852 (10-I-2)
47	3	-4.42 (10-II-2)	-2.66 (10-II-1)	-1.46 (10-I-2)	3219 (10-I-4)	869 (10-II-1)	862 (6)
47	4	-3.87 (10-II-2)	-2.87 (6)	-1.58 (10-I-2)	3419 (10-I-4)	1033 (10-II-1)	765 (6)
47	5	-3.28 (9-I-2)	-2.92 (6)	-1.52 (10-I-2)	3371 (10-I-3)	982 (10-II-1)	538 (6)
47	6	-2.82 (9-I-2)	-2.61 (6)	-1.37 (10-I-2)	3241 (10-I-3)	935 (10-II-1)	250 (6)
47	7	-2.63 (9-I-2)	-2.16 (6)	-1.20 (10-I-2)	2894 (10-I-3)	608 (10-II-1)	-127 (10-II-2)
47	8	-2.64 (9-I-2)	-2.40 (6)	-1.37 (10-I-2)	2822 (10-I-3)	339 (10-II-4)	-131 (10-II-2)
47	9	-2.32 (9-I-2)	-2.80 (10-II-1)	-1.79 (10-I-2)	2669 (10-I-3)	284 (9-II-1)	-104 (9-I-1)
47	10	-2.42 (10-I-4)	-3.46 (10-II-1)	-3.18 (10-I-2)	2577 (10-I-1)	-614 (10-I-4)	-507 (10-I-4)
47	11	-3.69 (10-I-4)	-3.23 (10-II-1)	-3.04 (10-I-2)	2671 (10-I-4)	-691 (10-I-4)	-154 (9-I-1)
47	12	-4.71 (10-I-4)	-3.03 (6)	-2.84 (10-I-2)	2948 (10-I-3)	-459 (10-I-4)	223 (10-I-2)
47	13	-5.31 (10-I-1)	-2.67 (6)	-2.46 (10-I-2)	2963 (10-II-2)	-196 (10-I-4)	578 (10-I-2)
47	14	-5.58 (10-II-2)	-2.23 (6)	-1.88 (10-I-2)	2798 (9-I-2)	247 (10-II-1)	896 (10-I-2)
47	15	-5.51 (10-II-2)	-1.77 (6)	-1.18 (10-I-2)	2541 (9-I-2)	462 (10-II-1)	1109 (10-I-2)
47	16	-5.22 (9-I-2)	-1.26 (9-I-3)	-0.41 (10-I-2)	1936 (9-I-2)	598 (10-II-1)	1269 (10-I-2)
47	17	-4.36 (9-I-2)	-0.88 (9-I-3)	0.52 (10-II-2)	1128 (9-I-2)	612 (9-I-3)	1411 (10-I-1)
47	18	-2.65 (9-I-2)	-0.60 (10-II-4)	1.17 (10-II-1)	-362 (9-II-4)	374 (9-I-3)	1538 (10-I-1)
47	19	2.14 (9-II-3)	-0.16 (9-I-1)	1.53 (10-II-4)	-2067 (9-II-3)	-258 (10-I-1)	1327 (10-I-4)
47	20	-2.65 (9-I-2)	-0.88 (10-II-4)	0.61 (10-II-1)	339 (9-I-4)	-249 (10-I-4)	611 (10-I-1)
47	21	-4.02 (9-I-2)	-1.22 (10-II-4)	-0.10 (10-I-2)	1516 (9-I-2)	232 (9-I-3)	644 (10-I-1)
47	22	-3.48 (9-I-2)	-2.97 (6)	-1.98 (10-I-2)	3193 (10-I-3)	646 (10-II-1)	571 (6)
47	23	-3.40 (10-II-2)	-3.16 (10-II-1)	-2.19 (10-I-2)	2946 (10-I-3)	269 (10-II-4)	412 (6)
47	24	-4.11 (10-I-1)	-3.04 (6)	-2.34 (10-I-2)	3044 (10-I-4)	267 (10-II-4)	621 (6)
47	25	-4.59 (10-II-2)	-2.85 (6)	-2.19 (10-I-2)	3133 (10-I-3)	370 (10-II-1)	784 (10-I-2)
47	26	-4.71 (10-II-2)	-2.69 (6)	-1.85 (10-I-2)	3184 (10-I-3)	557 (10-II-1)	889 (10-I-2)
47	27	-4.12 (10-II-2)	-2.87 (6)	-1.86 (10-I-2)	3290 (10-I-4)	727 (10-II-1)	771 (6)
48	1	-0.52 (10-II-4)	1.00 (9-I-4)	2.75 (9-II-4)	59 (9-I-3)	208 (9-I-3)	-74 (9-II-3)
48	2	-2.28 (10-II-3)	1.03 (9-I-3)	3.08 (9-II-4)	116 (10-II-3)	300 (9-I-1)	46 (10-II-3)
48	3	-2.93 (9-I-3)	0.86 (9-I-3)	3.23 (9-II-4)	135 (9-I-3)	232 (9-II-3)	24 (10-I-3)
48	4	-2.97 (9-II-1)	0.62 (9-I-3)	3.25 (9-II-4)	136 (9-I-3)	122 (10-II-2)	23 (10-I-3)
48	5	-1.19 (10-II-3)	0.97 (9-I-4)	2.84 (9-II-4)	42 (9-I-3)	186 (9-I-3)	-30 (9-II-3)
48	6	-2.47 (10-II-3)	0.95 (9-I-3)	3.30 (9-II-4)	104 (9-I-3)	280 (9-I-4)	96 (10-II-2)
48	7	-2.96 (10-II-3)	0.86 (9-I-3)	3.43 (9-II-4)	130 (9-I-4)	219 (9-II-3)	67 (9-II-4)
48	8	-3.00 (9-II-1)	0.82 (10-II-3)	3.40 (9-II-4)	132 (9-I-3)	117 (9-II-3)	54 (10-I-4)
48	9	-1.85 (10-II-3)	0.48 (9-I-4)	2.85 (9-II-4)	-45 (9-II-4)	184 (9-I-3)	11 (9-I-3)
48	10	-2.75 (10-II-3)	0.50 (9-I-3)	3.39 (9-II-4)	-20 (9-II-4)	247 (9-I-4)	119 (9-II-4)
48	11	-3.03 (10-II-3)	0.69 (10-II-3)	3.47 (9-II-4)	-14 (6)	181 (9-II-3)	81 (9-II-4)
48	12	-2.99 (9-I-3)	0.87 (10-II-3)	3.45 (9-II-4)	-19 (6)	87 (9-II-3)	55 (9-II-4)
48	13	-2.84 (10-II-3)	-1.15 (9-II-4)	2.76 (9-II-4)	-133 (10-II-3)	78 (9-I-3)	-102 (9-II-3)
48	14	-2.74 (10-II-3)	-0.71 (9-II-3)	3.06 (9-II-4)	-242 (10-II-3)	162 (9-I-4)	-32 (9-II-3)
48	15	-3.01 (10-II-3)	0.20 (10-II-3)	3.27 (9-II-4)	-297 (10-II-3)	109 (9-II-3)	-94 (9-II-3)
48	16	-3.01 (9-I-3)	0.88 (10-II-3)	3.33 (9-II-4)	-316 (10-I-2)	36 (9-II-3)	-122 (9-II-3)
49	1	0.67 (9-II-3)	1.02 (10-II-3)	2.10 (10-II-3)	-16 (6)	303 (9-II-4)	-144 (10-II-3)
49	2	-2.13 (9-I-3)	0.50 (9-I-3)	2.12 (10-II-3)	-144 (6)	258 (9-II-3)	-68 (10-II-3)
49	3	-2.94 (9-I-3)	0.12 (9-I-3)	2.19 (10-II-3)	-246 (10-I-2)	151 (9-II-3)	-79 (10-II-3)
49	4	-3.02 (9-II-4)	-0.51 (9-II-3)	2.22 (10-II-3)	-310 (9-II-4)	46 (10-II-3)	-79 (10-II-3)
49	5	-0.20 (9-I-3)	1.16 (9-I-3)	2.44 (10-II-3)	66 (10-II-3)	221 (9-I-3)	-118 (9-II-3)
49	6	-1.99 (9-I-3)	0.94 (9-I-3)	2.58 (10-II-3)	51 (10-II-3)	269 (9-II-3)	6 (10-II-3)
49	7	-2.85 (9-I-3)	0.57 (9-I-3)	2.51 (10-II-3)	20 (10-II-3)	189 (9-I-1)	26 (10-II-3)
49	8	-3.05 (9-II-4)	0.22 (9-I-3)	2.48 (10-II-3)	-25 (6)	88 (10-II-3)	43 (10-II-3)
49	9	-0.53 (10-II-4)	1.23 (9-I-3)	2.57 (10-II-3)	72 (10-II-3)	202 (9-I-3)	-102 (9-II-3)
49	10	-2.08 (9-I-3)	1.10 (9-I-3)	2.80 (10-II-3)	115 (10-II-3)	291 (9-I-1)	20 (10-II-3)
49	11	-2.88 (9-I-3)	0.85 (9-I-3)	2.83 (10-II-3)	131 (9-I-4)	217 (9-I-1)	26 (10-II-3)
49	12	-3.08 (9-II-4)	0.50 (9-I-3)	2.80 (10-II-3)	124 (9-I-4)	114 (10-II-3)	42 (10-II-3)
49	13	-1.04 (10-II-3)	1.15 (9-I-3)	2.62 (9-II-4)	72 (10-II-3)	170 (9-I-3)	-90 (9-II-3)
49	14	-2.21 (10-II-3)	0.95 (9-I-3)	2.90 (10-II-3)	103 (9-I-3)	282 (9-I-4)	24 (10-II-3)
49	15	-2.89 (9-I-3)	0.81 (9-I-3)	3.03 (10-II-3)	129 (9-I-3)	223 (9-I-1)	8 (6)
49	16	-3.13 (9-II-4)	0.69 (9-I-3)	3.06 (10-II-3)	130 (9-I-3)	123 (10-II-3)	14 (6)
50	1	0.89 (9-II-4)	0.81 (9-I-4)	1.46 (10-II-3)	28 (9-I-4)	-50 (6)	31 (10-I-3)
50	2	-1.83 (9-I-3)	0.56 (9-I-3)	1.70 (10-II-3)	73 (9-I-4)	280 (9-I-1)	88 (9-II-4)
50	3	-3.11 (9-I-1)	0.24 (9-I-3)	1.72 (10-II-3)	121 (9-I-4)	304 (9-II-3)	52 (9-II-4)
50	4	-3.63 (9-II-4)	-0.26 (6)	1.55 (10-II-3)	155 (9-I-4)	223 (10-II-3)	6 (6)
50	5	0.32 (9-II-3)	0.77 (9-I-4)	1.55 (10-II-3)	-40 (9-II-4)	-39 (6)	53 (10-I-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

Pagina 114 di
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
50	6	-1.92 (9-I-3)	0.58 (9-I-3)	2.00 (10-II-3)	54 (9-I-4)	265 (9-I-1)	134 (9-II-4)
50	7	-2.99 (9-II-1)	0.33 (9-I-3)	1.97 (10-II-3)	103 (9-I-4)	268 (9-II-3)	97 (9-II-4)
50	8	-3.42 (9-II-4)	-0.13 (6)	1.77 (10-II-3)	133 (9-I-4)	186 (10-II-3)	47 (9-II-4)
50	9	-0.56 (10-II-4)	0.33 (9-I-4)	1.71 (10-II-3)	-64 (9-II-4)	66 (9-I-4)	63 (10-I-3)
50	10	-2.10 (9-I-3)	0.24 (9-I-3)	2.13 (10-II-3)	-43 (9-II-4)	243 (9-II-3)	157 (9-II-4)
50	11	-2.91 (9-II-1)	0.19 (9-I-3)	2.13 (10-II-3)	-31 (9-II-4)	215 (9-II-3)	114 (9-II-4)
50	12	-3.24 (9-II-4)	-0.20 (9-II-3)	1.98 (10-II-3)	-24 (9-II-4)	131 (10-II-3)	62 (9-II-4)
50	13	-1.25 (10-II-3)	-0.84 (10-II-3)	1.83 (10-II-3)	-51 (6)	43 (9-I-4)	-38 (10-II-3)
50	14	-2.06 (9-I-3)	-0.74 (10-II-2)	2.00 (10-II-3)	-178 (10-II-4)	184 (9-I-1)	38 (10-I-3)
50	15	-2.82 (9-I-3)	-0.48 (9-II-3)	2.13 (10-II-3)	-267 (9-II-4)	147 (9-II-3)	-33 (10-II-3)
50	16	-3.11 (9-II-4)	-0.35 (9-II-3)	2.11 (10-II-3)	-315 (9-II-4)	68 (10-II-3)	-72 (10-II-3)
51	1	0.85 (9-II-4)	-0.72 (6)	0.17 (10-II-3)	153 (9-II-4)	53 (9-I-4)	-44 (10-II-3)
51	2	-1.54 (9-I-3)	-1.70 (6)	-0.24 (10-I-3)	91 (9-II-4)	292 (9-II-3)	-67 (10-II-3)
51	3	-2.71 (9-II-1)	-2.70 (9-II-4)	0.16 (10-II-3)	148 (9-II-4)	389 (9-II-4)	-59 (10-II-3)
51	4	-3.70 (9-II-1)	-3.99 (9-II-4)	1.01 (10-II-3)	180 (9-II-4)	655 (9-II-4)	-124 (9-II-4)
51	5	0.89 (9-II-4)	-0.19 (6)	0.65 (10-II-3)	57 (10-II-3)	-67 (6)	-52 (9-I-4)
51	6	-1.62 (9-I-3)	-0.68 (6)	0.70 (10-II-3)	154 (9-II-4)	313 (9-II-3)	-59 (9-I-4)
51	7	-3.08 (9-II-1)	-1.31 (6)	0.91 (10-II-3)	244 (9-II-4)	403 (9-II-4)	-41 (9-I-4)
51	8	-3.83 (9-II-4)	-1.50 (6)	1.04 (10-II-3)	268 (9-II-4)	382 (9-II-4)	-73 (9-II-4)
51	9	0.82 (9-II-4)	0.57 (9-I-4)	0.97 (10-II-3)	33 (9-I-3)	-94 (6)	-12 (9-I-4)
51	10	-1.69 (9-I-3)	0.23 (9-I-4)	1.12 (10-II-3)	143 (9-I-3)	308 (9-II-3)	23 (9-II-4)
51	11	-3.11 (9-II-1)	-0.43 (6)	1.22 (10-II-3)	232 (9-II-1)	388 (9-II-4)	-9 (9-I-4)
51	12	-3.80 (9-II-4)	-0.66 (6)	1.19 (10-II-3)	280 (9-II-4)	334 (9-II-4)	-50 (9-II-3)
51	13	0.63 (9-II-3)	0.78 (9-I-4)	1.19 (10-II-3)	32 (9-I-4)	-93 (6)	31 (10-I-3)
51	14	-1.78 (9-I-3)	0.42 (9-I-4)	1.39 (10-II-3)	97 (9-I-4)	284 (9-I-1)	67 (9-II-4)
51	15	-3.07 (9-II-1)	-0.19 (6)	1.47 (10-II-3)	156 (9-I-4)	344 (9-II-4)	27 (6)
51	16	-3.66 (9-II-4)	-0.40 (6)	1.38 (10-II-3)	199 (10-II-3)	278 (9-II-4)	-30 (10-II-2)
52	1	-0.34 (10-I-3)	0.70 (9-II-3)	-2.43 (9-II-3)	32 (9-I-4)	99 (9-I-4)	-36 (10-II-3)
52	2	-1.94 (10-I-3)	0.24 (9-I-4)	-2.85 (9-II-3)	67 (10-I-3)	387 (9-II-4)	-163 (9-II-4)
52	3	-2.91 (9-II-4)	-0.48 (6)	-3.04 (9-II-3)	78 (10-I-3)	481 (9-II-4)	-135 (9-II-4)
52	4	-2.68 (9-II-4)	-0.84 (6)	-3.20 (9-II-3)	16 (6)	466 (9-II-4)	11 (10-II-3)
52	5	0.55 (9-II-4)	0.50 (9-I-4)	-2.12 (9-II-3)	43 (10-I-3)	80 (9-I-4)	-17 (10-II-3)
52	6	-1.67 (9-I-3)	-0.26 (6)	-2.55 (9-II-3)	141 (9-II-4)	391 (9-II-4)	-139 (9-II-4)
52	7	-2.84 (9-II-4)	-0.75 (6)	-2.77 (9-II-3)	193 (9-II-4)	508 (9-II-4)	-152 (9-II-4)
52	8	-3.02 (9-II-4)	-1.28 (6)	-2.75 (9-II-3)	126 (9-II-4)	557 (9-II-4)	-43 (10-I-3)
52	9	1.13 (9-II-4)	0.19 (9-I-4)	-1.73 (9-II-3)	92 (9-II-4)	83 (9-I-4)	33 (10-I-3)
52	10	-1.47 (9-I-3)	-0.76 (6)	-1.99 (9-II-3)	168 (9-II-4)	362 (9-II-4)	-78 (9-II-4)
52	11	-2.77 (9-II-4)	-1.69 (6)	-2.20 (9-II-3)	243 (9-II-4)	486 (9-II-4)	-148 (9-II-4)
52	12	-3.28 (9-II-4)	-2.42 (9-II-4)	-2.24 (9-II-3)	214 (9-II-4)	691 (9-II-4)	-104 (9-II-4)
52	13	1.46 (9-II-4)	-0.43 (6)	-1.14 (9-II-3)	162 (9-II-4)	129 (9-I-4)	45 (10-I-3)
52	14	-1.48 (9-I-3)	-1.60 (6)	-1.06 (9-II-3)	99 (9-II-4)	319 (9-II-3)	-23 (10-II-3)
52	15	-2.54 (10-I-2)	-3.00 (9-II-4)	-1.09 (9-II-3)	122 (9-II-4)	402 (9-II-4)	-88 (10-II-3)
52	16	-3.44 (9-II-4)	-4.97 (9-II-4)	-1.52 (9-II-3)	275 (9-II-4)	822 (9-II-4)	-96 (9-II-1)
53	1	-2.56 (10-I-3)	-1.09 (10-I-3)	-2.88 (9-II-3)	-106 (6)	111 (9-I-4)	87 (9-II-3)
53	2	-2.68 (9-II-4)	-0.51 (6)	-3.10 (9-II-3)	-274 (9-II-4)	238 (9-II-4)	-18 (6)
53	3	-3.10 (9-II-4)	0.41 (9-II-3)	-3.13 (9-II-3)	-348 (9-II-4)	224 (9-II-4)	33 (9-I-1)
53	4	-1.83 (10-II-3)	1.18 (9-II-3)	-3.62 (9-II-3)	-332 (9-II-4)	275 (9-II-4)	118 (9-II-4)
53	5	-1.33 (10-I-3)	0.25 (9-I-4)	-2.98 (9-II-3)	-85 (9-II-4)	191 (9-I-4)	-39 (10-II-3)
53	6	-2.55 (9-II-4)	0.21 (10-II-3)	-3.58 (9-II-3)	-88 (9-II-4)	312 (9-II-4)	-170 (9-II-4)
53	7	-2.98 (9-II-4)	0.52 (9-II-3)	-3.75 (9-II-3)	-95 (9-II-4)	272 (9-II-4)	-86 (9-II-4)
53	8	-2.81 (10-II-2)	0.42 (10-II-2)	-3.52 (9-II-3)	-129 (9-II-2)	213 (6)	68 (10-II-3)
53	9	-0.48 (9-I-4)	0.62 (9-I-4)	-2.93 (9-II-3)	-29 (9-II-4)	171 (9-I-4)	-40 (10-II-3)
53	10	-2.26 (10-I-3)	0.49 (9-I-1)	-3.55 (9-II-3)	15 (9-I-4)	349 (9-II-4)	-167 (9-II-4)
53	11	-3.06 (9-II-4)	0.23 (10-II-3)	-3.68 (9-II-3)	-6 (9-II-4)	357 (9-II-4)	-98 (9-II-4)
53	12	-3.40 (9-II-4)	0.08 (10-II-3)	-3.39 (9-II-3)	-51 (9-II-2)	248 (9-II-4)	47 (10-II-3)
53	13	0.57 (9-II-4)	0.49 (9-I-4)	-2.80 (9-II-3)	15 (9-I-4)	161 (9-I-4)	-26 (10-II-3)
53	14	-1.97 (10-I-3)	0.20 (9-I-4)	-3.20 (9-II-3)	34 (9-I-4)	375 (9-II-4)	-155 (9-II-4)
53	15	-3.18 (9-II-4)	-0.30 (6)	-3.33 (9-II-3)	9 (10-I-3)	402 (9-II-4)	-111 (9-II-4)
53	16	-4.02 (9-II-4)	-0.44 (6)	-3.32 (9-II-3)	-23 (10-II-3)	305 (9-II-4)	34 (10-II-3)
54	1	-2.15 (10-I-3)	1.47 (9-II-4)	-3.68 (9-II-4)	86 (9-I-4)	306 (9-II-3)	198 (9-II-4)
54	2	-2.76 (10-I-3)	1.47 (9-II-3)	-4.00 (9-II-4)	90 (9-I-4)	319 (9-II-2)	61 (9-II-2)
54	3	-2.85 (10-I-4)	1.50 (9-II-3)	-3.91 (9-II-3)	75 (9-I-4)	217 (9-II-1)	88 (9-II-4)
54	4	-1.72 (10-II-2)	1.46 (9-II-4)	-3.52 (9-II-3)	-78 (9-II-4)	72 (9-II-1)	65 (10-II-1)
54	5	-1.44 (10-I-3)	1.37 (9-II-3)	-3.73 (9-II-4)	92 (9-I-4)	362 (9-II-3)	205 (9-II-4)
54	6	-2.59 (10-I-3)	1.27 (9-II-3)	-4.05 (9-II-4)	88 (9-I-4)	330 (9-II-4)	49 (10-II-3)
54	7	-3.14 (9-II-4)	1.22 (9-II-3)	-4.01 (9-II-3)	40 (9-I-4)	194 (9-II-1)	42 (10-II-3)
54	8	-2.87 (10-II-2)	1.06 (9-II-3)	-3.27 (9-II-3)	-126 (9-II-4)	-22 (10-I-4)	-25 (10-I-3)
54	9	-0.86 (10-I-3)	1.17 (9-II-3)	-3.56 (9-II-4)	68 (9-I-1)	387 (9-II-3)	204 (9-II-4)
54	10	-2.46 (10-I-3)	0.86 (9-II-3)	-3.78 (9-II-4)	-20 (6)	301 (9-II-4)	28 (10-II-4)
54	11	-3.33 (9-II-4)	0.27 (10-II-3)	-3.82 (9-II-3)	-113 (9-II-4)	153 (9-II-1)	6 (10-II-3)
54	12	-4.03 (9-II-4)	0.35 (10-II-2)	-3.06 (9-II-3)	-158 (9-II-4)	-62 (9-I-1)	-60 (10-I-3)
54	13	0.23 (9-II-4)	0.77 (9-II-3)	-3.07 (9-II-4)	-89 (6)	479 (9-II-3)	223 (9-II-3)
54	14	-2.50 (9-II-4)	-0.08 (6)	-3.09 (9-II-3)	-242 (9-II-4)	276 (9-II-4)	83 (9-II-3)
54	15	-3.38 (9-II-4)	-0.73 (6)	-3.06 (9-II-3)	-391 (9-II-4)	62 (9-II-1)	74 (9-II-3)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
54	16	-5.87(9-II-4)	-1.23(10-I-3)	-3.40(9-II-3)	-296(9-II-4)	-221(10-I-4)	40(9-II-3)
55	1	-3.64(10-I-3)	-0.15(6)	-2.73(9-II-4)	-163(10-I-3)	87(9-I-4)	141(9-II-4)
55	2	-3.13(10-I-3)	0.88(10-I-3)	-2.84(9-II-4)	-207(10-I-3)	125(9-I-3)	81(9-II-4)
55	3	-3.04(9-I-4)	2.01(10-I-3)	-2.91(9-II-4)	-207(9-I-4)	81(10-II-3)	128(9-II-4)
55	4	-1.81(9-I-4)	3.18(10-I-3)	-3.37(9-II-4)	-142(9-I-4)	47(9-II-2)	117(9-II-3)
55	5	-2.78(10-I-3)	1.11(9-I-4)	-3.13(9-II-4)	-10(9-II-3)	222(9-I-4)	93(9-II-4)
55	6	-3.17(10-I-3)	1.54(9-I-1)	-3.52(9-II-4)	47(10-II-4)	214(9-I-3)	-17(9-I-2)
55	7	-2.94(9-I-4)	2.25(10-I-3)	-3.63(9-II-4)	87(9-II-1)	128(10-II-3)	52(9-II-4)
55	8	-1.88(9-I-4)	2.76(10-I-3)	-3.71(9-II-4)	133(9-II-4)	42(10-II-3)	73(9-II-4)
55	9	-2.18(10-I-3)	1.41(9-II-3)	-3.42(9-II-4)	79(9-I-4)	263(9-I-4)	134(9-II-4)
55	10	-2.95(10-I-3)	1.81(9-II-3)	-3.79(9-II-4)	144(9-I-4)	267(9-II-1)	23(9-II-4)
55	11	-2.91(9-I-1)	2.07(9-II-3)	-3.92(9-II-3)	169(9-I-3)	173(9-II-1)	84(9-II-4)
55	12	-2.14(9-I-4)	2.24(10-I-3)	-3.73(9-II-3)	186(9-II-1)	45(9-I-4)	96(9-II-4)
55	13	-1.48(10-I-3)	1.13(9-II-3)	-3.58(9-II-4)	73(9-I-4)	312(9-II-3)	182(9-II-4)
55	14	-2.77(10-I-3)	1.59(9-II-3)	-3.89(9-II-4)	122(9-I-4)	304(9-II-2)	57(9-II-4)
55	15	-3.02(10-I-4)	1.93(9-II-3)	-3.87(9-II-3)	107(9-I-4)	180(9-II-1)	100(9-II-4)
55	16	-3.00(9-I-1)	2.07(9-II-3)	-3.72(9-II-3)	123(9-I-4)	34(9-I-3)	136(9-II-4)
56	1	-3.13(10-I-3)	1.16(9-I-4)	-2.30(9-II-4)	139(9-II-3)	274(9-I-4)	91(9-II-4)
56	2	-3.23(9-II-3)	1.24(9-I-4)	-2.41(9-II-4)	183(10-I-3)	266(9-I-4)	-9(9-II-1)
56	3	-3.14(9-II-4)	1.50(9-I-4)	-2.55(9-II-4)	206(9-II-3)	191(10-II-3)	5(10-I-4)
56	4	-2.80(10-II-3)	1.75(9-I-2)	-2.46(9-II-4)	200(9-II-3)	116(9-II-2)	-16(9-II-2)
56	5	-2.96(10-I-3)	1.38(9-I-4)	-2.20(9-II-4)	181(9-II-3)	298(9-I-2)	130(9-II-4)
56	6	-3.16(10-I-3)	1.60(9-I-4)	-2.55(9-II-4)	220(9-II-3)	267(9-I-3)	15(10-I-4)
56	7	-3.14(9-II-4)	1.73(9-I-4)	-2.64(9-II-4)	234(9-II-3)	181(10-II-3)	-12(9-II-1)
56	8	-2.96(10-II-3)	1.86(9-I-2)	-2.51(9-II-4)	219(9-II-3)	92(9-II-2)	-43(9-II-4)
56	9	-2.34(10-I-3)	1.36(9-I-2)	-2.38(9-II-4)	102(9-II-4)	294(9-I-2)	169(9-II-4)
56	10	-2.99(10-I-3)	1.63(9-I-4)	-2.58(9-II-4)	135(9-II-4)	224(9-I-3)	27(9-I-1)
56	11	-3.13(9-I-1)	1.77(9-I-4)	-2.64(9-II-4)	112(9-II-2)	143(10-II-3)	-15(9-II-1)
56	12	-3.23(9-II-4)	1.99(10-I-3)	-2.65(9-II-4)	96(9-II-2)	50(10-II-3)	-46(9-II-1)
56	13	-1.87(10-I-3)	1.48(9-II-3)	-2.37(9-II-4)	-123(10-I-3)	360(9-II-3)	223(9-II-4)
56	14	-3.16(10-I-3)	1.65(10-I-3)	-2.46(9-II-4)	-174(10-I-3)	185(9-II-1)	104(9-II-3)
56	15	-3.11(9-I-4)	1.83(10-I-3)	-2.50(9-II-4)	-201(9-I-4)	77(10-II-3)	97(9-II-3)
56	16	-3.50(9-II-4)	2.14(10-I-3)	-2.96(9-II-4)	-195(9-I-2)	-57(10-I-3)	55(10-I-4)
57	1	-4.23(9-II-4)	-0.50(9-II-4)	-1.68(9-II-4)	-212(9-II-4)	148(9-I-4)	49(9-II-4)
57	2	-3.58(9-II-4)	0.34(9-I-2)	-1.72(9-II-4)	-287(9-II-4)	121(9-I-4)	31(9-II-4)
57	3	-3.29(9-II-4)	0.98(10-I-3)	-1.85(9-II-4)	-306(9-II-1)	80(10-II-3)	76(9-II-4)
57	4	-2.85(9-II-1)	1.64(10-I-3)	-1.93(9-II-4)	-278(7)	50(9-II-3)	95(9-II-4)
57	5	-3.57(9-II-4)	0.63(9-I-4)	-1.82(9-II-4)	11(9-I-4)	248(9-I-4)	-24(9-I-4)
57	6	-3.61(9-II-4)	0.87(9-I-4)	-2.13(9-II-4)	15(10-I-4)	200(9-I-4)	-66(9-II-2)
57	7	-3.30(9-II-4)	1.29(9-I-2)	-2.16(9-II-4)	-6(6)	142(10-II-3)	-21(9-II-2)
57	8	-2.73(10-II-3)	1.66(9-I-2)	-2.19(9-II-4)	-18(6)	94(9-II-3)	6(10-I-1)
57	9	-3.12(9-II-3)	0.91(9-I-4)	-1.96(9-II-4)	112(10-I-3)	275(9-I-4)	15(9-II-4)
57	10	-3.43(9-II-3)	1.15(9-I-4)	-2.26(9-II-4)	158(10-I-3)	247(9-I-4)	-64(9-II-2)
57	11	-3.21(9-II-4)	1.39(9-I-2)	-2.34(9-II-4)	157(10-I-4)	181(10-II-3)	-27(9-II-2)
57	12	-2.67(10-II-3)	1.64(9-I-2)	-2.34(9-II-4)	134(10-I-4)	118(9-II-2)	-15(9-II-2)
57	13	-2.73(10-I-3)	0.84(9-I-4)	-2.08(9-II-4)	106(9-I-1)	296(9-I-4)	64(9-II-4)
57	14	-3.29(9-II-3)	1.21(9-I-2)	-2.33(9-II-4)	172(10-I-4)	274(9-I-3)	-32(9-II-2)
57	15	-3.17(9-II-4)	1.41(9-I-2)	-2.43(9-II-4)	180(10-I-4)	195(10-II-3)	-5(9-II-1)
57	16	-2.66(10-II-3)	1.54(9-I-2)	-2.41(9-II-4)	166(10-I-4)	116(9-II-2)	-8(9-II-2)
58	1	-3.75(9-II-4)	0.99(9-II-1)	-0.98(10-II-3)	134(9-II-4)	330(9-II-2)	52(10-II-3)
58	2	-3.69(9-II-4)	1.38(9-II-2)	-1.07(10-II-3)	175(9-II-3)	274(9-I-4)	21(6)
58	3	-3.33(9-II-2)	1.82(9-II-4)	-1.10(10-II-3)	172(10-II-2)	197(9-I-4)	14(6)
58	4	-2.66(9-I-3)	2.25(9-II-4)	-1.08(10-II-3)	149(10-II-2)	129(10-II-3)	9(10-II-4)
58	5	-3.54(9-II-4)	1.16(9-II-1)	-1.16(9-II-4)	163(9-II-4)	344(9-II-2)	85(10-II-3)
58	6	-3.64(9-II-4)	1.49(9-II-1)	-1.29(9-II-4)	187(9-II-3)	261(9-II-1)	28(6)
58	7	-3.34(9-II-2)	1.84(9-II-4)	-1.30(9-II-4)	164(9-II-3)	184(9-I-4)	-12(9-II-3)
58	8	-2.69(9-I-3)	2.17(9-II-4)	-1.25(9-II-4)	126(10-II-2)	121(9-II-3)	-31(9-II-3)
58	9	-3.33(9-II-3)	1.13(9-II-1)	-1.31(9-II-4)	78(9-II-4)	325(9-II-2)	109(10-II-3)
58	10	-3.56(9-II-3)	1.39(9-II-4)	-1.43(9-II-4)	61(9-II-3)	213(9-I-4)	25(6)
58	11	-3.33(9-II-2)	1.66(9-II-1)	-1.44(9-II-4)	23(10-II-2)	147(10-II-3)	-28(9-II-3)
58	12	-2.72(9-I-3)	1.99(9-II-1)	-1.42(9-II-4)	-16(6)	94(9-II-3)	-50(9-II-3)
58	13	-3.05(10-I-3)	0.89(9-II-4)	-1.33(9-II-4)	-212(9-II-4)	323(9-II-2)	139(9-II-4)
58	14	-3.64(9-II-4)	1.13(9-II-4)	-1.47(9-II-4)	-254(10-I-3)	169(9-II-1)	61(10-II-3)
58	15	-3.38(9-II-4)	1.35(9-II-1)	-1.58(9-II-4)	-292(9-II-1)	101(10-II-3)	62(10-II-3)
58	16	-2.73(9-I-3)	1.71(10-I-3)	-1.64(9-II-4)	-274(9-I-3)	56(9-II-3)	56(10-II-3)
59	1	-3.87(9-II-4)	0.60(10-I-3)	0.35(10-I-3)	-220(9-II-4)	248(9-II-3)	-89(10-I-3)
59	2	-3.83(9-II-3)	1.22(9-II-2)	0.44(10-I-3)	-271(9-II-2)	142(9-I-4)	-29(10-I-3)
59	3	-3.44(9-II-3)	1.86(9-II-2)	0.45(10-I-3)	-282(9-II-3)	80(9-I-4)	12(10-II-3)
59	4	-2.75(9-II-3)	2.54(9-II-2)	0.44(10-I-3)	-232(9-II-3)	37(10-II-3)	32(10-II-3)
59	5	-3.81(9-II-4)	1.12(9-II-2)	-0.36(10-II-3)	78(10-I-3)	314(9-II-3)	-85(10-I-3)
59	6	-3.79(9-II-4)	1.53(9-II-2)	-0.47(10-II-3)	81(10-I-3)	210(9-I-4)	-35(10-II-2)
59	7	-3.41(9-II-2)	2.06(9-II-2)	-0.49(10-II-3)	61(9-I-2)	143(9-I-4)	25(9-II-4)
59	8	-2.71(9-I-4)	2.60(9-II-2)	-0.54(10-II-3)	48(10-II-3)	90(10-II-3)	56(9-II-2)
59	9	-3.72(9-II-4)	1.19(9-II-2)	-0.57(10-II-3)	174(9-II-3)	342(9-II-2)	-49(10-I-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
59	10	-3.75(9-II-4)	1.63(9-II-2)	-0.67(10-II-3)	216(9-II-4)	263(9-I-4)	-29(10-II-2)
59	11	-3.36(9-II-2)	2.07(9-II-2)	-0.72(10-II-3)	203(9-II-4)	187(9-I-4)	13(9-II-1)
59	12	-2.66(9-I-4)	2.52(9-II-2)	-0.76(10-II-3)	174(10-II-3)	122(10-II-3)	39(9-II-4)
59	13	-3.60(9-II-4)	1.00(9-I-1)	-0.78(10-II-3)	138(9-II-3)	345(9-II-2)	20(10-II-3)
59	14	-3.71(9-II-4)	1.49(9-II-2)	-0.86(10-II-3)	193(9-II-4)	283(9-II-2)	-4(10-II-2)
59	15	-3.34(9-II-2)	1.95(9-II-2)	-0.91(10-II-3)	191(9-II-4)	202(9-I-4)	13(9-II-1)
59	16	-2.64(9-I-4)	2.35(9-II-4)	-0.94(10-II-3)	168(10-II-3)	132(10-II-3)	24(9-II-1)
60	1	-3.40(9-II-4)	1.06(9-II-2)	1.55(10-I-3)	136(9-II-4)	355(9-II-3)	-66(10-I-3)
60	2	-3.67(9-II-4)	1.63(9-II-2)	1.71(10-I-3)	196(9-II-4)	287(9-II-3)	-9(10-II-3)
60	3	-3.38(9-II-3)	2.11(9-II-2)	1.79(10-I-3)	197(9-II-1)	200(9-I-4)	-27(10-I-4)
60	4	-2.73(9-I-4)	2.54(9-II-2)	1.81(10-I-3)	176(9-I-3)	121(9-I-4)	-31(10-I-4)
60	5	-3.66(9-II-4)	1.24(9-II-2)	1.33(10-I-3)	163(9-II-4)	336(9-II-3)	-11(10-I-3)
60	6	-3.74(9-II-4)	1.71(9-II-2)	1.50(10-I-3)	213(9-II-4)	262(9-I-4)	26(10-I-3)
60	7	-3.40(9-II-3)	2.21(9-II-2)	1.56(10-I-3)	208(9-II-1)	187(9-I-4)	-20(10-II-3)
60	8	-2.75(9-I-4)	2.75(9-II-2)	1.58(10-I-3)	184(9-I-3)	118(9-I-4)	-40(10-II-3)
60	9	-3.87(9-II-4)	1.09(9-II-2)	1.08(10-I-3)	61(10-II-3)	300(9-II-2)	43(10-II-3)
60	10	-3.83(9-II-4)	1.56(9-II-2)	1.26(10-I-3)	76(10-II-3)	208(9-I-4)	35(10-I-3)
60	11	-3.44(9-II-2)	2.18(9-II-2)	1.27(10-I-3)	64(10-II-3)	143(9-I-4)	-25(10-II-2)
60	12	-2.78(9-I-4)	2.80(9-II-2)	1.27(10-I-3)	57(6)	88(9-I-4)	-51(10-II-2)
60	13	-4.12(9-II-3)	0.39(10-II-3)	0.85(10-I-3)	-226(9-II-4)	209(9-II-2)	39(10-II-3)
60	14	-3.83(9-II-4)	1.16(9-II-4)	0.83(10-I-3)	-274(9-II-3)	131(9-I-4)	9(10-II-3)
60	15	-3.44(9-II-2)	1.94(9-II-2)	0.87(10-I-3)	-281(9-II-3)	81(9-I-4)	-35(10-I-3)
60	16	-2.81(9-II-3)	2.76(9-II-2)	0.87(10-I-3)	-226(9-II-3)	46(10-II-3)	-49(10-I-3)
61	1	-2.56(10-II-3)	1.31(9-II-3)	2.09(9-II-3)	-180(10-II-3)	405(9-II-3)	-206(9-II-3)
61	2	-3.57(9-II-4)	1.47(9-II-3)	2.28(9-II-3)	-253(10-II-3)	200(9-I-1)	-107(9-II-4)
61	3	-3.41(9-II-4)	1.63(9-II-4)	2.42(9-II-3)	-300(10-II-3)	103(10-I-3)	-123(9-II-3)
61	4	-2.79(10-II-3)	1.87(10-II-3)	2.48(9-II-3)	-293(10-II-2)	32(10-I-2)	-119(9-II-3)
61	5	-3.01(10-II-3)	1.42(9-II-3)	2.13(9-II-3)	97(9-II-3)	364(9-II-3)	-162(9-II-3)
61	6	-3.43(9-II-4)	1.69(9-II-3)	2.31(9-II-3)	74(9-II-2)	231(9-I-4)	-35(6)
61	7	-3.34(9-II-4)	1.92(9-II-4)	2.30(9-II-3)	29(10-I-3)	147(9-I-4)	9(9-II-3)
61	8	-2.82(9-I-4)	2.24(9-II-4)	2.28(9-II-3)	-15(10-II-2)	75(10-I-2)	31(9-II-3)
61	9	-3.32(9-II-4)	1.38(9-II-3)	1.97(9-II-3)	167(9-II-4)	369(9-II-3)	-135(9-II-3)
61	10	-3.55(9-II-4)	1.75(9-II-3)	2.16(9-II-3)	195(9-II-4)	273(9-I-1)	-38(10-II-3)
61	11	-3.36(9-II-3)	2.11(9-II-2)	2.17(9-II-3)	174(9-II-2)	183(9-I-4)	-16(6)
61	12	-2.81(9-I-4)	2.43(9-II-4)	2.13(9-II-3)	136(10-I-2)	106(9-I-4)	17(9-II-2)
61	13	-3.69(9-II-4)	1.19(9-II-2)	1.76(10-I-3)	137(9-II-4)	340(9-II-3)	-100(10-I-3)
61	14	-3.64(9-II-4)	1.59(9-II-2)	1.93(10-I-3)	180(9-II-4)	279(9-II-3)	-31(10-II-3)
61	15	-3.36(9-II-3)	2.08(9-II-2)	1.99(10-I-3)	181(9-II-1)	196(9-I-4)	-31(10-I-4)
61	16	-2.82(9-I-4)	2.57(9-II-2)	1.99(10-I-3)	159(10-I-2)	121(9-I-4)	-22(10-I-3)
62	1	-2.17(10-II-3)	0.91(9-I-4)	2.93(9-II-3)	85(10-II-3)	312(10-II-3)	-95(9-II-4)
62	2	-3.15(10-II-3)	1.26(10-II-3)	3.30(9-II-3)	140(10-II-3)	301(9-I-4)	21(9-II-3)
62	3	-3.22(10-II-3)	1.47(10-II-3)	3.48(9-II-3)	143(9-II-2)	212(9-I-1)	-24(9-II-4)
62	4	-2.83(9-I-3)	1.61(10-II-3)	3.55(9-II-3)	129(9-II-2)	115(9-II-3)	-37(9-II-4)
62	5	-2.73(10-II-3)	0.95(10-II-3)	2.86(9-II-3)	86(10-II-3)	281(10-II-3)	-47(9-II-4)
62	6	-3.29(10-II-3)	1.21(10-II-3)	3.28(9-II-3)	128(10-II-3)	266(9-I-4)	61(9-II-3)
62	7	-3.25(10-II-3)	1.48(10-II-3)	3.41(9-II-3)	127(10-II-4)	190(9-I-4)	13(9-II-3)
62	8	-2.89(9-I-3)	1.84(10-II-3)	3.42(9-II-3)	114(10-I-2)	105(9-II-3)	-14(10-II-3)
62	9	-3.27(9-II-4)	0.58(10-II-3)	2.70(9-II-3)	-27(9-II-3)	250(10-II-3)	-26(9-II-4)
62	10	-3.50(9-II-4)	0.89(10-II-3)	3.14(9-II-3)	-19(9-II-3)	218(9-I-4)	65(9-II-3)
62	11	-3.32(9-II-4)	1.42(10-II-3)	3.17(9-II-3)	-26(9-II-3)	147(9-I-4)	12(10-I-3)
62	12	-2.91(9-I-3)	1.90(10-II-3)	3.18(9-II-3)	-29(10-II-2)	76(10-I-2)	-23(10-II-3)
62	13	-4.19(9-II-4)	-0.78(10-I-3)	2.47(9-II-3)	-202(9-II-4)	121(10-II-3)	-105(9-II-3)
62	14	-3.45(9-II-4)	0.26(10-II-3)	2.60(9-II-3)	-293(9-II-4)	130(9-I-4)	-69(9-II-4)
62	15	-3.29(10-II-3)	1.10(10-II-3)	2.77(9-II-3)	-320(10-II-2)	80(9-I-4)	-128(9-II-4)
62	16	-3.00(9-II-3)	1.94(10-II-3)	2.83(9-II-3)	-299(10-II-2)	31(10-I-2)	-152(9-II-3)
63	1	-1.00(10-II-3)	1.31(9-II-3)	2.81(9-II-3)	-82(10-II-3)	431(9-II-4)	-216(9-II-3)
63	2	-2.90(10-II-3)	1.12(10-II-3)	2.99(9-II-3)	-186(10-II-3)	268(9-II-3)	-103(9-II-3)
63	3	-3.15(10-II-3)	0.96(10-II-3)	3.14(9-II-3)	-266(10-II-3)	146(9-II-3)	-122(9-II-3)
63	4	-2.85(9-I-3)	0.87(10-II-3)	3.21(9-II-3)	-307(10-I-2)	39(9-II-3)	-121(9-II-3)
63	5	-1.71(10-II-3)	1.35(10-II-3)	3.09(9-II-3)	114(9-II-3)	334(9-II-4)	-168(9-II-3)
63	6	-2.75(10-II-3)	1.38(10-II-3)	3.34(9-II-3)	97(9-II-3)	279(9-II-3)	-15(6)
63	7	-3.10(10-II-3)	1.31(10-II-3)	3.34(9-II-3)	52(9-II-3)	183(9-II-3)	20(10-II-2)
63	8	-2.90(9-I-3)	1.28(10-II-3)	3.33(9-II-3)	-8(6)	84(9-II-3)	40(10-II-3)
63	9	-2.13(10-II-3)	1.31(9-I-2)	3.12(9-II-3)	138(10-II-3)	323(10-II-3)	-140(9-II-4)
63	10	-2.91(10-II-3)	1.44(10-II-3)	3.43(9-II-3)	178(10-II-3)	308(9-II-3)	-8(6)
63	11	-3.13(10-II-3)	1.51(10-II-3)	3.51(9-II-3)	175(9-II-3)	213(9-II-3)	6(10-II-2)
63	12	-2.92(9-I-3)	1.50(10-II-3)	3.50(9-II-3)	144(9-II-3)	112(9-II-3)	21(10-II-2)
63	13	-2.65(10-II-3)	1.11(9-I-4)	3.02(9-II-3)	106(10-II-3)	277(10-II-3)	-113(9-II-4)
63	14	-3.06(10-II-3)	1.20(10-II-3)	3.37(9-II-3)	143(10-II-3)	292(9-I-4)	4(9-II-3)
63	15	-3.15(10-II-3)	1.42(10-II-3)	3.54(9-II-3)	157(9-II-3)	211(9-I-1)	-27(10-I-2)
63	16	-2.96(9-I-3)	1.68(10-II-3)	3.59(9-II-3)	143(9-II-3)	120(9-II-3)	-28(9-II-4)
64	1	-2.90(10-I-3)	0.49(9-I-3)	3.16(9-II-4)	124(9-II-1)	20(10-II-3)	29(10-I-3)
64	2	-3.05(10-I-3)	0.47(9-I-3)	2.97(9-II-4)	118(10-I-3)	-18(6)	26(10-I-3)
64	3	-3.41(10-I-3)	0.59(9-I-3)	2.63(9-II-4)	113(10-I-3)	203(10-I-3)	-8(10-II-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
64	4	-2.88(10-I-3)	0.66(9-II-3)	2.23(9-II-4)	183(10-I-3)	708(10-I-3)	-171(10-II-2)
64	5	-2.89(10-I-3)	0.83(10-II-3)	3.29(9-II-4)	123(9-II-2)	21(10-II-3)	50(9-II-4)
64	6	-2.90(10-I-3)	0.96(10-II-3)	3.00(9-II-4)	123(9-II-4)	-23(6)	40(9-II-4)
64	7	-3.08(10-I-3)	1.24(10-II-3)	2.63(9-II-4)	141(10-I-3)	167(10-I-3)	-22(10-II-3)
64	8	-2.42(10-I-3)	1.37(10-II-4)	2.22(9-II-4)	178(10-I-3)	682(10-I-3)	-186(9-II-4)
64	9	-2.78(10-I-3)	1.10(10-II-3)	3.29(9-II-4)	-27(6)	-15(6)	48(9-II-4)
64	10	-2.65(10-I-3)	1.43(10-II-3)	2.89(9-II-4)	-19(6)	-48(6)	44(9-II-4)
64	11	-2.79(10-I-3)	1.90(10-II-3)	2.44(10-II-3)	53(9-II-4)	90(10-I-3)	-16(10-II-3)
64	12	-2.28(10-I-3)	2.29(10-II-3)	2.35(9-II-4)	101(10-I-3)	659(10-I-3)	-217(9-II-4)
64	13	-2.71(10-I-3)	1.43(10-II-3)	3.14(9-II-4)	-319(10-I-3)	-42(6)	-108(9-II-3)
64	14	-2.47(10-I-3)	2.05(10-II-3)	2.72(9-II-3)	-305(10-I-3)	-62(6)	-88(10-II-3)
64	15	-2.61(10-I-3)	2.56(10-II-3)	2.13(9-II-3)	-254(10-I-3)	61(10-I-3)	-50(10-II-3)
64	16	-2.12(10-I-3)	2.84(10-II-3)	2.17(9-II-4)	-137(10-I-1)	635(10-I-3)	-227(9-II-4)
65	1	-2.83(9-II-4)	-0.99(9-II-3)	2.15(10-II-3)	-325(9-II-4)	-56(10-I-3)	-71(10-II-3)
65	2	-2.73(10-I-3)	-1.93(9-II-3)	2.11(10-II-3)	-298(9-II-4)	-35(6)	-70(10-II-3)
65	3	-3.30(9-II-4)	-3.35(9-II-4)	2.11(10-II-3)	-217(9-II-3)	246(9-II-4)	-42(10-II-3)
65	4	-4.65(9-II-4)	-4.58(9-II-4)	2.36(10-II-3)	39(9-II-1)	1087(10-I-3)	-192(10-II-3)
65	5	-3.00(9-II-4)	-0.61(9-II-3)	2.51(10-II-3)	-44(9-II-4)	-16(10-I-3)	51(10-II-3)
65	6	-3.09(10-I-3)	-1.29(9-II-3)	2.57(10-II-3)	-31(10-II-4)	14(9-II-3)	43(10-II-3)
65	7	-3.48(10-I-3)	-1.90(9-II-3)	2.76(10-II-3)	31(10-I-3)	305(9-II-4)	31(9-II-2)
65	8	-3.11(9-II-4)	-1.84(9-II-3)	2.21(10-II-3)	152(10-I-3)	1026(10-I-3)	-155(10-II-3)
65	9	-3.02(10-I-3)	-0.27(9-II-3)	2.82(10-II-3)	109(9-I-3)	24(10-II-3)	52(10-II-3)
65	10	-3.08(10-I-3)	-0.71(9-II-3)	2.83(10-II-3)	113(10-I-3)	28(9-II-3)	48(9-II-4)
65	11	-3.39(10-I-3)	-0.71(9-II-3)	2.75(10-II-3)	151(10-I-3)	299(9-II-4)	33(9-II-2)
65	12	-2.48(9-II-4)	-0.37(9-II-3)	2.31(10-II-3)	142(10-I-3)	922(10-I-3)	-170(10-II-3)
65	13	-3.07(10-I-3)	0.45(9-I-3)	3.01(10-II-3)	120(10-I-4)	32(10-II-3)	25(10-I-3)
65	14	-3.04(10-I-3)	0.29(9-I-3)	2.91(10-II-3)	118(10-I-3)	33(9-II-3)	29(10-I-3)
65	15	-3.12(10-I-3)	0.33(9-I-3)	2.62(10-II-3)	133(10-I-3)	281(9-II-4)	21(9-II-2)
65	16	-2.00(10-I-3)	0.55(9-I-3)	2.31(9-II-4)	137(10-I-3)	830(10-I-3)	-189(10-II-3)
66	1	-3.57(9-II-4)	-0.53(9-II-3)	1.28(10-II-3)	201(10-II-2)	122(10-II-3)	-46(9-II-4)
66	2	-3.14(9-II-4)	-0.76(9-II-3)	1.10(10-II-3)	271(9-II-4)	122(9-II-4)	-77(9-II-4)
66	3	-2.51(9-II-4)	-1.04(9-II-3)	1.26(10-II-3)	320(9-II-4)	466(9-II-4)	-63(6)
66	4	-0.94(9-II-3)	-1.45(9-II-3)	1.65(10-II-3)	330(9-II-4)	1219(9-II-4)	-63(10-II-3)
66	5	-3.38(9-II-4)	-0.51(9-II-3)	1.47(10-II-3)	171(10-II-2)	96(10-II-3)	-7(9-I-3)
66	6	-3.13(9-II-4)	-0.86(9-II-3)	1.23(10-II-3)	235(9-II-4)	110(10-II-2)	-43(10-I-2)
66	7	-2.77(9-II-4)	-0.96(9-II-3)	1.41(10-II-3)	306(9-II-4)	460(9-II-4)	-79(6)
66	8	-0.88(9-II-3)	-1.14(9-II-3)	1.87(10-II-3)	313(9-II-4)	1291(9-II-4)	-114(10-II-3)
66	9	-3.18(9-II-4)	-0.58(9-II-3)	1.70(10-II-3)	12(10-II-2)	53(10-II-3)	16(9-II-3)
66	10	-3.01(9-II-4)	-1.07(9-II-3)	1.38(10-II-3)	71(10-II-2)	78(10-II-2)	-21(9-I-3)
66	11	-2.92(10-I-3)	-1.31(9-II-3)	1.40(10-II-3)	176(9-II-4)	403(9-II-4)	-73(6)
66	12	-1.10(10-I-3)	-1.29(9-II-3)	2.09(10-II-3)	249(9-II-4)	1368(9-II-4)	-170(10-II-3)
66	13	-3.04(9-II-4)	-0.57(9-II-3)	1.90(10-II-3)	-314(9-II-4)	-21(10-I-3)	-88(10-II-3)
66	14	-2.98(9-II-4)	-1.17(9-II-3)	1.63(10-II-3)	-266(9-II-4)	46(10-II-3)	-94(10-II-3)
66	15	-3.09(10-I-3)	-2.12(9-II-4)	1.42(10-II-3)	-143(10-I-3)	363(9-II-4)	-80(10-II-3)
66	16	-1.46(10-I-3)	-2.72(9-II-4)	2.11(10-II-3)	10(10-I-3)	1421(9-II-4)	-210(10-II-3)
67	1	-4.04(9-II-4)	-1.74(6)	1.90(10-II-3)	49(9-II-4)	63(9-II-4)	-235(9-II-4)
67	2	-3.43(9-II-4)	-0.34(10-II-3)	2.14(10-II-3)	-105(9-I-1)	70(9-II-4)	-108(9-II-4)
67	3	-2.52(9-II-4)	1.08(10-I-3)	1.84(10-II-3)	-310(10-I-4)	183(9-II-4)	-157(9-II-4)
67	4	0.68(9-II-4)	2.59(9-II-4)	0.77(10-II-3)	-41(10-I-3)	917(9-II-4)	-48(10-II-3)
67	5	-3.82(9-II-4)	-1.27(10-II-3)	1.22(10-II-3)	247(9-II-4)	194(9-II-4)	-116(9-II-4)
67	6	-3.28(9-II-4)	-0.36(10-II-3)	1.47(10-II-3)	187(9-II-4)	106(9-II-4)	-106(9-II-4)
67	7	-2.35(9-II-4)	0.86(10-I-3)	1.16(10-II-3)	206(9-II-4)	252(9-II-4)	-60(10-I-3)
67	8	0.36(10-II-3)	1.14(10-I-3)	0.78(10-II-3)	331(9-II-4)	1079(9-II-4)	133(9-II-4)
67	9	-3.76(9-II-4)	-0.71(10-II-2)	1.11(10-II-3)	310(9-II-4)	188(9-II-4)	-103(9-II-4)
67	10	-3.23(9-II-4)	-0.40(10-II-2)	1.06(10-II-3)	329(9-II-4)	126(9-II-4)	-116(9-II-4)
67	11	-2.28(9-II-4)	0.20(10-I-3)	0.94(10-II-3)	374(9-II-4)	362(9-II-4)	-30(10-I-3)
67	12	0.21(10-II-3)	-0.18(10-II-3)	1.07(10-II-3)	359(9-II-4)	1120(9-II-4)	109(10-I-4)
67	13	-3.62(9-II-4)	-0.51(10-II-2)	1.17(10-II-3)	245(10-II-3)	158(10-II-3)	-82(9-II-4)
67	14	-3.18(9-II-4)	-0.54(9-II-3)	1.00(10-II-3)	307(9-II-4)	132(10-II-3)	-106(9-II-4)
67	15	-2.41(10-I-3)	-0.69(9-II-3)	0.97(10-II-3)	358(9-II-4)	436(9-II-4)	-45(6)
67	16	-0.29(10-I-3)	-1.23(9-II-3)	1.47(10-II-3)	315(9-II-4)	1165(9-II-4)	29(10-I-3)
68	1	-3.44(9-II-4)	0.24(9-II-4)	-0.83(10-I-3)	-108(9-II-4)	-84(9-II-4)	-149(9-II-3)
68	2	-3.53(9-II-4)	0.57(9-II-4)	-0.62(10-I-3)	-106(9-II-4)	89(9-I-4)	-132(10-I-3)
68	3	-3.46(9-II-4)	1.40(9-II-4)	0.10(10-II-3)	-110(9-II-4)	106(9-II-3)	-101(10-I-3)
68	4	-2.24(10-I-3)	3.13(9-II-4)	0.41(9-II-4)	-47(10-II-1)	68(9-II-4)	26(9-II-4)
68	5	-3.21(9-II-4)	0.12(9-II-2)	-0.88(10-I-3)	10(10-I-3)	-138(9-II-4)	-143(9-II-4)
68	6	-3.64(9-II-4)	0.51(9-II-4)	-0.90(10-I-3)	102(10-I-4)	124(10-I-4)	-119(10-I-3)
68	7	-3.81(9-II-3)	1.33(9-II-4)	-0.67(10-I-3)	140(10-I-4)	170(9-II-3)	-84(9-I-4)
68	8	-2.79(10-I-3)	2.06(9-II-4)	0.18(10-II-3)	132(10-I-4)	181(9-II-4)	59(9-II-4)
68	9	-2.90(10-I-3)	-0.38(6)	-0.96(10-I-3)	101(9-II-3)	-177(9-II-4)	-102(9-II-4)
68	10	-3.75(9-II-4)	0.26(9-II-2)	-1.11(10-I-3)	274(9-II-3)	155(9-II-3)	-65(10-I-3)
68	11	-4.06(9-II-3)	0.71(9-II-4)	-1.00(10-I-3)	360(9-II-3)	220(9-II-3)	-79(9-I-4)
68	12	-4.07(10-I-3)	1.01(9-II-4)	0.40(10-II-3)	315(10-I-4)	302(9-II-4)	26(9-II-4)
68	13	-2.40(10-I-3)	-0.98(6)	-1.11(10-I-3)	295(9-II-4)	-31(9-II-4)	51(9-II-3)

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68	14	-3.67(9-II-4)	-0.35(6)	-1.24(10-I-3)	431(9-II-4)	151(9-II-3)	173(9-II-4)
68	15	-4.53(9-II-3)	0.27(9-II-2)	-0.92(10-I-3)	602(9-II-3)	215(9-II-3)	122(9-II-4)
68	16	-6.85(10-I-3)	0.60(9-II-4)	0.61(10-II-3)	626(10-I-4)	434(9-II-3)	73(9-II-4)
69	1	-4.33(9-II-4)	-0.88(9-I-4)	-1.72(9-II-3)	-389(9-II-4)	62(9-I-4)	-31(10-I-4)
69	2	-1.76(6)	-1.16(10-I-3)	-0.52(9-II-3)	-483(9-II-4)	37(10-I-2)	47(9-II-4)
69	3	-0.86(10-II-1)	-1.79(10-I-3)	0.50(6)	-582(9-II-4)	60(9-II-2)	-7(10-I-1)
69	4	-0.85(10-II-1)	-3.27(10-I-3)	1.88(10-I-4)	-1037(10-I-3)	-24(9-I-2)	54(10-II-1)
69	5	-3.44(9-II-4)	-0.26(9-I-4)	-1.08(10-I-3)	-210(9-II-4)	107(9-I-4)	-62(10-II-2)
69	6	-2.05(6)	-0.90(9-I-4)	-0.58(10-I-3)	-311(9-II-4)	44(9-I-4)	6(9-II-2)
69	7	-1.72(9-II-4)	-1.00(9-I-4)	0.82(9-II-4)	-458(9-II-4)	24(9-II-2)	-8(10-I-3)
69	8	-3.46(10-I-3)	-0.55(10-I-3)	1.24(10-I-4)	-680(9-II-4)	-20(9-I-2)	-21(10-I-3)
69	9	-3.26(9-II-4)	0.16(9-II-4)	-0.86(10-I-3)	-130(9-II-4)	95(9-I-4)	-82(10-I-4)
69	10	-2.85(9-II-4)	-0.30(9-I-4)	-0.46(10-I-3)	-226(9-II-4)	57(9-I-4)	-58(10-I-4)
69	11	-2.63(9-II-4)	0.18(9-II-4)	0.91(9-II-4)	-336(9-II-4)	34(9-II-3)	-67(10-I-3)
69	12	-2.37(9-II-2)	0.14(9-II-4)	1.11(9-II-4)	-411(9-II-4)	-13(9-I-4)	-82(10-I-3)
69	13	-3.06(9-II-4)	0.16(9-II-4)	-0.79(10-I-3)	-116(9-II-4)	43(9-I-4)	-116(9-II-3)
69	14	-3.27(9-II-4)	0.29(9-II-4)	-0.43(10-I-3)	-209(9-II-4)	64(9-I-4)	-108(10-I-4)
69	15	-3.31(9-II-4)	1.00(9-II-4)	0.52(10-II-3)	-256(9-II-4)	45(9-II-3)	-97(10-I-3)
69	16	-2.63(10-I-3)	2.47(9-II-4)	1.72(9-II-4)	-207(9-II-4)	-21(9-I-4)	-93(10-I-3)
70	1	-2.00(9-I-4)	0.98(9-I-1)	-3.26(9-II-4)	-124(9-II-4)	-185(9-II-4)	40(10-II-1)
70	2	-0.39(10-II-1)	0.56(9-I-1)	-2.43(9-II-3)	43(9-I-4)	-58(10-I-4)	113(10-I-3)
70	3	0.86(9-II-3)	0.20(9-I-4)	-1.54(9-II-3)	97(9-I-1)	-182(10-I-4)	183(10-I-3)
70	4	0.79(9-II-3)	-0.09(9-II-4)	0.25(6)	118(9-II-3)	-247(10-I-4)	196(10-I-3)
70	5	-1.96(10-II-2)	-0.21(6)	-3.07(9-II-4)	-180(9-II-4)	-118(9-II-4)	83(9-II-4)
70	6	-0.71(10-II-1)	-0.70(6)	-2.26(9-II-3)	-113(9-II-4)	-41(10-I-4)	144(10-I-3)
70	7	-0.25(10-II-1)	-1.25(10-I-1)	-1.37(9-II-3)	-102(9-II-4)	-173(10-I-4)	216(10-I-3)
70	8	-0.75(6)	-1.49(9-II-4)	0.36(6)	-62(10-II-2)	-305(10-I-4)	226(10-I-3)
70	9	-2.25(10-II-2)	-0.81(10-I-3)	-2.62(9-II-3)	-190(9-II-4)	-31(9-II-4)	77(9-II-4)
70	10	-1.17(10-II-1)	-1.52(10-I-3)	-1.83(9-II-3)	-281(9-II-4)	-46(10-II-2)	126(9-II-4)
70	11	-0.74(10-II-1)	-2.69(10-I-3)	-0.97(9-II-3)	-359(9-II-4)	-142(10-I-4)	214(10-I-3)
70	12	-1.93(10-I-3)	-3.17(9-II-3)	0.41(6)	-303(9-II-4)	-373(10-I-3)	276(10-I-3)
70	13	-1.89(10-II-2)	-1.25(10-I-3)	-2.24(9-II-3)	-271(9-II-4)	110(9-I-4)	-10(10-I-4)
70	14	-1.53(10-II-2)	-2.25(10-I-3)	-1.03(9-II-3)	-494(9-II-4)	-77(10-II-2)	69(9-II-4)
70	15	-1.57(10-II-2)	-3.45(10-I-3)	-0.07(9-II-3)	-639(9-II-4)	-166(10-I-3)	79(10-I-3)
70	16	-4.01(10-I-3)	-5.17(10-I-3)	0.59(10-I-1)	-695(9-II-4)	-457(10-I-3)	236(10-I-3)
71	1	1.15(9-II-4)	4.22(10-I-3)	-2.76(9-II-3)	-50(9-I-4)	22(9-II-4)	67(10-I-4)
71	2	1.17(9-II-4)	4.75(10-I-3)	-1.76(9-II-3)	77(9-II-4)	-148(10-I-3)	11(9-I-2)
71	3	2.30(9-II-3)	6.37(10-I-3)	-0.78(9-II-3)	142(10-II-1)	-391(10-I-3)	-50(9-II-3)
71	4	6.14(9-II-3)	9.97(9-II-3)	-2.50(9-II-2)	211(10-II-1)	-832(10-I-4)	295(10-I-3)
71	5	0.42(9-II-4)	3.02(10-I-3)	-3.09(9-II-3)	162(9-II-4)	-37(10-I-3)	42(9-I-2)
71	6	1.09(9-II-4)	3.86(10-I-3)	-2.24(9-II-3)	180(9-II-1)	-152(10-I-3)	17(9-I-2)
71	7	1.86(9-II-3)	5.09(9-II-3)	-2.18(9-II-3)	245(10-II-1)	-391(10-I-4)	51(6)
71	8	4.11(9-II-3)	4.28(9-II-3)	-0.98(9-II-2)	319(10-II-1)	-426(10-I-4)	263(10-I-3)
71	9	-0.41(9-I-4)	2.28(10-I-3)	-3.31(9-II-3)	183(9-II-1)	-62(9-II-4)	42(10-II-1)
71	10	0.63(9-II-4)	2.79(10-I-3)	-2.67(9-II-3)	193(9-II-1)	-139(10-I-4)	34(9-I-2)
71	11	1.59(9-II-3)	2.88(9-II-3)	-2.04(9-II-3)	257(9-II-4)	-318(10-I-4)	113(10-I-3)
71	12	2.59(9-II-3)	2.22(10-I-3)	-0.38(9-II-2)	293(9-II-4)	-321(10-I-4)	256(10-I-3)
71	13	0.34(9-II-4)	1.41(9-I-1)	-3.44(9-II-3)	108(9-I-4)	-136(9-II-4)	36(10-II-1)
71	14	0.40(9-II-4)	1.43(10-I-3)	-2.57(9-II-3)	120(9-I-1)	-113(10-I-4)	63(10-I-3)
71	15	0.82(9-II-3)	1.39(10-I-3)	-1.74(9-II-3)	203(9-II-4)	-263(10-I-4)	147(10-I-3)
71	16	1.11(9-II-3)	1.02(10-I-3)	0.09(6)	217(9-II-4)	-294(10-I-4)	215(10-I-3)
72	1	-2.00(10-II-3)	1.73(9-I-2)	-2.03(9-II-4)	165(9-II-3)	32(9-II-2)	-54(9-II-2)
72	2	-0.55(6)	1.05(9-I-2)	-1.34(9-II-4)	100(10-I-4)	-125(10-I-2)	-113(9-II-2)
72	3	1.03(9-II-3)	-1.07(9-II-2)	-0.81(10-II-3)	-69(9-II-1)	-380(10-I-3)	-159(9-II-3)
72	4	-2.14(6)	-3.96(9-II-2)	0.93(9-II-2)	-402(9-II-2)	-680(10-I-3)	144(9-II-2)
72	5	-2.36(10-II-3)	1.91(10-I-3)	-1.84(9-II-4)	185(9-II-3)	-14(10-I-3)	-91(9-II-4)
72	6	-0.93(6)	1.31(9-I-2)	-0.71(9-II-4)	139(9-II-3)	-154(10-I-3)	-143(9-II-4)
72	7	0.35(9-II-3)	-0.38(9-II-2)	0.40(10-I-3)	84(10-I-4)	-404(10-I-3)	-207(9-II-3)
72	8	-3.74(6)	-0.38(9-II-4)	0.16(10-I-3)	43(6)	-258(10-I-3)	-173(10-II-2)
72	9	-3.07(10-II-3)	2.33(10-I-3)	-1.75(9-II-4)	96(9-II-2)	-58(10-I-3)	-96(9-II-4)
72	10	-1.57(6)	2.12(10-I-3)	-0.30(9-II-4)	121(9-II-2)	-180(10-I-3)	-144(9-II-4)
72	11	-0.81(6)	1.93(10-I-3)	1.13(10-I-3)	187(9-II-2)	-422(10-I-3)	-176(9-II-3)
72	12	-2.88(6)	0.28(10-I-3)	0.25(10-I-3)	330(9-II-4)	-268(10-I-3)	-274(9-II-3)
72	13	-4.19(9-II-4)	2.69(10-I-3)	-1.87(9-II-4)	-128(6)	-146(10-I-3)	-27(6)
72	14	-2.00(6)	2.97(10-I-3)	-0.31(9-II-4)	59(9-II-2)	-225(10-I-3)	-85(9-II-4)
72	15	-1.16(6)	4.25(10-I-3)	0.67(10-I-3)	212(9-II-2)	-470(10-I-3)	-134(9-II-3)
72	16	-3.09(6)	6.95(9-II-3)	2.18(10-I-3)	625(9-II-4)	-818(10-I-4)	-493(10-I-4)
73	1	-1.97(10-II-3)	2.42(10-I-3)	-1.95(9-II-4)	-230(6)	16(9-II-3)	96(9-II-4)
73	2	-0.67(6)	3.75(9-II-4)	-2.05(9-II-4)	-182(6)	-137(10-I-2)	94(9-II-4)
73	3	0.83(9-II-2)	6.00(9-II-4)	-2.07(9-II-4)	-182(6)	-565(9-II-4)	97(9-II-2)
73	4	-0.87(6)	8.10(9-II-3)	-1.38(9-II-3)	-207(9-II-4)	-1400(9-II-2)	144(9-II-2)
73	5	-1.78(10-II-4)	2.10(10-I-3)	-2.31(9-II-4)	-41(6)	35(9-II-3)	11(9-I-3)
73	6	-0.49(6)	2.57(10-I-3)	-2.59(9-II-4)	-96(6)	-134(10-I-2)	11(9-II-1)
73	7	0.78(9-II-3)	3.06(10-I-3)	-2.94(9-II-4)	-174(9-II-1)	-567(9-II-4)	75(9-II-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
73	8	-2.14(6)	4.04(10-I-3)	-1.61(9-II-3)	-287(9-II-4)	-1383(9-II-2)	191(9-II-2)
73	9	-1.76(10-II-3)	1.81(9-I-2)	-2.38(9-II-4)	80(10-I-4)	45(9-II-3)	-22(9-II-2)
73	10	-0.50(6)	1.67(9-I-2)	-2.49(9-II-4)	-36(9-II-1)	-130(10-I-2)	-36(9-II-3)
73	11	0.60(9-II-3)	0.97(9-I-2)	-2.73(9-II-4)	-201(9-II-4)	-488(10-I-3)	53(9-II-2)
73	12	-3.08(6)	0.96(9-I-2)	-2.56(9-II-3)	-392(9-II-4)	-1347(9-II-2)	196(9-II-2)
73	13	-1.74(10-II-4)	1.56(9-I-2)	-2.24(9-II-4)	123(10-I-4)	33(9-II-3)	-37(9-II-2)
73	14	-0.46(6)	1.07(9-I-2)	-2.00(9-II-4)	36(10-I-4)	-136(10-I-2)	-74(9-II-3)
73	15	0.29(9-II-3)	-0.60(9-II-2)	-1.68(9-II-4)	-180(9-II-4)	-431(10-I-3)	-58(10-I-4)
73	16	-3.71(6)	-3.66(9-II-2)	-2.46(9-II-3)	-502(9-II-4)	-1244(9-II-2)	194(9-II-2)
74	1	-1.58(6)	2.64(9-II-4)	-1.01(10-II-3)	99(10-II-3)	38(10-II-3)	7(9-II-1)
74	2	-0.23(6)	2.89(9-II-4)	-0.86(10-II-3)	27(6)	-209(9-II-4)	8(9-II-2)
74	3	0.97(9-II-2)	2.82(9-II-4)	-0.68(9-II-4)	-78(9-II-2)	-758(9-II-2)	-24(6)
74	4	-1.65(10-II-1)	2.25(9-II-4)	0.48(10-I-3)	-180(9-II-2)	-1628(9-II-2)	-27(10-I-2)
74	5	-1.63(6)	2.53(9-II-4)	-1.12(9-II-4)	64(10-II-2)	32(10-II-2)	-37(9-II-3)
74	6	-0.24(6)	2.74(10-I-3)	-0.81(9-II-4)	-50(9-II-2)	-211(9-II-4)	-29(10-II-3)
74	7	1.12(9-II-2)	2.60(10-I-3)	-0.40(9-II-4)	-121(9-II-2)	-765(9-II-2)	-25(6)
74	8	-2.03(10-II-1)	2.86(9-II-4)	-0.38(9-II-2)	-191(9-II-2)	-1645(9-II-2)	33(9-II-3)
74	9	-1.72(6)	2.46(10-I-3)	-1.28(9-II-4)	-54(9-II-1)	18(9-II-3)	-61(9-II-3)
74	10	-0.44(6)	3.04(10-I-3)	-0.86(9-II-4)	-114(9-II-2)	-204(9-II-4)	-43(9-II-3)
74	11	0.81(9-II-3)	3.54(10-I-3)	-0.35(10-II-3)	-162(9-II-2)	-743(9-II-2)	16(9-II-2)
74	12	-1.83(10-II-1)	3.94(10-I-3)	-0.64(9-II-2)	-220(9-II-2)	-1668(9-II-2)	66(9-II-3)
74	13	-1.79(6)	2.33(10-I-3)	-1.53(9-II-4)	-232(6)	-20(6)	41(10-II-3)
74	14	-0.66(6)	3.42(10-I-3)	-1.24(9-II-4)	-190(6)	-209(9-II-4)	44(9-II-4)
74	15	0.48(9-II-3)	5.15(10-I-3)	-0.73(9-II-4)	-181(6)	-734(9-II-2)	81(9-II-4)
74	16	-1.78(10-II-1)	6.74(10-I-3)	-0.79(9-II-2)	-226(9-II-4)	-1706(9-II-2)	131(9-II-2)
75	1	-1.79(6)	3.45(9-II-2)	-0.32(10-II-3)	-145(9-I-4)	-18(10-I-3)	48(10-II-3)
75	2	-0.51(6)	4.74(9-II-2)	-0.53(10-II-3)	-49(6)	-165(9-II-3)	49(9-II-2)
75	3	1.31(9-II-2)	6.42(9-II-2)	-0.74(10-II-3)	15(9-II-4)	-586(9-II-3)	-12(10-I-3)
75	4	0.83(9-II-4)	7.82(9-II-2)	-0.43(10-II-3)	-113(9-II-3)	-1535(9-II-2)	-115(10-I-3)
75	5	-1.65(6)	3.24(9-II-2)	-0.67(10-II-3)	36(10-II-3)	24(10-II-3)	76(9-II-2)
75	6	-0.26(6)	3.90(9-II-2)	-0.94(10-II-3)	10(10-II-3)	-172(9-II-2)	65(9-II-2)
75	7	1.42(9-II-2)	4.37(9-II-2)	-1.17(10-II-3)	-76(9-II-2)	-649(9-II-2)	-25(9-II-1)
75	8	-0.33(9-I-4)	4.64(9-II-2)	-0.56(10-II-3)	-160(9-II-2)	-1593(9-II-2)	-106(10-I-3)
75	9	-1.55(6)	2.98(9-II-2)	-0.85(10-II-3)	120(10-II-3)	38(10-II-3)	53(9-II-2)
75	10	0.32(9-II-2)	3.27(9-II-2)	-0.99(10-II-3)	41(6)	-191(9-II-2)	42(9-II-2)
75	11	1.40(9-II-2)	3.11(9-II-2)	-1.07(10-II-3)	-90(9-II-2)	-715(9-II-2)	-28(10-I-2)
75	12	-0.83(10-II-1)	3.10(9-II-2)	-0.61(10-II-3)	-155(9-II-2)	-1609(9-II-2)	-81(10-I-2)
75	13	-1.53(9-I-4)	2.74(9-II-4)	-0.94(10-II-3)	118(10-II-3)	39(10-II-3)	28(9-II-4)
75	14	0.38(9-II-2)	2.94(9-II-4)	-0.93(10-II-3)	47(6)	-206(9-II-2)	22(9-II-2)
75	15	1.39(9-II-2)	2.86(9-II-4)	-0.78(10-II-3)	-84(9-II-2)	-751(9-II-2)	-22(6)
75	16	-1.41(10-II-2)	2.46(9-II-2)	-0.45(10-II-3)	-126(9-II-2)	-1634(9-II-2)	-41(10-I-2)
76	1	-1.81(9-I-4)	3.06(9-II-4)	1.76(10-I-3)	133(6)	38(6)	-25(10-I-4)
76	2	-0.74(6)	3.54(9-II-4)	1.57(10-I-3)	67(6)	-149(9-II-3)	-15(9-II-3)
76	3	0.58(9-II-2)	3.89(9-II-4)	1.12(10-I-3)	-53(9-II-3)	-537(9-II-3)	-28(9-II-3)
76	4	-0.87(9-I-2)	4.29(9-II-4)	0.56(10-I-3)	-125(9-II-3)	-1183(9-II-3)	-121(10-I-3)
76	5	-1.79(9-I-4)	3.34(9-II-2)	1.59(10-I-3)	140(6)	42(6)	-47(9-II-3)
76	6	-0.56(6)	3.88(9-II-2)	1.49(10-I-3)	72(6)	-141(9-II-3)	-43(9-II-3)
76	7	1.04(9-II-2)	4.08(9-II-4)	1.10(10-I-3)	-55(9-II-3)	-549(9-II-3)	-47(10-I-2)
76	8	-0.62(9-I-2)	4.23(9-II-4)	0.40(10-I-3)	-135(9-II-3)	-1263(9-II-3)	-125(10-I-3)
76	9	-1.78(9-I-4)	3.58(9-II-2)	1.29(10-I-3)	54(6)	29(6)	-66(9-II-3)
76	10	-0.47(6)	4.47(9-II-2)	1.28(10-I-3)	36(6)	-138(9-II-3)	-65(9-II-4)
76	11	1.33(9-II-2)	5.10(9-II-2)	1.10(10-I-3)	-39(9-II-3)	-550(9-II-3)	-56(10-I-2)
76	12	0.28(9-II-2)	5.21(9-II-2)	0.30(10-I-3)	-110(9-II-3)	-1331(9-II-2)	-115(10-I-3)
76	13	-1.83(9-I-4)	3.74(9-II-2)	0.82(10-I-3)	-136(9-I-4)	6(6)	-52(10-I-3)
76	14	-0.47(6)	5.17(9-II-2)	0.75(10-I-3)	-33(6)	-129(9-II-3)	-45(10-I-3)
76	15	1.51(9-II-2)	6.92(9-II-2)	0.66(10-I-3)	19(9-II-4)	-530(9-II-3)	-40(10-I-3)
76	16	1.14(9-II-2)	8.21(9-II-2)	0.35(10-I-3)	-53(9-II-3)	-1397(9-II-2)	-75(10-I-3)
77	1	-2.04(9-I-3)	2.42(10-II-3)	2.32(9-II-3)	-254(9-I-2)	-44(10-I-4)	-93(9-II-3)
77	2	-1.31(6)	3.10(10-II-3)	1.94(9-II-3)	-212(10-I-3)	-173(9-II-4)	-65(9-II-3)
77	3	-1.06(10-I-3)	3.88(10-II-3)	1.32(9-II-3)	-182(10-I-3)	-413(9-II-3)	-55(9-II-3)
77	4	-2.30(10-I-3)	4.54(10-II-3)	1.05(9-II-3)	-184(9-II-3)	-844(9-II-3)	-190(9-II-3)
77	5	-2.04(9-I-4)	2.62(9-II-4)	2.16(9-II-3)	-46(9-II-3)	-2(10-II-2)	50(9-II-3)
77	6	-1.16(6)	3.02(9-II-4)	1.81(9-II-3)	-89(9-II-3)	-137(9-II-3)	51(9-II-2)
77	7	-0.67(6)	3.28(10-II-3)	1.36(10-I-3)	-144(9-II-3)	-405(9-II-3)	-8(9-II-3)
77	8	-1.55(9-I-2)	3.54(10-II-3)	0.85(9-II-3)	-166(9-II-3)	-899(9-II-3)	-169(9-II-2)
77	9	-1.95(9-I-4)	2.80(9-II-4)	2.03(9-II-3)	85(6)	26(6)	33(9-II-2)
77	10	-0.93(6)	3.14(9-II-4)	1.78(10-I-3)	20(6)	-133(9-II-3)	36(9-II-2)
77	11	-0.35(6)	3.34(9-II-4)	1.37(10-I-3)	-88(9-II-3)	-454(9-II-3)	-11(9-II-3)
77	12	-1.10(9-I-2)	3.53(9-II-4)	0.80(9-II-3)	-137(9-II-3)	-967(9-II-3)	-152(9-II-2)
77	13	-1.92(9-I-4)	3.00(9-II-4)	1.91(10-I-3)	117(6)	40(6)	-9(10-I-3)
77	14	-0.74(6)	3.42(9-II-4)	1.69(10-I-3)	57(6)	-128(9-II-3)	6(10-II-3)
77	15	0.71(9-II-2)	3.81(9-II-4)	1.26(10-I-3)	-54(9-II-3)	-480(9-II-3)	-12(9-II-3)
77	16	-0.71(9-I-2)	4.33(9-II-4)	0.85(10-I-3)	-106(9-II-3)	-1049(9-II-3)	-127(9-II-2)
78	1	-2.26(10-I-3)	1.91(10-II-3)	3.50(9-II-3)	101(10-I-3)	19(9-II-2)	-31(9-II-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
78	2	-1.86(10-I-3)	2.24(10-II-3)	3.32(9-II-3)	56(10-I-3)	-98(10-II-3)	-14(10-II-3)
78	3	-2.04(10-I-3)	2.58(10-II-3)	2.83(9-II-3)	-29(10-II-3)	-213(10-II-3)	-6(9-II-3)
78	4	-3.02(10-I-3)	2.92(10-II-3)	2.50(9-II-3)	-158(9-II-4)	-332(10-II-3)	-70(9-II-3)
78	5	-2.31(10-I-3)	2.26(10-II-3)	3.42(9-II-3)	90(10-I-3)	24(9-II-2)	-20(10-II-3)
78	6	-1.71(10-I-3)	2.74(10-II-3)	3.27(9-II-3)	58(10-I-3)	-86(10-II-3)	-13(10-II-3)
78	7	-1.51(10-I-3)	3.17(10-II-3)	2.86(9-II-3)	-28(10-II-3)	-217(10-II-3)	-27(9-II-2)
78	8	-2.13(9-I-2)	4.03(10-II-3)	1.81(9-II-3)	-115(9-II-2)	-355(10-II-3)	-139(9-II-3)
78	9	-2.24(10-I-3)	2.53(10-II-3)	3.16(9-II-3)	-31(10-II-3)	11(9-II-2)	-31(10-II-3)
78	10	-1.48(6)	3.32(10-II-3)	3.00(9-II-3)	-34(10-II-3)	-87(10-II-3)	-25(10-II-3)
78	11	-1.07(6)	4.20(9-II-4)	2.57(9-II-3)	-46(10-II-3)	-245(10-II-3)	-43(9-II-2)
78	12	-1.34(9-I-2)	4.93(9-II-4)	1.37(9-II-3)	-86(10-II-3)	-381(10-II-3)	-176(9-II-3)
78	13	-2.30(10-I-3)	2.84(9-II-4)	2.71(9-II-3)	-246(9-I-2)	-14(10-II-2)	-142(9-II-3)
78	14	-1.35(6)	4.10(9-II-4)	2.43(9-II-3)	-176(9-I-2)	-76(10-II-3)	-112(9-II-3)
78	15	-0.60(6)	5.60(9-II-4)	1.91(9-II-3)	-139(9-I-2)	-227(10-II-3)	-71(9-II-3)
78	16	0.51(9-II-2)	6.74(9-II-3)	1.34(9-II-3)	-121(10-II-2)	-418(10-II-3)	-187(9-II-3)
79	1	-2.44(10-I-3)	0.94(10-II-3)	3.07(9-II-3)	-331(10-I-3)	-73(6)	-94(9-II-3)
79	2	-2.24(10-I-3)	0.88(10-II-3)	2.76(9-II-3)	-346(10-I-3)	-158(10-II-3)	-69(9-II-3)
79	3	-2.83(10-I-3)	0.67(10-II-3)	2.28(9-II-3)	-334(10-I-3)	-199(10-II-3)	-34(10-II-3)
79	4	-5.34(10-I-3)	-0.80(10-I-3)	2.43(9-II-4)	-136(9-II-4)	265(10-I-3)	-165(9-II-4)
79	5	-2.50(10-I-3)	1.24(10-II-3)	3.28(9-II-3)	-56(6)	-24(6)	56(10-II-3)
79	6	-2.26(10-I-3)	1.13(10-II-3)	3.06(9-II-3)	-97(9-II-1)	-107(10-II-3)	60(9-II-4)
79	7	-2.63(10-I-3)	0.86(10-II-3)	2.76(9-II-3)	-111(10-II-3)	-147(10-II-3)	54(10-I-2)
79	8	-4.08(10-I-3)	1.15(10-II-3)	1.99(9-II-3)	-38(10-II-3)	273(10-I-3)	-102(9-II-4)
79	9	-2.44(10-I-3)	1.49(10-II-3)	3.47(9-II-3)	94(10-I-3)	12(9-II-3)	36(10-II-3)
79	10	-2.07(10-I-3)	1.45(10-II-3)	3.29(9-II-3)	49(10-I-3)	-89(10-II-3)	49(9-II-4)
79	11	-2.29(10-I-3)	1.46(10-II-3)	2.85(9-II-3)	31(10-I-3)	-160(10-II-3)	58(10-I-2)
79	12	-3.20(10-I-3)	1.60(10-II-3)	1.81(10-II-2)	73(10-I-3)	219(10-I-3)	-87(9-II-3)
79	13	-2.46(10-I-3)	1.83(10-II-3)	3.53(9-II-3)	109(10-I-3)	26(9-II-3)	-15(9-II-4)
79	14	-1.91(10-I-3)	1.98(10-II-3)	3.33(9-II-3)	73(10-I-3)	-73(10-II-3)	9(10-I-3)
79	15	-1.82(10-I-3)	2.15(10-II-3)	2.86(9-II-3)	-25(10-II-3)	-160(10-II-3)	32(10-I-2)
79	16	-2.23(10-I-3)	2.21(10-II-3)	1.95(10-II-2)	63(10-I-3)	-185(10-II-3)	-60(9-II-3)
80	1	0.18(9-I-1)	-2.64(9-II-4)	0.48(10-I-4)	-48(10-I-4)	390(9-II-4)	242(9-II-4)
80	2	-0.34(9-II-4)	-3.96(9-II-3)	0.57(10-I-4)	103(9-II-1)	-63(10-I-4)	319(9-II-4)
80	3	-1.05(9-II-4)	-5.33(9-II-3)	1.01(10-I-4)	138(9-II-1)	-864(9-II-4)	164(9-II-4)
80	4	-2.49(10-I-3)	-4.83(10-I-4)	1.05(10-I-3)	-141(10-I-4)	-3100(9-II-4)	-180(10-II-3)
80	5	0.12(10-II-3)	-1.92(9-II-4)	1.51(10-I-4)	-44(10-I-4)	663(9-II-4)	188(9-II-4)
80	6	-0.70(10-I-3)	-2.29(9-II-4)	1.71(10-I-4)	-300(9-II-3)	-113(10-I-4)	249(9-II-4)
80	7	-1.24(9-II-4)	-2.19(9-II-3)	1.48(10-I-4)	-537(9-II-4)	-1288(9-II-4)	123(9-II-4)
80	8	-0.89(10-I-3)	-2.18(9-II-3)	0.91(10-I-4)	-591(9-II-4)	-3128(9-II-4)	17(10-I-4)
80	9	-0.81(10-I-3)	-1.82(9-II-4)	1.85(10-I-4)	47(6)	837(9-II-4)	-17(9-I-1)
80	10	-0.52(10-I-3)	-1.75(9-II-4)	1.89(10-I-4)	-257(9-II-3)	-132(9-II-4)	25(9-II-1)
80	11	-0.52(6)	-1.60(9-II-4)	1.37(10-I-4)	-522(9-II-4)	-1261(9-II-4)	124(9-II-4)
80	12	-0.51(10-II-4)	-1.54(9-II-4)	0.86(10-I-4)	-633(9-II-4)	-3246(9-II-4)	355(10-I-4)
80	13	-0.93(10-I-3)	-2.32(9-II-4)	1.85(10-I-4)	444(9-II-4)	758(9-II-4)	185(9-II-4)
80	14	-0.09(6)	-1.48(9-II-4)	1.36(10-I-4)	240(10-II-1)	-179(9-II-4)	-200(9-II-4)
80	15	0.30(10-I-4)	-1.03(10-II-4)	0.99(10-I-4)	393(9-II-4)	-760(9-II-4)	-48(10-II-1)
80	16	-1.01(10-II-4)	0.73(10-I-4)	0.60(10-I-4)	74(9-I-2)	-3184(9-II-4)	474(9-II-4)
81	1	2.47(9-II-4)	-1.79(9-II-4)	-1.97(9-II-3)	-1036(9-II-4)	-2100(9-II-4)	-420(9-II-4)
81	2	2.01(9-II-4)	-1.60(10-II-3)	-1.93(9-II-3)	-1204(9-II-4)	-2045(9-II-4)	-489(9-II-4)
81	3	3.17(9-II-4)	-1.01(9-II-4)	-1.76(9-II-3)	-943(9-II-4)	-1095(9-II-4)	-260(10-I-4)
81	4	3.29(9-II-4)	-1.04(9-II-4)	-1.40(9-II-3)	-988(9-II-4)	-1064(9-II-4)	-333(9-II-3)
81	5	3.54(9-II-4)	-0.95(9-II-4)	-1.25(9-II-3)	-734(9-II-4)	-977(6)	-464(9-II-3)
81	6	3.75(9-II-4)	-1.20(9-II-4)	-1.09(9-II-3)	-643(9-II-4)	-960(9-II-4)	-494(9-II-3)
81	7	2.46(9-II-4)	-1.66(9-II-4)	-1.32(9-II-3)	-1097(9-II-4)	-1946(9-II-4)	-391(9-II-3)
81	8	2.93(9-II-4)	-1.18(9-II-4)	-1.86(9-II-3)	-1087(9-II-4)	-1435(9-II-4)	-396(9-II-3)
82	1	2.40(9-II-3)	-2.21(9-II-3)	0.53(10-II-3)	-861(9-II-3)	-2263(9-II-3)	35(10-II-3)
82	2	2.44(9-II-3)	-2.28(9-II-3)	0.17(10-II-3)	-850(9-II-3)	-2109(9-II-3)	-133(10-I-3)
82	3	2.96(9-II-3)	-1.07(9-II-3)	-0.13(10-I-3)	-560(9-II-3)	-832(9-II-3)	314(10-II-3)
82	4	3.59(9-II-3)	-0.97(9-II-3)	0.40(10-II-3)	-612(9-II-3)	-849(9-II-3)	376(10-II-3)
82	5	3.46(9-II-3)	-0.83(9-II-3)	0.64(10-II-3)	-759(9-II-3)	-869(6)	372(10-II-3)
82	6	3.59(9-II-3)	-0.97(9-II-3)	0.86(10-II-3)	-907(9-II-4)	-1045(9-II-4)	269(10-II-3)
82	7	2.66(9-II-3)	-1.96(9-II-3)	0.52(10-II-3)	-975(9-II-3)	-2091(9-II-4)	57(10-II-3)
82	8	2.87(9-II-3)	-1.45(9-II-4)	0.52(10-II-3)	-956(9-II-3)	-1379(9-II-4)	119(10-II-3)
83	1	-2.01(10-I-3)	0.17(10-I-3)	-1.14(9-II-4)	-264(10-II-3)	233(10-I-3)	-176(9-II-4)
83	2	-1.81(10-I-3)	-0.22(10-II-3)	-1.46(9-II-4)	-169(10-II-3)	-60(10-II-3)	-391(9-II-4)
83	3	-0.89(10-I-3)	0.36(10-I-3)	-1.91(9-II-4)	-218(10-II-3)	-390(10-II-3)	-384(9-II-4)
83	4	-1.66(10-I-3)	0.99(9-II-4)	-1.84(9-II-4)	-475(10-II-3)	-420(10-II-3)	-428(9-II-4)
83	5	-1.77(10-I-3)	0.62(10-I-3)	-0.87(9-II-4)	-374(10-II-3)	350(10-I-3)	-197(9-II-4)
83	6	-2.23(10-I-3)	-0.24(10-II-3)	-1.29(9-II-4)	-254(10-II-3)	384(10-II-3)	-524(9-II-4)
83	7	-1.90(10-I-3)	0.11(10-I-3)	-1.29(9-II-4)	26(9-II-4)	246(10-I-3)	-260(9-II-4)
83	8	-1.79(10-I-3)	0.24(10-I-3)	-1.15(9-II-4)	-463(9-II-4)	198(10-I-3)	-113(9-II-4)
83	9	-2.42(10-I-3)	0.12(10-I-3)	-1.11(9-II-4)	-198(10-II-3)	359(9-I-1)	-418(9-II-4)
84	1	2.08(9-II-3)	-0.87(9-II-3)	1.38(9-II-4)	-540(9-II-3)	-617(9-II-3)	497(9-II-4)
84	2	1.83(9-II-3)	-1.61(9-II-3)	1.75(9-II-4)	-668(9-II-3)	-1709(9-II-3)	376(9-II-4)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
84	3	2.07 (9-II-3)	-0.73 (9-II-3)	1.56 (9-II-4)	-627 (9-II-3)	-587 (9-II-3)	442 (9-II-4)
84	4	1.66 (9-II-3)	-1.39 (9-II-3)	1.86 (9-II-4)	-747 (9-II-3)	-1748 (9-II-3)	398 (9-II-4)
84	5	2.09 (9-II-3)	-0.58 (10-I-3)	1.70 (9-II-4)	-695 (9-II-3)	-526 (9-II-3)	378 (9-II-4)
84	6	1.48 (9-II-3)	-1.22 (9-II-3)	1.94 (9-II-4)	-847 (9-II-3)	-1793 (9-II-3)	421 (9-II-4)
84	7	1.99 (9-II-3)	-0.34 (10-I-3)	1.75 (9-II-4)	-774 (9-II-3)	-441 (9-II-3)	318 (9-II-4)
84	8	1.23 (9-II-3)	-1.11 (10-I-3)	2.02 (9-II-4)	-962 (9-II-3)	-1843 (9-II-3)	447 (9-II-4)
85	1	1.24 (9-II-3)	-0.78 (9-II-3)	1.14 (10-I-3)	-324 (10-I-3)	-372 (10-I-3)	529 (9-II-4)
85	2	1.64 (9-II-3)	-1.73 (9-II-3)	1.43 (9-II-4)	-455 (9-II-4)	-1327 (9-II-3)	282 (9-II-4)
85	3	1.41 (9-II-3)	-0.64 (9-II-3)	1.44 (9-II-4)	-481 (9-II-3)	-439 (10-I-3)	579 (9-II-4)
85	4	1.47 (9-II-3)	-1.49 (9-II-3)	1.60 (9-II-4)	-536 (9-II-3)	-1377 (9-II-3)	312 (9-II-4)
85	5	1.64 (9-II-3)	-0.62 (10-I-3)	1.60 (9-II-4)	-570 (9-II-3)	-474 (10-I-3)	579 (9-II-4)
85	6	1.34 (9-II-3)	-1.29 (9-II-3)	1.78 (9-II-4)	-599 (9-II-3)	-1438 (9-II-3)	365 (9-II-4)
85	7	1.72 (9-II-3)	-0.52 (10-I-3)	1.71 (9-II-4)	-630 (9-II-3)	-467 (10-I-3)	545 (9-II-4)
85	8	1.14 (9-II-3)	-1.15 (10-I-3)	1.95 (9-II-4)	-669 (9-II-3)	-1511 (9-II-3)	423 (9-II-4)
86	1	-1.93 (9-II-4)	1.75 (9-II-4)	1.88 (9-II-3)	-2047 (9-II-4)	-828 (9-II-4)	260 (10-I-3)
86	2	-1.36 (9-II-4)	3.13 (9-II-4)	1.04 (9-II-3)	-1149 (9-II-4)	-857 (9-II-4)	434 (9-II-3)
86	3	-2.16 (9-II-4)	2.54 (9-II-4)	1.70 (9-II-3)	-2048 (9-II-4)	-808 (9-II-4)	330 (10-I-3)
87	1	0.85 (10-II-3)	0.31 (10-I-3)	-1.93 (9-II-4)	-725 (9-II-4)	75 (10-I-3)	-296 (9-II-4)
87	2	0.18 (10-II-3)	-0.25 (10-II-3)	-2.48 (9-II-4)	-863 (9-II-4)	-1226 (10-II-3)	-413 (9-II-4)
87	3	0.93 (10-II-3)	-0.17 (10-II-3)	-2.12 (9-II-4)	-585 (9-II-4)	-79 (6)	-342 (9-II-4)
87	4	0.55 (10-II-3)	-0.47 (10-II-3)	-2.50 (9-II-4)	-696 (9-II-4)	-1200 (10-II-3)	-388 (9-II-4)
87	5	0.82 (10-II-3)	-0.39 (10-II-3)	-2.09 (9-II-4)	-469 (9-II-4)	-155 (10-II-3)	-402 (9-II-4)
87	6	0.80 (10-II-3)	-0.75 (10-II-3)	-2.48 (9-II-4)	-564 (9-II-4)	-1177 (10-II-3)	-370 (9-II-4)
87	7	0.74 (10-II-3)	-0.60 (10-II-3)	-1.99 (9-II-4)	-359 (10-II-3)	-204 (10-II-3)	-457 (9-II-3)
87	8	1.05 (9-II-4)	-1.05 (10-II-3)	-2.43 (9-II-4)	-464 (10-II-3)	-1160 (10-II-3)	-355 (9-II-4)
88	1	3.70 (9-II-4)	-1.18 (9-II-4)	0.34 (10-II-3)	-819 (9-II-3)	-1214 (9-II-4)	190 (10-II-3)
88	2	2.72 (9-II-4)	-2.31 (9-II-4)	0.25 (10-II-3)	-982 (9-II-3)	-2311 (9-II-4)	-92 (10-I-3)
88	3	3.68 (9-II-4)	-1.20 (9-II-4)	0.56 (10-II-3)	-862 (9-II-4)	-1274 (9-II-4)	136 (10-II-3)
88	4	2.80 (9-II-4)	-2.26 (9-II-4)	0.47 (10-II-3)	-995 (9-II-3)	-2327 (9-II-4)	-53 (10-I-3)
88	5	3.61 (9-II-4)	-1.24 (9-II-4)	0.79 (10-II-3)	-860 (9-II-4)	-1293 (9-II-4)	82 (10-II-3)
88	6	2.86 (9-II-4)	-2.28 (9-II-4)	0.68 (10-II-3)	-1013 (9-II-4)	-2349 (9-II-4)	55 (10-II-3)
88	7	3.56 (9-II-4)	-1.26 (9-II-4)	1.16 (10-II-3)	-816 (9-II-4)	-1263 (9-II-4)	50 (10-II-3)
88	8	2.95 (9-II-4)	-2.32 (9-II-4)	0.89 (10-II-3)	-1004 (9-II-4)	-2381 (9-II-4)	89 (10-II-3)
89	1	0.27 (10-II-3)	-0.20 (10-II-3)	-2.06 (9-II-4)	-410 (10-II-3)	-107 (10-II-3)	-461 (9-II-4)
89	2	0.21 (10-II-3)	-0.55 (10-II-3)	-2.47 (9-II-4)	-422 (10-II-3)	-1018 (10-II-3)	-389 (9-II-4)
89	3	0.23 (10-II-3)	-0.38 (10-II-3)	-2.02 (9-II-4)	-346 (10-II-3)	-146 (10-II-3)	-489 (9-II-4)
89	4	0.44 (10-II-3)	-0.78 (10-II-3)	-2.36 (9-II-4)	-349 (10-II-3)	-980 (10-II-3)	-350 (9-II-4)
89	5	-0.35 (10-I-3)	-0.41 (10-II-3)	-1.92 (9-II-4)	-272 (10-II-3)	-147 (10-II-3)	-497 (9-II-4)
89	6	0.62 (10-II-3)	-1.04 (10-II-3)	-2.22 (9-II-4)	-293 (10-II-3)	-949 (10-II-3)	-312 (9-II-4)
89	7	-0.55 (10-I-3)	-0.52 (9-II-4)	-1.68 (9-II-3)	-144 (10-II-3)	-111 (10-II-3)	-470 (9-II-4)
89	8	0.87 (9-II-4)	-1.33 (9-II-4)	-2.05 (9-II-4)	-233 (9-I-3)	-926 (10-II-3)	-295 (9-II-4)
90	1	2.89 (9-II-4)	-0.71 (9-II-4)	-1.62 (9-II-3)	-868 (9-II-4)	-738 (9-II-4)	-555 (9-II-3)
90	2	2.33 (9-II-4)	-1.79 (9-II-4)	-1.72 (9-II-4)	-869 (9-II-4)	-1843 (9-II-4)	-324 (10-I-3)
90	3	2.81 (9-II-4)	-0.79 (9-II-4)	-1.46 (9-II-3)	-780 (9-II-4)	-675 (9-II-4)	-570 (9-II-3)
90	4	2.36 (9-II-4)	-1.90 (9-II-4)	-1.47 (9-II-3)	-805 (9-II-4)	-1753 (9-II-4)	-246 (10-I-3)
90	5	2.58 (9-II-4)	-0.85 (9-II-4)	-1.22 (9-II-3)	-654 (9-II-4)	-584 (9-II-4)	-563 (9-II-3)
90	6	2.37 (9-II-4)	-2.09 (9-II-4)	-1.26 (9-II-3)	-751 (9-II-4)	-1682 (9-II-4)	-181 (10-I-3)
90	7	2.50 (9-II-4)	-1.03 (9-II-4)	-0.81 (10-I-3)	-444 (10-II-3)	-478 (9-II-4)	-522 (9-II-3)
90	8	2.44 (9-II-4)	-2.31 (9-II-4)	-1.06 (10-I-3)	-677 (10-II-3)	-1627 (9-II-4)	-147 (10-I-3)
91	1	-1.28 (10-II-3)	-0.24 (10-I-3)	1.76 (9-II-4)	-156 (9-I-4)	214 (10-II-3)	513 (9-II-3)
91	2	-0.24 (10-II-3)	-0.54 (10-I-3)	1.92 (9-II-3)	-231 (9-I-4)	-476 (9-I-4)	339 (9-II-3)
91	3	-1.13 (10-II-3)	-0.18 (10-I-3)	1.81 (9-II-3)	-262 (9-I-4)	150 (10-II-3)	546 (9-II-3)
91	4	-0.41 (10-II-3)	-0.36 (10-I-3)	2.00 (9-II-3)	-286 (9-I-4)	-497 (9-I-4)	359 (9-II-3)
91	5	-1.04 (10-II-3)	-0.17 (10-I-3)	1.76 (9-II-3)	-320 (10-I-3)	114 (10-II-3)	544 (9-II-3)
91	6	-0.53 (10-II-3)	-0.16 (10-I-3)	2.07 (9-II-3)	-330 (9-I-4)	-521 (9-I-4)	391 (9-II-3)
91	7	-1.09 (10-II-3)	-0.07 (6)	1.68 (9-II-3)	-374 (10-I-3)	112 (10-II-3)	517 (9-II-3)
91	8	-0.69 (10-II-3)	0.24 (10-II-3)	2.12 (9-II-3)	-379 (9-I-4)	-548 (9-I-4)	426 (9-II-3)
92	1	-2.02 (10-I-3)	0.12 (9-II-3)	-1.25 (9-II-4)	-221 (10-II-3)	155 (10-I-3)	-401 (9-II-4)
92	2	-1.28 (10-I-3)	0.58 (9-II-3)	-1.90 (9-II-4)	-216 (10-II-3)	-251 (10-II-3)	-407 (9-II-4)
92	3	-1.89 (10-I-3)	-0.06 (10-II-3)	-1.38 (9-II-4)	-192 (10-II-3)	165 (10-I-3)	-432 (9-II-4)
92	4	-1.10 (10-I-3)	0.40 (10-I-3)	-1.89 (9-II-4)	-171 (10-II-3)	-238 (10-II-3)	-381 (9-II-4)
92	5	-1.87 (10-I-3)	0.07 (10-I-3)	-1.51 (9-II-4)	-150 (10-II-3)	207 (10-I-3)	-439 (9-II-4)
92	6	-1.00 (10-I-3)	0.25 (10-I-3)	-1.86 (9-II-4)	-132 (9-I-3)	-222 (10-II-3)	-356 (9-II-4)
92	7	-1.93 (10-I-3)	0.13 (10-I-3)	-1.58 (9-II-4)	-73 (9-I-4)	275 (10-I-3)	-407 (9-II-4)
92	8	-0.92 (10-I-3)	-0.14 (10-II-3)	-1.82 (9-II-4)	-99 (9-I-4)	-208 (10-II-3)	-348 (9-II-4)
93	1	-2.75 (9-II-4)	0.60 (9-II-4)	0.41 (10-I-3)	-176 (10-II-3)	512 (9-II-4)	35 (10-I-3)
93	2	-1.77 (9-II-4)	0.84 (9-II-4)	-0.57 (10-II-3)	-185 (9-I-3)	243 (9-II-4)	-147 (10-II-3)
93	3	-2.62 (9-II-4)	0.36 (9-II-4)	-0.36 (10-II-3)	-138 (10-II-3)	414 (9-II-4)	-56 (10-II-3)
93	4	-1.47 (9-II-4)	0.77 (9-II-4)	-0.65 (10-II-3)	-113 (9-I-4)	248 (9-II-4)	-138 (10-II-3)
93	5	-2.72 (9-II-4)	0.19 (9-II-4)	-0.57 (10-II-3)	-110 (9-I-4)	351 (9-II-4)	-101 (10-II-3)
93	6	-1.32 (9-II-4)	0.69 (9-II-3)	-0.69 (10-II-3)	-66 (9-I-4)	258 (9-II-4)	-126 (10-II-3)
93	7	-2.85 (9-II-4)	0.10 (9-II-3)	-0.70 (9-II-4)	-81 (9-I-4)	322 (9-II-4)	-145 (10-II-3)
93	8	-1.26 (9-II-3)	0.65 (9-II-3)	-0.73 (10-II-3)	61 (6)	274 (9-II-4)	-113 (10-II-3)
94	1	0.29 (10-I-3)	-0.52 (10-I-3)	1.69 (9-II-4)	80 (6)	145 (6)	254 (9-II-4)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
94	2	0.35(10-I-3)	-2.09(10-I-3)	1.32(9-II-4)	326(9-II-4)	-179(9-I-4)	304(9-II-4)
94	3	-0.21(10-II-3)	-0.25(10-I-3)	1.56(9-II-4)	-102(10-II-3)	111(6)	245(9-II-4)
95	1	-2.98(9-II-4)	0.21(9-II-4)	-0.39(10-II-3)	-94(9-I-4)	361(9-II-4)	-132(10-II-3)
95	2	-1.55(9-II-4)	0.85(9-II-3)	-0.50(10-II-3)	-50(9-I-4)	326(9-II-4)	-89(10-II-3)
95	3	-2.82(9-II-4)	0.23(9-II-4)	-0.58(10-II-3)	-100(9-I-4)	396(9-II-4)	-176(10-II-3)
95	4	-1.63(9-II-4)	0.89(9-II-3)	-0.51(10-II-3)	-70(9-I-4)	325(9-II-4)	-67(10-II-3)
95	5	-2.76(9-II-4)	0.40(9-II-3)	-0.74(10-II-3)	-114(9-I-4)	470(9-II-4)	-207(10-II-3)
95	6	-1.73(9-II-3)	0.94(9-II-3)	-0.52(10-II-3)	-111(9-I-4)	322(9-II-4)	-43(10-II-3)
95	7	-2.94(9-II-4)	0.66(9-II-3)	-0.96(9-II-4)	-123(9-I-4)	567(9-II-3)	-205(10-II-3)
95	8	-1.85(9-II-3)	1.01(9-II-3)	-0.54(10-II-3)	-169(9-I-4)	318(9-II-4)	-25(10-II-3)
96	1	-2.80(9-II-4)	0.37(9-II-4)	1.37(9-II-3)	-82(9-I-4)	492(9-II-4)	292(10-I-3)
96	2	-1.46(9-II-4)	0.65(9-II-4)	1.14(10-I-3)	-116(9-I-4)	202(9-II-4)	177(9-II-3)
96	3	-2.69(9-II-4)	0.24(9-II-4)	1.08(10-I-3)	-114(9-I-4)	408(9-II-4)	295(10-I-3)
96	4	-1.47(9-II-4)	0.70(9-II-4)	1.13(10-I-3)	-115(9-I-4)	195(9-II-4)	180(9-II-3)
96	5	-2.70(9-II-4)	0.16(9-II-4)	0.90(10-I-3)	-128(9-I-4)	362(9-II-4)	266(10-I-3)
96	6	-1.51(9-II-4)	0.77(9-II-4)	1.10(10-I-3)	-123(9-I-4)	189(9-II-4)	190(10-I-3)
96	7	-2.80(9-II-4)	0.23(9-II-4)	0.75(10-I-3)	-148(9-I-4)	359(9-II-4)	221(10-I-3)
96	8	-1.57(9-II-4)	0.90(9-II-4)	1.05(10-I-3)	-144(9-I-4)	184(9-II-4)	203(10-I-3)
97	1	-2.58(9-II-4)	-0.07(6)	1.04(10-I-3)	-126(9-I-4)	308(9-II-4)	234(10-I-3)
97	2	-1.21(9-II-4)	0.68(9-II-4)	1.23(10-I-3)	-162(9-I-4)	97(9-II-4)	223(10-I-3)
97	3	-2.37(9-II-4)	0.20(9-II-4)	0.92(10-I-3)	-180(9-I-4)	364(9-II-4)	180(10-I-3)
97	4	-1.46(9-II-4)	0.89(9-II-4)	1.17(10-I-3)	-232(9-I-4)	-84(9-I-4)	225(10-I-3)
97	5	-2.21(9-II-4)	0.44(9-II-4)	0.75(10-I-3)	-241(9-I-4)	449(9-II-4)	124(10-I-3)
97	6	-1.69(9-II-4)	1.13(9-II-4)	1.10(10-I-3)	-322(9-I-4)	-91(9-I-4)	228(10-I-3)
97	7	-2.34(9-II-4)	0.87(9-II-4)	0.41(10-I-3)	-327(10-I-3)	548(9-II-4)	86(10-I-3)
97	8	-1.97(9-II-4)	1.36(9-II-4)	1.03(10-I-3)	-435(9-I-4)	-97(9-I-4)	240(10-I-3)
98	1	1.02(9-I-4)	0.97(9-II-3)	-0.17(9-II-3)	-253(9-I-1)	-271(9-II-3)	48(9-II-3)
98	2	1.14(9-II-3)	0.88(9-II-3)	-0.19(9-II-3)	-304(9-I-1)	-151(9-I-4)	56(9-II-3)
98	3	1.07(9-I-4)	0.86(9-II-2)	-0.04(10-II-3)	-292(9-I-4)	-224(9-II-2)	-20(10-I-3)
98	4	0.96(9-I-4)	0.99(9-II-3)	-0.25(9-II-3)	-264(9-I-4)	-375(9-II-3)	58(9-II-3)
98	5	1.02(9-I-1)	0.98(9-II-3)	-0.18(9-II-3)	-229(9-I-1)	-201(9-II-3)	89(9-II-3)
98	6	1.02(9-I-4)	0.98(9-II-3)	-0.17(9-II-3)	-244(9-I-4)	-169(9-I-4)	46(9-II-3)
98	7	1.01(9-I-4)	0.98(9-II-3)	-0.17(9-II-3)	-262(9-I-1)	-346(9-II-3)	54(9-II-3)
98	8	1.02(9-I-4)	0.97(9-II-3)	-0.18(9-II-3)	-254(9-II-3)	-282(9-II-3)	88(9-II-3)
99	1	-0.76(10-I-3)	-0.44(10-I-3)	1.75(9-II-3)	-298(10-I-3)	-160(6)	518(9-II-3)
99	2	0.38(10-I-3)	-0.44(10-I-3)	2.14(9-II-3)	-380(10-I-3)	-720(10-I-3)	432(9-II-3)
99	3	-0.63(10-II-3)	-0.29(10-I-3)	1.76(9-II-3)	-379(10-I-3)	-113(6)	455(9-II-3)
99	4	-0.26(10-II-3)	-0.19(10-I-3)	2.12(9-II-3)	-474(10-I-3)	-744(10-I-3)	439(9-II-3)
99	5	-0.50(10-II-3)	-0.09(10-I-3)	1.69(9-II-3)	-460(10-I-3)	104(10-II-3)	373(9-II-3)
99	6	-0.51(10-II-3)	0.29(10-II-3)	2.09(9-II-3)	-592(10-I-3)	-770(10-I-3)	448(9-II-3)
99	7	-0.56(10-II-3)	0.45(10-II-3)	1.40(9-II-3)	-582(9-II-3)	209(10-II-3)	294(9-II-3)
99	8	-0.84(10-II-3)	0.53(10-II-3)	2.04(9-II-3)	-759(9-II-3)	-798(10-I-3)	467(9-II-3)
100	1	1.14(9-I-3)	1.14(9-II-3)	-0.25(10-II-3)	-282(9-I-3)	-316(9-II-3)	61(10-II-3)
100	2	1.25(9-II-3)	1.06(9-II-3)	-0.24(10-II-3)	-339(9-II-3)	-215(9-II-2)	73(10-II-3)
100	3	1.15(9-I-4)	0.92(9-II-2)	-0.12(10-II-3)	-312(9-I-4)	-236(9-II-2)	15(10-II-3)
100	4	1.08(9-I-4)	1.15(9-II-3)	-0.27(10-II-3)	-291(9-I-4)	-392(9-II-3)	62(10-II-3)
100	5	1.15(9-I-3)	1.15(9-II-3)	-0.25(10-II-3)	-262(9-II-3)	-263(9-II-3)	101(9-II-3)
100	6	1.14(9-I-3)	1.14(9-II-3)	-0.23(10-II-3)	-278(9-I-4)	-234(9-II-3)	64(10-II-3)
100	7	1.12(9-I-4)	1.16(9-II-3)	-0.23(10-II-3)	-288(9-II-3)	-373(9-II-3)	62(10-II-3)
100	8	1.13(9-I-3)	1.14(9-II-3)	-0.25(10-II-3)	-278(9-II-3)	-317(9-II-3)	94(10-II-3)
101	1	0.77(9-I-4)	0.80(9-II-1)	0.33(10-I-3)	-180(10-II-3)	-202(9-II-1)	-86(10-I-3)
101	2	0.62(9-I-4)	0.88(9-II-1)	0.37(10-I-3)	-189(9-I-4)	-336(9-II-4)	-62(6)
101	3	0.89(9-I-4)	0.84(9-I-3)	0.22(10-I-3)	-262(9-I-4)	-231(9-I-3)	-40(9-I-2)
101	4	0.84(9-II-3)	0.76(9-I-3)	0.40(9-II-4)	-196(9-I-4)	-107(9-I-3)	-158(9-II-4)
101	5	0.75(9-I-4)	0.80(9-II-1)	0.33(10-I-3)	-162(10-II-3)	-269(9-II-4)	-119(9-II-4)
101	6	0.77(9-I-4)	0.80(9-II-1)	0.33(10-I-3)	-202(10-II-3)	-309(9-II-4)	-64(10-I-3)
101	7	0.78(9-I-4)	0.80(9-II-1)	0.32(10-I-3)	-160(9-I-4)	-126(9-I-3)	-114(9-II-4)
101	8	0.77(9-I-4)	0.80(9-II-1)	0.32(9-II-4)	-128(9-I-4)	-177(9-I-3)	-130(9-II-4)
102	1	0.78(9-II-2)	1.04(9-II-1)	0.39(9-II-3)	-189(9-II-2)	-264(9-II-1)	-96(10-I-4)
102	2	0.63(10-II-3)	1.14(9-II-1)	0.37(9-II-3)	-188(9-II-2)	-393(9-II-4)	-73(6)
102	3	0.87(9-II-2)	1.04(9-I-3)	0.25(10-II-3)	-254(9-II-2)	-284(9-I-3)	-46(10-II-3)
102	4	0.88(9-II-2)	1.01(9-II-1)	0.43(9-II-4)	-206(9-II-2)	-183(9-I-3)	-164(9-II-4)
102	5	0.75(9-II-2)	1.03(9-II-1)	0.40(9-II-3)	-171(9-II-2)	-322(9-II-4)	-133(9-II-4)
102	6	0.78(9-II-2)	1.03(9-II-1)	0.37(10-I-4)	-212(9-II-2)	-361(9-II-4)	-76(10-I-4)
102	7	0.80(9-II-2)	1.03(9-II-1)	0.37(9-II-3)	-168(10-II-3)	-190(9-I-3)	-123(9-II-4)
102	8	0.78(9-II-2)	1.04(9-II-1)	0.39(9-II-4)	-139(10-II-3)	-244(9-II-1)	-141(9-II-4)
103	1	0.57(9-I-4)	0.58(9-II-1)	0.32(9-II-4)	-165(9-I-4)	-234(9-II-2)	-48(10-I-3)
103	2	0.89(9-I-4)	0.74(9-II-2)	0.14(10-I-3)	-263(9-I-4)	-195(9-II-2)	-23(10-I-3)
103	3	0.75(9-I-4)	0.48(9-I-3)	0.28(10-I-3)	-166(9-I-4)	-73(9-I-4)	-103(9-II-4)
104	1	0.81(9-II-2)	1.35(9-II-4)	0.27(9-II-3)	-195(9-II-2)	-353(9-II-4)	-79(9-II-3)
104	2	0.65(9-II-2)	1.41(9-II-4)	0.34(9-II-3)	-198(9-II-2)	-468(9-II-4)	-58(6)
104	3	0.87(9-II-2)	1.21(9-I-3)	0.18(10-II-3)	-249(9-II-2)	-328(9-I-3)	-35(10-II-3)
104	4	0.85(9-II-2)	1.32(9-II-4)	0.39(9-II-3)	-202(9-II-2)	-253(9-I-3)	-142(9-II-3)
104	5	0.80(9-II-2)	1.36(9-II-4)	0.28(9-II-3)	-188(9-II-2)	-417(9-II-4)	-101(9-II-4)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
104	6	0.80(9-II-2)	1.35(9-II-4)	0.28(9-II-3)	-217(9-II-2)	-447(9-II-4)	-56(9-II-3)
104	7	0.80(9-II-2)	1.37(9-II-4)	0.28(9-II-3)	-175(9-II-2)	-277(9-I-3)	-103(9-II-3)
104	8	0.80(9-II-2)	1.35(9-II-4)	0.28(9-II-3)	-150(9-II-2)	-324(9-II-4)	-116(9-II-4)
105	1	1.16(9-II-3)	1.47(9-II-3)	-0.31(10-II-3)	-302(9-II-3)	-418(9-II-3)	73(10-II-3)
105	2	1.26(9-II-3)	1.42(9-II-3)	-0.30(10-II-3)	-327(9-II-3)	-346(9-II-3)	91(10-II-3)
105	3	1.16(9-I-3)	0.96(9-II-3)	-0.17(10-II-3)	-313(9-I-3)	-256(9-II-3)	34(10-II-3)
106	1	1.14(9-II-3)	1.61(9-II-3)	-0.28(10-II-3)	-292(9-II-3)	-433(9-II-3)	68(10-II-3)
106	2	1.17(9-II-3)	1.52(9-II-3)	-0.26(10-II-3)	-322(9-II-3)	-402(9-II-3)	80(9-I-2)
106	3	1.09(9-II-3)	1.13(9-II-3)	-0.18(9-I-2)	-293(9-I-3)	-296(9-II-3)	42(9-I-2)
106	4	1.13(9-II-3)	1.56(9-II-3)	-0.26(10-II-3)	-296(9-II-3)	-414(9-II-3)	56(10-II-3)
106	5	1.15(9-II-3)	1.61(9-II-3)	-0.28(10-II-3)	-282(9-II-3)	-427(9-II-3)	85(10-II-3)
106	6	1.13(9-II-3)	1.61(9-II-3)	-0.26(10-II-3)	-296(9-II-3)	-423(9-II-3)	77(9-I-2)
106	7	1.12(9-II-3)	1.62(9-II-3)	-0.26(10-II-3)	-288(9-II-3)	-436(9-II-3)	62(10-II-3)
106	8	1.14(9-II-3)	1.61(9-II-3)	-0.27(10-II-3)	-276(9-II-3)	-424(9-II-3)	75(10-II-3)
107	1	0.99(9-II-2)	1.83(9-II-3)	-0.17(9-I-2)	-270(9-II-2)	-501(9-II-3)	58(9-I-3)
107	2	0.99(9-II-2)	1.19(9-II-3)	-0.09(9-I-2)	-267(9-II-2)	-312(9-II-3)	31(10-I-3)
107	3	1.05(9-II-2)	1.80(9-II-3)	-0.16(9-I-2)	-266(9-II-2)	-458(9-II-3)	29(9-I-2)
108	1	0.91(9-II-2)	1.79(9-II-4)	0.06(9-II-3)	-217(9-II-2)	-496(9-II-4)	-40(9-II-3)
108	2	0.72(9-II-2)	2.04(9-II-4)	0.05(9-II-3)	-194(9-II-2)	-520(9-II-4)	-22(6)
108	3	0.88(9-II-2)	1.21(9-I-3)	0.14(9-II-3)	-249(9-II-2)	-309(9-I-4)	8(10-I-3)
109	1	0.63(9-I-4)	0.41(10-II-3)	0.17(9-II-4)	-142(9-I-4)	-100(10-II-3)	-40(9-II-4)
109	2	0.50(9-I-4)	0.53(10-II-3)	0.20(9-II-4)	-154(9-I-4)	-228(9-II-2)	-20(9-II-4)
109	3	0.84(9-I-4)	0.66(9-II-2)	0.05(10-I-3)	-251(9-I-4)	-186(9-II-2)	15(10-II-3)
109	4	0.70(9-I-4)	0.42(10-II-3)	0.19(9-II-4)	-162(9-I-4)	45(6)	-97(9-II-4)
109	5	0.59(9-I-4)	0.41(10-II-3)	0.18(9-I-4)	-119(9-I-3)	-152(10-II-3)	-78(9-II-4)
109	6	0.63(9-I-4)	0.41(10-II-3)	0.16(9-II-4)	-158(9-I-3)	-185(10-II-3)	-25(9-II-4)
109	7	0.64(9-I-4)	0.40(10-II-3)	0.15(9-II-4)	-126(9-I-4)	36(6)	-64(9-II-4)
109	8	0.62(9-I-4)	0.41(10-II-3)	0.15(9-II-4)	-97(9-I-4)	-80(10-II-3)	-78(9-II-4)
110	1	0.56(9-I-4)	-0.14(6)	0.19(9-II-4)	-122(9-I-4)	35(6)	-77(9-II-4)
110	2	0.46(9-I-4)	0.23(10-II-3)	0.14(9-II-4)	-125(9-I-4)	-79(10-II-3)	-21(9-II-4)
110	3	0.74(9-I-4)	0.74(9-II-2)	-0.04(9-I-2)	-229(9-I-4)	-196(9-I-3)	28(10-II-3)
111	1	0.61(9-I-4)	0.42(9-I-4)	-0.14(10-I-3)	-134(9-I-4)	-124(9-I-4)	32(10-I-3)
111	2	0.67(9-I-1)	0.47(9-I-4)	-0.12(10-I-3)	-184(9-I-1)	-74(9-I-4)	47(9-II-2)
111	3	0.69(9-I-4)	0.88(9-I-4)	-0.04(10-I-3)	-194(9-II-3)	-234(9-I-4)	-18(10-II-3)
111	4	0.54(9-I-4)	0.55(9-I-4)	-0.19(10-I-3)	-146(9-I-4)	-218(9-I-4)	42(10-I-3)
111	5	0.60(9-I-4)	0.44(9-I-4)	-0.14(10-I-3)	-110(9-I-4)	-77(9-I-4)	64(10-I-3)
111	6	0.61(9-I-4)	0.43(9-I-4)	-0.12(10-I-3)	-127(9-I-4)	-51(9-I-4)	30(10-I-3)
111	7	0.59(9-I-4)	0.43(9-I-4)	-0.13(10-I-3)	-141(9-I-4)	-172(9-I-4)	37(10-I-3)
111	8	0.58(9-I-4)	0.41(9-I-4)	-0.16(10-I-3)	-131(9-I-4)	-122(9-I-4)	68(10-I-3)
112	1	0.51(9-I-4)	0.29(9-I-4)	-0.08(10-I-3)	-106(9-I-4)	-86(9-I-4)	19(10-I-3)
112	2	0.56(9-I-4)	0.36(9-I-4)	-0.09(10-I-3)	-155(9-I-4)	-63(9-I-4)	42(10-I-3)
112	3	0.62(9-I-4)	0.84(9-I-4)	-0.09(10-I-3)	-180(9-I-4)	-227(9-I-4)	11(10-I-3)
112	4	0.45(9-I-4)	0.43(9-I-4)	-0.15(10-I-3)	-119(9-I-4)	-167(9-I-4)	26(10-I-3)
112	5	0.49(9-I-4)	0.31(9-I-4)	-0.08(10-I-3)	-82(9-I-4)	-52(9-I-4)	43(10-I-3)
112	6	0.51(9-I-4)	0.30(9-I-4)	-0.06(10-I-3)	-102(9-I-4)	-32(9-I-4)	18(10-I-3)
112	7	0.50(9-I-4)	0.30(9-I-4)	-0.08(10-I-3)	-110(9-I-4)	-119(9-I-4)	20(10-I-3)
112	8	0.49(9-I-4)	0.28(9-I-4)	-0.10(10-I-3)	-98(9-I-4)	-81(9-I-4)	47(10-I-3)
113	1	0.46(9-I-4)	0.14(9-I-4)	-0.07(10-I-3)	-89(9-I-4)	-43(9-I-4)	12(10-I-3)
113	2	0.46(9-I-4)	0.26(9-I-4)	-0.04(10-I-3)	-136(9-I-4)	-69(9-I-4)	38(10-I-3)
113	3	0.61(9-I-4)	0.79(9-I-4)	-0.11(10-I-3)	-182(9-I-4)	-216(9-I-4)	23(9-I-2)
113	4	0.42(9-I-4)	0.30(9-I-4)	-0.10(10-I-3)	-104(9-I-4)	-93(9-I-4)	-23(10-II-3)
113	5	0.44(9-I-4)	0.16(9-I-4)	-0.06(10-I-3)	-66(9-I-4)	34(6)	26(10-I-3)
113	6	0.46(9-I-4)	0.15(9-I-4)	-0.04(10-I-3)	-90(9-I-4)	43(6)	16(9-I-4)
113	7	0.45(9-I-4)	0.15(9-I-4)	-0.06(10-I-3)	-88(9-I-4)	-50(9-I-4)	-14(10-II-3)
113	8	0.44(9-I-4)	-0.13(6)	-0.09(10-I-3)	-71(9-I-4)	37(6)	29(10-I-3)
114	1	0.73(9-I-1)	0.64(9-I-4)	-0.16(9-II-3)	-169(9-I-1)	-182(9-I-4)	37(9-II-3)
114	2	0.83(9-II-3)	0.62(9-I-4)	-0.14(9-II-3)	-222(9-II-3)	-93(9-I-4)	48(9-II-2)
114	3	0.80(9-I-1)	0.87(9-I-4)	-0.02(9-II-2)	-221(9-I-4)	-229(9-I-4)	-24(10-II-3)
114	4	0.65(9-I-4)	0.71(9-I-4)	-0.22(9-II-3)	-181(9-I-1)	-289(9-I-4)	52(9-II-3)
114	5	0.73(9-I-1)	0.65(9-I-4)	-0.16(9-II-3)	-147(9-I-1)	-123(9-I-4)	79(9-II-3)
114	6	0.72(9-I-1)	0.64(9-I-4)	-0.13(9-II-3)	-159(9-I-4)	-90(9-I-4)	33(9-II-3)
114	7	0.71(9-I-1)	0.65(9-I-4)	-0.14(9-II-3)	-179(9-I-1)	-246(9-I-4)	45(9-II-3)
114	8	0.71(9-I-1)	0.62(9-I-4)	-0.17(9-II-3)	-173(9-I-1)	-184(9-I-4)	82(9-II-3)
115	1	0.43(9-I-4)	-0.22(6)	0.12(9-II-4)	-80(9-I-4)	60(6)	-30(9-II-4)
115	2	0.41(9-I-4)	0.21(9-I-4)	0.11(9-II-4)	-125(9-I-4)	-79(9-I-3)	25(9-I-2)
115	3	0.66(9-I-4)	0.75(9-I-4)	-0.11(9-I-2)	-202(9-I-4)	-205(9-I-4)	32(9-I-2)
115	4	0.44(9-I-4)	0.20(9-I-4)	0.05(9-II-4)	-101(9-I-4)	-42(9-I-4)	-54(9-II-4)
115	5	0.39(9-I-4)	-0.21(6)	0.14(9-II-4)	-50(9-I-4)	52(6)	-40(9-II-4)
115	6	0.43(9-I-4)	-0.21(6)	0.13(9-II-4)	-87(9-I-4)	46(6)	-22(9-II-4)
115	7	0.44(9-I-4)	-0.22(6)	0.11(9-II-4)	-74(9-I-4)	79(6)	-44(9-II-4)
115	8	0.41(9-I-4)	-0.23(6)	0.09(9-II-4)	-48(9-I-4)	72(6)	-32(9-II-4)
116	1	0.88(9-I-4)	0.78(9-I-4)	-0.17(9-I-3)	-212(9-I-1)	-220(9-I-4)	44(9-II-3)
116	2	0.99(9-II-3)	0.74(9-I-4)	-0.16(9-II-3)	-264(9-I-1)	-119(9-I-4)	51(9-II-3)
116	3	0.94(9-I-4)	0.86(9-I-4)	0.03(9-I-2)	-258(9-I-4)	-226(9-I-4)	-29(9-I-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
116	4	0.81(9-I-4)	0.83(9-I-4)	-0.24(9-II-3)	-223(9-I-1)	-324(9-II-3)	59(9-II-3)
116	5	0.88(9-I-1)	0.79(9-I-4)	-0.17(9-II-3)	-187(9-I-1)	-157(9-I-4)	85(9-II-3)
116	6	0.88(9-I-1)	0.79(9-I-4)	-0.16(9-II-3)	-202(9-I-4)	-124(9-I-4)	40(9-II-3)
116	7	0.86(9-I-4)	0.79(9-I-4)	-0.16(9-II-3)	-222(9-I-1)	-288(9-II-3)	51(9-II-3)
116	8	0.86(9-I-1)	0.77(9-I-4)	-0.19(9-II-3)	-214(9-I-1)	-224(9-I-4)	89(9-II-3)
117	1	10.65(9-II-4)	2.03(9-II-4)	4.28(9-II-4)	103(10-II-4)	112(10-II-3)	-50(9-II-3)
117	2	-0.10(6)	0.30(10-I-4)	3.01(9-II-4)	270(9-II-4)	189(10-I-3)	107(10-I-3)
117	3	-3.32(9-II-4)	-2.14(9-II-4)	3.10(9-II-4)	226(10-II-2)	437(10-I-4)	272(10-I-4)
117	4	-6.26(9-II-4)	-0.48(9-II-1)	2.20(9-II-4)	276(10-I-4)	681(10-I-4)	554(10-I-4)
117	5	2.74(9-II-4)	0.17(10-I-4)	1.72(9-II-4)	154(10-I-4)	44(10-I-3)	63(10-I-4)
117	6	0.60(9-II-2)	1.13(9-II-4)	4.38(9-II-4)	121(10-I-4)	295(10-I-4)	89(10-I-4)
117	7	-1.83(9-II-4)	2.18(9-II-4)	3.74(9-II-4)	107(10-I-4)	709(10-I-4)	169(10-I-4)
117	8	-2.02(9-II-4)	2.18(9-II-4)	2.26(9-II-4)	109(10-I-4)	1279(10-I-4)	372(10-I-4)
117	9	-2.20(10-I-3)	-0.44(9-II-4)	1.07(9-II-4)	158(10-I-4)	59(10-I-4)	6(6)
117	10	-1.36(6)	0.68(10-I-3)	2.70(9-II-4)	175(10-I-4)	361(10-I-4)	8(6)
117	11	-0.65(6)	1.48(10-I-3)	3.19(9-II-4)	186(10-I-4)	921(10-I-4)	29(6)
117	12	-0.29(10-I-1)	2.11(10-I-3)	2.78(9-II-4)	177(10-I-4)	1634(10-I-4)	190(9-II-1)
117	13	-4.83(9-II-4)	-1.07(9-II-4)	0.50(9-II-4)	-35(9-I-1)	72(10-I-3)	-36(10-I-3)
117	14	-2.40(9-II-4)	1.59(10-I-3)	0.71(9-II-4)	-14(9-I-1)	348(10-I-3)	-14(10-I-4)
117	15	-1.67(10-I-2)	3.28(10-I-3)	1.30(9-II-4)	32(10-I-4)	875(10-I-4)	-48(10-I-4)
117	16	0.35(9-II-3)	4.12(10-I-3)	2.90(9-II-4)	153(10-I-4)	2062(10-I-4)	84(9-II-1)
118	1	-3.07(10-II-4)	-1.65(6)	0.31(10-II-2)	2441(10-I-2)	1016(6)	-528(10-II-2)
118	2	-3.11(10-II-4)	-1.78(6)	0.38(10-II-2)	3629(10-I-2)	1132(6)	-231(10-II-2)
118	3	-3.08(10-II-4)	-2.06(6)	0.48(10-II-2)	4292(10-I-3)	1301(6)	139(6)
118	4	-3.11(10-II-4)	-2.38(6)	0.68(10-I-4)	4709(10-I-3)	1551(6)	356(6)
118	5	-3.02(10-II-4)	-2.76(6)	1.10(10-I-4)	4900(10-I-3)	1592(10-I-3)	455(6)
118	6	-3.00(10-II-4)	-2.33(6)	0.66(10-I-4)	4769(10-I-3)	1539(10-I-3)	416(6)
118	7	-2.95(10-II-1)	-2.05(6)	0.44(10-II-2)	4216(10-I-3)	1193(6)	170(6)
118	8	-3.03(10-II-1)	-1.64(6)	0.29(10-II-2)	2853(10-I-2)	653(6)	-284(10-II-2)
118	9	-3.23(10-II-1)	-1.64(6)	0.35(10-II-2)	754(9-I-3)	-183(10-II-3)	-639(10-I-4)
118	10	-3.86(9-II-3)	-1.72(6)	1.20(10-II-2)	-2816(10-II-3)	-684(10-II-4)	-1210(9-II-3)
118	11	-2.79(9-II-3)	-1.97(6)	1.01(10-II-2)	-3103(10-II-1)	-262(10-II-3)	-1091(10-I-4)
118	12	-2.34(9-II-4)	-2.35(6)	0.48(10-II-2)	-2904(10-II-1)	279(6)	-1082(10-I-4)
118	13	-2.31(6)	-2.68(6)	-0.48(6)	-2172(10-II-3)	932(6)	-1078(10-I-4)
118	14	-2.66(6)	-1.99(6)	0.15(9-II-3)	-607(10-II-2)	909(6)	-1074(10-I-4)
118	15	-2.92(6)	-1.62(6)	0.29(10-II-2)	1118(9-I-3)	897(6)	-843(10-I-4)
118	16	-3.04(10-II-1)	-1.73(6)	0.36(10-II-2)	2530(10-I-2)	867(6)	-394(10-II-2)
118	17	-2.96(10-II-1)	-1.70(6)	0.42(10-II-2)	995(9-I-3)	526(6)	-864(10-I-4)
118	18	-2.83(10-II-1)	-2.01(6)	0.41(10-II-2)	-232(10-II-2)	230(6)	-848(10-I-4)
118	19	-2.81(10-II-4)	-1.97(6)	0.31(10-II-2)	-817(10-II-2)	472(6)	-1027(10-I-4)
119	1	-2.76(6)	-2.31(10-II-1)	0.63(10-I-4)	3275(10-I-2)	2007(10-II-1)	-1012(10-I-4)
119	2	-2.87(6)	-2.61(10-II-2)	0.69(10-I-4)	3876(10-I-2)	1962(10-II-1)	-1116(10-II-2)
119	3	-2.89(6)	-2.95(10-II-2)	0.72(10-I-4)	4170(10-I-2)	1885(10-I-3)	-1056(10-II-2)
119	4	-2.55(6)	-3.57(9-I-1)	1.01(10-I-4)	4512(10-I-3)	1807(10-I-3)	-1103(10-II-3)
119	5	-2.74(6)	-3.03(10-II-2)	0.77(10-I-4)	4274(10-I-3)	1888(10-I-3)	-1072(10-II-2)
119	6	-2.76(6)	-2.61(10-II-2)	0.76(10-I-4)	3867(10-I-2)	1900(9-I-1)	-1158(10-II-2)
119	7	-2.74(6)	-2.32(10-II-2)	0.77(10-I-4)	3185(10-I-2)	1861(9-I-2)	-1092(10-II-2)
119	8	-2.67(6)	-2.10(10-II-1)	0.76(10-I-4)	2038(6)	1779(9-I-2)	-895(10-II-4)
119	9	-2.65(6)	-1.84(10-II-1)	0.63(10-I-4)	766(7)	1817(9-I-2)	-537(10-I-4)
119	10	-2.56(6)	-1.68(10-II-1)	0.36(10-I-4)	-771(10-I-4)	1695(9-I-2)	68(6)
119	11	-2.12(6)	-1.60(10-II-1)	-0.60(9-I-2)	-1851(10-I-4)	2239(9-I-2)	298(10-II-4)
119	12	-2.34(6)	-1.31(10-II-1)	-0.18(7)	-1055(10-I-4)	2275(10-II-1)	156(6)
119	13	-2.48(6)	-1.27(10-II-1)	0.25(10-I-1)	162(7)	1942(10-II-1)	134(10-II-4)
119	14	-2.54(6)	-1.29(6)	0.41(10-II-2)	1680(10-II-4)	1681(10-II-1)	-201(10-I-4)
119	15	-2.64(6)	-1.93(10-II-1)	0.53(10-I-4)	2553(10-II-4)	2033(10-II-1)	-780(10-I-4)
119	16	-2.52(6)	-1.82(10-II-1)	0.54(10-I-4)	1525(9-I-3)	1879(10-II-1)	-558(10-I-4)
119	17	-2.71(6)	-2.15(10-II-1)	0.69(10-I-4)	2691(10-I-2)	1947(10-II-1)	-987(10-II-4)
120	1	-6.11(10-I-2)	-2.02(10-I-3)	1.11(10-II-2)	1813(6)	629(6)	-713(10-II-2)
120	2	-5.94(10-I-2)	-2.37(10-I-3)	1.42(10-II-2)	2089(6)	1015(6)	-530(10-II-2)
120	3	-5.50(10-I-2)	-2.77(10-I-3)	1.41(10-II-2)	2396(10-I-2)	1387(10-I-3)	-667(10-II-2)
120	4	-5.71(10-I-2)	-2.39(10-I-3)	1.25(10-II-2)	2993(9-I-2)	1125(10-I-3)	-917(10-II-2)
120	5	-5.71(9-I-3)	-2.13(10-I-3)	0.89(10-II-2)	3370(10-I-3)	1053(10-I-3)	-770(10-II-2)
120	6	-5.54(9-I-2)	-2.24(10-I-3)	0.45(10-II-3)	3712(10-I-3)	1079(10-I-3)	-487(10-II-2)
120	7	-5.61(9-I-2)	-2.46(10-I-3)	0.21(10-II-3)	3806(10-I-3)	1229(10-I-3)	-198(10-II-3)
120	8	-6.29(10-I-2)	-2.50(10-I-3)	0.36(10-II-3)	3293(10-I-3)	1085(10-I-3)	95(10-I-3)
120	9	-5.95(10-I-2)	-2.26(10-I-3)	0.44(10-II-3)	2952(10-I-3)	858(10-I-3)	483(10-I-3)
120	10	-5.25(6)	-1.48(10-I-3)	0.19(10-II-3)	2037(6)	291(6)	628(10-I-3)
120	11	-4.36(6)	-0.43(10-I-3)	-0.58(10-I-3)	832(6)	-156(10-II-3)	565(10-I-3)
120	12	-5.81(9-I-2)	-0.62(10-I-3)	-0.29(10-I-3)	464(6)	-286(10-II-3)	-365(10-II-3)
120	13	-6.22(10-I-2)	-1.36(10-I-3)	0.57(10-II-3)	1336(6)	456(10-I-3)	-687(10-II-2)
120	14	-5.53(9-I-2)	-1.60(10-I-3)	-0.22(10-I-3)	2329(6)	352(10-I-3)	-71(10-II-3)
120	15	-5.72(9-I-2)	-1.88(10-I-3)	0.23(10-II-3)	2849(10-I-2)	644(10-I-3)	-395(10-II-3)
120	16	-5.61(9-I-2)	-2.09(10-I-3)	-0.13(10-I-3)	3239(10-I-3)	897(10-I-3)	70(6)
121	1	-1.13(10-I-4)	1.06(9-II-4)	1.36(9-II-4)	-69(10-II-3)	-45(9-I-1)	-11(10-I-4)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
121	2	-1.57(10-I-4)	-0.06(10-I-3)	2.28(9-II-4)	29(10-I-3)	-19(10-II-2)	19(6)
121	3	-1.78(9-II-3)	-1.14(9-II-4)	3.00(9-II-4)	45(10-I-3)	44(9-I-4)	60(9-II-4)
121	4	-3.00(9-II-3)	-1.85(9-II-4)	3.48(9-II-4)	197(9-II-3)	46(9-I-4)	264(9-II-4)
121	5	-4.53(9-II-3)	-0.20(10-I-3)	1.77(9-II-4)	17(10-I-3)	260(9-II-4)	26(10-II-1)
121	6	-3.42(9-II-3)	-1.06(9-II-4)	3.44(9-II-4)	24(10-I-3)	100(9-II-1)	-37(9-II-4)
121	7	-2.46(9-II-3)	-1.30(9-II-4)	4.11(9-II-4)	28(10-I-3)	35(9-I-4)	-52(9-II-4)
121	8	-1.18(10-II-2)	-1.71(9-II-4)	3.62(9-II-4)	16(9-I-4)	28(9-I-1)	264(9-II-4)
121	9	-9.23(9-II-3)	-2.22(9-II-4)	1.75(9-II-4)	-121(10-I-4)	329(9-II-4)	116(9-II-4)
121	10	-5.64(9-II-3)	-2.47(9-II-4)	4.02(9-II-4)	-156(9-II-3)	-20(10-I-4)	7(9-I-1)
121	11	-1.76(10-II-2)	-2.40(9-II-4)	3.89(9-II-4)	-169(9-II-3)	-117(10-I-3)	-50(9-II-4)
121	12	1.07(10-I-3)	-2.21(9-II-4)	2.92(9-II-4)	-279(9-II-4)	103(9-I-1)	146(10-II-3)
121	13	-14.87(9-II-4)	-7.09(9-II-4)	2.78(9-II-4)	-1526(9-II-3)	381(9-II-4)	148(9-II-3)
121	14	-4.64(9-II-3)	-3.68(9-II-4)	1.49(9-II-4)	-1371(9-II-4)	-94(10-I-3)	233(9-II-3)
121	15	-0.85(10-II-3)	-1.31(10-II-3)	0.94(9-I-4)	-1115(10-I-3)	-247(10-I-3)	240(9-II-3)
121	16	2.45(10-I-3)	0.98(10-I-3)	1.09(9-II-4)	-1092(9-II-4)	-79(9-II-4)	155(10-II-2)
122	1	-2.65(10-II-2)	-2.79(10-II-1)	-0.93(10-I-2)	1783(10-II-1)	1805(9-II-2)	825(9-II-2)
122	2	-2.71(10-II-2)	-2.82(10-II-1)	-0.95(10-I-2)	2507(10-II-1)	2484(9-II-4)	1274(9-II-4)
122	3	-2.73(10-II-2)	-2.82(10-II-1)	-0.93(10-I-2)	2962(10-II-1)	2895(9-II-4)	1601(9-II-1)
122	4	-2.74(10-II-2)	-2.83(10-II-1)	-0.89(10-I-2)	3245(10-II-1)	3155(10-II-1)	1819(10-II-4)
122	5	-2.73(10-II-2)	-2.84(10-II-1)	-0.84(10-I-2)	3349(10-II-1)	3212(10-II-1)	1924(10-II-4)
122	6	-2.73(10-II-2)	-2.83(10-II-1)	-0.80(10-I-2)	3273(10-II-1)	3097(10-II-1)	1889(6)
122	7	-2.70(10-II-2)	-2.84(10-II-1)	-0.75(10-I-2)	2909(10-II-1)	2728(10-II-4)	1666(6)
122	8	-2.77(10-II-2)	-2.77(10-II-1)	-0.77(10-I-1)	2506(10-II-2)	2283(10-II-4)	1367(6)
122	9	-2.92(10-II-2)	-2.70(10-II-1)	-0.81(10-I-1)	1684(9-I-2)	1704(10-II-4)	912(6)
122	10	-2.43(10-II-2)	-2.79(10-II-1)	-0.67(10-I-1)	1956(9-I-2)	1641(6)	930(6)
122	11	-2.08(10-II-2)	-2.98(10-II-1)	-0.78(10-I-2)	2093(9-I-2)	1660(6)	1024(6)
122	12	-1.95(10-II-2)	-3.07(10-II-1)	-1.12(10-I-2)	1901(9-I-2)	1342(6)	816(6)
122	13	-2.14(10-II-2)	-2.94(10-II-1)	-1.11(10-I-2)	2568(10-II-2)	2008(6)	1382(6)
122	14	-2.27(10-II-2)	-2.79(10-II-1)	-1.08(10-I-2)	3043(10-II-1)	2464(10-II-4)	1654(6)
122	15	-2.40(10-II-2)	-2.69(10-II-1)	-1.01(10-I-2)	3235(10-II-1)	2760(10-II-4)	1826(6)
122	16	-2.51(10-II-2)	-2.62(10-II-4)	-0.94(10-I-2)	3087(10-II-1)	2806(9-II-4)	1810(6)
122	17	-2.58(10-II-2)	-2.60(10-II-4)	-0.86(10-I-2)	2614(10-II-1)	2611(9-II-4)	1651(9-II-1)
122	18	-2.60(10-II-2)	-2.55(10-II-4)	-0.78(10-I-2)	1812(9-II-2)	2094(9-II-3)	1324(9-II-4)
122	19	-2.53(10-II-2)	-2.50(10-II-4)	-0.73(10-I-2)	780(9-II-2)	1143(9-II-3)	805(9-II-2)
122	20	-2.31(10-II-2)	-2.37(10-II-1)	-0.71(10-I-2)	-1043(9-I-1)	-583(10-I-1)	210(9-II-2)
122	21	-2.11(10-I-2)	-1.95(10-II-2)	-0.78(9-II-3)	-4080(9-I-1)	-2757(10-I-2)	-1649(9-I-3)
122	22	-2.37(10-I-2)	-2.59(10-II-1)	-0.85(10-I-2)	-818(9-I-1)	-807(9-I-2)	-555(9-I-2)
122	23	-2.52(10-II-2)	-2.70(10-II-4)	-0.88(10-I-2)	791(9-II-2)	835(9-II-2)	328(9-II-2)
122	24	-2.52(10-II-2)	-2.66(10-II-4)	-0.83(10-I-2)	1428(9-II-2)	1484(9-II-2)	929(9-II-2)
122	25	-2.58(10-II-2)	-2.76(10-II-1)	-0.90(10-I-2)	2257(10-II-1)	2141(9-II-4)	1249(9-II-4)
122	26	-2.55(10-II-2)	-2.66(10-II-4)	-0.86(10-I-2)	2689(10-II-1)	2571(9-II-4)	1643(9-II-4)
122	27	-2.56(10-II-2)	-2.64(10-II-4)	-0.83(10-I-2)	2111(10-II-1)	2146(9-II-4)	1379(9-II-4)
122	28	-2.55(10-II-2)	-2.71(10-II-1)	-0.88(10-I-2)	2605(10-II-1)	2434(9-II-4)	1530(9-II-4)
122	29	-2.60(10-II-2)	-2.80(10-II-1)	-0.93(10-I-2)	2884(10-II-1)	2681(9-II-4)	1582(9-II-4)
122	30	-2.50(10-II-2)	-2.70(10-II-1)	-0.92(10-I-2)	3105(10-II-1)	2787(9-II-4)	1805(6)
122	31	-2.53(10-II-2)	-2.76(10-II-1)	-0.92(10-I-2)	3071(10-II-1)	2769(9-II-4)	1751(9-II-4)
122	32	-2.41(10-II-2)	-2.76(10-II-1)	-0.98(10-I-2)	3281(10-II-1)	2807(10-II-4)	1873(6)
122	33	-2.45(10-II-2)	-2.83(10-II-1)	-0.94(10-I-2)	3305(10-II-1)	2901(10-II-4)	1882(6)
122	34	-2.62(10-II-2)	-2.85(10-II-1)	-0.88(10-I-2)	3322(10-II-1)	3089(10-II-1)	1858(10-II-4)
122	35	-2.52(10-II-2)	-2.86(10-II-1)	-0.91(10-I-2)	3327(10-II-1)	2986(10-II-1)	1869(10-II-4)
122	36	-2.62(10-II-2)	-2.82(10-II-1)	-0.92(10-I-2)	3170(10-II-1)	2929(9-II-4)	1760(9-II-4)
122	37	-2.56(10-II-2)	-2.85(10-II-1)	-0.82(10-I-2)	3080(10-II-1)	2750(10-II-4)	1752(6)
122	38	-2.58(10-II-2)	-2.86(10-II-1)	-0.85(10-I-2)	3334(10-II-1)	3067(10-II-1)	1894(6)
122	39	-2.45(10-II-2)	-2.87(10-II-1)	-0.87(10-I-2)	3305(10-II-1)	2904(10-II-4)	1862(6)
122	40	-2.34(10-II-2)	-2.89(10-II-1)	-0.83(10-I-2)	2935(10-II-1)	2507(10-II-4)	1620(6)
122	41	-2.33(10-II-2)	-2.92(10-II-1)	-0.95(10-I-2)	3146(10-II-1)	2616(10-II-4)	1767(6)
122	42	-2.26(10-II-2)	-2.88(10-II-1)	-1.01(10-I-2)	3073(10-II-1)	2515(10-II-4)	1716(6)
123	1	0.18(9-II-2)	-1.73(10-II-1)	0.46(10-I-4)	1494(6)	1581(10-II-1)	-650(10-II-1)
123	2	-0.73(9-I-2)	-1.63(10-II-1)	0.56(10-I-4)	480(6)	1856(10-II-1)	-636(10-II-2)
123	3	-1.23(9-I-2)	-1.53(10-II-1)	0.67(9-I-1)	-783(9-II-1)	2289(10-II-1)	-412(6)
123	4	-1.84(9-I-2)	-1.30(10-II-1)	0.86(9-I-1)	-1574(9-II-1)	3157(10-II-1)	489(9-II-2)
123	5	-0.57(9-I-2)	-1.82(10-II-1)	-0.12(6)	-1237(9-II-1)	1039(10-II-1)	-1534(10-II-2)
123	6	-0.86(9-I-2)	-1.53(10-II-1)	0.31(10-I-4)	-1359(9-II-1)	1859(10-II-1)	-1553(10-II-2)
123	7	-1.31(9-I-2)	-1.27(10-II-1)	0.39(10-I-4)	-1720(9-II-2)	2859(10-II-1)	-1551(9-I-1)
123	8	-1.57(9-I-2)	-0.97(10-II-1)	0.28(10-I-4)	-2045(9-II-2)	4190(10-II-1)	-1748(10-I-4)
123	9	-0.74(9-I-2)	-1.62(10-II-1)	-0.27(9-II-1)	-3075(9-II-2)	547(10-II-1)	-1600(10-II-2)
123	10	-1.00(9-I-2)	-1.44(10-II-1)	-0.14(9-II-1)	-2912(9-II-2)	1610(10-II-1)	-1852(9-I-1)
123	11	-1.26(9-I-2)	-1.23(10-II-1)	-0.07(10-II-4)	-2763(9-II-2)	2786(10-II-1)	-1986(9-I-1)
123	12	-1.52(9-I-2)	-0.98(10-II-1)	0.07(10-I-4)	-2624(9-II-2)	3904(10-II-1)	-2102(9-I-1)
123	13	-0.91(9-I-2)	-1.19(10-II-1)	-0.34(9-II-1)	-5708(9-II-2)	-735(10-I-1)	-1042(9-I-1)
123	14	-1.00(9-I-2)	-1.43(10-II-1)	-0.28(9-II-1)	-4759(9-II-2)	1110(10-II-1)	-1411(9-I-1)
123	15	-1.25(9-I-2)	-1.37(10-II-1)	-0.28(10-I-4)	-3955(10-I-1)	2232(10-II-1)	-1693(9-I-1)
123	16	-1.48(9-I-2)	-1.26(10-II-1)	-0.31(10-II-4)	-3248(10-I-1)	3530(10-II-1)	-2151(9-I-1)
124	1	-2.47(10-II-1)	-1.70(10-II-1)	-0.55(9-II-4)	-2880(9-II-2)	1120(9-I-2)	-1518(10-II-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
124	2	-2.48(10-II-1)	-1.65(10-II-1)	-0.38(9-II-4)	-2956(9-II-2)	1484(9-I-2)	-1563(9-I-1)
124	3	-2.43(10-II-1)	-1.61(10-II-1)	-0.30(9-II-4)	-2864(9-II-2)	2117(10-II-1)	-1525(9-I-1)
124	4	-2.28(10-II-1)	-1.61(10-II-1)	-0.23(9-II-1)	-2685(9-II-2)	3051(10-II-1)	-1238(10-I-4)
124	5	-2.99(10-II-1)	-1.77(10-II-1)	-0.62(9-II-4)	-5954(9-II-2)	903(9-I-2)	-1950(9-I-1)
124	6	-2.63(10-II-1)	-1.73(10-II-1)	-0.50(9-II-4)	-4970(9-II-2)	1219(9-I-2)	-1987(9-I-1)
124	7	-2.43(10-II-1)	-1.62(10-II-1)	-0.52(9-II-4)	-4069(9-II-2)	1773(10-II-1)	-2151(9-I-1)
124	8	-2.37(10-II-1)	-1.28(10-II-1)	-0.70(9-I-4)	-3178(9-II-2)	2700(10-II-1)	-2448(9-I-1)
125	1	-6.00(9-I-2)	-2.49(10-I-3)	-0.91(9-I-3)	3065(10-II-1)	1115(6)	539(6)
125	2	-6.22(9-I-2)	-2.31(6)	-0.66(6)	2852(10-II-1)	1001(6)	411(6)
125	3	-6.27(10-I-3)	-2.29(6)	-0.28(6)	2686(10-II-1)	1008(6)	93(6)
125	4	-6.10(9-I-2)	-2.44(6)	-0.59(6)	2395(9-I-2)	990(6)	359(6)
125	5	-5.85(9-I-2)	-2.76(10-I-3)	-0.77(6)	2029(9-I-2)	1148(6)	562(6)
125	6	-5.38(9-I-3)	-2.82(10-I-3)	-0.86(6)	1448(9-I-2)	1199(10-I-3)	589(9-I-3)
125	7	-4.44(9-I-3)	-2.38(10-I-3)	-0.71(9-I-3)	694(9-I-2)	1101(10-I-3)	650(9-I-3)
125	8	-1.98(9-I-3)	-1.98(10-I-4)	-0.77(9-I-2)	-422(9-II-3)	538(10-I-4)	-228(10-II-3)
125	9	-3.77(9-I-3)	-3.09(10-I-3)	-1.48(9-I-3)	1789(9-I-3)	819(10-I-3)	289(10-I-3)
125	10	-5.20(9-I-3)	-3.30(10-I-3)	-1.58(10-I-2)	2479(9-I-3)	1182(10-I-3)	412(10-I-2)
125	11	-5.76(9-I-3)	-3.38(10-I-3)	-1.56(10-I-2)	2814(9-I-3)	1373(10-I-3)	617(6)
125	12	-5.41(9-I-2)	-3.26(10-I-3)	-1.26(10-I-2)	3154(10-II-2)	1572(10-I-3)	736(6)
125	13	-5.61(9-I-2)	-2.81(10-I-3)	-1.06(10-I-2)	3190(10-II-1)	1391(10-I-3)	646(6)
125	14	-5.66(9-I-2)	-2.76(10-I-3)	-0.90(9-I-3)	2959(9-I-3)	1325(10-I-3)	659(6)
125	15	-5.11(9-I-2)	-2.97(10-I-3)	-0.82(9-I-3)	2824(9-I-3)	1522(10-I-3)	603(6)
126	1	-3.26(10-I-3)	-3.14(9-I-2)	-0.79(10-II-4)	1116(9-I-3)	1735(10-I-3)	515(10-II-4)
126	2	-1.95(10-II-4)	-1.84(9-I-2)	0.29(9-II-3)	467(10-II-4)	476(9-I-2)	-386(9-II-3)
126	3	-2.78(10-I-2)	-3.87(10-I-3)	-1.02(10-I-4)	1316(10-I-3)	399(9-I-4)	104(10-II-4)
126	4	-3.09(10-I-3)	-4.68(10-I-3)	-0.83(10-II-4)	1264(10-I-3)	805(10-I-3)	247(10-II-4)
126	5	-2.78(10-I-2)	-4.47(10-I-3)	-1.03(10-II-4)	1168(10-I-2)	1446(10-I-3)	550(10-II-4)
126	6	-3.02(10-I-3)	-4.59(10-I-3)	-0.90(10-II-4)	1693(10-I-3)	2299(10-I-3)	591(10-II-4)
126	7	-3.21(10-I-3)	-5.00(10-I-3)	-0.75(10-II-4)	1755(10-I-3)	2537(10-I-3)	680(10-II-4)
126	8	-3.48(10-I-3)	-5.57(10-I-3)	-1.36(10-II-4)	1570(10-I-3)	2781(10-I-3)	691(10-II-3)
126	9	-3.70(10-I-3)	-4.40(10-I-3)	-1.46(10-II-4)	1395(10-I-3)	2278(10-I-3)	515(10-II-4)
127	1	-5.64(10-I-3)	-2.51(10-I-3)	-0.71(10-I-4)	2257(10-I-3)	-106(10-II-1)	122(9-I-1)
127	2	-5.65(10-I-3)	-2.64(10-I-3)	-0.58(10-I-4)	2259(10-I-3)	-147(10-II-1)	148(9-I-1)
127	3	-5.59(10-I-3)	-2.72(10-I-3)	-0.46(10-I-4)	2250(10-I-3)	-159(10-II-4)	197(9-I-1)
127	4	-5.47(10-I-3)	-2.79(10-I-3)	-0.35(10-I-4)	2202(10-I-3)	-176(10-II-4)	255(9-I-1)
127	5	-5.33(10-I-3)	-2.81(10-I-3)	-0.22(10-I-4)	2122(10-I-3)	-235(10-II-4)	328(9-I-1)
127	6	-5.13(10-I-3)	-2.83(10-I-3)	-0.11(10-I-4)	2006(10-I-4)	-259(9-I-3)	420(9-I-4)
127	7	-4.87(10-I-4)	-2.83(10-I-3)	0.11(10-II-4)	1872(10-I-4)	-212(9-I-3)	461(9-I-4)
127	8	-4.70(10-I-4)	-2.77(10-I-3)	-0.12(9-I-1)	1727(10-I-4)	-73(10-II-4)	391(9-I-1)
127	9	-4.63(10-I-4)	-2.76(10-I-3)	-0.19(9-I-1)	1682(10-I-4)	475(10-I-3)	338(9-I-1)
127	10	-4.32(10-I-4)	-2.76(10-I-3)	-0.20(9-I-1)	1746(6)	636(10-I-3)	364(9-I-1)
127	11	-3.97(10-I-4)	-2.59(10-I-3)	-0.43(9-I-1)	1364(6)	1228(10-I-3)	309(9-I-2)
127	12	-4.87(10-I-3)	-2.82(10-I-3)	-0.58(9-I-1)	1849(6)	1761(10-I-3)	334(9-I-1)
127	13	-5.46(10-I-3)	-3.06(10-I-3)	-0.77(10-I-3)	2335(6)	1732(10-I-3)	426(10-I-3)
127	14	-6.10(10-I-3)	-3.01(10-I-3)	-1.07(10-I-3)	2615(10-I-3)	1527(10-I-3)	423(10-I-3)
127	15	-5.83(10-I-3)	-2.94(10-I-3)	-0.93(10-I-3)	2600(9-I-2)	1634(10-I-3)	285(10-I-4)
127	16	-5.72(10-I-3)	-2.51(10-I-3)	-0.87(10-I-3)	2357(9-I-3)	1343(10-I-3)	122(10-I-4)
127	17	-5.47(10-I-2)	-1.98(10-I-3)	-0.70(10-I-4)	2127(9-I-3)	859(10-I-3)	107(10-I-4)
127	18	-5.58(10-I-3)	-2.33(10-I-3)	-0.73(10-I-4)	2192(9-I-3)	341(10-I-3)	121(10-I-4)
127	19	-5.61(10-I-3)	-2.41(10-I-3)	-0.77(10-I-4)	2235(10-I-3)	44(10-I-1)	108(10-I-4)
127	20	-5.54(10-I-3)	-2.73(10-I-3)	-0.58(10-I-4)	2350(10-I-3)	284(10-I-4)	184(10-I-4)
127	21	-5.46(10-I-3)	-2.79(10-I-3)	-0.58(10-I-4)	2413(10-I-3)	549(10-I-3)	199(10-I-4)
127	22	-5.53(10-I-3)	-2.91(10-I-3)	-0.84(10-I-3)	2581(10-I-3)	1447(10-I-3)	284(10-I-4)
127	23	-5.46(10-I-3)	-2.80(10-I-3)	-0.64(10-I-4)	2464(10-I-3)	844(10-I-3)	198(10-I-4)
127	24	-5.53(10-I-3)	-2.73(10-I-3)	-0.70(10-I-4)	2471(10-I-3)	1023(10-I-3)	189(10-I-4)
127	25	-5.56(10-I-3)	-2.65(10-I-3)	-0.64(10-I-4)	2368(10-I-3)	427(10-I-3)	191(10-I-4)
127	26	-5.53(10-I-3)	-2.48(10-I-3)	-0.76(10-I-4)	2348(9-I-3)	557(10-I-3)	194(10-I-4)
127	27	-5.49(10-I-3)	-2.78(10-I-3)	-0.51(10-I-4)	2343(10-I-3)	270(10-I-4)	202(10-I-4)
127	28	-5.01(10-I-3)	-2.86(10-I-3)	-0.22(9-I-1)	2081(10-I-4)	107(10-I-4)	308(9-I-1)
127	29	-4.88(10-I-4)	-2.90(10-I-3)	-0.31(9-I-1)	2070(10-I-4)	575(10-I-3)	339(9-I-1)
127	30	-5.06(10-I-3)	-2.87(10-I-3)	-0.38(9-I-1)	2276(10-I-3)	760(10-I-3)	256(9-I-1)
127	31	-5.36(10-I-3)	-2.93(10-I-3)	-0.66(10-I-4)	2499(10-I-3)	1243(10-I-3)	274(10-I-4)
127	32	-5.09(10-I-3)	-2.98(10-I-3)	-0.52(10-I-4)	2356(10-I-3)	1048(10-I-3)	248(10-I-4)
127	33	-5.26(10-I-3)	-3.02(10-I-3)	-0.69(10-I-4)	2429(10-I-3)	1426(10-I-3)	295(10-I-4)
127	34	-5.18(10-I-3)	-2.93(10-I-3)	-0.36(10-I-4)	2278(10-I-3)	525(10-I-3)	246(9-I-1)
127	35	-5.24(10-I-3)	-2.89(10-I-3)	-0.31(10-I-4)	2197(10-I-3)	152(10-I-4)	264(9-I-1)
127	36	-5.09(10-I-3)	-2.86(10-I-3)	-0.29(10-I-4)	2149(10-I-4)	260(10-I-4)	274(9-I-1)
127	37	-5.30(10-I-3)	-2.88(10-I-3)	-0.46(10-I-4)	2326(10-I-3)	580(10-I-3)	230(9-I-1)
127	38	-5.39(10-I-3)	-2.86(10-I-3)	-0.47(10-I-4)	2341(10-I-3)	425(10-I-3)	221(10-I-4)
127	39	-5.36(10-I-3)	-2.86(10-I-3)	-0.40(10-I-4)	2277(10-I-3)	245(10-I-4)	230(9-I-1)
127	40	-5.39(10-I-3)	-2.86(10-I-3)	-0.60(10-I-4)	2462(10-I-3)	975(10-I-3)	246(10-I-4)
127	41	-5.39(10-I-3)	-2.86(10-I-3)	-0.54(10-I-4)	2409(10-I-3)	680(10-I-3)	230(10-I-4)
127	42	-5.28(10-I-3)	-2.92(10-I-3)	-0.52(10-I-4)	2378(10-I-3)	811(10-I-3)	239(10-I-4)
128	1	-5.20(10-I-3)	-2.80(6)	1.34(9-I-2)	2295(10-I-3)	572(6)	-458(9-I-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
128	2	-5.32(10-I-3)	-2.26(6)	2.19(9-I-2)	1938(6)	588(6)	-822(9-I-2)
128	3	-4.79(10-I-3)	-3.06(6)	2.20(9-I-2)	1610(10-I-3)	1250(6)	-757(9-I-2)
128	4	-4.49(10-I-3)	-4.18(6)	2.18(9-I-2)	1778(10-I-3)	2000(9-I-2)	-806(10-I-2)
128	5	-3.98(10-I-3)	-5.08(10-I-2)	1.82(10-I-2)	1745(10-I-3)	2428(10-I-2)	-832(10-I-3)
128	6	-4.36(10-I-3)	-4.22(6)	1.21(9-I-1)	2134(10-I-3)	2212(10-I-3)	-780(10-I-3)
128	7	-4.43(10-I-3)	-3.60(6)	0.89(9-I-1)	1836(10-I-3)	1759(10-I-4)	-496(9-I-1)
128	8	-3.95(10-I-3)	-3.10(6)	0.57(9-I-1)	1387(10-I-3)	1072(6)	-301(9-I-1)
128	9	-4.84(10-I-3)	-3.15(6)	0.70(9-I-2)	2095(10-I-3)	689(6)	-356(9-I-2)
128	10	-4.53(10-I-3)	-3.48(6)	1.20(9-I-1)	2344(10-I-3)	1447(6)	-492(9-I-1)
128	11	-4.71(10-I-3)	-3.34(6)	1.55(9-I-2)	2336(10-I-3)	1296(6)	-632(9-I-2)
128	12	-4.42(10-I-3)	-3.82(6)	1.55(9-I-1)	2271(10-I-3)	1761(6)	-723(9-I-1)
129	1	-1.64(10-II-1)	-2.06(9-I-2)	0.35(6)	2145(10-II-1)	-1462(6)	2047(10-II-2)
129	2	-1.53(10-II-1)	-2.09(9-I-2)	0.33(6)	1909(10-II-1)	-1221(6)	2075(10-II-2)
129	3	-1.28(10-II-1)	-2.02(9-I-2)	0.37(6)	2944(10-II-1)	-1804(10-II-2)	2735(10-II-2)
129	4	-1.11(10-II-1)	-1.92(9-I-2)	0.42(6)	3529(10-II-1)	-1937(10-II-2)	2427(10-II-2)
129	5	-1.14(10-II-1)	-1.69(9-I-2)	0.44(6)	3932(10-II-1)	-2621(10-I-3)	2006(9-I-1)
129	6	-1.25(10-II-1)	-1.82(9-I-2)	0.38(6)	3328(10-II-1)	-1963(10-II-2)	2185(9-I-1)
129	7	-1.42(10-II-1)	-1.94(9-I-2)	0.37(6)	2805(10-II-1)	-1631(10-II-2)	2296(10-II-2)
129	8	-1.70(10-II-1)	-1.99(9-I-2)	0.38(9-I-1)	2199(10-II-1)	-1548(10-II-1)	2012(10-II-2)
129	9	-1.69(10-II-1)	-2.06(9-I-2)	0.35(6)	2235(10-II-1)	-1541(10-II-2)	2037(10-II-2)
129	10	-1.51(10-II-1)	-2.01(9-I-2)	0.35(6)	2657(10-II-1)	-1657(10-II-2)	2501(10-II-2)
130	1	-1.73(6)	-1.00(10-II-1)	0.44(10-I-1)	-2921(10-I-4)	5212(10-II-1)	1846(9-I-2)
130	2	-1.72(6)	-1.02(10-II-1)	0.33(10-I-4)	-2897(10-I-4)	4778(10-II-1)	1982(10-II-1)
130	3	-1.88(6)	-1.13(10-II-1)	0.34(10-I-1)	-2841(10-I-4)	4574(10-II-1)	1493(10-II-1)
130	4	-1.97(6)	-1.32(10-II-1)	0.36(10-I-1)	-3242(10-II-2)	4491(10-II-1)	947(10-II-1)
130	5	-2.17(6)	-1.33(10-II-1)	0.40(10-I-1)	-2563(10-II-2)	3535(10-II-1)	-238(9-I-2)
130	6	-1.77(6)	-1.48(10-II-1)	0.39(10-I-1)	-3508(10-II-2)	4006(10-II-1)	220(9-I-2)
130	7	-1.58(6)	-1.53(10-II-1)	0.35(10-I-1)	-3662(10-II-2)	4328(9-I-1)	617(9-I-1)
130	8	-1.49(6)	-1.34(10-II-1)	0.36(10-I-1)	-3033(10-II-3)	6921(9-I-2)	1429(6)
130	9	-1.66(6)	-0.95(10-II-1)	0.42(10-I-1)	-3151(10-II-4)	5703(10-II-1)	1901(10-II-1)
130	10	-1.79(6)	-1.14(10-II-1)	0.38(10-I-1)	-3119(10-I-4)	5082(10-II-1)	1542(10-II-1)
130	11	-1.80(6)	-1.34(10-II-1)	0.39(10-I-1)	-3550(10-II-2)	4914(10-II-1)	1059(10-II-1)
130	12	-1.70(6)	-1.27(10-II-1)	0.38(10-I-1)	-3527(10-II-2)	5369(10-II-1)	1397(10-II-1)
131	1	-1.77(6)	-0.59(10-II-1)	0.17(10-I-4)	-2741(9-II-2)	5515(10-II-1)	-2430(10-I-4)
131	2	-1.80(9-I-2)	-0.57(10-II-1)	0.23(10-II-2)	-2295(9-II-2)	5464(10-II-1)	-1992(10-I-4)
131	3	-1.86(9-I-2)	-0.42(10-II-1)	0.55(10-II-2)	-1828(9-II-1)	6242(10-II-1)	-573(10-I-4)
131	4	-1.82(9-I-2)	-0.64(10-II-1)	0.19(10-I-4)	-2321(9-II-2)	4851(10-II-1)	-2022(10-I-4)
131	5	-1.78(9-I-2)	-0.77(10-II-1)	0.06(10-I-4)	-2561(9-II-2)	4830(10-II-1)	-2308(10-I-4)
131	6	-1.86(9-I-2)	-0.67(6)	-0.24(10-II-4)	-2668(10-I-1)	4885(10-II-1)	-2488(9-I-1)
131	7	-1.85(9-I-2)	-0.62(10-II-1)	-0.16(6)	-2442(9-II-2)	5108(10-II-1)	-2669(9-I-1)
131	8	-1.81(6)	-0.61(10-II-1)	-0.20(6)	-2393(9-II-2)	5540(10-II-1)	-2998(9-I-1)
131	9	-1.39(6)	-0.87(10-II-1)	-0.35(6)	-1719(9-II-2)	6615(10-I-1)	-2729(9-I-1)
131	10	-1.83(6)	-0.35(10-II-1)	-0.26(6)	-2201(9-II-2)	5755(10-II-1)	-2916(9-I-1)
131	11	-1.75(6)	-0.61(10-II-1)	0.10(10-I-4)	-2691(9-II-2)	5620(10-II-1)	-2820(10-I-4)
131	12	-1.77(9-I-2)	-0.64(10-II-1)	-0.07(6)	-2574(9-II-2)	5363(10-II-1)	-2574(10-I-4)
132	1	-0.97(6)	-1.21(9-I-1)	0.75(10-I-1)	-1448(10-I-4)	3894(9-I-1)	4350(9-II-2)
132	2	-0.98(6)	-1.29(10-I-4)	0.74(6)	-1387(10-I-4)	4749(9-I-1)	3975(9-II-2)
132	3	-0.90(6)	-0.36(10-I-1)	0.55(6)	-672(9-II-3)	5622(9-I-1)	3352(10-II-1)
132	4	-1.22(10-II-2)	-1.73(9-I-1)	0.49(6)	-3362(9-II-3)	5183(9-I-1)	3213(10-II-1)
132	5	-1.13(6)	-1.16(9-I-1)	0.48(10-I-1)	-1561(10-I-4)	3364(9-I-1)	4554(9-II-2)
132	6	-1.21(6)	-1.44(10-II-2)	0.90(10-I-1)	-551(10-I-1)	3339(9-I-1)	4485(9-II-2)
132	7	-0.35(6)	-1.03(10-II-2)	1.40(10-II-2)	3393(10-II-1)	3905(9-I-1)	5211(9-II-3)
132	8	-1.21(6)	-1.02(10-II-2)	0.74(10-I-1)	497(10-II-1)	3226(9-I-1)	4084(9-II-2)
132	9	-1.07(6)	-1.02(10-II-2)	0.57(10-I-1)	-965(10-I-1)	3854(9-I-1)	4146(9-II-2)
132	10	-1.12(6)	-1.42(10-II-2)	0.61(10-I-1)	-583(10-I-1)	3556(9-I-1)	4045(9-II-2)
133	1	-1.02(10-II-1)	-1.71(6)	0.86(9-II-1)	4890(10-II-1)	-1799(9-II-2)	2529(10-I-4)
133	2	0.14(9-II-3)	-1.61(6)	1.24(9-I-1)	7044(10-II-1)	-1287(9-II-2)	3580(9-I-1)
133	3	-0.69(6)	-1.83(10-II-2)	0.62(9-II-1)	5130(10-II-1)	-2324(9-II-2)	2637(10-I-4)
133	4	-0.94(10-II-1)	-1.58(6)	0.59(9-II-1)	4690(10-II-1)	-2721(9-II-2)	2826(10-I-4)
133	5	-1.14(10-II-1)	-1.46(6)	0.58(9-II-4)	1703(10-II-1)	-4597(9-II-2)	4823(10-I-4)
133	6	-1.18(10-II-1)	-1.42(6)	0.86(9-II-4)	3767(10-II-1)	-2118(9-II-2)	2245(10-I-4)
133	7	-1.16(10-II-1)	-1.56(6)	0.90(9-II-4)	3583(10-II-1)	-1557(9-II-2)	1879(10-I-4)
133	8	-1.05(10-II-1)	-2.00(6)	0.75(9-II-4)	3108(10-II-1)	452(9-I-2)	1448(10-I-4)
133	9	-1.17(10-II-1)	-1.80(6)	0.86(9-II-4)	4174(10-II-1)	-1691(9-II-2)	1763(10-I-4)
134	1	-2.20(10-II-1)	-1.43(10-II-1)	-0.23(9-II-1)	-2233(9-II-2)	3721(10-II-1)	-686(10-I-4)
134	2	-2.23(10-II-1)	-1.46(10-II-1)	-0.24(9-II-1)	-2509(9-II-2)	3374(10-II-1)	-900(10-I-4)
134	3	-2.00(6)	-1.19(10-II-1)	-0.54(9-I-1)	-2258(9-II-2)	5544(10-II-1)	-2257(9-I-1)
134	4	-2.12(6)	-1.11(10-II-1)	-0.50(9-II-1)	-2102(9-II-2)	4388(10-II-1)	-1329(10-I-4)
134	5	-2.08(6)	-1.20(10-II-1)	-0.33(9-II-1)	-1941(9-II-2)	4097(10-II-1)	-886(10-I-4)
134	6	-2.30(6)	-1.05(10-II-1)	-0.20(9-II-1)	-1255(9-II-2)	3861(10-II-1)	-801(10-I-4)
134	7	-2.25(6)	-1.24(10-II-1)	-0.24(9-II-1)	-1753(9-II-2)	3911(10-II-1)	-465(10-I-4)
135	1	-3.05(9-II-3)	-0.34(9-II-3)	-1.39(9-II-3)	346(6)	4688(10-II-1)	-2764(10-I-4)
135	2	-1.18(9-II-4)	-0.37(9-II-3)	-1.50(9-II-3)	1082(6)	3360(6)	-2520(10-I-4)
135	3	-1.15(9-II-4)	-0.05(9-II-2)	-1.54(9-II-3)	777(6)	1821(6)	-2615(10-I-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
135	4	-1.50(9-II-4)	-0.24(9-II-2)	-0.98(9-I-1)	448(6)	-598(10-I-1)	-3018(9-II-3)
135	5	-0.98(9-II-1)	-0.10(10-II-3)	-1.02(9-I-1)	505(9-I-2)	5141(10-II-1)	-1978(10-I-4)
135	6	-1.00(9-II-4)	-0.16(9-II-2)	-1.42(9-II-3)	1086(9-I-2)	3113(6)	-2697(10-I-4)
135	7	-1.47(9-II-4)	-0.63(9-II-3)	-1.38(9-II-3)	1455(9-I-2)	1280(6)	-3127(9-II-3)
135	8	-2.98(9-II-4)	-1.08(9-II-3)	-1.85(9-II-3)	690(9-I-2)	-1518(10-I-1)	-2913(9-II-3)
136	1	-1.76(10-I-4)	-4.28(9-I-3)	1.19(9-II-3)	-326(10-II-2)	598(9-I-3)	341(6)
136	2	-1.86(6)	-4.49(9-I-3)	1.02(9-II-3)	170(10-I-2)	901(9-I-3)	320(6)
136	3	-2.22(10-I-2)	-4.49(10-I-2)	0.66(9-II-3)	615(10-I-2)	1130(9-I-3)	352(6)
136	4	-2.75(10-I-2)	-4.28(10-I-3)	0.24(9-II-3)	1026(10-I-2)	1357(9-I-3)	397(6)
136	5	-3.27(10-I-2)	-4.07(10-I-3)	-0.60(6)	1293(10-I-2)	1444(10-I-3)	443(6)
136	6	-3.85(10-I-2)	-3.65(10-I-3)	-1.00(6)	1612(10-I-2)	1637(10-I-3)	486(6)
136	7	-3.57(10-I-2)	-3.62(10-I-3)	-0.30(6)	1541(10-I-2)	2158(10-I-3)	204(6)
136	8	-3.38(10-I-2)	-3.58(10-I-3)	0.58(9-II-3)	1522(10-I-2)	2364(10-I-3)	-273(9-II-3)
136	9	-3.26(10-I-2)	-3.61(9-I-2)	1.08(9-II-3)	1509(10-I-2)	2443(10-I-3)	-563(9-II-3)
136	10	-2.95(10-I-3)	-3.84(9-I-2)	1.41(9-II-2)	1330(10-I-3)	2232(10-I-3)	-735(9-II-3)
136	11	-2.49(10-I-3)	-4.39(10-I-3)	1.49(10-I-3)	1066(10-I-3)	2079(6)	-833(9-II-3)
136	12	-1.84(6)	-4.90(10-I-3)	1.51(10-I-3)	966(10-I-3)	1918(6)	-783(10-I-3)
136	13	-1.30(6)	-5.29(6)	1.51(10-I-3)	375(6)	2051(6)	-643(10-I-3)
136	14	-1.96(10-I-3)	-5.10(10-I-3)	1.16(10-I-3)	977(6)	2400(10-I-3)	-632(10-I-3)
136	15	-1.98(10-I-3)	-4.66(10-I-3)	0.82(10-I-3)	1336(9-II-3)	1989(9-I-2)	-626(10-I-3)
136	16	-1.92(9-II-3)	-3.76(9-I-2)	0.63(10-I-1)	1026(9-II-3)	1139(9-I-2)	-139(10-I-2)
136	17	-1.95(10-I-4)	-3.99(9-I-2)	1.12(9-II-3)	180(10-I-4)	699(9-I-2)	93(10-II-1)
136	18	-2.46(10-I-3)	-4.20(10-I-3)	1.13(9-II-3)	1216(10-I-3)	2226(10-I-3)	-885(9-II-3)
136	19	-2.25(10-I-3)	-4.27(10-I-3)	1.01(9-II-3)	1078(10-I-3)	2035(9-I-3)	-806(10-I-4)
136	20	-2.44(10-I-3)	-4.11(10-I-2)	1.04(9-II-3)	970(10-I-3)	2013(9-I-3)	-710(9-II-3)
136	21	-2.02(10-I-3)	-4.20(9-I-3)	1.01(9-II-3)	429(10-I-3)	1520(9-I-3)	-418(9-II-3)
136	22	-2.27(10-I-3)	-4.20(10-I-2)	0.96(9-II-3)	582(10-I-2)	1675(9-I-3)	-405(9-II-3)
136	23	-2.81(10-I-3)	-3.91(10-I-3)	1.13(9-II-3)	1302(10-I-3)	2260(10-I-3)	-799(9-II-3)
136	24	-2.69(10-I-3)	-3.98(10-I-2)	0.99(9-II-3)	1091(10-I-2)	2112(10-I-2)	-641(9-II-3)
136	25	-2.97(10-I-3)	-3.85(10-I-2)	0.97(9-II-3)	1322(10-I-2)	2267(10-I-3)	-605(9-II-3)
136	26	-2.54(10-I-3)	-4.13(10-I-2)	0.83(9-II-3)	827(10-I-2)	1813(9-I-3)	-305(9-II-3)
136	27	-3.01(10-I-2)	-3.92(10-I-2)	0.64(9-II-3)	1211(10-I-2)	2053(10-I-3)	-246(9-II-3)
137	1	-3.01(10-II-2)	-3.28(6)	-1.70(10-I-4)	1281(10-II-2)	828(6)	103(10-I-4)
137	2	-3.27(10-II-2)	-3.44(10-II-4)	-1.40(10-I-1)	1678(10-II-2)	1523(6)	188(10-I-1)
137	3	-3.41(10-II-2)	-3.42(10-II-4)	-1.04(10-I-1)	1807(10-II-2)	2176(6)	368(10-I-1)
137	4	-3.19(10-II-2)	-3.36(10-II-4)	-0.76(10-I-1)	2248(10-I-4)	2642(6)	711(10-I-4)
137	5	-2.81(10-II-2)	-3.58(6)	-0.67(10-I-1)	2479(10-II-2)	2845(6)	1092(10-I-1)
137	6	-2.52(10-II-2)	-3.65(6)	-0.65(10-I-1)	2610(10-II-2)	2885(10-II-4)	1258(10-I-1)
137	7	-2.21(10-II-2)	-3.63(6)	-0.66(10-I-1)	2648(10-II-2)	2692(10-II-4)	1312(10-I-1)
137	8	-1.86(10-II-2)	-3.47(6)	-0.67(10-I-1)	2553(10-II-2)	2291(10-II-4)	1238(10-I-1)
137	9	-1.60(10-II-2)	-3.28(6)	-0.76(10-I-1)	2371(10-I-4)	1481(9-II-1)	1072(10-I-1)
137	10	-1.85(10-II-2)	-3.67(6)	-0.70(10-I-1)	2505(10-I-4)	2112(10-II-4)	1261(10-I-1)
137	11	-2.10(10-II-2)	-3.91(6)	-0.78(10-I-1)	2505(10-II-2)	2499(10-II-4)	1343(10-I-1)
137	12	-2.41(10-II-2)	-4.10(6)	-0.98(10-I-1)	2319(10-II-2)	2579(10-II-4)	1364(10-I-1)
137	13	-2.68(10-II-2)	-4.09(10-II-4)	-1.23(10-I-1)	2048(10-II-2)	2404(10-I-4)	1329(10-I-1)
137	14	-2.89(10-II-2)	-3.80(9-I-3)	-1.43(10-I-1)	1767(10-II-2)	2068(9-I-3)	1220(10-I-4)
137	15	-2.99(10-II-1)	-3.30(9-I-3)	-1.50(10-I-4)	1448(10-II-1)	1452(9-I-3)	1017(10-I-4)
137	16	-2.81(10-II-1)	-2.55(9-I-3)	-1.41(10-I-4)	1090(10-II-1)	733(9-I-3)	729(10-I-4)
137	17	-2.19(10-II-1)	-1.58(9-I-3)	-1.07(10-I-4)	345(10-II-1)	-157(10-I-4)	331(10-I-4)
137	18	1.58(10-I-4)	-0.68(9-I-1)	-0.46(10-I-4)	-1139(10-I-4)	-975(10-II-2)	-962(9-II-1)
137	19	-1.76(10-II-1)	-1.90(9-I-3)	-1.48(10-I-4)	739(10-II-1)	-892(10-I-4)	-747(9-II-1)
137	20	-2.53(10-II-1)	-2.82(6)	-1.81(10-I-4)	1253(10-II-1)	264(9-I-3)	-195(9-II-1)
137	21	-2.84(10-II-2)	-3.73(10-II-4)	-1.28(10-I-1)	1895(10-II-2)	2076(9-I-3)	1040(10-I-4)
137	22	-2.87(10-II-2)	-3.50(6)	-1.43(10-I-1)	1638(10-II-2)	1533(9-I-3)	802(10-I-4)
137	23	-2.97(10-II-2)	-3.63(10-II-4)	-1.26(10-I-1)	1884(10-II-2)	1911(6)	811(10-I-4)
137	24	-2.58(10-II-2)	-3.82(6)	-0.83(10-I-1)	2408(10-II-2)	2727(10-II-4)	1239(10-I-1)
137	25	-2.73(10-II-2)	-3.88(10-II-4)	-1.07(10-I-1)	2139(10-II-2)	2449(6)	1148(10-I-4)
137	26	-2.79(10-II-2)	-3.67(10-II-4)	-0.83(10-I-1)	2353(10-II-2)	2674(6)	1063(10-I-1)
137	27	-2.89(10-II-2)	-3.69(10-II-4)	-1.04(10-I-1)	2122(10-II-2)	2370(6)	943(10-I-4)
137	28	-3.06(10-II-2)	-3.55(10-II-4)	-0.93(10-I-1)	2218(10-II-2)	2385(6)	806(10-I-1)
138	1	-3.44(10-II-4)	-2.52(10-II-1)	-0.50(6)	4068(10-I-3)	1698(10-II-1)	185(6)
138	2	-3.66(10-II-4)	-2.70(6)	-0.35(6)	3796(10-I-3)	1731(10-II-1)	221(6)
138	3	-3.64(10-II-4)	-2.82(10-II-1)	-0.19(6)	3121(9-I-4)	1683(10-II-1)	316(6)
138	4	-3.60(10-II-4)	-2.57(10-II-1)	-0.33(6)	3790(10-I-3)	1752(10-II-1)	243(6)
138	5	-3.39(10-II-4)	-2.51(10-II-1)	-0.42(6)	4115(10-I-3)	1757(10-II-1)	201(6)
138	6	-3.13(10-I-2)	-2.33(10-II-1)	-0.48(6)	4039(10-I-3)	1669(10-II-1)	90(6)
138	7	-2.84(9-I-2)	-2.02(6)	-0.55(6)	3694(10-I-2)	1638(10-II-1)	-103(10-I-4)
138	8	-2.56(6)	-1.67(6)	-0.62(6)	3283(9-II-4)	1179(10-II-1)	-164(10-I-4)
138	9	-2.74(9-I-2)	-1.49(6)	-0.68(6)	3171(9-II-4)	1077(10-II-1)	-422(10-I-4)
138	10	-2.87(9-I-2)	-1.51(6)	-0.70(6)	2958(9-II-4)	932(10-II-1)	-573(10-I-4)
138	11	-2.96(9-I-2)	-1.56(6)	-0.80(6)	2870(9-II-3)	912(10-II-1)	-587(10-I-4)
138	12	-3.08(9-I-2)	-1.94(6)	-0.72(6)	3569(10-I-2)	1373(10-II-1)	-212(10-I-4)
138	13	-3.23(9-I-2)	-2.31(10-II-1)	-0.61(6)	3971(10-I-3)	1598(10-II-1)	59(6)
138	14	-2.90(9-I-2)	-1.77(6)	-0.69(6)	3464(10-I-2)	1377(10-II-1)	-212(10-I-4)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
139	1	-3.41(9-I-3)	-2.79(9-I-1)	0.83(10-II-3)	1664(9-I-3)	908(9-I-1)	-234(10-II-3)
139	2	-3.46(6)	-3.17(10-I-4)	0.73(10-II-2)	2257(9-I-3)	1410(9-I-1)	-409(10-II-3)
139	3	-3.39(6)	-3.29(10-I-2)	0.65(10-II-2)	2769(9-I-3)	1729(9-I-1)	-550(10-II-2)
139	4	-3.31(6)	-3.23(10-II-2)	0.54(10-I-4)	3319(10-I-2)	1984(10-II-1)	-720(10-I-4)
139	5	-3.26(6)	-3.02(10-II-2)	0.45(10-I-4)	3709(10-I-2)	2129(10-II-1)	-876(10-I-4)
139	6	-3.19(6)	-2.72(10-II-1)	0.38(10-I-4)	3830(10-I-2)	2214(10-II-1)	-996(10-I-4)
139	7	-3.08(6)	-2.43(10-II-1)	0.33(10-I-4)	3678(10-I-2)	2242(10-II-1)	-1050(10-I-4)
139	8	-2.91(6)	-2.09(10-II-1)	0.29(10-I-4)	3266(10-II-4)	2172(10-II-1)	-980(10-I-4)
139	9	-2.78(6)	-1.67(10-II-1)	0.27(10-I-4)	2992(10-II-4)	2027(10-II-1)	-870(10-I-1)
139	10	-3.04(6)	-2.02(10-II-1)	0.25(10-I-4)	3263(10-II-4)	2186(10-II-1)	-1041(10-I-4)
139	11	-3.23(6)	-2.34(10-II-1)	0.26(10-I-4)	3647(10-I-2)	2247(10-II-1)	-1047(10-I-4)
139	12	-3.40(6)	-2.58(10-II-1)	0.29(10-I-4)	3708(10-I-2)	2194(10-II-1)	-982(10-I-4)
139	13	-3.53(6)	-2.81(10-II-1)	0.34(10-I-4)	3474(9-I-3)	2068(10-II-1)	-808(10-I-4)
139	14	-3.60(6)	-3.06(10-I-1)	0.40(10-I-4)	2964(9-I-3)	1802(10-II-2)	-569(10-I-4)
139	15	-3.88(10-II-4)	-3.26(10-I-4)	0.25(10-II-2)	2138(9-I-3)	1530(10-II-2)	-212(10-I-4)
139	16	-4.03(6)	-3.14(10-I-4)	0.48(10-II-2)	1636(9-I-3)	1259(10-II-2)	261(6)
139	17	-3.89(6)	-2.83(10-I-4)	0.83(10-II-3)	1156(9-I-2)	922(10-II-2)	475(6)
139	18	-3.48(9-I-3)	-2.27(10-I-4)	1.07(10-II-3)	689(9-I-2)	664(10-I-4)	781(6)
139	19	-2.56(9-I-2)	-1.54(10-I-4)	1.04(10-II-3)	-538(10-II-3)	279(10-I-4)	1244(6)
139	20	0.97(9-II-1)	-1.15(10-I-4)	1.12(10-II-4)	-1917(10-II-4)	-291(10-II-4)	1286(10-I-4)
139	21	-2.28(9-I-1)	-1.61(9-I-1)	0.71(10-II-3)	199(9-I-1)	-281(10-II-4)	462(10-I-3)
139	22	-3.13(9-I-3)	-2.30(10-I-4)	0.74(10-II-3)	1080(9-I-2)	428(9-I-1)	190(6)
139	23	-3.34(6)	-2.99(10-II-2)	0.43(10-I-4)	3567(10-I-2)	2101(10-II-1)	-832(10-I-4)
139	24	-3.32(6)	-2.78(10-II-1)	0.36(10-I-4)	3744(10-I-2)	2189(10-II-1)	-935(10-I-4)
139	25	-3.44(6)	-2.92(10-II-1)	0.40(10-I-4)	3487(9-I-3)	2070(10-II-1)	-800(10-I-4)
139	26	-3.53(6)	-3.09(10-I-4)	0.78(10-II-3)	1929(9-I-3)	1110(9-I-1)	-100(10-II-2)
139	27	-3.51(6)	-3.12(10-II-2)	0.44(10-I-4)	3081(9-I-3)	1886(10-II-2)	-602(10-I-4)
139	28	-3.39(6)	-3.17(10-II-2)	0.49(10-I-4)	3224(9-I-3)	1944(10-II-2)	-664(10-I-4)
139	29	-3.65(6)	-3.21(10-I-4)	0.57(10-II-2)	2282(9-I-3)	1372(9-I-1)	-187(10-II-2)
139	30	-3.46(6)	-3.24(10-I-4)	0.57(10-II-2)	2759(9-I-3)	1696(10-II-2)	-461(10-I-4)
139	31	-3.62(6)	-3.20(10-I-4)	0.48(10-II-2)	2674(9-I-3)	1650(10-II-2)	-349(10-I-4)
140	1	-3.22(6)	-1.65(9-I-2)	0.52(6)	1524(10-I-3)	2094(9-I-2)	221(10-I-4)
140	2	-3.23(10-II-1)	-2.27(9-I-2)	0.55(6)	1743(6)	2262(9-I-2)	191(10-I-4)
140	3	-3.34(10-II-1)	-3.00(9-I-2)	0.25(6)	1551(10-II-1)	2210(9-I-2)	76(10-I-4)
140	4	-3.14(10-II-1)	-2.40(9-I-2)	-0.28(10-II-2)	1558(10-II-1)	2242(9-I-2)	-123(6)
140	5	-3.05(10-II-1)	-1.82(9-I-2)	-0.38(10-II-2)	1222(10-II-1)	2066(9-I-2)	-158(6)
140	6	-2.78(10-II-1)	-1.15(9-I-2)	-0.38(10-II-2)	771(10-II-4)	1370(9-I-1)	-118(6)
140	7	-2.30(10-II-4)	-0.42(9-I-2)	-0.24(10-II-2)	445(10-II-4)	786(9-I-1)	228(10-II-2)
140	8	-1.49(10-II-4)	1.12(9-II-1)	0.70(9-II-3)	-1038(10-I-4)	-663(9-II-4)	-550(10-I-3)
140	9	-2.09(10-II-4)	-0.84(9-I-1)	-0.63(10-I-4)	901(10-II-4)	-1182(10-I-4)	-466(10-I-2)
140	10	-2.65(10-II-4)	-1.37(9-I-1)	-0.80(10-I-4)	985(10-II-4)	-1136(10-I-4)	-263(6)
140	11	-2.95(10-II-1)	-1.75(9-I-1)	-0.67(10-I-4)	1137(10-II-1)	-1228(10-I-4)	-226(6)
140	12	-3.07(10-II-1)	-1.87(9-I-2)	-0.38(10-I-4)	1202(10-II-1)	-1232(10-I-4)	-164(6)
140	13	-3.11(6)	-1.81(9-I-2)	0.29(10-II-4)	1226(6)	-1207(10-II-4)	-102(6)
140	14	-3.08(10-I-3)	-1.61(9-I-3)	0.54(10-II-4)	1231(10-I-3)	-1154(10-II-4)	77(10-II-2)
140	15	-2.90(10-I-4)	-1.21(9-I-3)	0.66(6)	1172(10-I-4)	-1007(10-II-4)	183(10-II-2)
140	16	-2.44(10-I-4)	-0.66(9-I-3)	0.52(6)	1065(10-I-4)	-1023(10-II-4)	423(10-II-2)
140	17	-1.91(10-I-4)	1.15(9-II-3)	-0.72(9-II-1)	-608(10-II-4)	-591(9-II-3)	505(10-II-3)
140	18	-2.59(10-I-4)	-0.35(9-I-2)	0.16(6)	787(10-I-4)	825(9-I-3)	-172(6)
140	19	-2.99(6)	-1.04(9-I-2)	0.39(6)	1103(10-I-4)	1432(9-I-3)	162(10-I-4)
140	20	-2.91(6)	-1.79(9-I-2)	0.43(6)	1499(10-I-3)	-47(9-II-1)	74(10-I-4)
140	21	-2.83(10-I-3)	-1.45(9-I-2)	0.42(6)	1506(10-I-3)	323(9-I-1)	115(9-II-3)
140	22	-2.95(6)	-1.84(9-I-2)	0.43(6)	1664(10-I-3)	1038(9-I-2)	144(10-I-4)
140	23	-2.80(10-II-1)	-1.98(9-I-2)	-0.30(10-II-2)	1498(10-II-1)	942(9-I-2)	-107(6)
140	24	-2.62(10-II-1)	-1.61(9-I-2)	-0.39(10-II-2)	1321(10-II-4)	220(9-I-3)	-70(9-II-1)
140	25	-2.78(10-II-1)	-1.92(9-I-2)	-0.41(10-I-4)	1374(10-II-1)	-122(9-II-3)	-63(6)
140	26	-2.95(6)	-2.18(9-I-2)	0.37(6)	1687(6)	1311(9-I-2)	80(10-I-4)
140	27	-2.89(10-II-1)	-2.26(9-I-2)	-0.14(10-II-2)	1618(10-II-1)	1275(9-I-2)	-79(6)
140	28	-2.88(6)	-2.01(9-I-2)	0.26(6)	1481(6)	128(9-I-4)	55(10-I-4)
140	29	-2.84(10-II-1)	-2.07(9-I-2)	-0.20(10-I-4)	1443(10-II-1)	101(9-I-4)	-62(6)
141	1	-4.03(6)	-0.23(6)	1.36(9-II-4)	-1068(9-II-3)	-294(9-II-3)	182(9-I-2)
141	2	-3.87(6)	0.23(9-II-3)	1.15(9-II-4)	-2541(9-II-2)	-479(9-II-3)	-479(9-II-3)
141	3	-4.43(10-I-3)	-0.38(6)	1.07(9-II-4)	-3269(9-II-3)	-385(9-II-3)	-1007(9-II-2)
141	4	-4.23(6)	-0.69(6)	1.05(9-II-4)	-2432(9-II-3)	269(9-I-3)	-1085(9-II-2)
141	5	-3.92(6)	-0.96(6)	1.26(9-II-4)	-1133(9-II-3)	416(9-I-3)	-1097(9-II-2)
141	6	-4.72(6)	-0.63(6)	0.88(9-II-2)	1109(10-I-3)	459(6)	-424(9-II-4)
141	7	-4.43(6)	-0.32(6)	1.38(9-II-4)	452(6)	249(10-I-3)	-227(9-II-4)
141	8	-4.44(10-I-3)	-0.19(6)	0.81(9-II-4)	-1579(9-II-3)	-252(9-II-3)	-826(9-II-2)
142	1	-3.03(10-I-3)	-1.92(6)	-0.56(6)	3972(10-I-3)	517(9-I-3)	-211(9-I-3)
142	2	-3.03(10-I-3)	-1.87(6)	-1.46(6)	4157(10-I-3)	863(10-I-2)	138(9-II-3)
142	3	-3.79(10-I-3)	-1.81(6)	-1.30(6)	1822(10-I-3)	613(10-I-2)	-161(10-II-3)
142	4	-3.84(10-I-3)	-1.08(6)	0.27(9-I-3)	2946(10-I-3)	-393(9-I-3)	-629(9-II-2)
142	5	-3.36(10-I-3)	-2.09(10-I-3)	-0.65(6)	4603(10-I-3)	439(9-I-3)	108(9-II-3)
142	6	-3.46(10-I-3)	-1.79(6)	-0.71(6)	4023(10-I-3)	823(6)	196(9-II-3)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
142	7	-2.95(10-I-3)	-1.66(6)	-0.51(6)	3534(10-I-3)	352(9-I-3)	-381(9-II-1)
142	8	-2.70(10-I-3)	-1.74(6)	-0.42(6)	4272(10-I-3)	-328(9-II-3)	-252(9-I-3)
143	1	0.47(10-II-3)	-5.32(10-I-3)	-0.83(9-II-4)	1761(10-I-3)	1306(10-I-3)	124(10-II-2)
143	2	-0.25(10-I-3)	-5.99(10-I-3)	-1.79(9-II-4)	1779(10-I-3)	1489(10-I-3)	374(10-II-2)
143	3	0.17(10-II-3)	-4.92(10-I-3)	-0.53(9-II-1)	2302(10-I-3)	2774(10-I-3)	1661(9-II-4)
143	4	0.86(10-II-3)	-5.20(10-I-3)	-0.73(9-II-4)	1871(10-I-3)	2051(10-I-3)	418(6)
143	5	0.52(10-II-3)	-5.75(10-I-3)	-0.75(9-II-4)	2145(10-I-3)	970(10-I-3)	-911(9-II-3)
143	6	0.91(10-II-3)	-5.59(10-I-3)	-1.16(9-II-4)	1891(10-I-3)	826(10-I-3)	281(10-II-2)
143	7	0.74(10-II-3)	-5.56(10-I-3)	-1.01(9-II-4)	1906(10-I-3)	1872(10-I-3)	-48(9-II-3)
143	8	0.76(10-II-3)	-4.81(10-I-3)	-0.91(9-II-4)	2104(10-I-3)	590(10-I-3)	-575(9-II-3)
144	1	-3.50(10-I-3)	-4.70(10-I-3)	-1.39(9-II-1)	1602(10-I-3)	1747(10-I-3)	663(9-II-4)
144	2	-3.83(10-I-3)	-4.65(10-I-2)	-0.79(9-II-1)	1665(10-I-3)	1865(10-I-2)	383(9-II-1)
144	3	-3.69(10-I-3)	-4.72(10-I-2)	-0.30(9-II-1)	1467(10-I-3)	1956(10-I-2)	222(9-II-1)
144	4	-3.08(10-I-3)	-4.95(10-I-2)	0.33(9-I-1)	1215(10-I-3)	1999(10-I-2)	-171(9-I-1)
144	5	-3.48(10-I-3)	-4.94(10-I-2)	-0.44(9-II-1)	1506(10-I-3)	2101(10-I-2)	124(9-II-1)
144	6	-3.52(10-I-3)	-4.92(10-I-3)	-0.80(9-II-1)	1586(10-I-3)	2235(10-I-3)	402(9-II-1)
144	7	-3.12(10-I-3)	-5.00(10-I-3)	-1.09(9-II-1)	1455(10-I-3)	2622(10-I-3)	677(9-II-1)
144	8	-2.30(10-I-3)	-5.16(10-I-3)	-1.29(9-II-1)	959(10-I-3)	2926(10-I-3)	676(9-II-1)
144	9	-1.54(10-I-3)	-5.76(10-I-3)	-1.06(9-II-1)	610(10-I-3)	2799(10-I-3)	339(9-II-1)
144	10	-2.15(10-I-3)	-5.53(10-I-3)	-1.68(9-II-1)	599(10-I-3)	2012(10-I-3)	512(9-II-1)
144	11	-2.48(10-I-3)	-4.98(10-I-3)	-2.18(9-II-4)	626(10-I-3)	1999(10-I-3)	576(9-II-1)
144	12	-2.86(10-I-3)	-4.78(10-I-3)	-2.56(9-II-4)	992(10-I-3)	1319(6)	940(9-II-4)
144	13	-3.30(10-I-3)	-4.76(10-I-3)	-1.91(9-II-1)	1587(10-I-3)	1597(10-I-3)	927(9-II-4)
145	1	0.45(10-II-3)	-4.21(10-I-3)	-1.10(10-I-3)	2297(10-I-3)	2203(10-I-3)	1005(10-II-2)
145	2	0.18(10-II-3)	-4.48(10-I-3)	-1.71(10-II-2)	2576(10-I-3)	1833(10-I-3)	1048(10-II-2)
145	3	-0.24(10-I-3)	-4.69(10-I-3)	-1.26(10-II-4)	2547(10-I-3)	2732(10-I-3)	1359(9-II-4)
145	4	0.83(10-II-3)	-4.36(6)	-1.12(10-II-3)	2407(10-I-3)	2904(10-I-3)	777(10-II-2)
145	5	0.48(10-II-3)	-4.66(10-I-3)	-1.12(10-II-3)	2594(10-I-3)	1939(10-I-3)	88(6)
145	6	0.72(10-II-3)	-4.27(10-I-3)	-1.57(10-II-3)	2268(10-I-3)	1503(10-I-3)	1071(10-II-2)
145	7	0.69(10-II-3)	-4.50(6)	-1.33(10-II-3)	2475(10-I-3)	2801(10-I-3)	786(6)
145	8	0.76(10-II-3)	-3.83(10-I-3)	-1.07(10-II-3)	2716(10-I-3)	1661(10-I-3)	308(6)
146	1	-2.91(10-I-3)	-2.55(10-I-3)	-2.73(10-I-3)	4117(10-I-3)	916(10-I-3)	180(10-II-2)
146	2	-2.88(10-I-3)	-2.63(10-I-3)	-2.96(10-I-4)	3913(10-I-3)	1117(10-I-3)	618(10-II-2)
146	3	-2.56(10-I-3)	-2.32(6)	-2.54(10-I-3)	3408(10-I-3)	1463(10-I-3)	652(10-II-2)
147	1	-2.58(9-I-3)	-2.67(10-I-3)	1.30(10-I-2)	2854(10-I-3)	1515(10-I-2)	140(9-I-4)
147	2	-2.10(9-II-3)	-2.73(10-I-2)	1.12(10-I-2)	2417(10-I-3)	1453(10-I-2)	124(9-I-4)
147	3	-1.65(9-II-3)	-2.73(10-I-2)	0.91(9-II-1)	1582(10-I-4)	1209(10-I-2)	76(9-I-4)
147	4	-1.24(9-II-3)	-2.65(10-I-2)	0.77(9-II-1)	970(9-II-3)	1067(10-I-2)	-261(9-II-4)
147	5	-0.84(9-II-3)	-2.23(10-I-2)	0.94(9-II-4)	141(9-II-3)	656(10-I-2)	-242(9-II-4)
147	6	-1.39(9-II-3)	-2.74(10-I-2)	0.97(9-II-4)	-470(9-I-2)	1120(10-I-2)	105(9-I-1)
147	7	-1.80(9-II-3)	-2.81(10-I-2)	0.78(9-II-4)	-781(10-I-2)	1204(10-I-2)	-86(9-II-1)
147	8	-2.12(10-I-3)	-2.42(10-I-3)	0.41(9-II-1)	-1213(10-I-2)	990(10-I-3)	-184(10-I-2)
147	9	-2.05(9-II-4)	-1.67(10-I-3)	0.12(10-I-2)	-1667(10-I-2)	557(9-II-3)	-186(10-I-2)
147	10	0.94(9-I-3)	-1.24(9-II-3)	-0.47(10-II-2)	-1769(9-I-3)	-234(10-I-2)	-827(10-I-2)
147	11	-1.95(9-II-3)	-1.82(10-I-2)	-0.67(10-II-2)	447(9-II-3)	-301(10-II-3)	-583(10-I-2)
147	12	-3.38(9-II-3)	-1.84(10-I-2)	-0.65(6)	1320(9-II-3)	252(10-I-3)	-756(10-I-2)
147	13	-4.30(9-II-3)	-1.78(10-I-2)	-0.31(6)	2133(9-II-3)	504(10-I-3)	-805(10-I-2)
147	14	-5.01(9-II-3)	-1.69(10-I-2)	0.48(9-II-1)	2537(10-I-3)	623(10-I-3)	-628(10-I-2)
147	15	-5.48(10-I-3)	-1.68(10-I-2)	1.16(9-II-1)	2687(10-I-3)	690(10-I-3)	-543(9-II-1)
147	16	-4.38(9-II-3)	-2.23(10-I-3)	1.26(9-II-1)	3009(10-I-3)	1131(10-I-2)	-298(9-II-1)
147	17	-3.34(9-II-3)	-2.55(10-I-3)	1.31(9-II-1)	3063(10-I-3)	1416(10-I-2)	-77(9-II-1)
147	18	-2.37(9-II-3)	-2.25(10-I-3)	0.80(10-I-2)	429(9-II-3)	1297(10-I-3)	-46(9-II-1)
147	19	-2.39(9-II-3)	-2.33(10-I-3)	0.93(10-I-2)	1440(9-II-3)	1516(10-I-2)	97(6)
147	20	-2.05(9-II-3)	-2.51(10-I-2)	0.85(9-II-1)	613(9-II-3)	1475(10-I-2)	78(6)
147	21	-2.68(9-II-3)	-2.36(10-I-3)	1.06(10-I-2)	2029(10-I-3)	1448(10-I-3)	93(9-I-1)
147	22	-2.34(9-II-3)	-1.90(10-I-3)	0.56(10-I-2)	579(9-II-3)	817(10-I-3)	90(10-II-2)
147	23	-3.05(9-II-3)	-2.21(10-I-2)	0.65(10-I-2)	2038(9-II-3)	1006(10-I-3)	-156(9-II-1)
147	24	-2.94(9-II-3)	-2.03(10-I-3)	0.66(10-I-2)	1623(9-II-3)	932(10-I-3)	-133(9-II-1)
147	25	-2.71(9-II-3)	-2.18(10-I-3)	0.72(10-I-2)	1819(9-II-3)	1154(10-I-3)	-52(9-II-1)
147	26	-2.87(9-II-3)	-2.11(10-I-2)	0.36(10-I-2)	1957(9-II-4)	673(10-I-3)	-247(9-II-1)
147	27	-3.28(9-II-3)	-2.18(10-I-2)	0.75(10-I-2)	2332(10-I-3)	1104(10-I-3)	-180(9-II-1)
147	28	-3.41(9-II-3)	-2.30(10-I-2)	0.95(10-I-2)	2633(10-I-3)	1351(10-I-3)	-164(9-II-1)
147	29	-3.02(9-II-3)	-2.33(10-I-2)	0.96(10-I-2)	2327(10-I-3)	1371(10-I-3)	-126(9-II-1)
147	30	-3.68(9-II-3)	-2.02(10-I-2)	0.40(9-II-1)	2407(9-II-4)	765(10-I-3)	-290(9-II-1)
147	31	-4.09(9-II-3)	-2.11(10-I-2)	0.76(9-II-1)	2758(10-I-3)	993(10-I-3)	-312(9-II-1)
148	1	-4.92(10-I-3)	-3.80(10-I-3)	1.60(9-II-1)	2002(10-I-3)	1597(10-I-3)	-591(9-II-1)
148	2	-4.84(10-I-3)	-3.99(10-I-3)	1.13(9-II-1)	1921(10-I-3)	1696(10-I-3)	-455(9-II-1)
148	3	-5.04(10-I-3)	-3.67(10-I-3)	0.75(9-II-1)	1949(10-I-3)	1566(10-I-3)	-339(9-II-1)
148	4	-4.99(10-I-3)	-3.00(10-I-3)	0.47(9-II-1)	1217(10-I-3)	1214(10-I-3)	-213(9-II-1)
148	5	-4.76(10-I-3)	-3.47(10-I-3)	0.65(9-II-1)	2107(10-I-3)	1390(10-I-3)	-261(9-II-1)
148	6	-4.82(10-I-3)	-3.84(10-I-3)	0.99(9-II-1)	2069(10-I-3)	1593(10-I-3)	-418(9-II-1)
148	7	-4.98(10-I-3)	-3.66(10-I-3)	1.30(9-II-1)	2101(10-I-3)	1644(10-I-3)	-592(9-II-1)
148	8	-5.19(10-I-3)	-3.31(10-I-3)	1.59(9-II-1)	2239(10-I-3)	1619(10-I-2)	-792(9-II-1)
148	9	-5.67(10-I-3)	-2.70(10-I-3)	1.62(9-II-1)	2451(10-I-3)	1460(10-I-2)	-921(9-II-1)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
148	10	-5.66(10-I-3)	-2.32(10-I-3)	1.64(9-II-1)	2693(10-I-3)	1162(10-I-2)	-989(9-II-1)
148	11	-6.00(10-I-3)	-1.69(10-I-3)	1.61(9-II-1)	2558(10-I-3)	707(10-I-3)	-727(9-II-1)
148	12	-5.72(10-I-3)	-2.25(10-I-3)	2.07(9-II-1)	2295(10-I-3)	788(10-I-3)	-808(9-II-1)
148	13	-5.26(10-I-3)	-3.18(10-I-3)	1.99(9-II-1)	2057(10-I-3)	1273(10-I-3)	-790(9-II-1)
148	14	-5.39(10-I-3)	-2.73(10-I-3)	1.64(9-II-1)	2397(10-I-3)	1317(10-I-2)	-858(9-II-1)
149	1	-2.40(10-I-4)	-5.78(10-I-2)	0.73(6)	752(6)	1942(10-I-2)	-813(6)
149	2	-2.08(10-I-4)	-5.79(10-I-2)	0.59(10-II-2)	720(6)	1765(10-I-2)	-836(6)
149	3	-1.74(10-I-4)	-5.61(10-I-3)	0.45(10-II-2)	662(6)	1527(10-I-2)	-802(6)
149	4	-1.44(10-I-3)	-5.25(10-I-3)	0.29(10-II-2)	558(10-I-4)	1265(10-I-3)	-703(10-II-2)
149	5	-1.11(10-I-2)	-4.66(10-I-3)	0.21(10-II-2)	350(10-I-4)	1019(10-I-3)	-519(10-II-2)
149	6	-0.81(10-I-2)	-3.78(10-I-3)	-0.49(10-I-2)	193(10-I-2)	860(10-I-3)	-472(10-II-2)
149	7	-0.60(10-I-2)	-2.57(10-I-3)	-0.49(10-I-2)	-91(10-II-2)	459(10-I-2)	294(10-I-2)
149	8	-1.25(10-I-2)	-3.49(10-I-3)	0.65(10-II-2)	343(10-I-2)	1038(10-I-3)	471(10-I-2)
149	9	-1.74(10-I-2)	-4.29(10-I-3)	0.89(10-II-2)	532(10-I-2)	1249(10-I-3)	337(10-I-2)
149	10	-2.16(10-I-3)	-4.78(10-I-3)	1.06(10-II-2)	572(10-I-3)	1394(10-I-3)	327(10-I-2)
149	11	-2.39(10-I-3)	-5.09(10-I-3)	1.12(10-II-2)	685(10-I-3)	1963(10-I-3)	265(9-I-3)
149	12	-2.49(10-I-3)	-5.40(10-I-3)	1.14(10-II-2)	760(10-I-3)	2325(10-I-3)	-123(9-I-3)
149	13	-2.36(10-I-3)	-5.64(10-I-3)	1.30(6)	647(10-I-3)	2436(10-I-3)	-360(9-II-3)
149	14	-1.90(10-I-3)	-5.85(10-I-3)	1.51(6)	643(10-I-3)	2478(10-I-3)	-643(9-II-3)
149	15	-2.03(10-I-3)	-5.92(10-I-3)	1.06(6)	872(10-I-3)	2839(10-I-3)	-482(6)
149	16	-2.37(10-I-3)	-5.78(10-I-3)	0.66(6)	1082(10-I-3)	2962(10-I-3)	-356(6)
149	17	-2.65(10-I-3)	-5.60(10-I-3)	0.38(6)	1296(10-I-3)	2947(10-I-3)	-216(6)
149	18	-2.90(10-I-3)	-5.40(10-I-3)	0.35(6)	1399(10-I-3)	2863(10-I-3)	-109(6)
149	19	-3.06(10-I-3)	-5.21(10-I-2)	0.47(6)	1412(10-I-3)	2700(10-I-2)	-89(6)
149	20	-3.13(10-I-3)	-5.06(10-I-2)	0.75(6)	1323(10-I-3)	2430(10-I-2)	-199(6)
149	21	-3.14(10-I-3)	-4.87(10-I-2)	1.08(6)	1163(10-I-3)	2060(10-I-2)	-465(6)
149	22	-2.98(10-I-3)	-5.30(10-I-2)	0.98(6)	906(10-I-3)	2075(10-I-2)	-659(6)
149	23	-2.69(10-I-3)	-5.62(10-I-2)	0.86(6)	788(10-I-4)	2040(10-I-2)	-750(6)
149	24	-2.44(10-I-3)	-5.50(10-I-3)	0.74(6)	1282(10-I-3)	2878(10-I-3)	-296(6)
149	25	-2.61(10-I-3)	-5.46(10-I-3)	0.55(6)	1419(10-I-3)	2946(10-I-3)	-230(6)
149	26	-2.52(10-I-3)	-5.40(10-I-3)	0.67(6)	1415(10-I-3)	2836(10-I-3)	-255(6)
149	27	-2.73(10-I-3)	-5.41(10-I-3)	0.48(6)	1436(10-I-3)	2844(10-I-3)	-222(6)
149	28	-2.56(10-I-3)	-5.40(10-I-3)	0.57(6)	1384(10-I-3)	2733(10-I-3)	-310(6)
149	29	-2.51(10-I-3)	-5.52(10-I-2)	0.59(6)	1139(10-I-3)	2477(10-I-2)	-486(6)
149	30	-2.93(10-I-3)	-5.31(10-I-2)	0.71(6)	1195(10-I-3)	2450(10-I-2)	-406(6)
149	31	-2.72(10-I-3)	-5.47(10-I-2)	0.65(6)	1150(10-I-3)	2490(10-I-2)	-470(6)
149	32	-2.85(10-I-3)	-5.35(10-I-2)	0.54(6)	1358(10-I-3)	2694(10-I-2)	-282(6)
149	33	-2.30(10-I-3)	-4.89(10-I-3)	0.93(10-II-2)	902(10-I-3)	2072(10-I-3)	-111(10-II-2)
149	34	-2.47(10-I-3)	-5.28(10-I-3)	0.73(6)	1350(10-I-3)	2682(10-I-3)	-257(6)
149	35	-2.42(10-I-3)	-5.09(10-I-3)	0.82(10-II-2)	1164(10-I-3)	2402(10-I-3)	-229(10-II-2)
149	36	-2.47(10-I-3)	-5.28(10-I-3)	0.90(6)	1151(10-I-3)	2657(10-I-3)	-248(10-II-2)
149	37	-2.28(10-I-3)	-5.45(10-I-2)	0.55(10-II-2)	1043(10-I-3)	2297(10-I-3)	-510(6)
149	38	-2.42(10-I-3)	-5.28(10-I-3)	0.61(10-II-2)	1303(10-I-3)	2537(10-I-3)	-335(6)
149	39	-1.83(10-I-3)	-4.95(10-I-3)	0.49(10-II-2)	767(10-I-3)	1812(10-I-3)	-408(10-II-2)
149	40	-1.78(10-I-3)	-4.46(10-I-3)	0.53(10-II-2)	633(10-I-2)	1605(10-I-3)	-241(10-II-2)
149	41	-2.09(10-I-3)	-4.83(10-I-3)	0.71(10-II-2)	930(10-I-3)	1981(10-I-3)	-234(10-II-2)
149	42	-2.03(10-I-3)	-5.26(10-I-3)	0.52(10-II-2)	921(10-I-3)	2063(10-I-3)	-469(10-II-2)
149	43	-2.28(10-I-3)	-5.08(10-I-3)	0.68(10-II-2)	1169(10-I-3)	2267(10-I-3)	-300(10-II-2)
150	1	-1.78(10-I-3)	1.14(9-II-3)	0.82(9-I-4)	2253(10-I-3)	-1444(9-II-3)	-1012(9-I-4)
150	2	-1.96(10-I-3)	1.40(9-II-3)	0.24(9-I-4)	2134(10-I-3)	-1674(9-II-3)	-366(9-I-4)
150	3	-1.37(10-I-3)	1.22(9-II-3)	-0.33(9-II-4)	1546(10-I-3)	-1047(9-II-3)	597(9-II-4)
150	4	-1.43(10-I-3)	1.59(9-II-3)	0.44(9-I-4)	1451(10-I-3)	-1679(9-II-3)	-333(9-I-4)
150	5	-1.73(10-I-3)	1.29(9-II-3)	0.90(9-I-4)	1473(10-I-3)	-1298(9-II-3)	-827(9-I-4)
150	6	-1.60(10-I-3)	0.96(9-II-3)	1.26(9-I-1)	1417(10-I-3)	-908(9-II-2)	-1286(9-I-3)
150	7	-1.33(10-I-3)	0.60(9-II-2)	1.52(9-I-1)	1151(10-I-3)	-532(9-II-2)	-1745(10-I-2)
150	8	-1.03(10-I-3)	0.71(10-I-1)	1.63(10-I-2)	638(10-I-3)	-1154(10-I-1)	-2077(10-I-2)
150	9	-1.36(6)	0.36(9-II-2)	1.42(10-I-2)	1300(10-I-3)	-716(10-I-1)	-1592(10-I-2)
150	10	-1.90(6)	-0.64(6)	1.10(9-I-2)	2289(7)	-316(10-I-1)	-1309(9-I-1)
150	11	-2.16(6)	-0.55(6)	1.38(9-I-2)	2520(6)	677(6)	-1350(7)
150	12	-1.13(10-I-3)	0.29(9-II-2)	1.53(9-I-2)	1805(9-II-3)	375(6)	-1403(9-I-1)
150	13	-1.52(10-I-3)	0.85(9-II-3)	1.28(9-I-4)	1901(10-I-3)	-1117(9-II-3)	-1491(9-I-1)
150	14	-1.44(6)	0.32(9-II-2)	1.48(9-I-2)	1305(10-I-3)	-268(9-II-2)	-1663(9-I-1)
151	1	0.69(9-II-3)	-1.79(10-I-3)	-0.92(9-I-1)	-1177(9-II-3)	1526(10-I-3)	1506(9-I-3)
151	2	0.29(9-II-3)	-1.50(10-I-3)	-1.11(9-I-1)	-574(9-II-2)	1349(10-I-3)	1616(9-I-3)
151	3	-0.72(6)	-1.41(9-II-3)	-1.19(9-I-2)	643(6)	1568(9-I-3)	1218(9-I-1)
151	4	0.44(9-II-3)	-1.46(10-I-3)	-0.95(9-I-4)	-386(9-II-3)	2137(9-II-3)	702(10-II-2)
151	5	0.82(9-II-3)	-1.61(10-I-3)	-0.61(9-I-4)	-746(9-II-3)	2859(10-I-3)	449(9-I-1)
151	6	0.46(9-II-3)	-1.94(10-I-3)	0.23(9-II-1)	668(6)	3009(10-I-3)	-652(10-I-3)
151	7	0.83(9-II-3)	-2.04(10-I-3)	0.21(9-I-4)	465(6)	2758(10-I-3)	-729(9-II-4)
151	8	0.97(9-II-3)	-1.68(10-I-3)	0.34(9-II-4)	-419(9-II-3)	1947(10-I-3)	-999(9-II-4)
151	9	0.99(9-II-3)	-1.40(10-I-3)	0.47(9-II-4)	-1013(9-II-3)	405(6)	-401(9-II-4)
151	10	1.22(9-II-3)	-2.44(10-I-3)	0.23(9-I-4)	-1995(9-II-3)	649(10-I-3)	740(9-I-3)
151	11	1.03(9-II-3)	-2.16(10-I-3)	-0.38(9-I-4)	-1564(9-II-3)	1234(10-I-3)	1225(9-I-3)
152	1	0.75(9-II-2)	-0.80(10-I-3)	0.65(10-I-4)	-4033(9-II-3)	1640(10-I-3)	-1358(9-II-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
152	2	1.02 (9-II-2)	-0.58 (10-I-3)	-0.19 (9-I-3)	-4025 (9-II-3)	3515 (9-II-4)	-1799 (9-II-2)
152	3	0.91 (9-II-2)	-0.66 (10-I-3)	-0.16 (9-I-3)	-3658 (9-II-3)	5400 (9-II-4)	-941 (9-II-2)
152	4	1.00 (9-II-2)	-1.13 (10-I-3)	-0.17 (10-II-3)	-3834 (9-II-3)	4650 (9-II-3)	620 (10-II-3)
152	5	0.85 (10-I-1)	-1.93 (10-I-3)	0.22 (10-I-3)	-4173 (9-II-3)	3343 (9-II-3)	734 (9-I-2)
152	6	0.70 (9-II-2)	-1.36 (10-I-3)	-0.25 (10-II-3)	-4168 (9-II-3)	4660 (9-II-3)	519 (9-I-2)
152	7	0.76 (9-II-2)	-0.77 (10-I-3)	-0.18 (9-I-3)	-3700 (9-II-3)	5935 (9-II-4)	-1136 (9-II-2)
152	8	0.99 (9-II-2)	-0.27 (10-I-3)	-0.11 (9-I-3)	-2829 (10-II-3)	5644 (9-II-4)	-2474 (9-II-2)
152	9	1.07 (9-II-2)	-0.26 (10-I-3)	0.48 (9-II-3)	-1345 (10-II-3)	4522 (9-II-4)	-3213 (9-II-2)
152	10	0.74 (9-II-2)	0.18 (9-II-2)	0.73 (9-II-3)	594 (10-I-3)	1316 (9-I-3)	-1771 (9-II-2)
152	11	-0.39 (6)	-0.08 (6)	0.64 (9-II-3)	-1227 (10-II-3)	1012 (10-I-2)	-828 (9-II-2)
152	12	0.40 (9-II-2)	-0.52 (10-I-3)	0.50 (9-II-3)	-2476 (9-II-3)	759 (10-I-3)	-580 (9-II-2)
152	13	0.80 (9-II-2)	-0.71 (10-I-3)	0.27 (9-II-3)	-2421 (10-II-3)	2807 (9-II-4)	-2604 (9-II-2)
153	1	-0.31 (6)	0.47 (9-II-2)	-0.59 (10-I-3)	2192 (9-I-3)	-2221 (10-II-3)	4431 (9-II-2)
153	2	-0.33 (6)	0.38 (9-II-2)	-0.46 (9-II-3)	-687 (9-II-3)	-2317 (10-II-3)	3380 (9-II-2)
153	3	-0.24 (9-I-2)	0.50 (9-II-2)	-0.39 (10-I-3)	-1034 (9-II-3)	-2905 (10-II-3)	2877 (9-II-4)
153	4	-0.30 (10-I-3)	0.79 (9-II-2)	-0.50 (10-I-3)	-791 (9-II-3)	-4317 (9-II-3)	2608 (10-I-3)
153	5	-0.30 (10-I-3)	0.86 (9-II-2)	-0.44 (10-I-3)	344 (10-I-3)	-4945 (9-II-2)	2825 (10-I-3)
153	6	-0.19 (6)	0.50 (9-II-2)	-0.58 (10-I-3)	2465 (10-I-2)	-3090 (10-II-3)	4243 (10-I-3)
153	7	-0.25 (6)	-0.37 (6)	-0.92 (10-I-3)	3015 (10-I-2)	-2702 (10-II-3)	3642 (9-II-3)
153	8	-1.04 (9-I-2)	0.25 (10-II-3)	-1.05 (10-I-3)	2007 (7)	-2933 (10-II-3)	2613 (9-II-3)
153	9	-0.51 (6)	-0.20 (6)	-0.88 (10-I-3)	2937 (9-I-3)	-2113 (10-II-3)	3623 (9-II-3)
153	10	-0.30 (6)	0.46 (9-II-2)	-0.38 (10-I-3)	1724 (10-I-2)	-3019 (10-II-3)	4312 (9-II-2)
154	1	0.25 (10-II-3)	1.26 (9-II-2)	0.26 (10-II-3)	-308 (10-II-3)	-5854 (9-II-4)	259 (10-I-3)
154	2	0.32 (10-II-3)	0.86 (9-II-2)	0.44 (9-II-2)	-1273 (9-II-3)	-5854 (9-II-4)	-728 (9-II-2)
154	3	0.42 (10-II-3)	0.76 (9-II-2)	0.53 (9-II-4)	-1236 (9-II-3)	-6255 (9-II-4)	-1191 (9-II-2)
154	4	0.98 (10-II-3)	0.65 (9-II-2)	0.86 (9-II-4)	-1979 (9-II-3)	-6910 (9-II-4)	-2635 (9-II-2)
154	5	1.84 (9-II-3)	-0.57 (10-II-2)	0.60 (9-II-4)	-4320 (9-II-3)	-5976 (9-II-3)	-3335 (9-II-4)
154	6	1.83 (9-II-3)	-0.41 (10-II-2)	0.17 (9-II-3)	-4302 (9-II-3)	-5034 (9-II-3)	-2778 (9-II-3)
154	7	1.78 (9-II-3)	-0.29 (10-II-2)	-0.04 (6)	-4564 (9-II-3)	-4449 (9-II-3)	-3293 (9-II-3)
154	8	1.53 (9-II-3)	-0.18 (10-II-1)	-0.17 (9-II-2)	-5637 (9-II-3)	-3418 (9-II-2)	-4140 (9-II-3)
154	9	0.96 (10-II-3)	-0.48 (10-II-2)	-0.34 (9-II-2)	-8194 (9-II-3)	-1872 (9-II-2)	-3645 (9-II-3)
154	10	0.92 (10-II-3)	0.08 (10-I-1)	-0.14 (9-II-2)	-6762 (9-II-3)	-646 (9-II-2)	-2257 (9-II-3)
154	11	0.65 (10-II-2)	0.10 (9-II-3)	0.09 (9-I-2)	-5933 (9-II-3)	307 (9-I-2)	-2052 (10-I-3)
154	12	0.32 (10-II-2)	0.22 (9-II-3)	0.30 (10-I-2)	-5353 (9-II-2)	1375 (9-I-2)	-1644 (9-I-2)
154	13	0.31 (9-II-3)	-0.31 (9-I-2)	0.46 (10-I-1)	-5579 (9-II-3)	2759 (9-I-1)	-2400 (10-I-2)
154	14	-0.33 (6)	-0.70 (9-I-2)	0.34 (10-I-2)	-5972 (9-II-3)	2854 (10-II-2)	-1927 (10-I-2)
154	15	-0.42 (6)	-1.28 (10-II-2)	0.38 (10-I-1)	-4939 (9-II-3)	1499 (10-II-2)	-1192 (9-I-3)
154	16	0.44 (9-II-3)	-0.69 (6)	-0.45 (6)	-671 (10-II-2)	-3332 (10-I-3)	-1174 (9-II-1)
154	17	-0.46 (6)	-0.42 (6)	-0.95 (10-I-3)	4747 (10-I-3)	-4540 (9-II-2)	-482 (10-II-3)
154	18	-0.80 (10-I-3)	0.60 (9-II-2)	-1.25 (10-I-3)	3491 (10-I-3)	-3552 (9-II-3)	934 (10-I-3)
154	19	-0.32 (6)	0.23 (9-II-2)	-0.77 (10-I-3)	4771 (10-I-3)	-5084 (9-II-2)	957 (10-I-3)
154	20	-0.21 (10-I-3)	0.44 (9-II-2)	-0.43 (10-I-3)	4482 (10-I-3)	-6753 (9-II-2)	1396 (10-I-3)
154	21	0.25 (10-II-3)	0.39 (9-II-2)	-0.21 (10-I-3)	2520 (10-I-3)	-5715 (9-II-2)	1209 (10-I-3)
154	22	0.64 (9-II-3)	-0.10 (6)	0.18 (10-I-1)	-6495 (9-II-3)	678 (9-I-2)	-2670 (10-I-3)
154	23	0.61 (9-II-3)	-0.39 (6)	0.25 (9-I-2)	-6315 (9-II-3)	1709 (10-II-2)	-2569 (10-I-3)
154	24	0.70 (9-II-3)	-0.28 (10-II-1)	0.13 (10-I-1)	-6584 (9-II-3)	797 (10-II-2)	-2711 (10-I-3)
154	25	1.01 (9-II-3)	-0.32 (10-II-2)	-0.10 (9-II-2)	-7023 (9-II-3)	-1048 (9-II-2)	-2977 (10-I-3)
154	26	0.83 (10-II-2)	-0.25 (10-II-1)	-0.08 (9-II-2)	-6812 (9-II-3)	-361 (9-II-2)	-2786 (10-I-3)
154	27	0.89 (9-II-3)	-0.30 (10-II-1)	-0.04 (10-II-1)	-6698 (9-II-3)	-225 (10-I-2)	-2897 (10-I-3)
154	28	1.45 (9-II-3)	-0.31 (10-II-2)	-0.07 (6)	-4322 (9-II-3)	-4021 (9-II-2)	-3284 (9-II-4)
154	29	1.41 (9-II-3)	-0.24 (10-II-2)	-0.13 (6)	-5060 (9-II-3)	-3296 (9-II-2)	-3529 (9-II-3)
154	30	1.19 (9-II-3)	-0.27 (10-II-2)	-0.13 (6)	-5072 (9-II-3)	-2552 (9-II-2)	-3376 (9-II-4)
154	31	1.14 (9-II-3)	-0.28 (10-II-2)	-0.08 (6)	-6362 (9-II-3)	-1923 (9-II-2)	-3558 (9-II-3)
154	32	0.98 (9-II-3)	-0.30 (10-II-2)	-0.09 (6)	-6177 (9-II-3)	-1055 (10-I-2)	-3091 (10-I-3)
154	33	0.82 (9-II-3)	-0.33 (10-II-1)	0.07 (10-I-1)	-6569 (9-II-3)	419 (10-II-2)	-2865 (10-I-3)
154	34	0.33 (10-II-3)	0.30 (9-II-2)	-0.29 (10-I-3)	2910 (10-I-3)	-6805 (9-II-2)	502 (10-I-3)
154	35	0.43 (10-II-3)	0.53 (9-II-2)	0.19 (10-I-3)	1928 (10-I-3)	-7245 (9-II-2)	-299 (10-II-3)
154	36	0.88 (9-II-4)	0.30 (9-II-2)	0.50 (9-II-2)	-906 (10-II-2)	-6906 (9-II-2)	-2678 (9-II-2)
154	37	0.54 (10-II-3)	0.49 (9-II-2)	0.28 (9-II-4)	1683 (10-I-3)	-7188 (9-II-2)	-1020 (9-II-4)
154	38	0.81 (10-II-3)	-0.33 (6)	0.13 (9-II-2)	704 (10-I-2)	-5321 (9-II-2)	-3738 (9-II-2)
154	39	0.89 (10-II-3)	-0.29 (6)	0.23 (9-II-2)	-902 (10-II-2)	-5560 (9-II-2)	-3749 (9-II-2)
154	40	0.94 (10-II-3)	-0.34 (10-II-2)	0.12 (9-II-2)	-1182 (10-II-2)	-4901 (9-II-2)	-3858 (9-II-2)
154	41	0.64 (9-II-4)	0.23 (9-II-2)	-0.12 (6)	2064 (10-I-3)	-6736 (9-II-2)	-1241 (9-II-4)
154	42	0.69 (10-II-3)	0.25 (9-II-2)	0.29 (9-II-2)	961 (10-I-3)	-6818 (9-II-2)	-2330 (9-II-2)
154	43	0.62 (9-II-3)	-0.26 (6)	0.25 (9-II-2)	1105 (10-I-3)	-6238 (9-II-2)	-2076 (9-II-4)
154	44	0.84 (10-II-3)	-0.26 (6)	0.25 (9-II-2)	662 (10-I-2)	-6434 (9-II-2)	-3103 (9-II-2)
154	45	0.70 (10-II-3)	-0.26 (6)	0.17 (9-II-2)	1059 (10-I-3)	-6089 (9-II-2)	-2823 (9-II-2)
154	46	0.90 (10-II-3)	-0.40 (10-II-2)	-0.18 (6)	-1431 (10-II-2)	-4124 (9-II-2)	-3666 (9-II-4)
154	47	0.79 (10-II-3)	-0.39 (10-II-2)	-0.20 (6)	958 (10-I-2)	-4515 (9-II-2)	-3810 (9-II-2)
154	48	0.55 (10-II-3)	-0.56 (6)	-0.31 (6)	1424 (10-I-2)	-3900 (10-I-2)	-2879 (9-II-4)
154	49	0.53 (9-II-3)	-0.35 (6)	-0.30 (10-I-3)	1975 (10-I-3)	-6528 (9-II-2)	-1155 (9-II-4)
154	50	0.53 (10-II-3)	-0.36 (6)	-0.13 (6)	1282 (10-I-3)	-5658 (9-II-2)	-2477 (9-II-4)
154	51	1.00 (10-II-3)	-0.27 (10-II-2)	0.31 (9-II-2)	-1351 (10-II-2)	-5543 (9-II-2)	-3798 (9-II-2)
154	52	1.20 (9-II-3)	-0.41 (10-II-2)	0.36 (9-II-2)	-2161 (9-II-3)	-5615 (9-II-2)	-3674 (9-II-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
154	53	0.93(10-II-3)	-0.20(6)	0.45(9-II-2)	-1123(10-II-2)	-6247(9-II-2)	-3442(9-II-2)
154	54	1.09(10-II-3)	-0.37(10-II-2)	0.18(9-II-2)	-1826(10-II-2)	-5055(9-II-2)	-3808(9-II-2)
154	55	1.07(9-II-3)	-0.40(10-II-2)	-0.13(6)	-2303(9-II-3)	-4223(9-II-2)	-3574(9-II-4)
154	56	0.76(9-II-3)	-0.49(10-II-2)	-0.21(6)	-5960(9-II-3)	-357(10-I-2)	-2013(10-I-2)
154	57	0.68(9-II-3)	-0.42(6)	-0.34(10-I-3)	-3673(9-II-3)	-2287(9-II-2)	-2102(9-II-1)
154	58	0.77(9-II-3)	-0.40(10-II-2)	-0.22(6)	-5353(9-II-3)	-1207(10-I-2)	-2330(10-I-2)
154	59	0.79(9-II-3)	-0.40(6)	-0.24(6)	-2256(10-II-2)	-3053(10-I-2)	-3045(9-II-4)
154	60	0.97(9-II-3)	-0.35(10-II-2)	-0.20(6)	-3050(9-II-3)	-3233(9-II-2)	-3405(9-II-4)
154	61	0.88(9-II-3)	-0.34(10-II-2)	-0.24(6)	-4303(9-II-3)	-2584(10-I-2)	-2532(10-I-2)
154	62	1.40(9-II-3)	-0.34(10-II-2)	0.32(9-II-2)	-3315(9-II-3)	-5305(9-II-2)	-3526(9-II-4)
154	63	1.43(9-II-3)	-0.42(10-II-2)	-0.11(6)	-3967(9-II-3)	-4118(9-II-2)	-3370(9-II-4)
154	64	1.26(9-II-3)	-0.36(10-II-2)	0.11(9-II-2)	-2992(9-II-3)	-4241(9-II-2)	-3591(9-II-4)
154	65	1.11(9-II-3)	-0.32(10-II-2)	-0.15(6)	-3616(9-II-3)	-3501(9-II-2)	-3441(9-II-4)
154	66	0.70(9-II-3)	-0.46(6)	0.11(9-II-3)	-6285(9-II-3)	1398(10-II-2)	-2373(10-I-2)
154	67	0.84(9-II-3)	-0.37(10-II-2)	-0.13(6)	-5852(9-II-3)	-602(10-I-2)	-2682(10-I-3)
154	68	1.01(9-II-3)	-0.31(10-II-2)	-0.19(6)	-4800(9-II-3)	-2410(10-I-2)	-2950(9-II-1)
155	1	-0.04(10-I-3)	-1.60(9-II-4)	1.51(9-II-3)	93(6)	-172(9-I-4)	479(9-II-3)
155	2	0.11(10-II-3)	-1.55(10-II-2)	1.42(9-II-4)	190(10-II-3)	-238(10-I-3)	598(9-II-3)
155	3	0.17(10-II-3)	-1.50(9-II-4)	1.29(9-II-3)	463(10-II-3)	-319(10-I-3)	643(9-II-3)
155	4	0.48(10-II-3)	-1.17(9-II-4)	0.94(9-II-3)	732(10-II-3)	-506(9-II-4)	502(10-II-3)
155	5	0.70(10-II-2)	-0.78(10-II-3)	0.75(10-II-2)	795(10-II-3)	-692(9-II-4)	162(10-II-3)
155	6	0.93(10-II-2)	-0.56(9-II-4)	0.72(9-II-3)	-255(10-I-3)	-1342(9-II-4)	-247(10-I-3)
155	7	0.80(10-II-2)	-0.73(9-II-4)	0.69(10-II-3)	-222(10-I-3)	-789(10-I-4)	364(9-II-4)
155	8	0.54(10-II-2)	-0.59(9-II-3)	0.66(10-II-2)	-635(9-II-4)	-888(9-II-3)	442(9-II-4)
155	9	0.18(10-I-4)	-0.57(10-I-4)	0.61(9-II-3)	-1085(9-II-4)	-851(9-II-3)	584(9-II-3)
155	10	0.16(10-II-2)	-0.24(10-I-4)	0.93(10-II-2)	-1467(9-II-4)	-683(9-II-3)	597(9-II-3)
155	11	-0.22(10-I-3)	-0.20(10-I-3)	0.72(10-II-3)	-1066(9-II-4)	-119(10-I-3)	496(9-II-3)
155	12	3.33(9-II-4)	-0.85(10-I-3)	0.64(10-II-3)	-792(9-II-4)	350(10-II-3)	410(9-II-4)
155	13	1.02(9-II-2)	-0.38(10-I-4)	0.63(10-I-4)	-173(9-II-4)	135(9-II-4)	187(9-I-1)
155	14	0.16(9-II-2)	-0.88(10-II-3)	1.49(9-II-3)	-71(10-I-3)	-240(9-I-2)	221(9-I-1)
155	15	0.05(10-II-3)	-0.14(10-I-4)	1.22(9-II-3)	-484(9-II-4)	-170(10-I-3)	-11(10-II-3)
155	16	-0.14(10-I-3)	-0.27(6)	1.41(9-II-4)	-144(9-II-4)	-140(10-I-3)	42(9-I-1)
155	17	-0.08(10-I-3)	-0.72(6)	1.44(9-II-3)	-127(9-II-4)	-123(9-I-4)	59(9-II-3)
155	18	0.26(10-II-2)	-0.71(10-I-4)	1.07(10-II-2)	-625(9-II-4)	-374(9-II-3)	86(9-II-3)
155	19	0.13(10-II-3)	-0.55(10-I-4)	0.96(10-II-3)	-912(9-II-4)	-466(9-II-3)	159(9-II-3)
155	20	0.69(10-II-2)	-0.90(10-I-4)	0.98(10-II-2)	-717(9-II-4)	-529(9-II-3)	214(9-II-4)
155	21	-0.11(10-I-3)	-0.45(10-I-4)	1.18(10-II-3)	-634(9-II-4)	-300(9-II-4)	35(9-II-3)
155	22	0.66(10-II-2)	-0.88(9-II-4)	1.03(10-II-2)	-72(10-I-3)	-460(9-II-3)	-24(6)
155	23	0.60(10-II-2)	-0.68(9-II-4)	0.87(10-II-2)	-548(9-II-4)	-453(10-I-4)	67(9-II-3)
155	24	0.45(10-II-2)	-0.75(10-I-4)	1.11(10-II-2)	-362(9-II-4)	-357(9-II-3)	29(9-II-3)
155	25	0.37(10-II-3)	-0.99(9-II-4)	1.14(9-II-3)	187(10-II-3)	-310(10-I-3)	113(9-II-3)
155	26	0.25(10-II-3)	-0.76(10-I-4)	1.25(9-II-3)	-255(9-II-4)	-231(10-I-3)	33(9-II-3)
155	27	0.13(10-II-3)	-0.93(6)	1.33(9-II-3)	44(6)	-227(10-I-3)	100(9-II-3)
156	1	-0.83(9-II-3)	-2.06(9-II-1)	1.33(10-I-4)	4821(9-II-4)	1401(9-II-4)	530(9-I-3)
156	2	-2.48(9-II-4)	-3.71(9-II-4)	-0.13(10-II-4)	5788(9-II-4)	3906(9-II-4)	348(9-I-3)
156	3	-2.60(9-II-4)	-2.60(9-II-1)	0.21(9-I-4)	4642(9-II-4)	3182(9-II-4)	720(9-II-1)
156	4	-2.56(9-II-3)	-2.53(9-II-1)	0.37(9-I-1)	3052(9-II-4)	1941(10-I-3)	59(10-II-4)
156	5	-2.34(9-II-3)	-2.59(10-I-2)	0.45(10-II-2)	1484(9-II-4)	1611(10-I-2)	-335(10-I-4)
156	6	-2.17(9-II-3)	-2.49(10-I-2)	0.69(9-II-3)	303(9-II-2)	1336(10-I-2)	-475(10-I-4)
156	7	-2.05(9-II-3)	-1.97(10-I-2)	1.02(9-II-1)	-1088(9-I-1)	812(10-I-2)	-534(10-I-3)
156	8	-1.48(9-II-3)	1.75(10-II-2)	1.20(9-II-4)	-2808(10-II-2)	-1192(10-II-2)	491(10-II-2)
156	9	-1.98(9-II-3)	-2.15(10-I-2)	1.50(9-II-3)	-2431(10-II-2)	849(10-I-2)	226(10-II-2)
156	10	-2.23(9-II-3)	-2.77(10-I-2)	1.34(10-II-2)	-1599(10-II-2)	1279(10-I-2)	-299(10-I-3)
156	11	-2.19(9-II-3)	-3.38(10-I-2)	1.16(10-II-2)	-1440(10-II-2)	1434(10-I-2)	-333(10-I-3)
156	12	-2.24(9-II-3)	-3.70(10-I-2)	0.89(10-II-2)	-1624(10-II-2)	1596(10-I-2)	-438(10-I-3)
156	13	-2.28(9-II-3)	-3.79(9-II-4)	0.54(10-II-2)	-1851(9-I-1)	1633(9-II-4)	-695(10-I-3)
156	14	-2.30(9-II-4)	-3.62(9-II-4)	-0.33(10-I-2)	-2162(9-I-3)	1422(9-II-3)	-992(10-I-3)
156	15	-2.44(10-I-2)	-3.04(9-II-3)	-0.44(10-I-2)	-2608(9-I-3)	897(9-II-3)	-1207(10-I-3)
156	16	-2.64(10-I-2)	-2.16(10-II-2)	0.31(10-II-2)	-3401(9-I-3)	-514(10-I-2)	-1108(10-I-3)
156	17	-2.72(9-II-4)	1.14(10-I-2)	1.12(9-I-3)	-5016(9-I-3)	-2123(10-I-2)	-1216(10-I-2)
156	18	-2.80(9-II-3)	-1.37(6)	1.17(9-I-2)	-603(9-I-2)	-1449(9-I-4)	-141(10-I-3)
156	19	-3.19(9-II-3)	-1.71(6)	1.62(10-II-2)	2920(9-II-4)	-789(9-I-4)	-127(10-I-4)
156	20	-4.12(9-II-3)	-2.18(6)	2.16(10-I-4)	5265(9-II-4)	1059(6)	109(10-II-4)
156	21	-1.12(9-II-3)	-1.77(6)	1.55(10-I-4)	4645(9-II-4)	643(9-II-4)	526(10-II-4)
156	22	-2.25(9-II-3)	-2.34(9-II-4)	0.92(9-I-1)	1017(9-II-4)	936(9-II-3)	-173(10-I-4)
156	23	-2.54(9-II-4)	-2.04(9-II-3)	0.65(9-I-2)	-1231(9-I-3)	645(9-II-3)	-309(10-I-4)
156	24	-2.45(9-II-3)	-1.90(9-II-4)	1.34(9-I-3)	467(9-II-2)	-313(9-I-3)	167(10-II-4)
156	25	-2.33(9-II-4)	-2.71(9-II-3)	0.43(10-II-2)	-1112(9-I-3)	1377(9-II-3)	-476(10-I-4)
156	26	-2.16(9-II-4)	-2.65(9-II-4)	0.58(9-I-1)	992(9-II-4)	1584(9-II-3)	-294(10-I-4)
156	27	-1.86(9-II-3)	-2.72(9-II-4)	0.66(9-I-1)	2506(9-II-4)	1724(9-II-3)	-263(10-I-4)
156	28	-1.53(9-II-3)	-2.69(9-II-4)	0.71(9-I-1)	3868(9-II-4)	1710(9-II-4)	-269(10-I-4)
156	29	-2.20(9-II-3)	-2.10(9-II-4)	1.55(10-I-4)	2608(9-II-4)	389(9-II-4)	230(10-II-4)
156	30	-1.48(9-II-3)	-2.55(9-II-4)	1.56(10-I-4)	3612(9-II-4)	837(9-II-4)	185(10-II-4)
156	31	-1.86(9-II-3)	-2.47(9-II-4)	1.14(9-I-1)	2317(9-II-4)	962(9-II-3)	-121(10-I-4)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
156	32	-2.52(9-II-3)	-2.67(9-II-1)	0.39(10-II-2)	1633(9-II-4)	2236(10-I-3)	95(10-II-4)
156	33	-2.41(9-II-3)	-2.89(10-I-2)	0.58(10-II-2)	473(9-II-1)	1818(10-I-2)	-245(10-I-4)
156	34	-2.44(9-II-3)	-3.06(10-I-3)	0.53(10-II-2)	-189(9-I-2)	2054(10-I-3)	-223(10-I-4)
156	35	-2.39(9-II-4)	-3.06(9-II-4)	0.33(10-II-2)	-750(9-I-2)	1899(9-II-4)	-468(10-I-4)
156	36	-2.48(9-II-3)	-3.11(9-II-4)	0.40(10-II-2)	-352(9-I-2)	2141(9-II-4)	-332(10-I-4)
156	37	-2.55(9-II-3)	-2.63(9-II-4)	0.21(9-I-1)	2379(9-II-4)	2785(9-II-4)	-149(10-I-4)
156	38	-2.69(9-II-4)	-2.54(9-II-1)	0.34(10-II-2)	2014(9-II-4)	2651(9-II-4)	125(10-II-4)
156	39	-2.75(9-II-4)	-2.65(9-II-1)	0.25(9-I-1)	3167(9-II-4)	3075(9-II-4)	87(10-II-4)
156	40	-2.52(9-II-3)	-2.75(9-II-4)	0.28(10-II-2)	1306(9-II-4)	2429(9-II-4)	-161(10-I-4)
156	41	-2.23(9-II-4)	-2.67(9-II-4)	0.23(9-I-1)	3857(9-II-4)	2860(9-II-4)	-255(10-I-4)
156	42	-2.34(9-II-4)	-2.80(9-II-4)	0.35(9-I-1)	1087(9-II-4)	2158(9-II-4)	-314(10-I-4)
156	43	-2.27(9-II-4)	-2.69(9-II-4)	0.30(9-I-1)	2533(9-II-4)	2454(9-II-4)	-279(10-I-4)
157	1	-5.64(9-II-4)	-1.92(10-I-3)	1.79(9-II-4)	3345(9-II-4)	2010(9-II-3)	77(9-I-3)
157	2	-5.23(9-II-4)	-2.02(10-I-3)	2.24(9-II-4)	2287(9-II-4)	178(9-II-3)	383(10-I-3)
157	3	-1.60(9-II-4)	-1.06(10-I-3)	0.77(10-I-3)	1252(10-I-3)	496(9-II-4)	-796(10-II-2)
157	4	-1.36(9-II-4)	-1.13(10-I-3)	0.75(10-I-3)	1483(10-I-3)	881(9-II-4)	-1169(9-II-3)
157	5	-0.65(10-II-3)	-0.68(10-I-3)	-0.22(10-II-4)	1730(10-I-3)	1319(9-II-4)	-1473(9-II-3)
157	6	-5.10(9-II-4)	-1.12(10-I-3)	0.65(10-I-4)	5627(9-II-4)	1530(9-II-4)	-1596(9-II-3)
157	7	-5.66(9-II-4)	-2.01(10-I-3)	1.78(10-I-4)	4562(9-II-4)	2166(9-II-4)	-1084(9-II-3)
157	8	-3.02(9-II-4)	-2.09(10-I-3)	1.10(10-I-3)	2333(9-II-4)	1151(9-II-4)	-1034(9-II-3)
158	1	-2.45(10-I-3)	-1.87(9-II-4)	-0.41(10-II-2)	1955(10-I-2)	1094(9-II-4)	800(10-II-2)
158	2	-2.77(10-I-2)	-1.16(9-II-4)	-0.51(10-II-2)	988(10-I-2)	-174(10-II-2)	379(10-II-2)
158	3	-2.12(10-I-2)	0.60(9-I-3)	-0.40(10-II-2)	-1676(10-II-2)	-1519(10-II-2)	-598(10-I-2)
158	4	-2.75(10-I-2)	-1.13(10-I-2)	-0.61(10-II-2)	951(10-I-2)	-659(10-II-2)	-238(10-I-2)
158	5	-2.60(10-I-3)	-1.78(10-I-2)	-0.38(10-II-2)	1748(10-I-2)	766(9-II-1)	416(10-II-2)
158	6	-2.47(10-I-3)	-2.06(9-II-4)	-0.20(10-II-2)	2377(10-I-3)	1733(9-II-1)	844(10-II-2)
158	7	-2.50(10-I-3)	-2.14(9-II-4)	-0.14(10-II-2)	2851(10-I-3)	2711(9-II-4)	1371(10-II-2)
158	8	-2.91(10-I-3)	-2.41(9-II-4)	-0.53(10-II-2)	3355(9-II-4)	3174(9-II-4)	2533(9-II-3)
158	9	-1.10(10-I-3)	-1.80(9-II-4)	0.31(10-I-3)	3636(9-II-4)	984(10-I-3)	1347(10-II-2)
158	10	-1.79(10-I-3)	-2.22(9-II-4)	0.15(10-I-2)	3229(10-I-3)	1853(9-II-4)	1700(10-II-2)
158	11	-2.14(10-I-3)	-2.21(9-II-4)	-0.23(10-II-2)	2697(10-I-3)	1836(9-II-4)	1244(10-II-2)
159	1	-1.30(10-I-3)	-2.08(9-II-4)	2.00(9-II-4)	1790(10-I-3)	3212(10-I-3)	554(9-II-1)
159	2	-1.10(10-I-3)	-2.17(9-II-4)	1.93(9-II-4)	1495(10-I-3)	3584(10-I-3)	-210(10-II-2)
159	3	-0.69(6)	-4.06(10-I-3)	1.81(6)	1401(10-I-3)	3981(10-I-3)	-173(10-II-2)
159	4	-1.10(10-I-3)	-2.46(10-I-3)	1.84(6)	1531(10-I-3)	3768(10-I-3)	-344(10-II-2)
159	5	-1.30(10-I-3)	-1.50(9-II-4)	1.70(10-II-3)	1555(10-I-3)	3410(10-I-3)	176(10-I-3)
159	6	-0.71(10-I-3)	-0.41(9-II-4)	1.18(10-II-3)	704(10-I-3)	3027(10-I-3)	834(9-II-4)
159	7	-0.56(10-I-3)	-0.25(9-II-4)	1.41(10-II-3)	818(10-I-3)	3090(10-I-3)	939(10-II-3)
159	8	-0.88(10-I-3)	-0.81(9-II-4)	1.35(10-II-3)	1257(10-I-3)	3168(10-I-3)	1050(9-II-4)
159	9	-1.27(10-I-3)	-0.83(9-II-4)	1.60(10-II-3)	1512(10-I-3)	3226(10-I-3)	446(10-I-3)
160	1	-4.37(10-I-3)	-1.14(9-II-2)	-1.17(9-II-3)	1877(10-I-2)	1574(10-I-3)	932(10-II-2)
160	2	-4.31(10-I-3)	-0.60(9-II-2)	-0.49(9-II-3)	649(10-I-2)	989(10-I-3)	865(10-II-2)
160	3	-3.48(9-II-4)	0.41(10-II-2)	0.93(9-I-3)	-570(10-II-2)	865(10-I-3)	1130(10-II-2)
160	4	-1.72(9-II-1)	0.84(9-I-3)	1.97(10-I-2)	-2181(10-II-2)	-335(10-II-3)	533(10-II-2)
160	5	-2.89(9-II-4)	-0.91(10-I-2)	0.47(10-I-2)	1031(10-I-2)	-335(10-II-2)	354(10-II-2)
160	6	-2.85(10-I-3)	-1.56(10-I-2)	-0.31(10-II-2)	2414(10-I-3)	798(10-I-2)	648(10-II-2)
160	7	-2.29(10-I-3)	-2.05(10-I-3)	-0.62(10-II-2)	3533(10-I-3)	1115(10-I-3)	727(10-II-2)
160	8	-1.41(10-I-3)	-2.20(6)	-0.84(10-II-3)	4059(10-I-3)	1096(10-I-3)	515(10-II-3)
160	9	-0.52(10-I-3)	-1.65(6)	-1.07(10-II-3)	3516(10-I-3)	908(10-I-3)	-143(10-I-3)
160	10	-1.48(10-I-3)	-1.87(10-I-3)	-1.49(10-II-3)	3737(10-I-3)	1328(10-I-3)	419(10-II-3)
160	11	-2.69(10-I-3)	-1.68(10-I-3)	-1.84(9-II-3)	3745(10-I-3)	1457(10-I-3)	652(10-II-2)
160	12	-3.79(10-I-3)	-1.66(9-II-4)	-2.19(9-II-3)	3489(10-I-3)	1492(10-I-3)	530(10-II-2)
160	13	-3.99(10-I-3)	-1.51(9-II-4)	-1.75(9-II-3)	2782(10-I-3)	1531(10-I-3)	749(10-II-2)
160	14	-3.44(10-I-3)	-1.31(9-II-4)	-0.62(9-II-3)	2465(10-I-3)	943(10-I-3)	846(10-II-2)
160	15	-2.99(10-I-3)	-1.73(9-II-4)	-1.20(9-II-3)	3435(10-I-3)	1278(10-I-3)	746(10-II-2)
161	1	-1.43(10-I-2)	-4.11(10-II-2)	-0.18(10-II-2)	-82(9-I-1)	-3334(9-I-1)	707(6)
161	2	-2.08(9-II-1)	-3.82(10-II-2)	-0.39(10-II-2)	502(10-II-4)	-3156(9-I-1)	734(6)
161	3	-2.64(9-II-1)	-3.53(10-II-2)	-0.37(10-II-2)	757(10-II-1)	-3019(9-I-2)	817(6)
161	4	-2.99(9-II-1)	-3.31(10-II-2)	0.37(10-I-2)	873(10-II-1)	-2926(9-I-2)	919(6)
161	5	-3.14(10-II-1)	-3.11(10-II-2)	0.69(10-I-2)	796(10-II-1)	-2980(9-I-3)	1096(6)
161	6	-3.16(10-II-1)	-2.93(10-II-2)	1.15(10-I-2)	348(10-II-2)	-3396(10-I-2)	1447(6)
161	7	-2.75(10-II-2)	-2.74(10-II-2)	1.63(10-I-2)	-1192(10-I-2)	-4110(10-I-2)	1973(10-I-2)
161	8	-1.96(10-II-2)	-3.39(9-I-1)	1.91(10-I-2)	-2853(10-I-2)	-4942(10-I-2)	2351(9-I-1)
161	9	-2.57(10-II-2)	-3.00(9-I-2)	1.36(10-I-2)	-594(10-I-2)	-3982(10-I-2)	1326(9-I-2)
161	10	-2.77(10-II-1)	-3.07(10-II-2)	0.97(10-I-2)	874(10-II-2)	-2868(10-I-2)	881(9-I-1)
161	11	-2.73(10-II-1)	-3.22(10-II-2)	0.70(10-I-2)	1277(10-II-1)	-2004(9-I-3)	581(9-I-1)
161	12	-2.52(9-II-1)	-3.34(10-II-2)	0.58(10-I-2)	1414(10-II-1)	-1236(9-I-3)	301(10-II-2)
161	13	-2.33(9-II-1)	-3.36(10-II-2)	0.56(10-I-2)	1408(9-II-1)	-435(9-I-2)	-169(9-II-1)
161	14	-2.22(9-II-1)	-3.37(10-II-2)	0.61(10-I-2)	1099(9-II-1)	589(9-II-2)	-440(9-II-1)
161	15	-2.16(9-II-1)	-3.39(10-II-2)	0.80(10-I-1)	366(9-II-1)	1387(9-II-4)	-800(9-II-2)
161	16	-2.22(9-II-1)	-3.74(9-II-4)	0.90(10-I-1)	-622(9-I-1)	2453(9-II-4)	-1465(9-II-3)
161	17	-2.00(9-II-1)	-4.74(9-II-3)	0.57(10-I-1)	-1094(9-I-1)	4406(9-II-4)	-1750(10-I-4)
161	18	-1.42(9-II-1)	-4.03(9-II-4)	0.40(10-I-1)	-1006(9-I-1)	2405(9-II-4)	-746(10-I-4)
161	19	-1.02(6)	-3.33(9-II-4)	0.39(10-I-1)	-1844(9-I-1)	-429(9-I-2)	254(6)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
161	20	1.06(10-II-2)	-3.06(9-II-4)	1.44(10-II-2)	-2311(10-II-2)	-4980(9-I-1)	1293(10-II-2)
161	21	-0.67(10-I-2)	-4.01(10-II-2)	0.31(9-I-1)	-1078(10-II-2)	-3756(10-II-2)	912(6)
161	22	-2.46(9-II-1)	-3.50(10-II-2)	0.30(10-I-2)	923(9-II-1)	-2040(9-I-2)	608(10-II-2)
161	23	-2.64(9-II-1)	-3.41(10-II-2)	0.44(10-I-2)	1180(10-II-4)	-1839(9-I-2)	569(10-II-2)
161	24	-2.40(9-II-1)	-3.41(10-II-2)	0.47(10-I-2)	1143(9-II-1)	-1174(9-I-2)	332(10-II-2)
161	25	-1.74(9-II-1)	-3.58(10-II-2)	0.64(10-I-1)	-218(9-I-1)	-403(9-I-2)	122(6)
161	26	-1.36(9-II-1)	-3.68(10-II-2)	0.71(9-I-1)	-678(9-I-1)	-1052(9-I-2)	476(6)
161	27	-1.64(9-II-1)	-3.73(10-II-2)	0.41(10-I-1)	139(9-II-1)	-1867(9-I-2)	622(6)
161	28	-2.17(9-II-1)	-3.47(10-II-2)	0.54(10-I-2)	825(9-II-1)	-781(9-I-2)	148(10-II-2)
161	29	-2.07(9-II-1)	-3.64(10-II-2)	0.30(10-I-2)	626(9-II-1)	-1884(9-I-2)	562(10-II-2)
162	1	-3.47(10-II-1)	-1.41(10-II-1)	-0.28(9-II-1)	4464(10-II-1)	1452(10-II-1)	129(9-II-1)
162	2	-3.38(10-II-1)	-1.60(10-II-1)	-0.21(9-II-1)	4526(10-II-1)	1382(10-II-1)	326(9-II-1)
162	3	-3.28(10-II-1)	-1.78(10-II-1)	-0.15(9-II-1)	4132(9-II-4)	1230(10-II-1)	475(9-II-4)
162	4	-3.16(10-II-1)	-1.92(10-II-1)	0.12(9-I-1)	3131(9-II-2)	871(10-II-1)	613(9-II-4)
162	5	-3.02(6)	-1.99(10-II-1)	0.19(9-I-1)	1547(9-II-2)	334(10-II-2)	692(9-II-3)
162	6	-2.88(9-II-4)	-1.94(10-II-2)	0.29(9-I-4)	-1426(9-I-2)	-889(10-I-2)	675(9-II-3)
162	7	-2.78(9-II-1)	-1.36(10-II-2)	0.61(10-I-2)	-6272(9-I-2)	-2150(10-I-2)	792(10-II-2)
162	8	-2.83(9-II-1)	-2.03(10-II-2)	0.17(9-I-4)	-1439(9-I-2)	-964(10-II-2)	558(10-II-2)
162	9	-2.99(9-II-1)	-1.99(10-II-1)	-0.12(9-II-1)	1580(9-II-2)	206(10-II-2)	547(9-II-3)
162	10	-3.14(6)	-1.95(10-II-1)	-0.16(9-II-1)	3175(9-II-2)	767(10-II-1)	508(9-II-3)
162	11	-3.27(10-II-1)	-1.84(10-II-1)	-0.22(9-II-1)	4217(9-II-4)	1095(10-II-1)	422(9-II-4)
162	12	-3.36(10-II-1)	-1.69(10-II-1)	-0.30(9-II-1)	4696(10-II-1)	1232(10-II-1)	286(9-II-4)
162	13	-3.44(10-II-1)	-1.58(10-II-1)	-0.39(9-II-1)	4705(10-II-1)	1237(10-II-1)	168(9-II-4)
162	14	-3.52(10-II-1)	-1.45(10-II-1)	-0.52(9-II-1)	4244(6)	1135(10-II-1)	55(9-II-1)
162	15	-3.61(10-II-1)	-1.37(10-II-1)	-0.68(9-II-4)	3317(6)	943(10-II-1)	-165(9-I-1)
162	16	-3.69(10-II-1)	-1.29(10-II-1)	-0.83(9-II-4)	1823(6)	639(9-I-2)	-338(9-I-1)
162	17	-3.69(10-II-1)	-1.21(10-II-1)	-0.76(9-II-4)	1693(6)	680(9-I-2)	-415(9-I-1)
162	18	-3.62(10-II-1)	-1.13(10-II-1)	-0.71(9-II-4)	1586(6)	766(9-I-2)	-482(9-I-1)
162	19	-3.51(6)	-1.02(10-II-1)	-0.73(9-II-1)	1570(9-I-2)	886(9-I-2)	-549(9-I-1)
162	20	-3.56(6)	-1.06(10-II-1)	-0.54(9-II-1)	3070(6)	1210(10-II-1)	-359(9-I-1)
162	21	-3.52(10-II-1)	-1.21(10-II-1)	-0.39(9-II-1)	3997(6)	1384(10-II-1)	-186(9-I-1)
162	22	-3.46(10-II-1)	-1.44(10-II-1)	-0.32(9-II-1)	4493(10-II-1)	1347(10-II-1)	110(9-II-1)
162	23	-3.40(10-II-1)	-1.56(10-II-1)	-0.28(9-II-1)	4665(10-II-1)	1323(10-II-1)	241(9-II-1)
162	24	-3.47(10-II-1)	-1.48(10-II-1)	-0.38(9-II-1)	4567(10-II-1)	1279(10-II-1)	137(9-II-1)
162	25	-3.61(10-II-1)	-1.26(10-II-1)	-0.63(9-II-4)	3174(6)	971(10-II-1)	-216(9-I-1)
162	26	-3.59(10-II-1)	-1.16(10-II-1)	-0.58(9-II-1)	3100(6)	1056(10-II-1)	-284(9-I-1)
162	27	-3.54(10-II-1)	-1.35(10-II-1)	-0.49(9-II-1)	4105(6)	1173(10-II-1)	-100(9-I-1)
162	28	-3.53(10-II-1)	-1.28(10-II-1)	-0.44(9-II-1)	4026(6)	1252(10-II-1)	-148(9-I-1)
163	1	-0.80(6)	-2.42(6)	0.38(9-II-1)	799(10-II-1)	-1276(9-II-2)	1132(9-I-1)
163	2	-4.19(10-II-1)	-2.76(10-II-2)	-0.20(9-I-1)	934(10-II-1)	-3118(9-II-2)	1710(10-I-4)
163	3	-2.71(6)	-1.91(10-II-4)	0.83(9-II-1)	-212(9-II-3)	-3079(9-II-2)	1852(9-I-1)
163	4	-1.63(6)	-1.30(6)	0.91(6)	574(6)	-2709(9-II-2)	1396(9-I-1)
163	5	-1.12(6)	-0.50(6)	0.96(6)	-576(10-I-4)	-3344(9-II-2)	1298(9-I-1)
163	6	-0.60(9-I-2)	0.32(9-II-3)	0.29(6)	-612(9-I-1)	-1343(9-II-2)	1020(10-II-2)
163	7	0.12(9-II-2)	-0.41(6)	0.07(6)	-577(10-I-4)	-326(9-II-2)	867(10-II-2)
163	8	0.19(9-II-2)	1.12(9-II-3)	0.72(9-II-4)	-687(10-I-4)	246(10-II-3)	710(10-II-2)
163	9	-0.15(9-I-2)	-1.15(6)	0.33(6)	189(6)	-287(9-II-2)	1049(9-I-1)
164	1	-2.96(10-II-1)	-0.83(6)	1.01(10-I-4)	-433(9-II-2)	3391(9-I-1)	1320(9-II-2)
164	2	-3.63(10-II-1)	-2.32(9-I-1)	1.14(10-I-4)	-1734(9-II-3)	2440(9-I-1)	1209(9-II-2)
164	3	-2.56(6)	-0.76(9-I-2)	1.15(10-I-4)	-665(9-II-3)	1937(9-I-2)	257(9-II-2)
164	4	-1.77(6)	0.22(9-II-2)	0.84(10-II-2)	-393(9-II-3)	1620(10-II-1)	-362(9-I-2)
164	5	-1.03(6)	1.01(9-II-2)	0.53(6)	-925(10-I-4)	652(10-II-1)	-494(10-II-2)
164	6	-2.16(6)	0.54(9-II-2)	1.10(10-I-4)	189(10-II-1)	1860(10-II-1)	124(9-II-2)
164	7	-2.84(6)	0.30(9-II-2)	1.48(10-I-4)	847(10-II-1)	2805(10-II-1)	371(9-II-2)
164	8	-2.64(6)	-0.23(6)	1.81(10-I-4)	903(10-II-1)	4230(9-I-1)	807(9-II-2)
164	9	-2.69(10-II-1)	-0.53(6)	1.40(10-I-4)	636(10-II-1)	4012(9-I-1)	1235(9-II-2)
164	10	-2.97(6)	-0.38(6)	1.44(10-I-4)	280(10-II-1)	2831(9-I-2)	585(9-II-2)
165	1	-2.20(6)	-1.66(9-II-1)	-1.49(6)	645(10-II-1)	2455(10-II-4)	685(10-I-1)
165	2	-2.10(6)	-1.38(6)	-1.59(6)	1344(10-II-1)	2418(10-II-4)	241(10-I-1)
165	3	-2.00(6)	-1.22(6)	-1.77(10-I-2)	2035(10-II-1)	2219(10-II-1)	-294(9-II-2)
165	4	-1.85(6)	-1.38(6)	-1.99(10-I-3)	2549(10-II-1)	2012(10-II-1)	-598(9-II-3)
165	5	-1.76(6)	-1.45(6)	-2.35(9-II-4)	3698(9-I-2)	2023(10-II-1)	-1088(9-II-3)
165	6	-1.65(6)	-1.30(6)	-2.16(9-II-4)	2339(10-II-1)	1668(10-II-1)	-686(9-II-2)
165	7	-1.11(6)	-1.01(6)	-1.71(9-II-4)	1173(10-II-1)	1010(10-II-4)	-390(9-II-2)
165	8	0.76(9-II-2)	-1.23(6)	-1.07(6)	-481(10-I-3)	-212(10-I-4)	320(9-I-2)
165	9	-0.58(6)	-2.18(9-II-4)	-1.65(6)	-769(10-I-3)	167(10-II-4)	834(10-I-4)
165	10	-1.30(6)	-3.13(9-II-4)	-2.36(9-II-4)	-1380(9-I-1)	270(10-II-4)	1230(10-I-4)
165	11	-5.60(10-II-2)	-4.37(9-II-4)	-2.58(9-II-4)	647(9-II-4)	1752(10-II-4)	2699(10-I-4)
165	12	-3.15(10-II-2)	-2.77(9-II-4)	-1.89(9-II-4)	-1096(9-I-2)	2506(10-II-4)	1931(10-I-4)
165	13	-2.45(6)	-2.13(9-II-4)	-1.61(6)	-504(9-I-2)	2536(10-II-4)	1233(10-I-4)
165	14	-1.65(6)	-1.33(6)	-1.65(6)	1158(10-II-1)	1910(10-II-4)	69(10-I-1)
165	15	-1.63(6)	-1.55(9-II-1)	-1.57(6)	-232(10-I-1)	1787(10-II-4)	707(10-I-4)
166	1	-3.36(6)	-1.35(10-II-2)	0.62(10-I-4)	3957(6)	1997(10-II-1)	-677(10-II-2)
166	2	-3.24(6)	-1.65(10-II-2)	0.59(10-I-4)	4211(10-II-4)	1717(10-II-1)	-509(10-II-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
166	3	-3.16(6)	-1.90(10-II-2)	0.56(9-I-1)	3979(9-II-4)	1374(10-II-2)	-266(10-II-2)
166	4	-3.07(6)	-2.10(10-II-2)	0.54(9-I-1)	3211(9-II-4)	895(10-II-2)	92(9-I-1)
166	5	-2.98(9-II-4)	-2.20(10-II-2)	0.54(9-I-4)	1859(9-II-2)	214(10-II-2)	513(9-I-1)
166	6	-2.88(9-II-4)	-2.08(10-II-2)	0.57(10-I-4)	-856(9-I-2)	-1093(10-I-2)	965(10-II-2)
166	7	-2.68(9-II-4)	-1.61(10-II-2)	1.22(10-I-2)	-5060(9-I-3)	-2394(10-II-2)	1725(10-II-2)
166	8	-2.85(9-II-4)	-2.11(9-I-4)	0.59(10-I-1)	-872(9-I-2)	-1195(10-I-2)	680(10-II-2)
166	9	-2.95(9-II-4)	-2.18(10-II-2)	0.49(9-I-4)	1854(9-II-2)	-141(10-I-2)	378(9-I-1)
166	10	-3.05(6)	-2.07(10-II-2)	0.51(9-I-1)	3234(9-II-4)	811(10-II-2)	-50(10-I-2)
166	11	-3.15(6)	-1.92(10-II-2)	0.52(9-I-1)	4021(9-II-4)	1286(10-II-2)	-347(10-I-4)
166	12	-3.23(6)	-1.70(10-II-2)	0.54(10-I-4)	4305(10-II-4)	1620(10-II-1)	-577(10-II-2)
166	13	-3.37(6)	-1.42(10-II-2)	0.53(10-I-4)	4085(10-II-4)	1820(10-II-1)	-773(10-II-2)
166	14	-3.48(10-II-4)	-1.13(10-II-2)	0.47(10-I-2)	3514(6)	1885(10-II-1)	-839(10-II-2)
166	15	-3.61(10-II-4)	-0.90(10-II-2)	0.39(6)	2595(6)	1733(10-II-1)	-806(9-I-2)
166	16	-3.64(10-II-4)	-0.62(10-II-2)	0.19(6)	1223(9-I-2)	1486(9-I-2)	-665(9-I-2)
166	17	-3.66(6)	-0.44(10-II-2)	0.11(6)	1249(9-I-2)	1654(9-I-2)	-776(9-I-2)
166	18	-3.75(6)	-0.37(6)	-0.11(9-II-1)	1345(9-I-2)	1843(9-I-2)	-949(9-I-2)
166	19	-4.02(6)	-0.18(6)	0.09(6)	1434(9-I-2)	2243(9-I-1)	-1134(9-I-2)
166	20	-3.64(6)	-0.52(10-II-2)	0.51(10-I-2)	2417(6)	2436(10-II-1)	-796(9-I-1)
166	21	-3.48(6)	-0.95(10-II-2)	0.57(10-I-2)	3276(6)	2152(10-II-1)	-801(10-II-2)
166	22	-3.61(6)	-0.71(10-II-2)	0.43(6)	2259(6)	2156(10-II-1)	-831(9-I-2)
166	23	-3.52(6)	-0.84(10-II-2)	0.49(10-I-2)	3107(6)	2059(10-II-1)	-852(10-II-2)
166	24	-3.61(6)	-0.72(10-II-2)	0.35(6)	2306(6)	1883(10-II-1)	-790(9-I-2)
167	1	-2.93(9-II-4)	-2.26(10-II-2)	0.73(10-I-4)	3008(9-II-4)	961(10-II-2)	-164(9-II-1)
167	2	-2.96(6)	-2.12(10-II-2)	0.78(10-I-4)	3678(9-II-4)	1506(10-II-2)	-492(9-II-1)
167	3	-2.98(6)	-1.93(10-II-2)	0.87(10-I-4)	3887(9-II-1)	1948(10-II-1)	-698(6)
167	4	-3.02(6)	-1.66(10-II-2)	0.97(10-I-4)	3684(10-II-4)	2274(10-II-1)	-759(6)
167	5	-3.12(6)	-1.25(10-II-2)	1.10(10-I-4)	3115(6)	2634(10-II-1)	-677(6)
167	6	-3.39(6)	-0.70(10-II-2)	1.17(10-I-4)	2284(6)	2799(10-II-1)	-533(6)
167	7	-3.80(10-II-1)	0.22(9-II-2)	1.30(10-I-4)	1452(9-I-2)	3653(10-II-1)	-545(9-I-2)
167	8	-3.12(6)	-0.51(6)	1.27(10-I-4)	2210(10-II-4)	3107(10-II-1)	-175(6)
167	9	-2.87(6)	-0.89(10-II-2)	1.31(10-I-4)	2534(10-II-4)	2471(10-II-1)	100(9-II-1)
167	10	-2.79(6)	-1.16(10-II-2)	1.26(10-I-4)	2834(10-II-4)	1599(10-II-1)	245(9-II-1)
167	11	-2.84(6)	-1.52(10-II-2)	1.23(6)	3126(10-II-4)	682(10-II-1)	280(9-II-1)
167	12	-3.11(9-II-4)	-2.13(10-II-2)	1.12(6)	3681(9-II-4)	-529(10-I-1)	142(9-I-3)
167	13	-3.70(9-II-4)	-2.97(10-II-2)	1.07(6)	4310(9-II-4)	-1548(10-I-4)	-334(10-I-4)
167	14	-4.89(9-II-4)	-3.25(10-II-1)	1.21(10-II-2)	5002(9-II-4)	-2316(9-I-1)	-2025(9-II-4)
167	15	-3.76(9-II-4)	-2.54(10-II-1)	0.71(10-II-2)	3902(9-II-4)	-966(9-I-1)	-1030(9-II-3)
167	16	-3.27(9-II-1)	-2.31(10-II-1)	0.58(10-II-2)	3218(9-II-4)	202(10-II-1)	-505(9-II-3)
167	17	-3.19(6)	-2.29(10-II-1)	0.60(9-I-1)	2373(9-II-1)	672(10-II-1)	195(9-I-3)
167	18	-3.17(10-I-2)	-2.42(10-II-2)	0.63(9-I-1)	1779(9-II-1)	783(10-II-1)	603(9-I-3)
167	19	-3.21(10-I-2)	-2.53(10-II-2)	0.63(9-I-1)	1309(9-II-1)	721(10-II-2)	908(9-I-3)
167	20	-3.21(10-I-2)	-2.53(10-II-2)	0.61(9-I-2)	719(9-II-2)	492(10-II-2)	1147(9-I-2)
167	21	-3.24(6)	-2.45(10-II-2)	0.69(10-I-1)	-544(9-I-2)	-472(10-I-2)	1399(9-I-1)
167	22	-3.24(9-II-4)	-2.22(10-II-2)	0.89(10-I-2)	-1726(9-I-3)	-1216(10-I-2)	1755(10-II-2)
167	23	-2.70(9-II-3)	-2.04(10-II-2)	1.53(10-I-2)	-4313(10-I-2)	-2479(10-II-2)	1906(10-II-2)
167	24	-2.84(9-II-4)	-2.22(10-II-2)	0.86(10-I-2)	-581(9-I-2)	-1296(10-I-2)	1166(9-I-1)
167	25	-2.92(9-II-4)	-2.33(10-II-2)	0.74(10-I-1)	1673(9-II-2)	-215(10-I-2)	548(9-I-1)
167	26	-3.00(6)	-2.29(10-II-2)	0.76(10-I-4)	2692(9-II-4)	955(10-II-2)	311(9-I-2)
167	27	-3.09(6)	-2.39(10-II-2)	0.71(9-I-2)	1977(9-II-2)	786(10-II-2)	690(9-I-2)
167	28	-3.03(6)	-2.39(10-II-2)	0.74(10-I-1)	1487(9-II-2)	373(10-II-2)	781(9-I-1)
167	29	-3.09(6)	-2.36(10-II-2)	0.71(9-I-1)	2357(9-II-1)	1008(10-II-2)	495(9-I-3)
167	30	-2.98(6)	-2.19(10-II-2)	0.79(10-I-4)	3381(9-II-1)	1411(10-II-2)	-204(9-II-2)
167	31	-3.05(6)	-2.30(10-II-1)	0.66(10-I-4)	2944(9-II-1)	929(10-II-1)	129(9-I-3)
167	32	-3.11(6)	-2.31(10-II-2)	0.69(9-I-1)	2544(9-II-1)	1001(10-II-1)	355(9-I-3)
167	33	-3.04(6)	-2.25(10-II-2)	0.71(10-I-4)	3156(9-II-1)	1222(10-II-1)	148(9-I-3)
167	34	-3.01(6)	-2.23(10-II-2)	0.75(10-I-4)	3188(9-II-1)	1342(10-II-2)	117(9-I-3)
167	35	-2.88(6)	-2.05(10-II-2)	0.88(10-I-4)	3682(9-II-1)	1466(10-II-1)	-164(10-II-2)
167	36	-2.96(6)	-2.17(10-II-2)	0.77(10-I-4)	3519(9-II-1)	1351(10-II-1)	-144(9-II-3)
167	37	-2.93(6)	-2.19(10-II-2)	0.81(10-I-4)	3699(9-II-4)	1011(10-II-1)	-112(10-II-2)
167	38	-3.03(6)	-2.35(10-II-2)	0.70(10-I-4)	3578(9-II-4)	382(10-II-1)	-188(9-II-3)
167	39	-3.01(6)	-2.19(10-II-2)	0.66(10-I-4)	3480(9-II-4)	999(10-II-1)	-190(9-II-3)
167	40	-2.85(6)	-2.07(10-II-2)	0.94(6)	3658(9-II-4)	1035(10-II-1)	-58(10-II-2)
167	41	-2.83(6)	-1.86(10-II-2)	1.07(6)	3499(10-II-4)	909(10-II-1)	129(9-I-3)
167	42	-2.93(6)	-2.21(10-II-2)	0.88(6)	3748(9-II-4)	330(10-II-1)	-95(10-II-2)
167	43	-2.80(6)	-1.56(10-II-2)	1.16(10-I-4)	3275(10-II-4)	1625(10-II-1)	83(9-I-3)
167	44	-2.83(6)	-1.87(10-II-2)	1.03(10-I-4)	3578(9-II-4)	1554(10-II-1)	-106(10-II-2)
167	45	-2.96(6)	-2.01(10-II-2)	0.87(10-I-4)	3762(9-II-1)	1837(10-II-1)	-438(9-II-2)
167	46	-2.95(6)	-2.09(10-II-2)	0.83(10-I-4)	3636(9-II-1)	1633(10-II-1)	-243(9-II-3)
167	47	-2.93(6)	-1.49(10-II-2)	1.12(10-I-4)	3251(6)	2386(10-II-1)	-368(6)
167	48	-2.86(6)	-1.37(10-II-2)	1.22(10-I-4)	3149(6)	2313(10-II-1)	-198(6)
167	49	-2.87(6)	-1.69(10-II-2)	1.07(10-I-4)	3518(10-II-4)	1988(10-II-1)	-225(10-II-2)
167	50	-2.96(6)	-1.78(10-II-2)	0.99(10-I-4)	3683(10-II-4)	2162(10-II-1)	-504(10-II-2)
167	51	-2.89(6)	-1.92(10-II-2)	0.94(10-I-4)	3684(9-II-1)	1853(10-II-1)	-287(10-II-2)
168	1	-0.76(10-I-2)	0.68(9-II-4)	-0.37(9-II-3)	-2776(9-II-2)	978(9-I-2)	2606(9-II-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
168	2	0.73 (9-II-3)	0.74 (9-II-3)	-1.27 (9-II-2)	-3399 (9-II-2)	-1946 (9-II-2)	3442 (9-II-2)
168	3	1.03 (9-II-2)	0.83 (10-I-1)	-0.75 (9-II-3)	-851 (9-II-2)	3660 (9-I-2)	-2931 (9-I-2)
168	4	0.38 (9-II-3)	-0.50 (9-II-2)	-0.07 (9-II-3)	-4209 (9-II-2)	834 (9-I-2)	-715 (9-I-2)
168	5	-0.66 (6)	0.15 (10-I-3)	-0.33 (9-II-3)	-3894 (9-II-2)	590 (9-I-2)	935 (9-II-2)
168	6	-0.39 (6)	0.21 (10-I-3)	-0.62 (9-II-3)	-2795 (9-II-2)	1020 (9-I-2)	2667 (9-II-2)
168	7	-0.40 (10-I-2)	0.33 (10-I-3)	-0.31 (9-II-3)	-4004 (9-II-2)	578 (9-I-2)	2197 (9-II-2)
168	8	-1.48 (10-I-2)	0.33 (10-I-3)	-0.41 (9-II-3)	-2621 (9-II-4)	215 (9-I-2)	1256 (9-II-2)
169	1	-0.80 (10-I-2)	0.63 (9-II-3)	-0.55 (6)	3601 (9-I-2)	-5018 (10-I-4)	-3088 (9-II-3)
169	2	0.31 (9-II-3)	0.70 (10-I-4)	-0.13 (10-I-1)	2191 (9-I-2)	-3017 (9-II-2)	-1844 (9-II-2)
169	3	0.47 (9-II-3)	-0.65 (6)	-1.62 (9-II-4)	4535 (9-I-2)	-4268 (10-I-1)	-4149 (9-II-3)
169	4	-1.40 (6)	0.79 (9-II-3)	-0.93 (6)	3625 (9-I-2)	-3955 (10-I-4)	-4973 (9-II-3)
169	5	-2.45 (9-I-2)	-0.43 (7)	-1.24 (9-II-4)	1927 (9-I-2)	-5619 (9-II-3)	-3170 (9-II-3)
169	6	-1.36 (9-I-3)	-0.37 (6)	-0.58 (9-I-3)	3226 (9-I-2)	-4518 (9-II-3)	-3622 (9-II-3)
170	1	-1.26 (10-II-1)	-2.76 (10-II-2)	0.08 (9-II-3)	2592 (9-I-1)	-1797 (9-II-2)	-734 (9-II-2)
170	2	-2.32 (10-II-1)	-2.45 (10-II-1)	-0.25 (10-I-4)	1059 (9-I-1)	-1537 (9-II-2)	221 (9-I-1)
170	3	-0.56 (9-I-3)	-3.57 (10-II-2)	-0.51 (10-II-4)	4748 (9-I-1)	-2221 (9-II-2)	-2498 (9-II-2)
170	4	-1.02 (10-II-1)	-3.04 (10-II-2)	-0.58 (10-II-4)	4172 (9-I-1)	-2084 (9-II-2)	-1722 (9-II-2)
170	5	-0.95 (10-II-1)	-2.88 (10-II-2)	-0.44 (10-II-4)	3659 (9-I-1)	-2033 (9-II-2)	-1461 (9-II-2)
170	6	-0.99 (10-II-1)	-3.05 (10-II-2)	-0.41 (10-II-4)	3832 (9-I-1)	-2370 (9-II-2)	-1508 (9-II-2)
170	7	-1.22 (10-II-1)	-3.19 (10-II-2)	-0.46 (10-II-4)	4550 (9-I-1)	-1937 (9-II-2)	-2075 (9-II-2)
170	8	-0.70 (10-II-1)	-3.07 (10-II-2)	-0.60 (10-II-4)	4740 (9-I-1)	-1633 (9-II-2)	-2283 (9-II-2)
171	1	-3.74 (10-II-1)	-1.79 (10-II-1)	0.49 (10-I-1)	1560 (10-II-4)	1153 (9-I-1)	1000 (9-II-2)
171	2	-4.10 (10-II-1)	-1.94 (10-II-1)	0.14 (10-I-1)	3352 (10-II-1)	1409 (9-I-1)	844 (9-II-2)
171	3	-3.88 (10-II-1)	-1.66 (10-II-1)	0.53 (10-I-1)	1985 (10-II-4)	514 (9-I-2)	747 (9-II-1)
171	4	-3.95 (10-II-1)	-1.60 (10-II-2)	0.72 (10-I-1)	186 (9-I-1)	495 (9-I-2)	1055 (9-II-1)
171	5	-4.28 (10-II-1)	-2.13 (10-II-1)	1.52 (10-II-3)	-3189 (10-II-2)	-1004 (9-II-2)	2806 (9-II-2)
171	6	-2.78 (10-II-1)	-2.02 (10-II-1)	0.26 (10-I-1)	1230 (10-I-4)	514 (9-I-2)	1328 (9-II-2)
171	7	-3.35 (10-II-1)	-2.02 (10-II-1)	0.68 (10-I-1)	676 (10-I-4)	673 (9-I-1)	1352 (9-II-2)
172	1	-5.69 (10-I-3)	-1.34 (10-I-2)	0.67 (10-I-2)	2338 (10-I-3)	61 (10-I-2)	-155 (9-II-1)
172	2	-5.60 (10-I-3)	-1.37 (10-I-2)	0.86 (10-I-2)	2271 (10-I-3)	143 (10-I-2)	-165 (9-II-1)
172	3	-5.32 (10-I-3)	-1.40 (10-I-2)	1.00 (10-I-2)	2124 (10-I-3)	238 (10-I-2)	-156 (10-I-2)
172	4	-4.82 (10-I-3)	-1.44 (10-I-2)	1.10 (10-I-2)	1886 (10-I-3)	339 (10-I-2)	-144 (10-I-2)
172	5	-4.10 (10-I-4)	-1.46 (10-I-2)	1.16 (10-I-2)	1575 (9-II-3)	431 (10-I-2)	-140 (10-I-2)
172	6	-3.27 (9-II-3)	-1.42 (10-I-2)	1.16 (10-I-2)	1221 (9-II-3)	484 (10-I-2)	-158 (10-I-2)
172	7	-2.32 (9-II-3)	-1.29 (10-I-2)	1.14 (10-I-2)	843 (9-II-3)	477 (10-I-2)	-226 (10-I-2)
172	8	-1.07 (9-II-3)	-1.23 (10-I-2)	1.05 (10-I-2)	377 (9-II-3)	502 (10-I-2)	-416 (10-I-2)
172	9	-2.28 (9-II-3)	-1.43 (10-I-2)	0.94 (10-I-2)	953 (9-II-3)	641 (10-I-2)	-633 (10-I-2)
172	10	-3.24 (9-II-3)	-1.50 (10-I-2)	0.92 (10-I-2)	1369 (9-II-3)	718 (10-I-2)	-682 (10-I-2)
172	11	-4.04 (10-I-4)	-1.53 (10-I-2)	0.87 (10-I-2)	1728 (9-II-3)	805 (10-I-2)	-656 (10-I-2)
172	12	-4.72 (10-I-3)	-1.50 (10-I-2)	0.84 (10-I-2)	2044 (10-I-3)	881 (10-I-2)	-596 (10-I-2)
172	13	-5.19 (10-I-3)	-1.47 (10-I-2)	0.81 (10-I-2)	2263 (10-I-3)	960 (10-I-2)	-516 (10-I-2)
172	14	-5.46 (10-I-3)	-1.46 (10-I-2)	0.76 (10-I-2)	2392 (10-I-3)	1044 (10-I-2)	-425 (10-I-2)
172	15	-5.55 (10-I-3)	-1.47 (10-I-2)	0.68 (9-II-1)	2440 (10-I-3)	1123 (10-I-2)	-329 (10-I-2)
172	16	-5.51 (10-I-3)	-1.48 (10-I-2)	0.54 (9-II-1)	2415 (10-I-3)	1177 (10-I-3)	-220 (10-I-2)
172	17	-5.39 (10-I-3)	-1.69 (10-I-3)	0.21 (9-II-1)	2253 (10-I-2)	972 (10-I-3)	-172 (10-I-2)
172	18	-5.52 (10-I-3)	-1.01 (10-I-3)	-0.09 (9-I-1)	2256 (10-I-2)	140 (10-I-2)	-133 (9-II-1)
172	19	-5.63 (10-I-3)	-1.29 (10-I-3)	0.42 (10-I-2)	2328 (10-I-3)	-33 (10-II-2)	-118 (9-II-1)
173	1	-2.50 (9-II-3)	-0.89 (10-I-2)	0.78 (10-I-2)	1253 (9-II-3)	1217 (10-I-2)	-858 (10-I-2)
173	2	-3.38 (9-II-3)	-1.02 (10-I-2)	1.07 (10-I-2)	1565 (9-II-3)	1106 (10-I-2)	-846 (10-I-2)
173	3	-4.11 (10-I-4)	-1.01 (10-I-2)	1.30 (10-I-2)	1833 (10-I-4)	971 (10-I-2)	-829 (10-I-2)
173	4	-4.68 (10-I-3)	-0.94 (10-I-2)	1.44 (10-I-2)	2043 (10-I-3)	834 (10-I-2)	-795 (10-I-2)
173	5	-5.07 (10-I-3)	-0.85 (10-I-2)	1.49 (10-I-2)	2177 (10-I-3)	693 (10-I-2)	-734 (10-I-2)
173	6	-5.27 (10-I-3)	-0.74 (10-I-2)	1.45 (10-I-2)	2240 (10-I-3)	549 (10-I-2)	-649 (10-I-2)
173	7	-5.33 (10-I-3)	-0.64 (10-I-2)	1.31 (10-I-2)	2242 (10-I-3)	399 (10-I-2)	-547 (10-I-2)
173	8	-5.30 (10-I-3)	-0.51 (10-I-2)	1.11 (10-I-2)	2205 (10-I-3)	212 (10-I-2)	-463 (10-I-2)
173	9	-5.36 (10-I-3)	-0.61 (10-I-2)	1.31 (10-I-2)	2216 (10-I-3)	119 (10-I-2)	-568 (10-I-2)
173	10	-5.30 (10-I-3)	-0.75 (10-I-2)	1.48 (10-I-2)	2202 (10-I-3)	76 (10-I-2)	-617 (10-I-2)
173	11	-5.06 (10-I-3)	-0.87 (10-I-2)	1.60 (10-I-2)	2133 (10-I-3)	-34 (10-II-2)	-616 (10-I-2)
173	12	-4.63 (10-I-3)	-0.99 (10-I-2)	1.67 (10-I-2)	1988 (10-I-3)	-86 (10-II-2)	-581 (10-I-2)
173	13	-3.99 (10-I-4)	-1.11 (10-I-2)	1.70 (10-I-2)	1763 (10-I-4)	-143 (10-II-2)	-521 (10-I-2)
173	14	-3.21 (9-II-3)	-1.20 (10-I-2)	1.70 (10-I-2)	1488 (9-II-3)	-233 (10-II-2)	-441 (10-I-2)
173	15	-2.29 (9-II-3)	-1.18 (10-I-2)	1.61 (10-I-2)	1169 (9-II-3)	-430 (10-II-2)	-330 (10-I-2)
173	16	-1.32 (9-II-3)	-0.88 (10-I-2)	1.27 (10-I-2)	623 (9-II-3)	-989 (10-II-2)	-224 (10-I-2)
173	17	1.10 (9-I-3)	2.73 (10-II-2)	0.52 (9-II-4)	-1029 (9-I-3)	-1884 (10-II-2)	674 (9-I-2)
173	18	-0.95 (9-II-3)	1.03 (10-II-2)	0.73 (9-II-4)	-453 (9-I-3)	745 (10-I-2)	-404 (9-II-3)
173	19	-1.51 (9-II-3)	-0.53 (10-I-2)	0.48 (9-II-1)	810 (9-II-3)	1347 (10-I-2)	-838 (10-I-3)
174	1	-0.47 (6)	-3.23 (9-I-3)	0.41 (9-II-3)	-255 (9-II-3)	801 (9-I-3)	712 (9-I-3)
174	2	-1.27 (10-I-2)	-3.55 (9-I-3)	-0.58 (9-I-3)	594 (10-I-2)	1108 (9-I-3)	619 (9-I-3)
174	3	-2.18 (10-I-2)	-3.70 (10-I-2)	-0.85 (9-I-3)	994 (10-I-2)	1267 (9-I-3)	612 (6)
174	4	-3.02 (10-I-2)	-3.81 (10-I-3)	-1.11 (6)	1286 (10-I-2)	1400 (10-I-3)	631 (6)
174	5	-3.47 (10-I-2)	-3.73 (10-I-3)	-1.32 (6)	1540 (10-I-2)	1551 (10-I-3)	566 (6)
174	6	-2.98 (10-I-2)	-3.53 (10-I-3)	-1.20 (6)	1242 (10-I-2)	1788 (10-I-3)	391 (6)
174	7	-2.46 (10-I-2)	-3.37 (9-I-3)	-0.89 (9-I-3)	977 (10-I-2)	1914 (10-I-3)	218 (9-I-3)
174	8	-1.84 (10-I-2)	-3.13 (9-I-3)	-0.59 (9-I-3)	715 (10-I-2)	2048 (10-I-3)	-224 (9-I-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

Pagina 138 di
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
174	9	-1.15 (10-I-2)	-2.69 (9-I-3)	-0.34 (9-I-3)	502 (10-I-2)	2220 (10-I-2)	-551 (9-II-3)
174	10	-0.43 (6)	-2.02 (9-I-3)	-0.37 (6)	544 (9-II-3)	2154 (9-I-3)	-983 (9-II-3)
174	11	0.59 (9-I-3)	-1.90 (9-I-3)	-0.58 (10-II-1)	1146 (9-II-3)	1587 (9-I-3)	-1132 (10-I-3)
174	12	-1.39 (9-II-3)	-2.15 (9-I-2)	-0.13 (6)	1167 (9-II-3)	881 (9-I-2)	111 (10-II-2)
174	13	2.25 (9-I-3)	-2.22 (9-I-3)	-0.57 (10-II-2)	-1185 (9-I-3)	-1246 (9-II-3)	625 (10-II-1)
174	14	0.24 (9-I-4)	-2.31 (9-I-3)	0.81 (9-II-3)	-1119 (9-I-4)	-1288 (9-II-3)	882 (9-I-3)
175	1	-3.45 (9-I-3)	-0.56 (10-I-2)	-0.71 (9-I-4)	1291 (9-I-3)	727 (10-I-3)	627 (10-I-4)
175	2	-2.78 (9-I-3)	0.14 (10-II-1)	-0.74 (9-I-3)	930 (9-I-3)	387 (10-I-4)	681 (9-I-4)
175	3	2.56 (9-II-3)	0.93 (10-II-4)	0.43 (9-II-3)	-1279 (9-II-3)	-415 (10-II-4)	-226 (9-II-3)
175	4	-2.72 (9-I-3)	0.21 (10-II-4)	-0.92 (9-I-4)	1127 (9-I-3)	-440 (10-II-1)	-303 (9-II-3)
175	5	-3.42 (9-I-3)	-0.60 (10-I-3)	-1.00 (9-I-1)	1433 (9-I-3)	-301 (9-II-3)	-126 (9-II-4)
175	6	-4.00 (9-I-3)	-0.87 (10-I-3)	-0.87 (9-I-1)	1685 (10-I-2)	-235 (9-II-3)	65 (9-I-1)
175	7	-4.60 (10-I-2)	-1.04 (10-I-3)	-0.62 (9-I-1)	1972 (10-I-2)	-179 (9-II-3)	70 (9-I-1)
175	8	-5.09 (10-I-2)	-0.91 (10-I-3)	-0.21 (9-I-1)	2283 (10-I-2)	114 (10-I-2)	110 (9-I-1)
175	9	-4.98 (10-I-2)	-1.59 (10-I-3)	0.16 (9-II-1)	2666 (10-I-3)	962 (10-I-3)	159 (9-I-1)
175	10	-4.63 (10-I-2)	-1.16 (10-I-2)	-0.38 (9-I-1)	1946 (10-I-2)	1083 (10-I-3)	281 (9-I-1)
175	11	-4.06 (10-I-2)	-0.89 (10-I-2)	-0.56 (9-I-1)	1601 (9-I-3)	929 (10-I-3)	465 (10-I-4)
176	1	-0.61 (10-II-2)	-0.86 (9-II-4)	-0.78 (10-II-3)	396 (9-II-2)	20 (9-II-3)	-287 (9-I-1)
176	2	1.35 (9-II-4)	-0.67 (9-II-4)	-0.50 (10-II-2)	163 (9-II-1)	-223 (9-I-4)	-284 (10-I-4)
176	3	2.73 (9-II-4)	-0.34 (10-I-3)	-0.04 (9-I-4)	71 (9-I-4)	-217 (10-I-3)	-234 (9-I-1)
176	4	1.90 (9-II-2)	-0.42 (10-II-3)	0.14 (6)	902 (9-II-4)	-148 (9-II-4)	388 (9-II-4)
176	5	0.65 (9-II-4)	0.16 (9-II-4)	0.27 (9-II-4)	355 (9-II-2)	-136 (10-II-3)	80 (9-II-4)
176	6	-0.70 (10-I-3)	-1.02 (9-II-4)	-0.96 (9-II-4)	174 (9-II-1)	-720 (9-II-4)	-396 (10-I-4)
176	7	1.15 (9-II-4)	-0.78 (9-II-4)	-0.40 (9-II-4)	145 (9-II-1)	-340 (10-I-4)	-254 (10-I-4)
177	1	-6.10 (10-I-2)	-3.10 (10-I-3)	-1.32 (10-I-3)	2639 (10-I-2)	1164 (10-I-3)	293 (6)
177	2	-6.58 (10-I-2)	-2.59 (10-I-3)	-1.22 (10-I-3)	2810 (10-I-3)	1100 (10-I-3)	426 (10-I-3)
177	3	-5.94 (10-I-2)	-2.35 (10-I-3)	-1.49 (10-I-3)	2506 (10-I-2)	1140 (10-I-3)	880 (10-I-3)
177	4	-3.95 (6)	-2.18 (10-I-3)	-1.41 (9-I-1)	1783 (6)	1649 (10-I-3)	1097 (10-I-3)
177	5	-3.19 (6)	-1.60 (6)	-2.19 (10-I-3)	1195 (6)	1041 (6)	1689 (10-I-3)
177	6	-3.02 (6)	-1.10 (6)	-1.99 (10-I-2)	-332 (10-I-1)	578 (6)	1003 (10-I-3)
177	7	-2.79 (6)	-0.95 (6)	-2.12 (10-I-3)	-992 (10-I-1)	69 (7)	628 (9-I-1)
177	8	-0.91 (6)	-0.91 (6)	-1.96 (10-I-2)	893 (6)	-149 (10-II-3)	62 (7)
177	9	-3.78 (6)	-2.86 (10-I-3)	-2.28 (10-I-3)	1792 (6)	499 (10-I-3)	532 (6)
177	10	-3.52 (6)	-1.72 (6)	-2.03 (10-I-3)	1563 (6)	889 (10-I-3)	950 (10-I-2)
178	1	-0.14 (10-I-2)	-1.56 (10-II-3)	-1.06 (10-II-1)	278 (9-I-1)	53 (9-I-1)	-52 (9-II-2)
178	2	0.44 (10-II-1)	-1.68 (10-II-1)	-0.50 (9-II-1)	24 (10-I-3)	-14 (10-II-3)	29 (9-I-1)
178	3	0.23 (9-II-1)	-1.71 (10-II-1)	0.37 (10-II-1)	-41 (10-II-2)	-16 (10-II-2)	16 (9-I-4)
178	4	-0.61 (9-I-1)	-1.28 (10-II-3)	1.01 (9-II-1)	227 (9-I-4)	72 (9-II-2)	56 (9-I-3)
178	5	-0.24 (10-II-4)	-0.90 (10-II-3)	-0.88 (10-II-1)	76 (9-I-1)	66 (10-II-2)	-53 (9-II-2)
178	6	0.19 (10-II-1)	-1.40 (10-II-1)	-0.45 (9-II-1)	28 (10-I-3)	21 (10-I-3)	18 (10-II-2)
178	7	0.13 (9-II-1)	-1.44 (10-II-1)	0.36 (10-II-1)	24 (9-I-3)	-6 (10-II-2)	41 (9-I-4)
178	8	-0.28 (10-II-4)	-0.67 (9-II-1)	0.61 (9-II-1)	52 (9-I-3)	69 (9-I-1)	69 (9-I-4)
178	9	0.09 (6)	-0.43 (10-II-3)	-0.66 (10-II-1)	9 (9-I-2)	82 (10-II-2)	-42 (9-II-1)
178	10	-0.03 (9-I-2)	-1.18 (10-II-1)	-0.32 (9-II-1)	20 (9-I-4)	36 (9-I-1)	11 (10-II-2)
178	11	-0.07 (9-I-1)	-1.24 (10-II-1)	0.23 (10-II-3)	21 (9-I-3)	15 (9-II-1)	49 (9-I-4)
178	12	-0.13 (10-II-4)	-0.55 (9-II-1)	0.34 (9-II-1)	-14 (10-II-1)	47 (9-II-1)	51 (9-I-4)
178	13	0.26 (6)	0.45 (6)	-0.46 (6)	-2 (9-I-1)	118 (10-II-2)	-50 (9-II-1)
178	14	-0.11 (10-II-1)	-1.15 (10-II-1)	-0.09 (9-II-1)	8 (9-I-4)	46 (9-I-4)	9 (9-I-1)
178	15	-0.12 (6)	-1.18 (9-II-1)	0.09 (10-II-3)	6 (9-II-1)	24 (9-II-1)	46 (9-I-4)
178	16	-0.10 (6)	-0.64 (9-II-1)	0.08 (9-II-1)	-15 (10-II-1)	31 (9-II-4)	34 (9-I-4)
179	1	-0.96 (9-II-3)	-0.05 (10-II-3)	-0.99 (10-II-1)	80 (10-II-3)	34 (10-II-3)	25 (9-II-2)
179	2	-1.13 (9-II-2)	0.09 (10-I-3)	-1.28 (10-II-1)	103 (10-II-3)	64 (10-II-1)	36 (9-II-2)
179	3	-0.85 (9-II-1)	0.44 (9-II-1)	-1.44 (10-II-1)	108 (9-II-1)	44 (9-II-1)	80 (9-II-2)
179	4	1.56 (9-I-1)	1.77 (9-II-3)	-2.17 (9-II-2)	-93 (9-I-1)	-69 (10-II-3)	94 (9-II-2)
179	5	-0.67 (9-II-3)	1.26 (9-II-3)	-0.95 (10-II-1)	44 (10-II-3)	42 (10-II-3)	52 (9-II-2)
179	6	-0.75 (9-II-2)	1.15 (9-II-3)	-1.32 (10-II-1)	37 (10-II-3)	46 (10-II-3)	68 (9-II-2)
179	7	-0.45 (9-II-1)	1.18 (9-I-1)	-1.80 (10-II-1)	-18 (9-I-1)	42 (10-II-2)	77 (9-II-2)
179	8	1.06 (9-I-1)	0.45 (9-I-1)	-1.53 (9-II-2)	-74 (10-II-1)	-24 (10-II-3)	18 (9-II-4)
179	9	-0.33 (9-I-1)	2.46 (10-II-1)	-0.75 (10-II-1)	19 (10-II-3)	51 (10-II-3)	49 (9-II-2)
179	10	-0.37 (9-II-3)	1.99 (10-II-1)	-1.10 (10-II-1)	5 (9-II-1)	50 (10-II-1)	52 (9-II-2)
179	11	-0.20 (9-II-1)	1.29 (10-II-1)	-1.34 (10-II-1)	-28 (9-II-2)	35 (9-I-4)	43 (9-II-2)
179	12	0.37 (9-I-1)	0.38 (9-I-1)	-0.97 (9-II-2)	-47 (10-II-1)	-38 (10-II-3)	-6 (10-II-3)
179	13	-0.05 (10-II-1)	3.78 (10-II-1)	-0.30 (10-II-1)	4 (10-II-3)	55 (10-II-1)	39 (9-II-2)
179	14	-0.05 (9-I-1)	2.82 (10-II-1)	-0.45 (10-II-1)	0	47 (10-II-1)	40 (9-II-2)
179	15	-0.07 (9-I-1)	1.56 (10-II-1)	-0.51 (10-II-1)	-11 (9-II-1)	28 (9-I-4)	25 (9-II-2)
179	16	-0.13 (9-II-2)	0.38 (9-I-1)	-0.38 (9-II-2)	-36 (9-II-2)	-48 (9-II-2)	-25 (10-II-3)
180	1	0.53 (9-I-1)	-1.72 (9-II-3)	0.21 (10-II-1)	81 (10-II-1)	100 (10-II-2)	-40 (9-II-2)
180	2	0.86 (9-I-1)	-1.24 (9-II-3)	0.57 (10-II-1)	102 (10-II-1)	32 (10-II-2)	-17 (9-II-2)
180	3	0.99 (10-II-1)	-0.94 (10-II-1)	0.53 (10-II-1)	102 (10-II-1)	12 (10-II-2)	8 (9-I-1)
180	4	1.10 (10-II-1)	-0.74 (10-II-1)	0.25 (10-II-1)	100 (10-II-1)	3 (10-II-2)	9 (9-I-1)
180	5	-0.31 (10-II-1)	-1.44 (10-II-1)	-0.20 (10-I-1)	40 (10-II-1)	77 (10-II-2)	32 (10-II-2)
180	6	0.40 (10-II-1)	-1.13 (10-II-1)	-0.07 (10-I-1)	64 (10-II-1)	66 (10-II-2)	28 (9-I-1)
180	7	1.09 (10-II-1)	-0.86 (10-II-1)	0.11 (10-II-1)	83 (10-II-1)	33 (10-II-2)	32 (10-II-2)
180	8	1.88 (10-II-1)	-0.72 (10-II-1)	0.05 (10-II-1)	95 (10-II-1)	6 (10-II-2)	30 (10-II-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
180	9	-0.66(10-II-2)	-1.22(10-II-1)	-0.47(10-I-4)	64(10-II-1)	152(9-II-4)	127(10-II-2)
180	10	0.09(10-II-1)	-0.97(10-II-1)	-0.27(10-I-4)	108(10-II-1)	48(9-II-4)	78(10-II-2)
180	11	0.93(10-II-1)	-0.79(10-II-1)	-0.17(10-I-4)	102(10-II-1)	17(9-II-4)	58(10-II-2)
180	12	1.85(10-II-1)	-0.69(10-I-3)	-0.04(10-I-1)	97(10-II-1)	5(9-II-4)	48(10-II-2)
180	13	-1.48(10-I-4)	-0.66(10-II-1)	-0.08(9-I-1)	5(9-II-4)	-36(10-II-2)	98(10-II-2)
180	14	-0.30(10-I-1)	-0.84(10-II-1)	-0.20(9-I-1)	-9(9-I-4)	-14(9-I-1)	26(9-I-1)
180	15	0.77(10-II-1)	-0.76(10-II-1)	-0.17(10-II-1)	-18(10-II-2)	-7(9-I-1)	34(10-II-2)
180	16	1.49(10-II-1)	-0.72(10-II-1)	-0.07(10-II-1)	-20(10-II-2)	-2(9-I-1)	33(10-II-2)
181	1	1.16(9-I-1)	1.39(9-I-2)	1.11(9-I-1)	128(10-II-2)	-211(10-II-3)	157(10-II-1)
181	2	0.40(9-I-1)	0.66(9-I-2)	1.12(10-II-1)	122(10-II-3)	32(9-I-1)	63(9-II-2)
181	3	0.15(9-I-1)	0.07(9-I-2)	0.95(10-II-1)	43(10-II-3)	-80(6)	45(9-II-2)
181	4	-0.09(10-II-2)	-0.50(10-II-1)	0.79(10-II-1)	-112(6)	-199(6)	-61(6)
181	5	0.26(9-I-1)	-0.68(6)	0.97(9-II-2)	-99(10-II-1)	-279(10-II-3)	134(10-II-1)
181	6	0.59(9-I-1)	-0.38(6)	1.42(9-II-2)	-102(6)	-63(6)	62(10-II-1)
181	7	0.41(9-I-1)	-0.35(6)	1.28(10-II-1)	-60(6)	-140(6)	-40(6)
181	8	0.31(9-II-1)	-0.25(6)	0.80(10-II-1)	-56(6)	-326(6)	57(9-I-3)
181	9	-0.50(10-II-3)	-0.92(6)	0.84(9-II-1)	-116(10-II-1)	-266(6)	85(10-II-1)
181	10	0.37(9-I-1)	-0.90(6)	1.32(9-II-1)	-126(6)	-133(6)	117(10-II-1)
181	11	0.65(9-II-2)	-0.54(6)	1.20(10-II-1)	-74(6)	-197(6)	73(9-I-4)
181	12	0.84(9-II-1)	-0.33(6)	0.80(10-II-1)	-54(6)	-320(6)	78(9-I-4)
181	13	-1.30(10-II-1)	-1.30(6)	1.28(10-II-1)	53(9-I-2)	-123(6)	86(10-II-1)
181	14	0.27(9-I-1)	-0.91(6)	1.08(10-II-1)	-37(6)	-169(6)	126(10-II-1)
181	15	0.83(9-II-2)	-0.64(6)	0.98(10-II-1)	-45(6)	-236(6)	93(9-I-4)
181	16	1.28(9-II-1)	-0.35(6)	0.70(10-II-1)	-48(6)	-336(6)	93(9-I-4)
182	1	0.10(10-I-3)	-0.76(9-II-3)	0.63(10-II-1)	29(10-II-1)	54(10-II-3)	-14(9-II-2)
182	2	1.48(10-II-1)	-0.48(10-II-1)	0.57(10-II-1)	35(10-II-3)	39(10-II-3)	-29(9-II-2)
182	3	2.99(10-II-1)	-0.22(10-II-1)	0.41(10-II-1)	44(10-II-1)	21(10-II-3)	-30(9-II-2)
182	4	4.63(10-II-1)	0.02(9-II-3)	0.15(10-II-1)	50(10-II-1)	5(10-II-3)	-28(9-II-2)
182	5	0.08(9-I-3)	-0.57(10-II-1)	0.25(10-II-1)	42(10-II-1)	54(10-II-2)	15(9-I-4)
182	6	1.70(10-II-1)	-0.37(10-II-1)	0.21(10-II-1)	42(10-II-1)	33(10-II-2)	10(9-I-4)
182	7	3.39(10-II-1)	-0.16(10-II-1)	0.14(10-II-1)	48(10-II-1)	18(10-II-3)	9(9-I-4)
182	8	5.14(10-II-1)	0.06(10-II-1)	0.05(10-II-1)	52(10-II-1)	4(10-II-3)	-8(9-II-4)
182	9	0.18(9-I-3)	-0.48(10-II-1)	0.03(9-I-2)	42(10-II-1)	54(10-I-4)	32(9-I-1)
182	10	1.82(10-II-1)	-0.32(10-II-1)	-0.06(10-I-1)	41(10-I-4)	27(10-I-4)	23(9-I-1)
182	11	3.50(10-II-1)	-0.14(10-II-1)	-0.06(10-I-1)	43(10-I-4)	12(10-I-4)	19(9-I-1)
182	12	5.21(10-II-1)	0.03(10-II-1)	-0.02(10-I-1)	44(10-I-4)	2(10-I-4)	16(9-I-1)
182	13	0.35(9-II-1)	-0.34(9-I-2)	-0.16(10-I-4)	14(10-I-4)	13(10-I-1)	46(9-I-1)
182	14	1.84(10-II-1)	-0.24(9-I-2)	-0.17(9-II-3)	16(10-I-4)	-13(10-II-1)	27(9-I-1)
182	15	3.41(10-II-1)	-0.12(9-I-2)	-0.13(9-II-3)	17(10-I-1)	-9(10-II-1)	18(9-I-1)
182	16	5.03(10-II-1)	-0.02(10-I-1)	-0.04(9-II-2)	17(10-I-1)	-2(10-II-1)	15(10-I-4)
183	1	0.32(10-I-3)	-2.40(10-II-3)	0.39(9-I-1)	120(9-II-1)	-1973(9-I-1)	90(9-II-2)
183	2	-0.11(10-II-3)	-2.33(10-II-3)	-0.07(10-II-3)	15(9-I-1)	-1933(9-I-1)	67(9-I-1)
183	3	-0.03(9-I-1)	-1.54(10-II-3)	-0.30(10-II-3)	5(9-I-1)	-1459(9-I-1)	-36(9-I-3)
183	4	0.14(10-I-3)	0.34(10-I-3)	0.21(10-I-3)	17(9-I-1)	-428(9-I-1)	-88(9-I-1)
183	5	0.27(10-I-3)	-2.65(10-II-3)	-0.18(10-I-1)	-175(9-I-1)	-2034(9-I-1)	109(10-I-4)
183	6	0.11(10-II-1)	-2.17(10-II-3)	-0.18(10-II-3)	-39(9-I-1)	-1954(9-I-1)	110(9-I-1)
183	7	-0.47(10-I-3)	-1.81(10-II-3)	-0.76(10-II-3)	-26(9-II-1)	-1586(9-I-1)	-82(9-I-2)
183	8	0.63(10-I-3)	-0.55(10-II-3)	0.78(10-I-3)	140(9-I-1)	-520(9-I-1)	-279(9-I-1)
183	9	-0.14(10-II-3)	-2.44(10-II-3)	-0.69(10-I-1)	-248(9-I-1)	-2092(9-I-1)	142(9-I-1)
183	10	0.24(10-II-1)	-1.95(10-II-3)	-0.43(10-I-1)	-131(9-I-1)	-1973(9-I-1)	159(9-I-1)
183	11	-1.02(10-I-3)	-2.17(10-II-3)	-0.84(10-II-3)	-37(9-II-1)	-1833(9-I-1)	-89(9-I-3)
183	12	-1.26(10-II-3)	1.41(10-I-3)	1.59(10-I-3)	390(9-I-1)	-913(9-I-1)	-548(9-I-1)
183	13	-0.49(10-II-2)	-1.60(10-II-3)	-1.13(10-I-1)	-312(9-I-1)	-2167(9-I-1)	127(9-I-1)
183	14	0.50(10-II-1)	-1.72(10-II-3)	-0.61(10-I-1)	-291(9-I-1)	-1983(9-I-1)	181(9-I-1)
183	15	-2.00(10-I-3)	-2.37(10-II-3)	-0.52(10-I-1)	-160(9-II-1)	-2158(9-I-1)	-91(10-II-4)
183	16	-0.46(10-I-1)	-3.85(10-II-3)	-2.19(10-II-3)	619(9-I-1)	-2375(9-I-1)	-1263(9-I-1)
184	1	2.08(10-II-2)	3.76(9-I-1)	2.57(9-I-1)	-355(10-II-1)	-374(9-II-2)	-174(9-II-2)
184	2	0.81(10-II-2)	0.66(10-II-1)	0.10(9-I-1)	74(10-II-1)	-23(9-II-2)	53(10-II-2)
184	3	0.18(10-II-2)	0.10(10-II-1)	0.05(9-I-4)	-8(9-II-2)	8(9-I-2)	26(10-II-2)
184	4	-0.03(9-I-1)	-0.02(10-I-1)	-0.02(10-I-4)	8(10-II-2)	6(10-II-2)	8(10-II-2)
184	5	2.66(10-II-2)	0.75(10-II-1)	1.66(9-I-1)	39(10-II-2)	-122(9-II-2)	-67(9-II-2)
184	6	0.39(9-I-1)	1.03(10-II-1)	1.02(10-II-1)	62(10-II-1)	-24(9-II-2)	78(10-II-2)
184	7	0.18(10-II-1)	0.23(10-II-1)	0.32(10-II-1)	30(10-II-1)	-4(9-II-2)	31(10-II-2)
184	8	0.11(10-II-1)	-0.02(10-I-1)	0.07(10-II-1)	26(10-II-2)	4(9-I-2)	15(10-II-2)
184	9	2.22(9-II-3)	-0.51(10-I-1)	1.04(9-I-1)	174(10-II-1)	49(10-II-2)	-68(9-II-2)
184	10	0.70(9-I-1)	0.33(10-II-1)	1.16(10-II-1)	119(10-II-1)	-39(9-II-2)	44(10-II-2)
184	11	0.24(10-II-1)	0.16(10-II-1)	0.58(10-II-1)	60(10-II-1)	-4(9-II-2)	29(10-II-2)
184	12	0.08(10-II-1)	-0.01(10-I-2)	0.12(10-II-1)	46(10-II-2)	-2(9-II-2)	13(10-II-2)
184	13	1.68(9-I-1)	-0.92(10-I-3)	0.60(10-II-1)	244(10-II-1)	118(10-II-2)	-78(9-II-2)
184	14	0.94(9-I-1)	-0.39(10-I-1)	1.07(10-II-1)	138(10-II-1)	-17(9-II-2)	-5(9-II-2)
184	15	0.64(10-II-1)	-0.24(10-I-2)	0.71(10-II-1)	84(10-II-1)	-8(9-II-2)	20(10-II-2)
184	16	0.38(10-II-1)	-0.30(10-II-1)	0.18(10-II-1)	64(10-II-2)	-3(9-II-2)	11(10-II-2)
185	1	-0.34(10-II-3)	-1.31(6)	1.25(10-II-1)	73(9-I-2)	89(9-I-2)	24(9-II-2)
185	2	0.47(9-II-2)	-1.09(6)	0.86(10-II-1)	61(9-I-2)	-184(6)	104(10-II-1)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
185	3	0.92(9-II-1)	-0.67(6)	0.81(10-II-1)	-22(6)	-257(6)	88(9-I-4)
185	4	1.48(9-II-1)	-0.35(6)	0.60(10-II-1)	-42(6)	-348(6)	101(9-I-3)
185	5	-0.15(10-II-3)	-1.26(6)	1.06(10-II-1)	51(9-I-2)	82(9-I-2)	33(9-II-1)
185	6	0.42(9-II-2)	-0.95(6)	0.81(10-II-1)	52(9-I-2)	-185(6)	68(9-II-1)
185	7	1.00(9-II-1)	-0.65(6)	0.69(10-II-1)	10(9-I-2)	-263(6)	82(9-II-1)
185	8	1.65(9-II-1)	-0.36(6)	0.53(10-II-1)	-34(6)	-351(6)	97(9-II-2)
185	9	-0.08(6)	-1.24(6)	0.89(10-II-1)	30(9-I-2)	-68(6)	46(10-II-2)
185	10	0.46(9-II-2)	-0.89(6)	0.72(10-II-1)	35(9-I-2)	-176(6)	59(9-II-2)
185	11	1.06(9-II-1)	-0.61(6)	0.60(10-II-1)	14(9-I-2)	-267(6)	74(9-II-2)
185	12	1.75(9-II-1)	-0.35(6)	0.47(10-II-1)	-26(6)	-352(6)	93(9-II-2)
185	13	-0.08(6)	-1.16(6)	0.70(10-II-1)	18(9-I-2)	-91(6)	50(10-II-2)
185	14	0.50(9-II-1)	-0.85(6)	0.62(10-II-1)	22(9-I-2)	-174(6)	55(9-II-2)
185	15	1.12(9-II-1)	-0.58(6)	0.51(10-II-1)	12(9-I-2)	-265(6)	68(9-II-2)
185	16	1.82(9-II-1)	-0.33(6)	0.42(10-II-1)	-22(6)	-351(6)	87(9-II-2)
186	1	1.32(10-I-3)	-3.08(10-I-3)	1.03(10-II-1)	-216(9-I-1)	-1816(9-I-1)	171(9-I-1)
186	2	1.04(10-I-3)	-2.90(10-I-3)	1.03(10-II-1)	-137(9-I-1)	-1641(9-I-1)	362(9-I-1)
186	3	0.64(9-I-1)	-4.45(10-I-3)	1.02(10-I-3)	65(9-II-1)	-1602(9-I-1)	617(9-I-1)
186	4	-2.82(10-I-3)	-5.96(10-I-3)	2.42(10-I-3)	116(10-II-4)	-1822(9-I-1)	916(9-I-1)
186	5	-0.49(10-II-1)	-1.80(10-I-3)	0.41(10-I-3)	180(9-II-1)	-1286(9-I-1)	174(9-I-1)
186	6	0.35(10-II-1)	-1.28(10-I-3)	0.78(10-I-3)	220(9-II-1)	-1127(9-I-1)	301(9-I-1)
186	7	1.24(10-II-1)	-0.78(10-II-3)	0.76(10-I-3)	336(9-II-1)	-796(9-I-1)	405(9-I-1)
186	8	2.09(10-II-1)	-0.59(10-I-3)	-0.09(10-I-1)	441(9-II-1)	-410(10-II-4)	321(9-I-1)
186	9	-0.68(10-I-3)	-1.58(10-II-1)	-0.80(10-II-3)	-139(9-I-1)	-1273(9-I-1)	200(9-II-3)
186	10	-0.07(6)	-1.16(10-II-1)	-0.91(10-II-3)	197(9-II-1)	-1103(9-I-1)	244(9-II-2)
186	11	0.74(10-I-3)	-0.80(10-I-3)	-0.74(10-II-3)	293(9-II-1)	-779(9-I-1)	302(9-II-2)
186	12	1.69(10-II-1)	-0.58(10-II-3)	-0.16(10-I-3)	377(9-II-1)	-413(9-II-3)	234(9-II-2)
186	13	-0.61(10-I-3)	-2.14(10-II-1)	-1.14(10-II-1)	-181(9-I-1)	-1639(9-I-1)	193(9-II-3)
186	14	-0.52(10-I-1)	-2.29(10-II-3)	-1.06(10-I-3)	-107(9-I-4)	-1515(9-I-1)	233(9-II-4)
186	15	0.52(10-II-1)	-3.47(10-II-3)	-0.91(10-II-1)	-78(9-II-1)	-1512(9-I-1)	460(9-II-4)
186	16	-1.53(10-II-3)	-4.50(10-II-3)	-1.87(10-II-3)	-162(9-II-1)	-1697(9-I-1)	739(9-II-4)
187	1	-0.43(10-II-1)	-1.59(10-I-3)	1.24(10-II-3)	-273(9-I-1)	-1809(9-I-1)	227(10-I-4)
187	2	-0.51(10-II-3)	-1.84(10-I-3)	0.88(10-II-3)	-160(9-I-1)	-1687(9-I-1)	211(10-I-4)
187	3	-1.09(10-II-3)	-2.80(10-I-3)	0.76(10-I-1)	-220(9-II-2)	-1758(9-I-1)	507(9-I-1)
187	4	-2.35(10-I-1)	-4.80(10-I-3)	2.49(10-I-3)	567(9-I-2)	-1770(9-I-1)	1267(9-I-1)
187	5	-0.30(10-II-3)	-2.25(10-I-3)	0.81(10-I-1)	94(9-II-1)	-1672(9-I-2)	227(10-I-4)
187	6	0.24(10-I-3)	-1.87(10-I-3)	0.92(10-I-1)	-49(10-I-4)	-1479(9-I-1)	273(9-I-1)
187	7	-0.29(10-I-1)	-1.59(10-I-3)	1.35(10-I-1)	-91(9-II-3)	-1101(9-I-1)	574(9-I-1)
187	8	-1.23(10-I-1)	-0.12(10-I-3)	0.78(10-I-3)	-161(9-II-3)	-265(9-I-1)	637(9-I-1)
187	9	0.23(9-II-2)	-1.87(10-I-3)	0.58(10-I-1)	102(9-II-1)	-1589(9-I-2)	248(9-I-1)
187	10	0.35(10-II-1)	-1.39(10-I-3)	-0.64(10-II-1)	-44(10-I-4)	-1297(9-I-1)	300(9-I-1)
187	11	0.23(10-II-1)	-0.77(10-I-3)	0.54(10-I-1)	-66(10-I-4)	-815(9-I-1)	433(9-I-1)
187	12	0.47(10-II-1)	-0.08(10-I-3)	-0.24(10-II-1)	-133(9-I-1)	-210(9-I-1)	392(9-I-1)
187	13	1.11(10-II-1)	1.17(10-II-1)	-0.96(10-II-1)	107(9-II-2)	-1611(9-I-2)	247(9-I-1)
187	14	0.06(10-II-1)	-0.74(10-I-1)	-0.43(10-II-1)	-24(10-I-1)	-1214(9-I-1)	218(9-I-1)
187	15	-0.03(10-I-1)	-0.32(10-I-1)	-0.27(10-II-1)	-29(9-I-1)	-723(9-I-1)	231(9-I-1)
187	16	0.07(10-II-1)	-0.06(10-I-1)	-0.09(10-II-1)	-73(9-I-1)	-184(9-I-1)	150(9-I-1)
188	1	0.11(9-II-1)	-1.01(6)	0.40(10-II-1)	-10(6)	-113(6)	61(9-I-1)
188	2	0.61(9-II-1)	-0.74(6)	0.34(10-II-1)	-10(6)	-178(6)	67(10-II-2)
188	3	1.18(9-II-1)	-0.51(6)	0.29(10-II-1)	-9(6)	-262(6)	76(10-II-2)
188	4	1.84(9-II-1)	-0.33(6)	0.27(10-II-1)	-14(6)	-346(6)	85(10-II-1)
188	5	0.15(10-II-1)	-0.66(6)	-0.14(10-I-1)	15(9-II-2)	-101(6)	74(9-I-1)
188	6	0.64(10-II-1)	-0.56(6)	-0.12(10-I-1)	16(9-II-3)	-169(6)	95(10-II-2)
188	7	1.14(10-II-1)	-0.43(6)	0.08(10-II-1)	23(9-I-1)	-244(6)	108(10-II-2)
188	8	1.67(10-II-1)	-0.35(6)	0.14(10-II-1)	23(10-I-4)	-329(6)	113(10-II-2)
188	9	0.15(10-II-1)	-0.54(6)	-0.16(10-I-1)	20(9-II-2)	209(9-II-2)	79(9-I-1)
188	10	0.58(10-II-1)	-0.48(6)	-0.12(10-I-1)	22(9-II-3)	137(9-II-2)	139(10-II-2)
188	11	1.03(10-II-1)	-0.37(6)	-0.05(10-I-1)	40(9-II-3)	-199(6)	175(10-II-2)
188	12	1.49(10-II-1)	-0.31(6)	0.06(10-II-1)	44(10-I-4)	-327(6)	167(10-II-2)
188	13	-0.10(10-I-1)	-0.78(6)	-0.25(9-I-3)	162(9-II-4)	579(9-II-2)	224(10-I-4)
188	14	0.40(10-II-1)	-0.62(6)	0.04(10-II-2)	193(9-II-3)	246(9-II-2)	187(10-II-2)
188	15	1.04(10-II-1)	-0.47(6)	-0.03(9-I-3)	136(9-II-3)	-165(6)	186(10-II-2)
188	16	1.59(10-II-1)	-0.25(6)	-0.09(9-I-3)	82(10-I-4)	-345(6)	158(10-II-2)
189	1	-1.82(6)	-0.72(10-II-1)	-0.47(9-I-3)	317(9-II-4)	625(9-II-2)	145(10-I-4)
189	2	0.30(9-II-2)	-0.60(6)	-0.21(9-I-3)	224(9-II-3)	269(9-II-2)	72(6)
189	3	1.14(10-II-1)	-0.51(6)	-0.19(9-II-1)	118(9-II-3)	-160(6)	116(6)
189	4	1.86(10-II-1)	-0.31(6)	-0.27(10-II-1)	57(10-I-4)	-348(6)	93(6)
189	5	-0.73(6)	-0.36(10-II-1)	0.47(10-I-4)	-55(10-I-1)	287(9-II-3)	303(10-I-4)
189	6	0.33(9-II-2)	-0.60(10-II-1)	-0.22(10-II-1)	-48(6)	246(9-II-2)	98(6)
189	7	1.23(10-II-1)	-0.47(6)	-0.32(10-II-1)	39(9-II-3)	-149(6)	117(6)
189	8	2.02(10-II-1)	-0.31(6)	-0.43(10-II-1)	16(10-I-1)	-335(6)	78(6)
189	9	-0.19(6)	-0.83(10-II-1)	0.49(10-I-1)	-28(10-I-1)	283(9-II-3)	256(10-I-4)
189	10	0.72(9-II-2)	-0.63(10-II-1)	-0.13(10-II-1)	-56(6)	194(9-II-3)	198(6)
189	11	1.41(10-II-1)	-0.49(6)	-0.44(10-II-1)	-31(6)	-170(6)	157(6)
189	12	2.13(10-II-1)	-0.31(6)	-0.58(10-II-1)	-33(6)	-338(6)	80(6)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
189	13	0.42(9-II-3)	-1.10(10-II-1)	0.32(10-I-1)	22(10-II-1)	376(9-II-3)	239(10-I-4)
189	14	1.07(10-II-1)	-0.73(10-II-1)	-0.32(10-II-1)	-36(6)	134(9-II-3)	230(6)
189	15	1.64(10-II-1)	-0.48(6)	-0.58(10-II-1)	-43(6)	-227(6)	186(6)
189	16	2.22(10-II-1)	-0.32(6)	-0.69(10-II-1)	-57(6)	-352(6)	81(6)
190	1	0.76(9-II-3)	-1.09(10-II-1)	-0.22(10-II-1)	48(10-II-1)	472(10-II-1)	231(10-I-4)
190	2	1.30(10-II-1)	-0.63(6)	-0.58(10-II-1)	-68(6)	86(9-II-2)	236(6)
190	3	1.73(10-II-1)	-0.38(6)	-0.69(10-II-1)	-97(6)	-293(6)	195(6)
190	4	2.29(10-II-1)	-0.30(6)	-0.75(10-II-1)	-106(6)	-372(6)	64(6)
190	5	1.12(10-II-1)	-0.84(6)	-0.47(10-II-1)	-17(6)	538(9-II-3)	205(10-I-4)
190	6	1.40(10-II-1)	-0.39(6)	-0.80(10-II-1)	-166(6)	-67(6)	213(6)
190	7	1.72(10-II-1)	-0.21(6)	-0.72(10-II-1)	-232(6)	-344(6)	201(6)
190	8	2.35(10-II-1)	-0.26(6)	-0.70(10-II-1)	-221(6)	-398(6)	76(6)
190	9	1.56(10-II-1)	-0.32(6)	-0.73(10-II-1)	-143(6)	561(9-II-3)	154(10-I-4)
190	10	1.38(10-II-1)	0.28(9-II-4)	-0.94(10-II-1)	-374(10-II-1)	-92(6)	137(6)
190	11	1.60(10-II-1)	0.20(9-II-4)	-0.58(10-II-1)	-543(10-II-1)	-360(6)	195(6)
190	12	2.47(10-II-1)	-0.24(6)	-0.53(10-II-1)	-495(6)	-446(6)	133(6)
190	13	2.13(10-II-1)	1.58(10-II-1)	-0.83(10-II-1)	-372(9-II-3)	528(9-II-3)	51(10-I-4)
190	14	1.15(10-II-1)	0.67(10-II-1)	-0.59(10-II-1)	-742(10-II-1)	-127(6)	-20(10-II-1)
190	15	1.35(9-II-3)	0.15(9-II-4)	-0.40(10-II-1)	-1102(10-II-1)	-375(6)	62(6)
190	16	2.88(10-II-1)	-0.12(6)	-0.17(10-II-1)	-1145(10-II-1)	-463(6)	222(6)
191	1	1.86(9-II-3)	0.52(9-II-2)	0.44(10-I-4)	-242(10-II-2)	451(10-II-1)	-274(10-II-1)
191	2	1.28(9-II-3)	0.38(9-II-2)	0.34(9-II-3)	-617(10-II-1)	-81(6)	-280(9-II-4)
191	3	1.39(9-II-3)	-0.15(6)	-0.08(9-I-3)	-935(10-II-1)	-219(6)	-272(9-II-3)
191	4	2.37(6)	0.15(6)	-0.19(6)	-1258(10-II-1)	-134(6)	-165(10-II-1)
191	5	1.09(9-I-1)	-1.34(9-I-2)	-0.20(10-I-3)	-113(10-I-3)	191(10-II-3)	-451(10-II-1)
191	6	1.47(9-II-3)	-0.75(9-I-2)	0.26(9-II-3)	-230(10-I-3)	-59(6)	-518(10-II-1)
191	7	1.76(9-II-3)	-0.26(9-I-2)	0.17(9-II-3)	-355(9-I-2)	-102(6)	-489(10-II-1)
191	8	2.44(9-II-3)	-0.09(6)	-0.12(6)	-432(9-I-2)	-45(9-I-2)	-414(10-II-1)
191	9	1.03(9-I-2)	-1.56(9-I-1)	-0.74(10-II-3)	-54(10-I-3)	-235(10-I-3)	-482(10-II-1)
191	10	1.47(9-I-2)	-0.93(9-I-2)	-0.74(9-I-2)	116(9-II-3)	-58(6)	-496(10-II-1)
191	11	1.69(9-II-3)	-0.48(9-I-2)	-0.52(9-I-2)	260(9-II-3)	30(9-II-3)	-514(10-II-1)
191	12	2.53(9-II-3)	-0.05(9-I-2)	-0.21(9-I-2)	329(9-II-3)	21(9-II-3)	-449(10-II-1)
191	13	2.03(9-I-2)	-1.50(10-II-3)	-1.48(10-II-2)	227(9-II-3)	-284(6)	-297(9-I-2)
191	14	1.17(9-I-2)	-1.11(10-II-3)	-1.09(9-I-2)	583(9-II-3)	38(9-II-3)	-409(9-I-2)
191	15	1.29(9-II-3)	-0.53(10-II-3)	-0.83(9-I-2)	933(9-II-3)	131(9-II-3)	-474(9-I-2)
191	16	2.45(9-II-3)	-0.23(9-I-4)	-0.43(9-I-2)	1241(9-II-3)	73(9-II-3)	-461(9-I-2)
192	1	-2.89(10-II-3)	1.11(10-II-3)	0.85(6)	-180(9-I-2)	-1245(9-I-3)	164(10-II-2)
192	2	-3.13(10-II-3)	-1.66(10-I-3)	0.71(6)	-125(10-I-4)	-1051(9-I-3)	173(9-I-2)
192	3	-3.47(10-II-3)	-3.33(10-I-3)	0.86(10-I-3)	-203(9-II-3)	-956(9-I-3)	349(9-I-2)
192	4	-5.66(10-I-1)	-4.19(10-I-3)	2.04(10-I-3)	-277(9-II-3)	-988(9-I-3)	573(9-I-2)
192	5	-1.65(10-II-2)	0.22(9-II-2)	2.13(10-I-3)	-279(9-I-3)	-1094(9-I-3)	47(9-I-2)
192	6	-2.14(9-II-3)	-0.14(6)	1.89(10-I-3)	-366(9-I-3)	-716(9-I-3)	147(9-I-2)
192	7	-2.44(9-II-3)	-0.17(10-II-3)	1.28(10-I-3)	-450(9-I-3)	-356(9-I-3)	213(9-I-2)
192	8	-2.82(9-II-3)	-0.26(10-I-1)	0.38(10-II-3)	-535(9-I-3)	-42(9-II-1)	204(9-I-2)
192	9	-1.52(10-II-3)	-0.99(6)	1.69(10-I-1)	-126(9-I-3)	-710(9-I-3)	-210(10-I-2)
192	10	-1.63(10-II-3)	-0.73(10-I-3)	1.48(10-I-1)	-180(9-I-3)	-519(9-I-3)	-161(9-I-3)
192	11	-1.75(10-II-3)	-0.37(10-I-3)	1.08(10-I-1)	-250(9-I-3)	-263(9-I-3)	-166(9-I-3)
192	12	-1.10(10-II-3)	0.21(10-I-1)	0.45(10-II-3)	-326(9-I-3)	-67(9-II-3)	-147(9-I-3)
192	13	-0.79(10-I-1)	-2.85(10-II-1)	-0.71(6)	99(9-II-3)	-406(9-I-3)	-275(9-II-3)
192	14	-0.54(9-II-3)	-3.04(10-II-1)	-0.76(6)	140(9-I-2)	-541(9-I-3)	-250(9-II-3)
192	15	-0.73(10-II-3)	-4.38(10-II-1)	-0.80(6)	238(9-I-3)	-755(9-I-3)	-200(9-I-3)
192	16	-3.55(10-II-3)	-5.06(10-II-1)	-2.33(10-II-1)	316(9-I-3)	-1074(9-I-3)	-486(9-I-3)
193	1	-2.96(9-II-2)	-1.57(10-II-1)	-2.78(10-II-3)	574(9-I-2)	-361(9-II-2)	104(9-I-3)
193	2	-2.79(10-II-1)	-1.16(9-II-2)	-3.03(10-II-3)	913(9-I-2)	-92(9-II-2)	-160(9-II-3)
193	3	-2.82(10-II-1)	-0.99(10-II-3)	-3.28(10-II-3)	1030(9-I-2)	148(9-I-2)	-215(9-II-3)
193	4	-2.37(10-II-1)	-1.04(10-I-3)	-3.53(9-II-3)	1068(9-I-2)	-133(9-II-3)	-302(9-II-3)
193	5	-1.54(9-II-2)	0.60(9-I-2)	-1.77(10-II-3)	276(9-I-2)	-549(9-II-3)	290(9-I-3)
193	6	-2.27(10-II-1)	-0.61(10-II-3)	-3.04(10-II-3)	517(9-I-2)	-221(9-II-3)	-398(9-II-3)
193	7	-2.63(10-II-1)	-1.13(10-I-1)	-3.43(10-II-3)	825(9-I-2)	-77(9-I-1)	-452(9-II-3)
193	8	-2.57(10-II-1)	-1.85(10-I-1)	-3.26(9-II-3)	1103(9-I-3)	-157(9-II-3)	-345(9-II-3)
193	9	-0.64(9-II-2)	0.64(10-I-3)	-1.21(10-II-3)	-219(9-II-3)	-924(9-II-3)	421(9-I-3)
193	10	-1.12(10-II-1)	-0.52(10-II-3)	-2.15(10-II-3)	-276(9-II-3)	-390(9-II-3)	-507(9-II-3)
193	11	-2.15(10-II-1)	-1.73(10-II-3)	-3.57(10-II-3)	614(9-I-3)	-203(9-I-1)	-605(9-II-3)
193	12	-4.01(10-II-1)	-2.90(10-I-1)	-2.88(10-II-3)	1178(9-I-3)	-254(9-I-4)	-443(9-II-3)
193	13	0.09(9-I-2)	1.70(9-II-3)	-0.46(10-II-3)	-110(9-II-3)	-1201(9-II-3)	426(9-I-3)
193	14	-0.05(10-I-3)	0.61(10-I-3)	-0.80(10-II-3)	-106(9-II-3)	-516(9-II-3)	-484(9-II-3)
193	15	-0.18(9-II-2)	-2.88(10-II-3)	-1.63(10-II-3)	143(9-I-3)	-249(9-I-1)	-649(9-II-3)
193	16	-6.34(10-II-3)	-6.42(10-II-3)	-4.33(10-II-3)	1149(9-I-3)	-689(9-I-4)	-735(9-II-3)
194	1	-2.05(10-I-1)	-0.40(10-II-3)	2.19(10-II-3)	155(9-I-3)	-159(9-II-3)	293(9-II-3)
194	2	-2.78(10-I-1)	-0.19(10-II-3)	1.81(10-II-3)	103(9-I-3)	-113(9-II-3)	224(9-II-3)
194	3	-3.16(10-I-1)	0.13(6)	1.29(10-II-3)	88(10-I-2)	-72(10-II-4)	160(9-II-3)
194	4	-3.11(10-I-1)	0.24(6)	0.63(10-II-3)	42(9-I-3)	-144(9-I-3)	55(9-II-2)
194	5	-2.03(10-I-1)	-0.95(10-II-3)	1.47(10-II-3)	570(9-I-3)	-379(9-II-3)	367(9-II-3)
194	6	-2.30(10-I-1)	-0.46(10-II-3)	1.33(10-II-3)	443(9-I-3)	-277(9-II-3)	327(9-II-3)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
194	7	-2.68(10-I-1)	-0.32(10-II-3)	0.95(10-II-3)	324(9-I-3)	-209(9-II-1)	261(9-II-3)
194	8	-3.00(10-I-1)	-0.13(9-II-3)	0.67(9-II-3)	241(9-I-3)	-351(9-I-3)	-73(9-I-3)
194	9	-2.77(10-I-3)	-2.43(10-II-3)	0.93(10-II-3)	1165(9-I-3)	-337(9-I-3)	579(9-II-3)
194	10	-2.88(10-I-1)	-1.34(10-II-3)	1.43(10-I-1)	924(9-I-3)	-267(9-II-1)	599(9-II-3)
194	11	-2.57(10-I-1)	-0.85(10-II-3)	1.51(10-I-1)	702(9-I-3)	-418(9-II-3)	563(9-II-3)
194	12	-2.28(10-I-1)	-0.39(10-II-3)	1.17(10-I-1)	498(9-I-3)	-565(9-II-3)	-321(9-I-3)
194	13	-4.53(10-I-3)	-0.79(10-II-3)	3.25(10-I-1)	1682(9-I-3)	-1261(9-I-3)	-1375(9-I-3)
194	14	-2.39(10-I-1)	-1.58(10-I-1)	2.81(10-I-1)	775(9-I-3)	-629(9-I-3)	-1000(9-I-3)
194	15	-0.94(10-I-1)	-1.23(10-I-1)	1.79(10-I-1)	446(9-I-3)	-682(9-II-3)	-808(9-I-3)
194	16	0.35(10-II-2)	-0.87(10-I-1)	1.15(10-I-1)	343(9-I-3)	-1594(9-II-3)	-487(9-I-3)
195	1	-0.25(9-II-3)	-0.78(9-II-3)	-0.79(9-II-3)	-48(9-II-2)	-312(10-I-3)	127(9-II-3)
195	2	0.16(9-I-3)	-0.55(9-II-3)	-0.55(9-II-3)	-55(9-II-2)	-63(9-I-3)	169(9-II-3)
195	3	-0.29(9-II-3)	-0.25(9-II-3)	-0.32(9-II-3)	-72(9-II-3)	16(10-I-3)	155(9-II-3)
195	4	-0.65(9-II-3)	-0.14(9-I-3)	-0.10(9-II-3)	-71(9-II-3)	18(10-I-2)	108(9-II-3)
195	5	-0.16(9-II-3)	-0.16(6)	-0.50(9-II-3)	-16(9-I-3)	-111(9-I-3)	97(10-I-1)
195	6	-0.49(9-II-3)	-0.14(9-II-3)	-0.53(9-II-3)	-26(9-II-2)	-61(9-I-3)	148(10-I-1)
195	7	-0.74(9-II-3)	-0.15(9-II-3)	0.41(9-I-3)	-53(9-II-3)	-26(10-II-1)	145(10-I-1)
195	8	-1.12(9-II-3)	-0.13(9-I-3)	0.18(9-I-3)	-70(9-II-3)	-6(10-II-1)	122(10-I-1)
195	9	-0.20(9-I-3)	-0.37(10-I-4)	0.27(9-I-3)	-9(6)	112(9-II-3)	95(9-I-2)
195	10	-0.37(9-II-3)	-0.38(9-II-3)	0.54(9-I-3)	-57(9-II-3)	-60(10-II-1)	102(10-I-1)
195	11	-0.92(9-II-3)	-0.33(9-II-3)	0.74(9-I-3)	-113(9-II-3)	-54(10-II-1)	115(10-I-1)
195	12	-1.67(9-II-3)	-0.04(10-II-1)	0.36(9-I-3)	-152(9-II-3)	-17(10-II-2)	114(10-I-1)
195	13	-0.36(9-I-3)	-1.86(10-I-2)	0.24(9-II-2)	-69(9-II-3)	-95(6)	87(9-I-3)
195	14	-0.75(9-I-3)	-1.47(10-I-2)	-0.18(10-I-4)	-235(9-II-3)	-132(10-II-1)	114(9-I-3)
195	15	-0.25(9-II-3)	-0.95(10-I-1)	-0.52(9-II-3)	-426(9-II-3)	-140(10-II-3)	128(9-I-3)
195	16	-2.73(9-II-3)	-0.38(9-II-3)	-0.64(9-II-3)	-503(9-II-3)	-40(10-II-4)	76(10-I-1)
196	1	-0.86(9-II-2)	0.04(10-II-3)	0.93(10-II-3)	487(9-II-2)	25(10-I-2)	-126(9-II-2)
196	2	-1.32(9-II-3)	0.11(10-I-3)	0.67(10-II-3)	423(9-II-2)	69(9-II-1)	-193(9-II-3)
196	3	-1.30(9-II-3)	0.31(10-I-3)	0.29(10-II-3)	207(10-I-2)	38(10-I-2)	-168(9-II-3)
196	4	-0.48(10-II-3)	0.85(10-I-3)	-0.42(10-I-3)	167(9-I-3)	7(9-II-1)	-145(9-II-3)
196	5	-0.56(9-II-2)	0.12(10-I-3)	0.76(10-II-3)	98(9-II-1)	-177(9-II-3)	-73(9-II-3)
196	6	-0.80(9-II-3)	0.34(10-I-3)	0.55(10-II-3)	82(9-II-1)	47(10-I-2)	-256(9-II-3)
196	7	-0.72(9-II-3)	0.47(10-I-3)	-0.31(10-I-3)	79(9-II-1)	45(9-II-1)	-265(9-II-3)
196	8	-0.31(10-II-2)	0.25(10-I-3)	-0.32(10-I-3)	42(9-II-1)	49(9-II-3)	-223(9-II-3)
196	9	-0.29(10-I-3)	-0.28(10-II-3)	0.48(10-II-3)	17(9-I-3)	-310(9-II-3)	-120(9-II-3)
196	10	-0.34(9-II-3)	0.38(10-I-3)	0.35(10-II-3)	-16(9-II-3)	-57(9-II-3)	-237(9-II-3)
196	11	-0.32(9-II-3)	0.35(10-I-3)	-0.21(10-I-3)	29(9-II-3)	50(9-II-2)	-256(9-II-3)
196	12	-0.22(9-II-3)	0.15(10-I-3)	-0.19(10-I-3)	64(9-II-3)	120(9-II-3)	-219(9-II-3)
196	13	-0.09(9-II-2)	0.57(10-I-3)	0.18(10-II-3)	-28(9-II-3)	-322(9-II-3)	-135(9-II-3)
196	14	-0.06(9-II-2)	0.56(10-I-3)	0.12(10-II-3)	-18(9-II-2)	-95(9-II-3)	-186(9-II-3)
196	15	-0.06(9-II-3)	0.45(10-I-3)	-0.07(10-I-3)	9(9-II-3)	51(9-II-2)	-198(9-II-3)
196	16	-0.11(9-II-3)	0.31(10-I-3)	-0.10(9-II-3)	42(9-II-3)	207(9-II-3)	-150(9-II-3)
197	1	0.08(6)	0.01(6)	-0.06(6)	-6(9-I-4)	6(6)	4(9-I-4)
197	2	0.13(6)	0.21(6)	-0.22(6)	-6(9-I-3)	44(6)	8(9-I-4)
197	3	0.19(10-II-1)	0.47(6)	-0.44(6)	-6(9-I-3)	120(6)	10(9-I-4)
197	4	0.47(9-II-1)	0.79(6)	-0.75(10-II-1)	-43(9-II-1)	253(6)	-28(6)
197	5	0.48(6)	-0.02(10-II-1)	-0.14(6)	-14(10-II-1)	6(6)	6(9-I-4)
197	6	0.55(6)	-0.01(6)	-0.37(6)	-13(10-II-1)	39(6)	7(9-I-4)
197	7	0.66(10-II-1)	-0.04(10-II-2)	-0.55(6)	-10(9-I-4)	103(6)	-10(6)
197	8	0.62(10-II-1)	-0.04(6)	-0.66(6)	-10(9-I-3)	186(6)	-43(6)
197	9	0.92(6)	0.01(6)	-0.11(6)	-9(6)	5(6)	8(9-I-4)
197	10	0.90(6)	-0.02(6)	-0.33(6)	-4(10-II-2)	35(6)	10(9-I-4)
197	11	0.91(10-II-1)	-0.03(6)	-0.50(6)	7(6)	96(6)	10(9-I-4)
197	12	0.94(10-II-1)	-0.06(6)	-0.67(6)	23(6)	190(6)	-35(6)
197	13	1.31(6)	0.02(6)	-0.10(6)	4(9-I-3)	4(6)	11(9-I-4)
197	14	1.24(6)	-0.01(6)	-0.29(6)	8(9-I-3)	34(6)	15(9-I-4)
197	15	1.23(10-II-1)	-0.02(6)	-0.47(6)	17(6)	97(6)	16(9-I-4)
197	16	1.25(10-II-1)	-0.04(6)	-0.63(10-II-1)	35(6)	194(6)	-27(6)
198	1	1.58(6)	0.01(6)	-0.10(6)	11(9-I-3)	4(6)	13(9-I-1)
198	2	1.49(6)	0.01(9-II-2)	-0.28(6)	14(9-I-3)	35(6)	18(9-I-1)
198	3	1.46(10-II-1)	-0.02(6)	-0.44(10-II-1)	23(6)	99(6)	19(9-I-4)
198	4	1.49(10-II-1)	-0.06(6)	-0.59(10-II-1)	41(6)	198(6)	-24(6)
198	5	1.78(6)	0.00(9-II-4)	-0.10(10-II-1)	15(9-I-3)	5(6)	14(9-I-1)
198	6	1.65(6)	-0.01(6)	-0.27(10-II-1)	17(9-I-3)	36(6)	19(9-I-1)
198	7	1.61(10-II-1)	-0.03(6)	-0.42(10-II-1)	26(6)	101(6)	21(9-I-1)
198	8	1.63(10-II-1)	-0.06(6)	-0.56(10-II-1)	43(6)	200(6)	-20(6)
198	9	1.97(6)	0.00(9-II-4)	-0.10(10-II-1)	17(9-I-3)	5(6)	15(9-II-1)
198	10	1.80(6)	-0.03(6)	-0.26(10-II-1)	19(9-I-3)	36(6)	21(9-II-1)
198	11	1.75(10-II-1)	-0.04(6)	-0.41(10-II-1)	27(6)	102(6)	22(9-II-1)
198	12	1.75(10-II-1)	-0.07(6)	-0.53(10-II-1)	45(6)	202(6)	-17(6)
198	13	2.18(6)	-0.14(10-II-1)	-0.07(10-II-1)	18(9-I-3)	5(6)	16(9-II-1)
198	14	1.93(6)	-0.03(6)	-0.25(10-II-1)	20(9-I-3)	37(6)	22(9-II-1)
198	15	1.87(10-II-1)	-0.03(6)	-0.39(10-II-1)	27(6)	103(6)	21(9-II-1)
198	16	1.87(10-II-1)	-0.11(6)	-0.51(10-II-1)	44(6)	203(6)	-14(6)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
199	1	2.65(6)	0.05(10-II-1)	-0.08(10-II-1)	11(9-II-1)	5(6)	21(10-II-1)
199	2	2.41(10-II-1)	0.02(10-II-1)	-0.23(10-II-1)	14(9-II-1)	35(6)	27(10-II-1)
199	3	2.24(10-II-1)	0.00(9-II-1)	-0.34(10-II-1)	21(6)	99(6)	26(10-II-1)
199	4	2.10(10-II-1)	0.02(9-I-3)	-0.42(10-II-1)	36(6)	197(6)	8(9-I-1)
199	5	3.42(10-II-1)	0.13(10-II-1)	-0.06(10-II-1)	-5(6)	4(6)	29(10-II-2)
199	6	3.02(10-II-1)	0.02(10-II-1)	-0.17(10-II-1)	4(9-II-1)	33(6)	37(10-II-2)
199	7	2.62(10-II-1)	-0.00(9-II-2)	-0.24(10-II-1)	11(6)	93(6)	36(10-II-2)
199	8	2.24(10-II-1)	0.06(6)	-0.27(10-II-1)	28(6)	187(6)	21(9-I-1)
199	9	4.01(10-II-1)	0.18(10-II-1)	-0.04(10-II-1)	-4(10-I-1)	5(6)	37(10-II-2)
199	10	3.40(10-II-1)	0.03(10-II-1)	-0.10(10-II-1)	5(10-II-1)	35(6)	46(10-II-2)
199	11	2.82(10-II-1)	-0.00(9-II-2)	-0.13(10-II-1)	12(6)	97(6)	48(10-II-2)
199	12	2.25(10-II-1)	0.07(6)	-0.15(10-II-1)	27(6)	191(6)	40(10-II-2)
199	13	3.99(10-II-1)	0.18(10-II-1)	0.05(10-II-1)	20(10-II-1)	6(6)	37(10-II-2)
199	14	3.38(10-II-1)	0.00(10-II-1)	0.14(10-II-1)	22(10-II-1)	40(6)	47(10-II-2)
199	15	2.82(10-II-1)	-0.08(10-I-3)	0.19(10-II-1)	26(10-II-1)	109(6)	48(10-II-2)
199	16	2.31(10-II-1)	-0.13(10-I-3)	0.23(9-II-1)	40(6)	212(6)	48(6)
200	1	3.31(10-II-1)	0.11(10-II-1)	0.12(10-II-1)	33(10-II-1)	6(6)	34(6)
200	2	2.92(10-II-1)	-0.01(10-II-1)	0.36(10-II-1)	35(10-II-1)	43(6)	44(6)
200	3	2.54(10-II-1)	-0.12(10-II-1)	0.51(10-II-1)	38(10-II-1)	115(6)	45(6)
200	4	2.16(10-II-1)	-0.26(10-II-1)	0.59(10-II-1)	56(6)	220(6)	51(6)
200	5	2.67(10-II-1)	0.04(10-II-1)	0.17(10-II-1)	29(10-II-1)	6(6)	33(6)
200	6	2.44(10-II-1)	-0.00(6)	0.47(10-II-1)	31(10-II-1)	42(6)	42(6)
200	7	2.26(10-II-1)	-0.06(6)	0.67(10-II-1)	33(10-II-1)	113(6)	42(6)
200	8	2.13(10-II-1)	-0.16(10-II-1)	0.74(10-II-1)	47(6)	213(6)	56(6)
200	9	1.88(6)	0.01(6)	0.20(10-II-1)	24(10-II-1)	6(6)	30(6)
200	10	1.88(10-II-1)	-0.01(6)	0.55(10-II-1)	26(10-II-1)	42(6)	39(6)
200	11	1.93(10-II-1)	-0.06(6)	0.78(10-II-1)	29(10-II-1)	111(6)	40(6)
200	12	2.00(10-II-1)	-0.11(10-II-1)	0.90(10-II-1)	43(6)	209(6)	61(6)
200	13	1.01(6)	-0.04(9-II-3)	0.21(10-II-1)	20(10-II-1)	6(6)	28(6)
200	14	1.24(10-II-1)	0.01(10-I-1)	0.58(10-II-1)	21(10-II-1)	43(6)	36(6)
200	15	1.51(10-II-1)	0.03(10-I-1)	0.85(10-II-1)	25(6)	113(6)	38(6)
200	16	1.82(10-II-1)	-0.02(6)	1.02(10-II-1)	40(6)	212(6)	66(6)
201	1	0.35(6)	-0.05(10-II-1)	0.18(10-II-1)	15(10-II-1)	7(6)	24(6)
201	2	0.69(10-II-1)	0.08(9-II-3)	0.51(10-II-1)	17(10-II-1)	46(6)	33(6)
201	3	1.08(10-II-1)	0.19(9-II-3)	0.82(10-II-1)	22(6)	118(6)	36(6)
201	4	1.54(10-II-1)	0.22(10-I-3)	1.06(10-II-1)	37(6)	219(6)	72(6)
201	5	-0.18(10-I-3)	-0.01(10-II-1)	0.09(6)	12(10-II-2)	8(6)	20(6)
201	6	0.27(10-II-1)	0.19(9-II-3)	0.29(6)	14(6)	50(6)	28(6)
201	7	0.62(10-II-1)	0.43(9-II-3)	0.64(10-II-1)	19(6)	125(6)	33(6)
201	8	1.17(10-II-1)	0.60(9-II-3)	1.04(10-II-1)	31(6)	230(6)	74(6)
201	9	-0.21(9-II-3)	0.01(9-II-3)	-0.05(10-I-3)	10(6)	10(6)	14(6)
201	10	-0.07(10-I-1)	0.20(10-II-1)	-0.07(10-I-3)	11(6)	57(6)	21(6)
201	11	-0.15(10-I-1)	0.54(10-II-1)	0.15(6)	15(6)	139(6)	29(6)
201	12	0.45(10-II-1)	0.98(9-II-3)	0.79(10-II-1)	19(6)	255(6)	73(6)
201	13	-0.05(9-II-3)	-0.03(9-II-3)	-0.05(9-II-3)	5(6)	11(6)	6(6)
201	14	-0.03(10-I-3)	-0.15(10-I-3)	-0.12(9-II-3)	4(6)	62(6)	11(6)
201	15	-0.02(10-I-1)	-0.25(10-I-3)	-0.18(10-I-3)	11(6)	154(6)	19(6)
201	16	-1.38(10-I-4)	0.45(6)	-0.48(10-I-4)	-43(10-II-1)	309(6)	44(6)
202	1	1.76(10-I-3)	-1.55(9-II-4)	0.16(10-I-3)	-17(10-I-4)	-803(10-I-4)	-33(10-I-3)
202	2	2.06(10-I-3)	-0.97(9-II-4)	-0.17(9-II-4)	34(9-II-1)	-313(10-I-4)	-199(10-I-3)
202	3	1.75(9-II-4)	-0.42(9-II-4)	-0.29(9-II-4)	94(9-II-1)	-83(6)	-176(10-I-3)
202	4	1.80(9-II-4)	-0.07(9-II-4)	-0.20(9-II-4)	133(9-II-4)	-10(10-I-3)	-118(10-I-3)
202	5	1.88(10-I-3)	-1.58(9-II-4)	-0.29(10-II-3)	-84(10-I-4)	-944(10-I-3)	-57(10-I-3)
202	6	2.18(10-I-3)	-0.85(9-II-4)	-0.50(9-II-4)	-15(6)	-323(10-I-3)	-189(10-I-3)
202	7	1.73(10-I-3)	-0.28(9-II-4)	-0.48(9-II-4)	92(10-I-3)	-55(6)	-154(10-I-3)
202	8	1.61(9-II-4)	-0.05(10-II-3)	-0.23(9-II-4)	159(10-I-3)	6(10-I-3)	-106(10-I-3)
202	9	2.26(10-I-3)	-1.20(9-II-4)	-0.50(10-II-3)	-131(9-II-3)	-1073(10-I-3)	-78(6)
202	10	2.23(10-I-3)	-0.41(10-II-3)	-0.82(9-II-4)	23(10-I-2)	-303(10-I-3)	-155(10-I-3)
202	11	1.68(10-I-3)	-0.19(10-II-3)	-0.57(9-II-4)	158(10-I-3)	-32(10-II-2)	-109(10-I-3)
202	12	1.41(9-II-4)	-0.06(10-II-3)	-0.24(9-II-4)	231(10-I-3)	21(10-I-3)	-82(10-I-3)
202	13	3.15(10-I-3)	0.57(10-I-3)	-0.93(9-II-4)	-185(9-II-4)	-1131(10-I-3)	-30(6)
202	14	2.08(10-I-3)	0.46(10-I-3)	-0.73(9-II-4)	173(10-I-3)	-265(10-I-3)	-48(10-I-3)
202	15	1.41(10-I-3)	0.11(10-I-3)	-0.51(9-II-4)	305(10-I-3)	-17(10-II-3)	-28(10-I-3)
202	16	1.14(10-I-3)	-0.07(10-II-3)	-0.25(9-II-4)	363(10-I-3)	25(10-I-3)	-34(10-I-3)
203	1	1.07(9-II-4)	4.73(9-II-4)	1.61(9-II-4)	21(10-I-4)	100(9-II-4)	121(9-II-4)
203	2	0.10(9-II-4)	1.62(9-II-4)	0.64(9-II-4)	15(9-II-4)	13(9-II-4)	86(9-II-4)
203	3	-0.10(9-II-4)	0.27(9-II-2)	0.21(9-II-4)	13(9-II-4)	-64(6)	43(9-II-4)
203	4	-0.10(9-II-4)	0.03(9-II-2)	0.08(9-II-2)	10(9-II-4)	-28(6)	2(9-II-4)
203	5	0.20(9-II-4)	1.37(9-II-4)	1.96(9-II-4)	99(10-I-3)	104(9-II-4)	148(9-II-4)
203	6	0.71(9-II-4)	0.56(9-II-4)	1.86(9-II-4)	61(10-I-4)	-11(6)	113(9-II-4)
203	7	0.56(9-II-4)	-0.56(10-II-3)	0.53(9-II-4)	40(9-II-4)	-90(6)	59(9-II-4)
203	8	-0.05(10-II-3)	-0.20(10-II-3)	-0.04(10-II-3)	45(9-II-4)	-50(10-II-3)	-16(10-II-3)
203	9	-0.48(9-I-4)	-0.38(10-II-3)	2.62(9-II-4)	194(10-I-3)	119(9-II-4)	137(9-II-4)
203	10	1.49(9-II-4)	-1.13(6)	2.22(9-II-4)	103(10-I-3)	-44(6)	84(9-II-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
203	11	1.25 (9-II-4)	-1.34 (6)	0.88 (9-II-4)	29 (9-II-4)	-110 (6)	63 (9-II-4)
203	12	-0.25 (10-II-3)	-1.39 (6)	-0.62 (10-II-3)	92 (9-II-4)	-157 (9-II-3)	-44 (10-II-3)
203	13	0.21 (6)	-2.52 (9-II-4)	3.55 (9-II-4)	325 (10-I-3)	-75 (6)	115 (9-II-4)
203	14	2.26 (9-II-4)	-1.78 (6)	2.12 (9-II-4)	126 (9-I-2)	-64 (6)	-51 (10-I-3)
203	15	1.62 (9-II-4)	-1.90 (6)	1.31 (9-II-4)	58 (9-II-4)	-82 (6)	-44 (10-I-3)
203	16	3.32 (9-II-2)	-5.36 (6)	-0.98 (10-II-3)	19 (10-I-3)	-778 (9-II-2)	-416 (9-II-3)
204	1	1.31 (9-II-4)	-3.44 (9-II-4)	0.66 (10-I-3)	144 (10-II-3)	-327 (10-I-4)	47 (9-II-3)
204	2	1.77 (9-II-4)	-2.50 (10-I-4)	0.65 (10-I-3)	156 (10-II-2)	-154 (10-I-3)	-22 (10-I-3)
204	3	2.50 (9-II-4)	-2.52 (10-I-4)	0.40 (6)	-51 (10-I-3)	-121 (6)	-35 (10-I-3)
204	4	0.79 (9-II-4)	-5.06 (10-I-4)	1.87 (6)	-546 (10-I-3)	-1139 (9-II-2)	557 (9-II-2)
204	5	1.40 (9-II-4)	-2.71 (9-II-4)	0.61 (10-I-3)	129 (9-II-4)	-352 (10-I-4)	17 (10-II-2)
204	6	1.94 (9-II-4)	-2.33 (9-II-4)	0.40 (10-I-3)	77 (10-II-3)	-193 (10-I-4)	-89 (10-I-3)
204	7	1.89 (9-II-4)	-2.12 (10-I-4)	0.86 (10-I-3)	-117 (10-I-3)	-168 (6)	-160 (10-I-3)
204	8	0.70 (9-II-4)	-0.50 (6)	0.68 (10-I-4)	-195 (10-I-3)	-237 (9-II-4)	-17 (10-I-3)
204	9	1.49 (9-II-4)	-2.18 (9-II-4)	0.48 (10-I-3)	57 (9-II-1)	-473 (10-I-4)	-32 (10-I-2)
204	10	1.93 (9-II-4)	-1.87 (9-II-4)	0.32 (10-I-3)	45 (10-II-3)	-246 (10-I-4)	-168 (10-I-3)
204	11	1.70 (9-II-4)	-1.21 (10-I-4)	0.42 (9-I-4)	-32 (10-I-3)	-154 (6)	-188 (10-I-3)
204	12	1.70 (9-II-4)	-0.24 (10-I-4)	0.12 (9-I-4)	-57 (10-I-3)	-73 (6)	-101 (10-I-3)
204	13	1.75 (9-II-4)	-1.70 (9-II-4)	0.47 (10-I-3)	-7 (10-II-2)	-634 (10-I-4)	-34 (10-I-3)
204	14	2.04 (10-I-3)	-1.24 (9-II-4)	0.11 (9-I-3)	55 (9-II-1)	-279 (10-I-4)	-196 (10-I-3)
204	15	1.70 (9-II-4)	-0.64 (9-II-4)	0.05 (9-I-4)	67 (9-II-1)	-112 (6)	-186 (10-I-3)
204	16	1.77 (9-II-4)	-0.11 (10-I-3)	-0.12 (9-II-4)	77 (9-II-2)	-30 (6)	-123 (10-I-3)
205	1	1.98 (10-I-3)	0.49 (10-I-3)	-1.02 (9-II-4)	-85 (6)	-1100 (10-I-3)	80 (9-II-4)
205	2	2.19 (10-I-3)	0.50 (10-I-3)	-0.46 (10-II-3)	155 (10-I-3)	-242 (10-I-3)	15 (9-II-3)
205	3	1.52 (10-I-3)	0.22 (6)	-0.35 (9-II-4)	312 (10-I-3)	19 (10-I-3)	25 (10-II-3)
205	4	1.20 (10-I-3)	0.06 (9-II-4)	-0.21 (9-II-4)	380 (10-I-3)	34 (9-II-4)	-10 (6)
205	5	1.22 (10-I-3)	-1.32 (9-II-3)	-1.52 (9-II-4)	-104 (10-I-3)	-965 (10-I-3)	50 (9-II-1)
205	6	1.89 (10-I-3)	-0.42 (9-II-3)	-0.62 (10-II-3)	17 (9-I-4)	-272 (10-I-3)	47 (9-II-2)
205	7	1.48 (10-I-3)	-0.06 (10-II-3)	-0.31 (9-II-3)	163 (10-I-3)	-19 (9-II-3)	17 (9-II-3)
205	8	1.11 (10-I-3)	-0.02 (10-II-3)	-0.11 (9-II-3)	249 (10-I-3)	17 (10-I-3)	9 (9-II-3)
205	9	1.01 (10-I-3)	-1.58 (9-II-4)	-1.69 (9-II-4)	-123 (9-II-4)	-810 (10-I-3)	43 (10-I-3)
205	10	1.76 (10-I-3)	-0.90 (9-II-3)	-0.97 (9-II-4)	-17 (9-II-4)	-294 (10-I-3)	75 (9-II-2)
205	11	1.40 (10-I-3)	-0.32 (9-II-3)	-0.41 (9-II-3)	82 (10-I-3)	-47 (9-II-4)	54 (9-II-2)
205	12	1.06 (10-I-3)	-0.07 (9-II-3)	-0.10 (9-II-3)	149 (10-I-3)	12 (10-I-3)	32 (9-II-2)
205	13	0.70 (10-I-3)	-1.44 (9-II-3)	-2.10 (9-II-4)	-67 (9-II-4)	-648 (10-I-3)	66 (9-II-1)
205	14	1.28 (10-I-3)	-0.77 (9-II-3)	-1.17 (9-II-4)	26 (9-I-4)	-292 (10-I-3)	90 (10-I-3)
205	15	1.13 (10-I-3)	-0.32 (9-II-3)	-0.56 (9-II-3)	61 (10-I-3)	-71 (9-II-4)	88 (10-I-3)
205	16	0.95 (10-I-3)	-0.05 (9-I-1)	-0.15 (9-II-3)	97 (10-I-3)	-7 (10-II-3)	55 (10-I-3)
206	1	-1.05 (10-II-3)	-0.86 (9-II-3)	-2.32 (9-II-4)	47 (10-II-3)	-510 (10-I-3)	73 (10-I-3)
206	2	0.95 (10-I-3)	-0.61 (9-II-3)	-1.33 (9-II-4)	-20 (9-II-4)	-272 (10-I-3)	87 (10-I-3)
206	3	1.03 (10-I-3)	-0.32 (9-II-3)	-0.67 (9-II-3)	37 (10-I-2)	-79 (9-II-4)	96 (10-I-3)
206	4	0.90 (10-I-3)	-0.10 (9-II-3)	-0.19 (9-II-3)	63 (10-I-3)	-9 (10-II-3)	68 (10-I-3)
206	5	-1.14 (10-II-3)	-0.72 (10-I-3)	-2.14 (9-II-4)	33 (10-II-3)	-404 (10-I-3)	50 (10-I-3)
206	6	0.49 (10-I-3)	-0.64 (10-I-3)	-1.54 (9-II-4)	-45 (9-II-2)	-256 (10-I-3)	64 (10-I-3)
206	7	0.70 (10-I-3)	-0.31 (10-I-3)	-0.78 (9-II-3)	-73 (9-II-2)	-95 (9-II-4)	86 (10-I-3)
206	8	0.72 (10-I-3)	-0.07 (10-I-3)	-0.22 (9-II-3)	-83 (9-II-2)	-18 (10-II-3)	73 (10-I-3)
206	9	-1.00 (10-II-3)	-0.59 (10-I-3)	-2.01 (9-II-4)	-54 (9-II-2)	-322 (10-I-3)	46 (10-I-2)
206	10	-0.45 (10-II-3)	-0.47 (10-I-3)	-1.56 (9-II-4)	-82 (9-II-2)	-234 (10-I-3)	41 (10-I-3)
206	11	0.42 (10-I-3)	-0.32 (10-I-3)	-0.85 (9-II-3)	-127 (9-II-2)	-98 (9-II-4)	81 (10-I-3)
206	12	0.53 (10-I-3)	-0.09 (9-II-3)	-0.27 (9-II-3)	-150 (9-II-2)	-17 (10-II-3)	75 (10-I-3)
206	13	-0.90 (10-II-3)	-0.19 (9-I-2)	-2.15 (9-II-4)	-180 (9-II-2)	-241 (10-I-3)	77 (10-I-3)
206	14	-0.99 (10-II-3)	0.11 (9-II-2)	-1.29 (9-II-4)	-156 (9-II-2)	-211 (10-I-3)	64 (10-I-3)
206	15	-0.68 (10-II-3)	-0.13 (10-I-3)	-0.82 (9-II-3)	-169 (9-II-2)	-110 (9-II-4)	112 (10-I-3)
206	16	-0.59 (10-II-3)	-0.10 (9-II-3)	-0.36 (9-II-3)	-192 (10-II-3)	-35 (9-II-3)	81 (10-I-3)
207	1	-3.83 (9-II-3)	0.71 (9-II-3)	-0.59 (10-I-3)	184 (9-II-3)	1063 (9-II-3)	-141 (10-I-3)
207	2	-3.02 (9-II-3)	0.25 (9-II-3)	0.30 (10-II-3)	113 (9-II-2)	288 (9-II-2)	-69 (6)
207	3	-1.54 (10-II-3)	-0.18 (6)	0.22 (10-II-3)	80 (9-II-2)	-129 (9-I-2)	-110 (6)
207	4	-0.93 (10-II-3)	-0.08 (10-I-3)	-0.07 (6)	64 (10-I-3)	-82 (10-II-3)	-169 (6)
207	5	-3.96 (9-II-3)	1.11 (9-II-3)	0.47 (10-II-3)	222 (9-II-3)	1140 (9-II-3)	-130 (10-I-2)
207	6	-3.12 (9-II-3)	-0.05 (9-I-3)	0.75 (10-II-3)	151 (9-II-3)	311 (9-II-2)	-75 (6)
207	7	-1.31 (10-II-3)	-0.60 (9-I-4)	0.35 (10-II-3)	103 (9-II-2)	-196 (9-I-2)	-124 (6)
207	8	-0.93 (10-II-3)	-0.24 (9-I-4)	-0.23 (6)	110 (10-I-3)	-132 (10-II-3)	-235 (6)
207	9	-4.55 (9-II-3)	0.39 (9-II-3)	0.92 (10-II-3)	230 (9-II-3)	1201 (9-II-3)	-111 (10-I-2)
207	10	-3.08 (9-II-3)	-0.71 (9-II-2)	1.32 (10-II-3)	81 (9-II-3)	308 (9-II-2)	-88 (6)
207	11	-1.04 (9-II-3)	-0.97 (9-II-2)	0.55 (10-II-3)	-23 (10-II-3)	-248 (9-I-2)	-90 (10-II-3)
207	12	-0.90 (10-II-3)	-0.84 (9-II-3)	-0.72 (6)	162 (10-I-3)	-348 (10-II-3)	-303 (10-II-3)
207	13	-5.89 (9-II-3)	-2.47 (9-II-2)	1.52 (10-II-3)	142 (9-II-4)	1223 (9-II-2)	-132 (9-I-3)
207	14	-2.67 (9-II-3)	-2.02 (9-II-2)	1.14 (10-II-3)	-138 (9-II-3)	274 (9-II-2)	-107 (10-II-2)
207	15	0.32 (6)	-1.41 (9-II-2)	0.72 (10-II-3)	-169 (9-II-2)	-215 (6)	-78 (10-II-3)
207	16	1.42 (9-II-2)	-2.02 (9-II-2)	-0.80 (10-I-3)	131 (6)	-1609 (9-II-2)	-703 (10-II-3)
208	1	0.73 (9-II-2)	4.22 (9-II-2)	-0.08 (9-I-4)	676 (10-I-3)	568 (10-I-3)	232 (10-I-4)
208	2	-1.44 (10-I-4)	2.10 (9-II-2)	0.19 (6)	845 (10-I-3)	365 (10-I-4)	-19 (10-II-1)
208	3	-2.17 (9-II-3)	0.88 (9-II-2)	0.17 (6)	658 (10-I-4)	160 (10-I-4)	-22 (10-II-1)
208	4	-3.29 (9-II-4)	0.38 (9-II-2)	0.07 (6)	514 (10-I-4)	56 (10-I-4)	-39 (10-II-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
208	5	1.38(9-II-2)	3.40(9-II-3)	1.32(9-II-3)	417(10-I-3)	164(9-II-4)	252(10-I-3)
208	6	-1.23(10-I-4)	2.00(9-II-2)	1.03(9-II-4)	498(10-I-3)	279(10-I-4)	25(10-I-1)
208	7	-2.06(9-II-3)	0.87(9-II-2)	0.72(9-II-4)	487(10-I-4)	137(10-I-4)	-41(10-II-1)
208	8	-3.08(9-II-4)	0.11(9-II-2)	0.33(9-II-4)	435(10-I-4)	29(10-I-4)	-38(10-II-1)
208	9	0.96(9-II-2)	1.90(10-I-3)	1.56(10-I-4)	275(9-II-4)	20(10-II-4)	234(10-I-3)
208	10	-1.01(10-I-4)	1.43(9-II-3)	1.72(9-II-4)	282(10-I-1)	169(9-II-4)	58(10-I-1)
208	11	-1.73(9-II-3)	0.60(9-II-2)	1.26(9-II-4)	305(10-I-3)	103(10-I-4)	-43(10-II-1)
208	12	-2.65(9-II-4)	0.07(9-II-2)	0.56(9-II-4)	313(10-I-4)	19(10-I-4)	-36(10-II-1)
208	13	0.28(9-II-2)	0.79(10-I-3)	1.64(10-I-4)	168(9-II-4)	-106(10-I-4)	163(10-I-3)
208	14	-0.78(10-I-4)	0.51(10-I-3)	2.03(9-II-3)	133(10-II-1)	71(9-II-4)	33(10-I-1)
208	15	-1.28(10-I-4)	0.14(10-I-3)	1.60(9-II-4)	141(10-II-1)	70(9-II-4)	-53(10-II-1)
208	16	-1.91(9-II-3)	-0.04(6)	0.73(9-II-4)	166(10-II-1)	20(10-I-4)	-37(10-II-1)
209	1	-3.39(9-II-4)	-0.17(9-I-2)	-2.40(9-II-4)	-113(9-II-2)	-236(10-I-3)	112(10-I-3)
209	2	-0.83(10-II-3)	0.45(9-II-4)	-1.18(9-II-3)	-165(9-II-2)	-127(10-I-3)	100(10-I-3)
209	3	-0.38(10-II-3)	0.33(9-II-4)	-0.64(9-II-3)	-134(10-II-3)	-41(10-II-3)	128(10-I-3)
209	4	-0.46(10-II-3)	0.09(9-II-3)	-0.28(9-II-3)	-125(10-II-3)	12(10-I-3)	88(10-I-3)
209	5	-3.40(9-II-4)	0.71(9-II-2)	-2.30(9-II-4)	-19(10-I-3)	-128(10-I-3)	58(10-I-3)
209	6	-1.55(10-II-3)	0.35(9-II-3)	-1.33(9-II-3)	-51(10-I-3)	-98(10-I-3)	77(10-I-3)
209	7	-0.88(10-II-3)	0.25(9-II-3)	-0.47(9-II-3)	-41(10-I-2)	-40(10-I-2)	107(10-I-3)
209	8	-0.72(10-II-3)	0.03(9-II-3)	-0.08(9-II-3)	-30(9-I-3)	-9(10-II-3)	89(10-I-3)
209	9	-3.55(9-II-4)	1.51(9-II-2)	-1.83(9-II-4)	73(9-II-3)	67(10-II-3)	37(10-I-3)
209	10	-2.02(10-II-3)	0.58(10-II-3)	-1.06(9-II-3)	92(9-II-3)	-61(10-I-3)	67(10-I-3)
209	11	-1.16(10-II-3)	0.12(10-II-3)	-0.31(9-II-3)	135(9-II-3)	-36(10-I-2)	104(10-I-3)
209	12	-0.82(9-II-3)	-0.04(10-I-3)	-0.02(10-I-3)	172(9-II-3)	-9(10-I-2)	88(10-I-3)
209	13	-4.07(9-II-2)	2.32(9-II-3)	-1.11(9-II-3)	172(9-II-3)	77(10-II-3)	-21(10-II-3)
209	14	-2.36(9-II-4)	0.60(9-II-3)	-0.55(10-I-3)	191(9-II-3)	-27(10-I-3)	49(10-I-3)
209	15	-1.33(10-II-3)	-0.18(10-I-3)	-0.21(10-I-3)	257(9-II-3)	-24(10-I-2)	85(10-I-3)
209	16	-0.89(9-II-3)	-0.11(10-I-3)	-0.05(10-I-3)	343(9-II-3)	23(9-II-3)	88(10-I-3)
210	1	-4.03(9-II-3)	-1.95(9-II-2)	1.28(10-II-3)	132(9-II-2)	1454(9-II-2)	-250(9-II-4)
210	2	-2.50(9-II-3)	-1.94(9-II-2)	0.75(10-II-3)	-144(9-II-3)	310(9-II-2)	-73(10-II-3)
210	3	-0.27(9-II-3)	-1.36(9-II-3)	0.35(10-II-3)	-143(9-II-2)	-222(10-II-3)	-51(10-II-3)
210	4	1.77(9-II-2)	-2.04(9-II-3)	1.07(10-II-3)	-546(9-II-2)	-1656(9-II-2)	894(10-I-3)
210	5	-3.49(9-II-3)	-0.48(10-II-3)	1.98(9-II-3)	262(9-II-2)	1451(9-II-2)	-286(9-II-4)
210	6	-1.91(9-II-3)	-1.43(10-II-3)	0.95(10-II-3)	74(9-II-4)	402(9-II-2)	-152(9-II-4)
210	7	-0.11(10-II-3)	-1.50(10-II-3)	0.39(10-II-3)	-98(9-II-2)	-205(10-II-3)	-47(9-II-2)
210	8	-0.30(10-II-3)	-1.09(9-I-4)	0.82(10-II-3)	-175(9-II-2)	-374(10-II-3)	251(9-I-2)
210	9	-3.13(9-II-3)	-1.22(10-II-3)	2.71(9-II-3)	236(9-II-2)	1351(9-II-2)	-280(9-II-4)
210	10	-1.12(9-II-3)	-1.71(10-II-3)	1.21(10-II-3)	95(9-II-4)	505(9-II-2)	-198(9-II-2)
210	11	-0.06(9-II-3)	-1.05(10-II-3)	0.24(10-II-3)	8(6)	-119(6)	-52(9-II-2)
210	12	-0.22(6)	-0.29(10-II-3)	0.21(6)	-53(9-II-2)	-125(10-II-3)	105(9-I-2)
210	13	-2.71(9-II-3)	-4.79(10-II-3)	3.22(9-II-3)	176(9-II-2)	1281(9-II-2)	-289(9-II-4)
210	14	-0.29(9-II-3)	-1.02(10-II-3)	0.25(10-II-3)	13(9-II-4)	557(9-II-2)	-136(9-II-4)
210	15	0.14(9-II-3)	-0.45(6)	-0.09(9-II-2)	18(9-II-4)	-51(6)	-36(9-II-2)
210	16	0.07(9-II-3)	-0.13(6)	-0.07(9-II-2)	-8(9-I-4)	-73(10-II-3)	34(9-I-2)
211	1	-0.21(6)	-0.27(9-II-4)	1.80(10-I-4)	87(9-II-3)	-141(10-I-4)	113(10-I-3)
211	2	-0.83(10-I-4)	-0.35(9-II-4)	2.17(9-II-3)	51(10-II-1)	16(9-II-4)	14(10-I-1)
211	3	-1.26(10-I-4)	-0.26(9-II-4)	1.68(9-II-3)	54(10-II-1)	36(10-II-1)	-47(10-II-1)
211	4	-1.61(9-II-3)	-0.05(9-II-4)	0.74(9-II-4)	52(10-II-1)	6(10-II-1)	-35(10-II-1)
211	5	-0.73(6)	-1.63(9-II-4)	1.96(10-I-4)	-19(6)	-223(10-I-4)	120(10-I-3)
211	6	-0.57(10-I-4)	-1.40(9-II-4)	2.15(9-II-3)	-2(10-I-1)	-42(9-I-4)	37(10-I-1)
211	7	-0.72(10-I-4)	-0.78(9-II-4)	1.53(9-II-3)	19(10-II-1)	23(10-II-1)	-12(10-II-1)
211	8	-0.86(9-II-3)	-0.17(9-II-4)	0.58(9-II-3)	26(10-II-1)	12(10-II-1)	-18(10-II-1)
211	9	-1.08(10-I-3)	-3.43(9-II-3)	2.00(10-I-4)	-122(9-II-4)	-315(10-I-4)	133(10-I-4)
211	10	-0.30(10-I-4)	-2.54(9-II-3)	1.75(9-II-3)	-21(10-I-4)	-71(10-I-4)	42(10-I-1)
211	11	-0.29(9-II-3)	-1.13(9-II-3)	1.08(9-II-3)	-3(10-I-1)	10(10-II-1)	5(10-I-1)
211	12	-0.40(9-II-3)	-0.22(9-II-3)	0.35(9-II-3)	11(10-II-1)	9(10-II-1)	-12(10-II-1)
211	13	-0.39(9-II-4)	-6.74(9-II-3)	1.74(10-I-3)	-249(10-I-3)	-321(10-I-3)	142(10-I-3)
211	14	0.09(10-I-4)	-3.37(9-II-3)	0.62(9-II-3)	35(10-I-3)	-93(10-I-4)	26(10-I-1)
211	15	0.10(10-I-4)	-1.29(9-II-3)	0.42(9-II-3)	-12(10-I-4)	-7(10-I-1)	6(10-I-1)
211	16	0.07(9-II-3)	-0.21(9-II-3)	0.12(9-II-3)	4(10-II-1)	8(10-II-1)	-6(10-II-1)
212	1	-3.51(10-II-2)	-1.03(9-II-2)	-1.15(9-II-2)	-93(9-I-2)	752(9-II-3)	-125(9-II-2)
212	2	-2.07(10-II-3)	-0.18(10-I-3)	-0.64(10-I-3)	-279(10-II-3)	86(9-II-2)	56(10-II-3)
212	3	-1.29(10-II-3)	0.09(10-II-3)	-0.34(10-I-3)	-349(10-II-3)	-88(10-II-3)	62(10-II-3)
212	4	-0.99(10-II-3)	0.04(10-I-3)	-0.16(10-I-3)	-375(10-II-3)	-39(10-II-3)	-28(10-I-3)
212	5	-3.24(10-II-2)	0.60(10-II-3)	-1.08(10-I-3)	108(9-II-2)	881(9-II-3)	-185(9-II-2)
212	6	-2.43(10-II-3)	0.14(10-II-3)	-0.78(10-I-3)	-57(10-II-3)	149(9-II-2)	-93(10-I-3)
212	7	-1.50(10-II-3)	0.03(9-II-2)	-0.30(10-I-3)	-176(10-II-3)	-83(10-II-3)	-66(10-I-3)
212	8	-1.03(10-II-3)	-0.02(10-II-3)	-0.09(6)	-247(10-II-3)	-45(10-II-3)	-72(10-I-3)
212	9	-3.11(10-II-2)	0.95(10-II-3)	-0.86(10-I-3)	155(9-II-3)	927(9-II-3)	-167(9-II-4)
212	10	-2.61(10-II-2)	0.32(9-II-3)	-0.58(10-I-3)	85(9-II-2)	218(9-II-2)	-111(10-I-3)
212	11	-1.58(10-II-3)	-0.07(6)	-0.24(6)	-69(10-II-3)	-83(10-II-3)	-94(10-I-3)
212	12	-1.04(10-II-3)	-0.04(6)	-0.07(6)	-158(10-II-3)	-47(10-II-3)	-101(6)
212	13	-3.28(10-II-2)	0.59(10-II-3)	-0.66(10-I-3)	172(9-II-3)	982(9-II-3)	-138(10-I-3)
212	14	-2.83(9-II-3)	0.25(10-II-3)	-0.33(10-I-3)	86(9-II-2)	255(9-II-2)	-91(10-I-3)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
212	15	-1.55(10-II-3)	-0.06(6)	-0.15(6)	44(10-I-3)	-95(9-I-2)	-100(6)
212	16	-0.96(10-II-3)	-0.06(10-II-3)	-0.07(6)	-99(10-II-3)	-57(10-II-3)	-124(6)
213	1	-2.73(10-II-3)	1.75(9-II-3)	-0.63(10-II-2)	-253(9-II-2)	136(9-II-3)	47(10-II-3)
213	2	-2.18(10-II-3)	0.66(9-II-3)	-0.81(9-II-3)	-319(10-I-3)	-39(10-I-3)	104(10-II-2)
213	3	-1.32(10-II-3)	0.13(9-II-3)	-0.44(10-II-2)	-405(10-I-3)	-68(10-I-3)	97(9-II-3)
213	4	-0.55(10-II-3)	0.03(9-II-2)	-0.22(10-II-2)	-537(10-I-3)	-58(10-I-3)	92(9-II-3)
213	5	-2.89(10-II-3)	0.65(10-II-3)	-0.59(10-II-2)	-147(10-I-3)	278(9-II-3)	33(10-II-3)
213	6	-2.23(10-II-3)	0.41(9-II-3)	-0.38(9-I-2)	-250(10-I-3)	-29(10-I-3)	93(10-II-3)
213	7	-1.36(10-II-3)	-0.13(10-I-3)	-0.32(6)	-347(10-I-3)	-76(10-I-3)	83(10-II-3)
213	8	-0.67(10-II-3)	-0.05(10-I-3)	-0.17(10-II-2)	-429(10-I-3)	-37(10-I-3)	71(10-II-3)
213	9	-3.20(10-II-3)	-0.31(10-I-3)	-0.63(9-II-3)	-97(10-I-3)	400(9-II-3)	-60(10-I-3)
213	10	-2.26(10-II-3)	-0.34(10-I-3)	-0.27(6)	-215(10-I-3)	-27(6)	78(10-II-3)
213	11	-1.39(10-II-3)	-0.21(10-I-3)	-0.30(6)	-303(10-I-3)	-80(9-II-3)	68(10-II-3)
213	12	-0.81(10-II-3)	-0.06(10-I-3)	-0.17(6)	-363(10-I-3)	-29(9-II-3)	56(10-II-3)
213	13	-3.64(10-II-3)	-1.43(9-II-2)	-0.39(10-I-3)	-112(9-I-2)	541(9-II-3)	-60(10-I-3)
213	14	-2.38(10-II-3)	-0.65(9-II-2)	-0.41(10-I-3)	-300(10-II-3)	-40(9-I-2)	67(10-II-3)
213	15	-1.35(10-II-3)	-0.21(9-II-2)	-0.34(10-I-3)	-364(10-II-3)	-106(10-II-3)	71(10-II-3)
213	16	-0.91(10-II-3)	-0.10(10-I-3)	-0.21(6)	-397(10-II-3)	-42(10-II-3)	45(10-II-3)
214	1	-2.25(10-I-1)	-5.31(9-II-2)	-2.52(9-II-2)	31(10-I-4)	-119(9-II-2)	155(9-II-3)
214	2	-0.40(9-I-2)	-1.06(9-II-4)	-0.57(10-I-3)	-467(9-I-2)	-205(9-II-3)	204(10-II-1)
214	3	-0.47(9-I-2)	0.92(9-I-1)	-0.69(10-I-3)	-791(9-I-1)	-259(9-I-2)	138(10-II-2)
214	4	1.82(9-II-3)	3.70(9-II-3)	-2.44(10-I-3)	-1259(10-I-4)	-558(10-I-3)	-72(10-I-1)
214	5	-1.87(9-II-3)	-1.00(9-II-2)	-1.48(9-II-2)	24(9-I-1)	110(9-I-2)	-121(10-I-4)
214	6	-0.45(9-I-2)	-1.77(9-II-2)	-2.10(9-II-2)	-227(10-I-3)	-218(9-II-2)	-57(10-I-1)
214	7	0.14(9-II-2)	-0.48(9-II-2)	-1.99(9-II-3)	-456(10-I-4)	-306(9-I-1)	-132(9-II-2)
214	8	1.36(9-II-2)	-0.83(9-II-2)	-1.58(10-I-3)	-557(10-I-4)	-452(9-I-1)	-195(9-II-2)
214	9	-0.78(9-II-3)	-0.64(9-II-2)	-1.04(9-II-2)	24(10-II-2)	197(9-I-2)	-193(10-I-4)
214	10	-0.26(9-I-2)	-1.46(9-II-2)	-1.86(9-II-2)	-94(9-II-4)	-204(9-II-2)	-158(10-I-1)
214	11	-0.05(6)	-2.29(9-II-2)	-1.84(9-II-2)	-174(10-I-3)	-341(9-II-3)	-192(9-II-2)
214	12	0.50(9-II-2)	-2.99(9-II-2)	-1.04(9-II-3)	-197(10-I-4)	-376(9-I-2)	-186(9-II-2)
214	13	0.14(10-I-3)	-0.27(9-II-2)	-0.54(9-II-2)	45(9-I-1)	296(9-I-2)	-193(10-I-4)
214	14	-0.03(6)	-1.84(9-II-2)	-0.76(9-II-2)	-20(9-II-2)	-205(9-II-2)	-150(9-II-4)
214	15	-0.09(9-II-4)	-3.75(9-II-2)	-0.75(9-II-2)	-24(9-II-4)	-346(9-II-3)	-171(9-II-2)
214	16	-0.23(9-II-2)	-5.29(9-II-2)	-0.47(9-II-3)	-35(10-I-3)	-323(10-II-1)	-173(9-II-2)
215	1	1.38(6)	-1.84(9-II-4)	-1.14(9-II-2)	268(10-II-4)	-378(9-I-1)	396(10-I-4)
215	2	1.46(6)	0.53(6)	-0.53(9-II-3)	284(9-I-2)	-153(10-I-4)	249(10-I-4)
215	3	0.89(6)	0.50(6)	-0.34(9-II-3)	274(9-I-4)	-28(9-II-3)	176(10-I-4)
215	4	0.56(10-I-3)	0.35(9-II-3)	-0.29(9-II-3)	289(9-I-4)	19(9-I-4)	123(10-I-4)
215	5	-0.56(10-I-4)	-1.07(9-II-1)	-1.74(9-II-4)	-326(10-I-4)	-1086(10-I-4)	384(10-I-3)
215	6	0.46(10-II-3)	-1.07(9-II-4)	-1.37(9-II-2)	-360(10-I-4)	-477(10-I-4)	303(10-I-3)
215	7	0.56(6)	-0.59(9-II-4)	-0.75(9-II-2)	-318(10-I-4)	-169(10-I-4)	206(10-I-3)
215	8	0.37(10-II-3)	0.02(9-II-2)	-0.20(9-II-2)	-296(10-I-4)	-21(10-I-4)	166(10-I-3)
215	9	-0.17(10-I-1)	-0.48(10-II-1)	-1.17(9-II-2)	-300(10-I-4)	-1185(10-I-4)	122(9-I-2)
215	10	-0.19(9-II-2)	-0.57(10-II-1)	-1.45(9-II-2)	-369(10-I-4)	-653(10-I-4)	160(10-I-3)
215	11	-0.76(9-II-2)	-0.30(10-II-1)	-1.21(9-II-2)	-408(10-I-4)	-251(10-I-4)	153(10-I-3)
215	12	-1.43(9-II-2)	-0.09(9-II-3)	-0.49(9-II-2)	-416(10-I-4)	-44(10-I-4)	132(10-I-3)
215	13	0.43(10-II-2)	2.25(9-II-2)	-0.85(9-II-2)	-231(10-I-4)	-1350(10-I-4)	-27(10-II-2)
215	14	-0.41(9-II-2)	1.25(9-II-2)	-0.77(9-II-2)	-61(9-I-2)	-561(10-I-4)	95(10-I-2)
215	15	-1.49(9-II-2)	0.51(9-II-2)	-0.58(9-II-2)	41(9-II-2)	-173(10-I-4)	126(10-I-2)
215	16	-2.93(9-II-2)	-0.20(9-II-2)	-0.24(9-II-2)	74(9-II-2)	-6(9-I-4)	118(10-I-3)
216	1	3.02(9-II-3)	-2.02(9-II-3)	0.39(9-II-3)	387(9-II-4)	2159(9-II-4)	-448(10-I-3)
216	2	0.94(9-II-4)	-0.14(9-I-4)	0.31(9-II-4)	25(10-II-1)	574(9-II-4)	-119(9-I-2)
216	3	0.61(9-II-4)	0.12(6)	0.19(9-II-4)	-86(10-I-1)	128(10-II-3)	38(9-II-4)
216	4	0.41(9-II-4)	-0.04(9-II-2)	0.09(9-II-2)	-81(9-II-4)	-2(10-I-3)	47(9-II-4)
216	5	0.48(9-II-3)	-1.65(9-II-3)	-1.47(10-I-4)	309(10-I-4)	1826(9-II-4)	-191(10-I-2)
216	6	0.88(9-II-3)	-1.12(9-II-4)	-0.60(10-I-3)	424(10-I-4)	903(9-II-4)	-142(10-I-3)
216	7	0.54(9-II-4)	-0.45(9-II-4)	-0.13(10-I-4)	482(9-II-4)	297(9-II-4)	15(10-II-3)
216	8	0.56(9-II-4)	-0.04(6)	0.03(10-II-1)	473(9-II-4)	44(9-II-3)	44(9-II-4)
216	9	-0.49(9-I-3)	-0.74(9-II-4)	-1.69(10-I-4)	320(6)	1796(6)	135(6)
216	10	-0.47(9-I-4)	-0.75(9-II-4)	-0.98(9-II-3)	488(6)	950(9-II-4)	237(9-II-4)
216	11	-0.21(9-I-4)	-0.41(9-II-4)	-0.56(9-II-4)	599(10-I-4)	322(9-II-4)	128(9-II-3)
216	12	0.31(9-II-4)	-0.03(6)	-0.16(9-II-4)	621(10-I-4)	38(10-I-4)	74(9-II-3)
216	13	-1.20(9-I-4)	-1.69(9-II-4)	-1.04(9-II-3)	599(9-II-4)	2045(6)	522(6)
216	14	-0.80(9-I-4)	-0.83(10-I-4)	-1.12(9-II-4)	468(9-I-1)	693(9-II-4)	309(10-I-4)
216	15	-0.53(9-I-4)	-0.55(10-I-4)	-0.85(9-II-4)	427(9-I-4)	204(10-I-4)	128(10-I-4)
216	16	-0.52(9-I-1)	-0.35(9-II-2)	-0.50(9-II-4)	421(9-I-4)	21(10-I-3)	59(10-I-4)
217	1	3.52(6)	6.51(9-II-4)	1.26(6)	1363(9-II-4)	517(9-II-4)	73(9-I-4)
217	2	-2.52(9-II-4)	3.93(10-I-4)	-1.55(9-II-3)	1006(9-II-4)	328(9-II-3)	-24(9-II-4)
217	3	-2.42(9-II-4)	2.27(10-I-4)	-2.83(9-II-4)	612(9-II-3)	142(9-II-3)	35(9-I-4)
217	4	-1.39(6)	0.85(10-I-3)	-2.80(9-II-4)	293(9-II-3)	123(10-I-4)	-114(9-II-4)
217	5	2.08(6)	1.89(9-II-4)	-0.23(9-II-2)	128(10-I-3)	-182(10-I-4)	71(9-I-4)
217	6	0.79(6)	2.00(9-II-4)	0.41(6)	186(10-I-3)	128(9-II-3)	-61(9-II-4)
217	7	-1.02(9-II-4)	1.72(9-II-4)	-0.59(9-II-2)	219(10-I-3)	227(9-II-4)	-93(9-II-4)
217	8	-2.26(10-I-4)	1.32(9-II-4)	-0.97(9-II-3)	260(10-I-3)	313(9-II-4)	-284(9-II-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
217	9	1.20(6)	0.65(9-II-4)	0.28(6)	-16(9-II-4)	-304(9-II-4)	49(9-I-4)
217	10	0.90(6)	0.79(9-II-4)	0.61(6)	69(9-I-3)	-20(10-I-2)	34(9-I-4)
217	11	0.42(10-II-3)	0.49(9-II-4)	0.30(6)	120(10-I-3)	219(9-II-4)	-83(9-II-4)
217	12	-1.08(10-I-4)	0.30(9-II-4)	-0.87(9-II-2)	124(10-I-3)	313(9-II-4)	-281(9-II-4)
217	13	0.26(9-II-4)	0.59(10-I-3)	0.24(6)	-14(9-II-4)	-290(9-II-4)	58(9-I-4)
217	14	0.25(10-II-4)	1.05(6)	0.65(6)	35(9-I-4)	-83(10-I-2)	64(9-I-4)
217	15	1.52(6)	1.17(6)	1.33(6)	157(10-I-3)	97(9-II-4)	68(9-I-4)
217	16	3.54(9-II-2)	-2.40(9-II-2)	0.64(6)	875(9-II-2)	244(9-II-4)	145(10-II-3)
218	1	0.49(9-II-1)	-0.59(9-I-1)	-0.21(10-II-1)	-7(10-II-4)	-77(10-II-1)	53(9-I-1)
218	2	1.81(10-II-1)	-0.38(9-I-2)	-0.24(10-II-1)	-17(10-II-1)	-54(10-II-1)	29(10-I-4)
218	3	3.25(10-II-1)	-0.19(9-I-2)	-0.19(10-II-1)	-20(10-II-1)	-27(10-II-1)	17(10-I-4)
218	4	4.84(10-II-1)	-0.07(9-II-2)	-0.06(10-II-1)	-24(10-II-1)	-6(10-II-1)	12(10-I-4)
218	5	0.55(9-II-1)	-0.86(9-I-1)	-0.35(10-II-1)	-8(10-II-1)	-142(10-II-1)	45(10-I-4)
218	6	1.81(10-II-1)	-0.57(9-I-1)	-0.38(10-II-1)	-26(10-II-1)	-85(10-II-1)	27(10-I-4)
218	7	3.15(10-II-1)	-0.28(9-I-1)	-0.31(10-II-1)	-26(10-II-1)	-37(10-II-1)	15(10-I-4)
218	8	4.64(10-II-1)	-0.05(9-I-2)	-0.13(10-II-1)	-27(10-II-1)	-6(10-II-1)	-11(9-II-1)
218	9	0.63(10-II-1)	-1.23(10-II-1)	-0.61(10-II-1)	9(10-I-1)	-221(10-II-1)	34(10-I-4)
218	10	1.80(10-II-1)	-0.80(10-II-1)	-0.66(10-II-1)	-24(10-II-1)	-114(10-II-1)	29(10-I-4)
218	11	2.97(10-II-1)	-0.38(10-II-1)	-0.55(10-II-1)	-11(10-II-1)	-43(10-II-1)	16(10-I-4)
218	12	4.30(10-II-1)	-0.06(10-II-1)	-0.23(10-II-1)	14(10-I-1)	-6(10-II-1)	-12(9-II-1)
218	13	0.73(10-II-1)	-1.53(10-II-1)	-1.03(10-II-1)	32(10-I-1)	-293(10-II-1)	20(10-I-4)
218	14	1.78(10-II-1)	-0.97(10-II-1)	-1.08(10-II-1)	25(10-I-1)	-137(10-II-1)	42(10-I-4)
218	15	2.69(10-II-1)	-0.45(10-II-1)	-0.89(10-II-1)	53(10-I-1)	-45(10-II-1)	24(10-I-4)
218	16	3.73(10-II-1)	-0.08(10-II-1)	-0.37(10-II-1)	68(9-II-2)	-3(10-II-1)	15(10-I-4)
219	1	-0.16(10-I-1)	-1.09(10-II-1)	0.26(10-I-1)	-151(10-II-1)	-260(10-II-2)	161(10-II-2)
219	2	0.13(10-II-1)	-0.76(10-II-1)	-0.26(10-II-1)	-200(10-II-1)	-70(10-II-2)	82(10-II-2)
219	3	0.60(10-II-1)	-0.46(10-II-1)	-0.29(10-II-1)	-128(10-II-1)	-14(10-II-2)	52(10-II-2)
219	4	1.20(10-II-1)	-0.18(10-II-1)	-0.14(10-II-1)	-103(10-II-2)	-2(9-I-1)	37(10-II-2)
219	5	0.09(10-II-1)	-1.01(10-II-1)	-0.27(10-II-1)	-47(10-II-2)	-150(10-II-2)	68(10-II-2)
219	6	0.33(10-II-1)	-0.58(10-II-1)	-0.47(10-II-1)	-89(10-II-1)	-88(10-II-2)	92(10-II-2)
219	7	0.55(10-II-1)	-0.27(10-II-1)	-0.51(10-II-1)	-102(10-II-2)	-32(10-II-2)	71(10-II-2)
219	8	0.85(10-II-1)	-0.03(10-I-1)	-0.25(10-II-1)	-99(10-II-2)	-5(10-II-2)	48(10-II-2)
219	9	0.25(10-II-1)	-0.57(10-II-2)	-0.63(10-II-1)	-17(10-II-2)	-84(10-II-2)	43(10-II-2)
219	10	0.44(10-II-1)	-0.20(10-I-1)	-0.78(10-II-1)	-34(10-II-2)	-82(10-II-2)	62(10-II-2)
219	11	0.35(10-II-1)	-0.07(10-I-1)	-0.57(10-II-1)	-52(10-II-2)	-47(10-II-2)	58(10-II-2)
219	12	0.43(10-II-1)	-0.05(10-I-4)	-0.23(10-II-1)	-62(10-II-2)	-11(10-II-2)	40(10-II-2)
219	13	0.67(10-II-1)	1.37(10-II-1)	-0.93(10-II-1)	-3(9-I-1)	-55(10-II-2)	38(10-II-2)
219	14	0.06(10-II-1)	0.81(10-II-1)	-0.49(10-II-1)	-5(10-II-2)	-73(10-II-2)	42(10-II-2)
219	15	0.03(10-II-1)	0.31(10-II-1)	-0.28(10-II-1)	-12(10-II-2)	-53(10-II-2)	37(10-II-2)
219	16	0.07(10-II-1)	0.02(10-II-1)	-0.09(10-II-1)	-18(10-II-2)	-17(10-II-2)	20(10-II-2)
220	1	2.30(10-II-1)	1.18(9-I-2)	2.92(10-II-1)	-488(10-II-1)	176(9-II-2)	38(10-II-1)
220	2	-0.46(10-I-1)	1.16(10-II-1)	2.38(10-II-1)	-327(10-II-1)	159(9-II-4)	-18(10-I-1)
220	3	-1.27(10-II-1)	0.98(10-II-1)	1.87(10-II-1)	-341(10-II-1)	112(10-I-4)	36(10-II-1)
220	4	-1.60(10-II-1)	0.83(10-II-1)	1.48(10-II-1)	-332(10-II-1)	89(10-I-1)	36(9-II-1)
220	5	0.89(10-II-1)	0.83(10-II-1)	1.75(10-II-1)	-133(10-II-1)	336(10-II-1)	-20(10-II-1)
220	6	0.24(10-II-1)	1.26(10-II-1)	2.17(10-II-1)	-172(10-II-1)	245(9-II-4)	-124(10-I-4)
220	7	-0.54(9-II-3)	1.55(10-II-1)	1.89(10-II-1)	-160(10-II-1)	154(9-II-4)	-95(10-I-4)
220	8	-0.88(10-II-1)	1.68(10-II-1)	1.52(10-II-1)	-151(10-II-1)	74(9-II-4)	-66(10-I-4)
220	9	0.22(10-II-1)	0.95(10-II-1)	1.07(10-II-1)	42(10-II-1)	519(10-II-1)	-68(10-II-1)
220	10	0.12(10-II-1)	1.46(10-II-1)	1.31(10-II-1)	-24(10-I-4)	375(9-II-4)	-103(10-II-2)
220	11	-0.15(10-I-1)	1.93(10-II-1)	1.36(10-II-1)	-36(10-II-2)	241(9-II-4)	-59(10-I-4)
220	12	-0.35(10-II-1)	2.30(10-II-1)	1.19(10-II-1)	-42(10-II-1)	139(9-II-4)	-38(10-I-4)
220	13	-0.02(10-I-1)	1.45(10-II-1)	0.28(10-II-1)	44(10-II-1)	762(10-II-1)	-96(10-II-1)
220	14	-0.01(10-I-1)	1.88(10-II-1)	0.44(10-II-1)	7(10-II-4)	500(10-II-1)	-72(10-II-2)
220	15	-0.04(10-I-1)	2.47(10-II-1)	0.51(10-II-1)	8(10-II-1)	300(9-II-4)	-40(10-I-4)
220	16	-0.07(10-II-1)	3.07(10-II-1)	0.49(10-II-1)	2(9-II-1)	171(9-II-4)	-24(10-I-4)
221	1	-1.00(10-I-1)	0.37(10-II-1)	-2.24(9-II-3)	-47(10-I-4)	-315(10-II-1)	193(10-II-1)
221	2	-0.28(10-I-1)	0.64(10-II-1)	-1.14(9-II-3)	131(10-II-1)	-26(10-II-3)	272(10-II-1)
221	3	0.15(10-II-1)	0.34(10-II-1)	-0.56(9-II-3)	269(10-II-1)	72(10-II-1)	291(10-II-1)
221	4	0.21(9-II-1)	0.02(9-I-1)	-0.11(9-I-1)	275(10-II-1)	39(10-II-1)	267(10-II-1)
221	5	-2.00(10-I-1)	0.65(9-II-3)	-1.62(9-II-3)	-57(9-I-1)	-176(10-II-1)	247(10-II-1)
221	6	-1.27(10-I-1)	0.31(9-II-3)	-0.81(9-II-3)	11(6)	10(10-I-3)	440(10-II-1)
221	7	-0.55(10-I-4)	0.06(9-II-3)	-0.14(10-I-4)	49(10-II-4)	49(10-II-1)	412(10-II-1)
221	8	-0.11(10-I-4)	-0.05(9-I-2)	0.04(9-II-4)	88(10-II-1)	27(10-II-1)	335(10-II-1)
221	9	-3.37(9-II-3)	1.05(9-II-3)	-0.90(9-II-3)	-14(9-II-2)	176(10-I-3)	287(10-II-1)
221	10	-2.12(9-II-3)	0.22(9-II-3)	0.12(10-I-1)	29(10-I-4)	37(6)	423(10-II-1)
221	11	-0.74(10-I-4)	-0.13(10-II-1)	0.12(9-II-2)	-41(9-II-2)	-5(9-II-2)	426(10-II-1)
221	12	0.11(9-II-1)	-0.04(9-I-2)	0.06(9-II-2)	-58(9-II-1)	-12(9-II-2)	355(10-II-1)
221	13	-6.21(9-II-3)	-0.10(9-II-2)	1.21(10-I-4)	-149(9-II-2)	247(9-I-2)	297(10-II-1)
221	14	-1.50(9-II-3)	-0.75(9-II-2)	0.40(10-I-4)	-52(9-II-1)	78(9-I-2)	336(10-II-1)
221	15	-0.44(10-I-4)	-0.44(9-II-2)	0.08(9-II-2)	-160(9-II-1)	-23(9-II-1)	332(10-II-1)
221	16	0.22(9-II-1)	-0.16(10-II-1)	-0.10(10-II-3)	-290(9-II-1)	-35(9-II-1)	271(10-II-1)
222	1	-0.97(9-II-3)	0.11(10-II-1)	0.90(9-II-3)	-243(9-II-2)	-1079(9-II-2)	523(10-I-4)
222	2	-0.59(9-II-3)	0.19(9-I-2)	0.33(10-I-3)	-190(9-II-1)	-119(9-II-2)	219(9-I-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
222	3	-0.06(10-I-4)	0.08(9-I-2)	0.08(10-I-3)	-273(9-II-1)	24(10-I-4)	160(9-I-2)
222	4	0.84(9-II-1)	0.07(10-II-2)	-0.12(10-II-3)	-366(9-II-1)	10(10-I-4)	120(9-I-2)
222	5	-0.57(6)	-1.19(9-II-2)	0.70(10-I-4)	-392(9-II-2)	-1071(9-II-2)	348(10-I-4)
222	6	0.04(10-II-1)	-0.73(9-II-2)	0.29(10-I-4)	-473(9-II-2)	-336(9-II-2)	305(9-I-1)
222	7	0.34(10-II-1)	-0.25(9-II-1)	-0.06(9-II-2)	-480(9-II-2)	-52(9-II-2)	186(9-I-2)
222	8	0.80(9-II-1)	-0.05(6)	-0.07(9-II-4)	-451(9-II-2)	10(10-I-4)	144(9-I-2)
222	9	-0.31(6)	-1.57(9-II-2)	0.31(10-I-4)	-366(9-II-2)	-1029(9-II-2)	164(9-I-1)
222	10	0.37(10-II-2)	-0.75(9-II-1)	-0.35(9-II-2)	-506(9-II-2)	-420(9-II-2)	186(9-I-1)
222	11	0.41(10-II-1)	-0.37(9-II-1)	-0.32(9-II-2)	-501(9-II-2)	-79(9-II-3)	209(9-I-1)
222	12	0.66(9-II-1)	-0.07(7)	-0.13(9-II-4)	-443(9-II-3)	-6(10-II-1)	168(9-I-1)
222	13	1.01(9-II-3)	-0.24(10-I-2)	-0.71(9-II-2)	-575(9-II-2)	-1253(9-II-2)	-169(9-II-2)
222	14	0.36(10-II-1)	-0.56(10-I-3)	-0.59(9-II-1)	-496(9-II-3)	-316(9-II-3)	131(9-I-1)
222	15	0.30(10-II-1)	-0.46(9-II-3)	-0.47(9-II-1)	-400(10-II-2)	-50(10-II-2)	207(10-I-4)
222	16	0.36(10-II-1)	-0.23(10-I-3)	-0.27(9-II-2)	-335(10-II-2)	14(9-II-2)	189(10-I-4)

Verifica Degli Spostamenti Relativi

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Interp.	Comb.	η_{Xv}	η_{Xh}	η_{Yv}	η_{Yh}	Nodo1	Nodo2	η	η_{Amm}	Cs
		mm	mm	mm	mm			mm	mm	
0-1	(9+10)-II-3	0.01	0.00	0.01	0.00	3	2	0.01	5.60	>100
0-1	(9+10)-IV-3	0.01	0.00	0.02	0.00	4	5	0.02	5.60	>100
0-1	(9+10)-III-3	0.01	0.00	0.02	0.00	6	7	0.02	5.60	>100
0-1	(9+10)-V-3	0.04	0.00	0.02	0.00	8	9	0.04	5.60	>100
0-1	(9+10)-VII-3	0.04	0.00	0.01	0.00	10	11	0.04	5.60	>100
0-1	(9+10)-I-3	0.01	0.00	0.01	0.00	12	13	0.01	5.60	>100
0-1	(9+10)-VIII-3	0.01	0.00	0.01	0.00	14	15	0.01	5.60	>100
0-1	(9+10)-V-3	0.01	0.00	0.00	0.00	16	17	0.01	5.60	>100
0-1	(9+10)-III-3	0.01	0.00	0.00	0.00	18	19	0.01	5.60	>100
0-1	(9+10)-I-3	0.01	0.00	0.00	0.00	20	21	0.01	5.60	>100
0-1	(9+10)-I-3	0.01	0.00	0.00	0.00	22	23	0.01	5.60	>100
0-1	(9+10)-V-3	0.01	0.00	0.00	0.00	24	25	0.01	5.60	>100
0-1	(9+10)-VII-3	0.01	0.00	0.00	0.00	26	27	0.01	5.60	>100
0-1	(9+10)-V-4	0.01	0.00	0.00	0.00	28	29	0.01	5.60	>100
0-1	(9+10)-VI-4	0.01	0.00	0.00	0.00	30	31	0.01	5.60	>100
0-1	(9+10)-IV-4	0.01	0.00	0.01	0.00	32	33	0.01	5.60	>100
1-2	(9+10)-I-3	0.01	0.00	0.01	0.00	1	2058	0.01	7.75	>100
1-2	(9+10)-V-4	0.02	0.00	0.01	0.00	2	2079	0.02	7.75	>100
1-2	(9+10)-V-4	0.02	0.00	0.01	0.00	5	2077	0.02	7.75	>100
1-2	(9+10)-V-4	0.02	0.00	0.01	0.00	7	2075	0.02	7.75	>100
1-2	(9+10)-V-4	0.04	0.00	0.01	0.00	9	2073	0.04	7.75	>100
1-2	(9+10)-V-4	0.05	0.00	0.00	0.00	11	2071	0.06	7.75	>100
1-2	(9+10)-VII-3	0.07	0.00	0.01	0.00	13	2068	0.08	7.75	>100
1-2	(9+10)-IV-4	0.08	0.00	0.02	0.00	15	2066	0.08	7.75	98
1-2	(9+10)-IV-4	0.05	0.00	0.02	0.00	17	2064	0.05	7.75	>100
1-2	(9+10)-IV-4	0.04	0.00	0.05	0.00	19	2059	0.05	7.75	>100
1-2	(9+10)-VIII-4	0.03	0.00	0.00	0.00	21	2065	0.04	7.75	>100
1-2	(9+10)-VII-3	0.05	0.00	0.01	0.00	23	2067	0.05	7.75	>100
1-2	(9+10)-V-3	0.05	0.00	0.01	0.00	25	2069	0.05	7.75	>100
1-2	(9+10)-V-4	0.04	0.00	0.00	0.00	27	2072	0.05	7.75	>100
1-2	(9+10)-V-4	0.02	0.00	0.01	0.00	29	2074	0.03	7.75	>100
1-2	(9+10)-V-4	0.02	0.00	0.01	0.00	31	2076	0.02	7.75	>100
1-2	(9+10)-VI-3	0.02	0.00	0.02	0.00	33	2078	0.02	7.75	>100
1-2	(9+10)-VII-3	0.06	0.00	0.01	0.00	53	2070	0.07	7.75	>100
2-4	(9+10)-III-4	0.16	3.50	0.10	0.04	2001	4001	3.67	27.25	7.4
2-4	(9+10)-III-4	0.16	3.50	0.11	0.48	2002	4002	3.67	27.25	7.4
2-4	(9+10)-III-4	0.16	3.50	0.13	0.96	2003	4003	3.67	27.25	7.4
2-4	(9+10)-III-4	0.17	3.17	0.10	0.04	2004	4004	3.34	27.25	8.2
2-3	(9+10)-III-4	0.00	0.14	0.06	0.02	2005	3005	0.15	7.25	49
2-4	(9+10)-III-4	0.17	3.17	0.13	0.96	2006	4006	3.34	27.25	8.2
2-4	(9+10)-III-4	0.18	2.89	0.10	0.04	2007	4007	3.07	27.25	8.9
2-3	(9+10)-I-3	0.05	0.12	0.04	0.02	2008	3008	0.16	7.25	44
2-4	(9+10)-III-4	0.18	2.89	0.13	0.96	2009	4009	3.07	27.25	8.9
2-4	(9+10)-VII-3	0.19	2.88	0.10	0.03	2010	4010	3.07	27.25	8.9
2-3	(9+10)-VII-3	0.15	0.16	0.08	0.01	2011	3011	0.31	7.25	24
2-4	(9+10)-VII-3	0.19	2.88	0.13	0.95	2012	4012	3.07	27.25	8.9
2-4	(9+10)-VII-3	0.20	3.19	0.10	0.03	2013	4013	3.39	27.25	8.0
2-3	(9+10)-V-4	0.11	0.10	0.07	0.02	2014	3014	0.21	7.25	34
2-4	(9+10)-VII-3	0.20	3.19	0.13	0.95	2015	4015	3.39	27.25	8.0

Interp .	Comb.	η_{Xv}	η_{Xh}	η_{Yv}	η_{Yh}	Nodo1	Nodo2	η	η_{Amm}	Cs
2-4	(9+10)-VII-3	0.21	3.49	0.10	0.03	2016	4016	3.70	27.25	7.4
2-4	(9+10)-VII-3	0.21	3.49	0.11	0.48	2017	4017	3.70	27.25	7.4
2-4	(9+10)-VII-3	0.21	3.49	0.13	0.95	2018	4018	3.70	27.25	7.4
2-3	(9+10)-IV-4	0.00	0.00	0.08	0.03	2028	3028	0.12	7.25	63
2-3	(9+10)-VI-3	0.02	0.02	0.10	0.03	2029	3029	0.13	7.25	55
2-3	(9+10)-VIII-3	0.01	0.01	0.04	0.03	2031	3031	0.08	7.25	95
2-3	(9+10)-III-4	0.00	0.14	0.06	0.01	2032	3032	0.14	7.25	51
2-3	(9+10)-VI-3	0.00	0.02	0.09	0.03	2033	3033	0.13	7.25	56
2-3	(9+10)-IV-4	0.02	0.00	0.07	0.03	2036	3036	0.10	7.25	72
2-3	(9+10)-VIII-3	0.00	0.01	0.05	0.03	2037	3037	0.08	7.25	85
2-3	(9+10)-VI-3	0.01	0.02	0.09	0.03	2038	3038	0.12	7.25	58
2-3	(9+10)-IV-4	0.01	0.00	0.00	0.03	2042	3042	0.03	7.25	>100
2-3	(9+10)-VIII-3	0.02	0.01	0.02	0.03	2043	3043	0.05	7.25	>100
2-3	(9+10)-I-4	0.11	0.03	0.07	0.01	2044	3044	0.15	7.25	50
2-3	(9+10)-IV-4	0.01	0.00	0.02	0.03	2047	3047	0.05	7.25	>100
2-3	(9+10)-I-3	0.04	0.03	0.02	0.01	2048	3048	0.07	7.25	>100
2-3	(9+10)-I-3	0.07	0.08	0.05	0.01	2049	3049	0.15	7.25	49
2-3	(9+10)-I-4	0.15	0.03	0.05	0.00	2050	3050	0.18	7.25	40
2-3	(9+10)-IV-4	0.01	0.00	0.03	0.03	2053	3053	0.06	7.25	>100
2-3	(9+10)-V-3	0.18	0.03	0.05	0.01	2054	3054	0.21	7.25	34
2-3	(9+10)-VIII-3	0.05	0.01	0.17	0.02	2056	3056	0.19	7.25	38
2-3	(9+10)-VII-3	0.11	0.04	0.07	0.01	2057	3057	0.15	7.25	47
2-3	(9+10)-III-4	0.09	0.00	0.01	0.00	2058	3058	0.09	7.25	79
2-3	(9+10)-IV-4	0.10	0.00	0.13	0.01	2059	3059	0.13	7.25	54
2-3	(9+10)-VIII-3	0.12	0.01	0.17	0.02	2060	3060	0.19	7.25	38
2-3	(9+10)-IV-4	0.09	0.00	0.11	0.01	2064	3064	0.11	7.25	64
2-3	(9+10)-III-4	0.09	0.00	0.10	0.00	2066	3066	0.10	7.25	71
2-3	(9+10)-VII-3	0.10	0.01	0.02	0.00	2068	3068	0.11	7.25	69
2-3	(9+10)-VII-3	0.13	0.01	0.02	0.00	2069	3069	0.14	7.25	51
2-3	(9+10)-VII-3	0.12	0.01	0.02	0.00	2070	3070	0.13	7.25	58
2-3	(9+10)-V-4	0.12	0.00	0.02	0.00	2071	3071	0.12	7.25	60
2-3	(9+10)-VII-3	0.11	0.01	0.01	0.00	2072	3072	0.12	7.25	59
2-3	(9+10)-VI-4	0.10	0.01	0.02	0.00	2073	3073	0.10	7.25	71
2-3	(9+10)-VII-3	0.07	0.01	0.00	0.00	2074	3074	0.08	7.25	92
2-3	(9+10)-VI-4	0.07	0.01	0.00	0.00	2075	3075	0.08	7.25	93
2-3	(9+10)-V-4	0.05	0.01	0.02	0.00	2076	3076	0.06	7.25	>100
2-3	(9+10)-VI-4	0.07	0.01	0.01	0.00	2077	3077	0.08	7.25	89
2-3	(9+10)-VI-4	0.06	0.01	0.02	0.02	2078	3078	0.07	7.25	98
2-3	(9+10)-V-4	0.07	0.00	0.02	0.00	2079	3079	0.07	7.25	97
2-3	(9+10)-V-4	0.11	0.03	0.02	0.01	2084	3084	0.14	7.25	53
2-3	(9+10)-V-4	0.10	0.04	0.07	0.02	2085	3085	0.14	7.25	50
3-4	(9+10)-III-4	0.17	3.03	0.17	0.47	3005	4005	3.19	20.00	6.3
3-4	(9+10)-III-4	0.12	2.77	0.16	0.48	3008	4008	2.90	20.00	6.9
3-4	(9+10)-VII-3	0.01	2.72	0.01	0.48	3011	4011	2.73	20.00	7.3
3-4	(9+10)-VII-3	0.09	3.09	0.05	0.48	3014	4014	3.17	20.00	6.3
Minimo										
3-4	(9+10)-III-4	0.17	3.03	0.17	0.47	3005	4005	3.19	20.00	6.3

Verifica delle travi

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Simbologia:

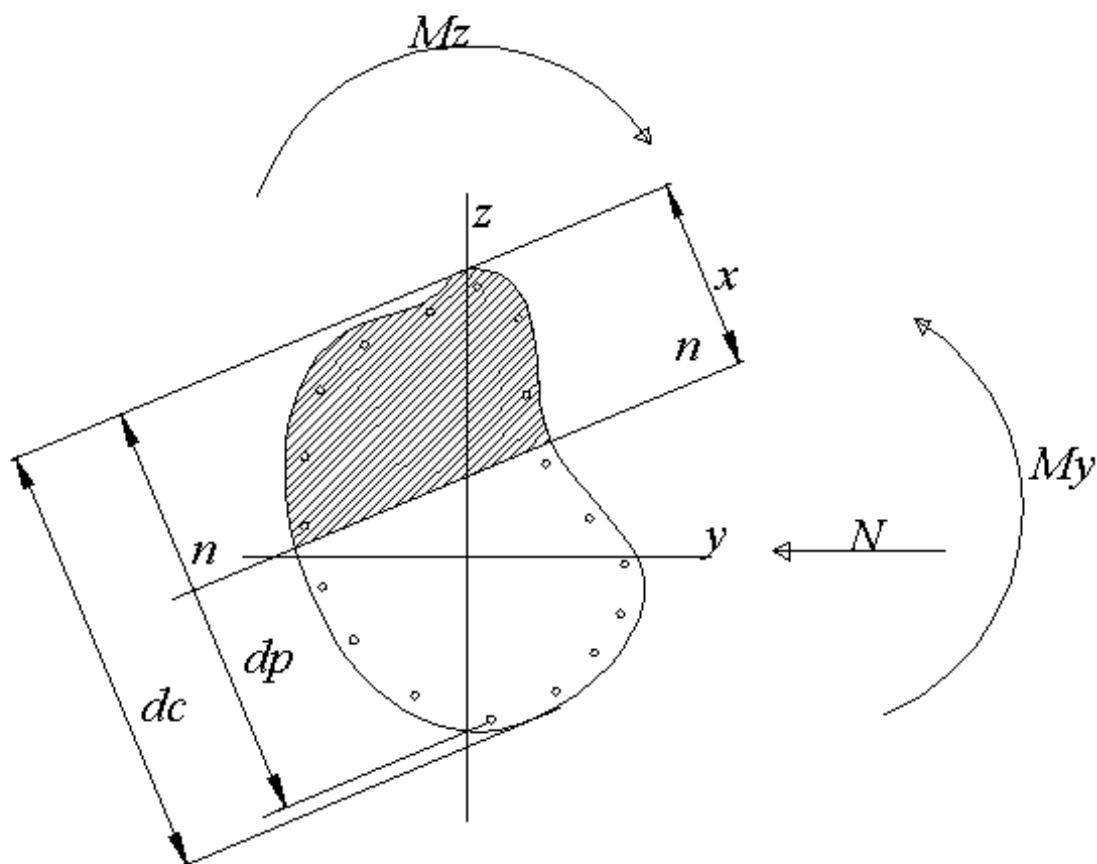
Terreno Nome della stratigrafia per travi Winkler
 L [cm] Lunghezza teorica elemento (distanza tra i nodi)
 Ln [cm] Lunghezza netta elemento (tiene conto dei concii rigidi)
 L2,L3 [cm] Lunghezze libere di inflessione
 Sez. R: Sezione Rettangolare
 By[cm]: Larghezza (asse locale y)
 Bz[cm]: Larghezza (asse locale z)
 Sez. T: Sezione a T (rovescia e non)
 Ba[cm]: Larghezza base inferiore
 Ha[cm]: Altezza inferiore
 Bs[cm]: Larghezza superiore
 Hs[cm]: Altezza superiore
 Sez. L: Sezione ad L (rovescia e non)
 Ba[cm]: Larghezza base inferiore
 Ha[cm]: Altezza inferiore

Bs[cm]:	Larghezza superiore
Hs[cm]:	Altezza superiore
Sez. C:	Sezione circolare
	R[cm]: Raggio
Sez. G:	Sezione generica
	B[cm]: Larghezza
	H[cm]: Altezza
Fatt.Ampl.Sisma	Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)
X [cm]	Punto di verifica
ILN	Inizio luce netta
CAMP	Punto di massimo momento sia superiore che inferiore ad esclusione degli estremi
FLN	Fine luce netta
M- [kg*m]	Momento negativo massimo di calcolo ⁽¹⁾
N- [kg]	Sforzo normale corrispondente ad M-
M+ [kg*m]	Momento positivo massimo di calcolo ⁽¹⁾
N+ [kg]	Sforzo normale corrispondente ad M+
ΔM- [kg*m]	Incremento di M- per la traslazione del diagramma del momento a causa del taglio
ΔM+ [kg*m]	Incremento di M+ per la traslazione del diagramma del momento a causa del taglio
Afs [cmq]	Area di ferro superiore
Afi [cmq]	Area di ferro inferiore
esc-	Deformazione nel cls per effetto di M:-N- ⁽⁴⁾
esc+	Deformazione nel cls per effetto di M+:N+ ⁽⁴⁾
esf-	Deformazione nell'acciaio per effetto di M:-N- ⁽⁴⁾
esf+	Deformazione nell'acciaio per effetto di M+:N+ ⁽⁴⁾
C-	Combinazione di carico generatore di M:-N-
C+	Combinazione di carico generatore di M+:N+
x- [cm]	Profondità asse neutro per la combinazione C- ⁽⁵⁾
d- [cm]	Altezza utile della sezione per la combinazione C- ⁽⁶⁾
x+ [cm]	Profondità asse neutro per la combinazione C+ ⁽⁵⁾
d+ [cm]	Altezza utile della sezione per la combinazione C+ ⁽⁶⁾
Mr- [kg*m]	Momento resistente superiore
Mr+ [kg*m]	Momento resistente inferiore
Stato-	Stato della sezione per la combinazione C- ⁽⁷⁾
Stato+	Stato della sezione per la combinazione C+ ⁽⁷⁾
Comb	Combinazione di carico: quando Comb non è sismica è individuata dal codice [C], quando è sismica è individuata dal codice [(Cx+Cy) Cm Sc].
- C	Individua la Combinazione di Carico non sismica (1, 2, ecc. come da scenario);
- Cx	Individua la Combinazione di Carico sismica in direzione x (SismaX, come da scenario);
- Cy	Individua la Combinazione di Carico sismica in direzione y (SismaY, come da scenario);
- Cm	Individua la Combinazione spostamento masse (I, II, III, IV, V, ecc. come da Combinazioni Sisma in Spostamento masse impalcato);
- Sc	Individua la sottocombinazione ottenuta mediante la permutazione dei segni (1, 2, 3, 4, 5, 6, 7, 8):
1)	Sc = + SismaZ*fz + SismaX*fx + SismaY*fy
2)	Sc = + SismaZ*fz + SismaX*fx - SismaY*fy
3)	Sc = + SismaZ*fz - SismaX*fx + SismaY*fy
4)	Sc = + SismaZ*fz - SismaX*fx - SismaY*fy.
5)	Sc = - SismaZ*fz + SismaX*fx + SismaY*fy
6)	Sc = - SismaZ*fz + SismaX*fx - SismaY*fy
7)	Sc = - SismaZ*fz - SismaX*fx + SismaY*fy
8)	Sc = - SismaZ*fz - SismaX*fx - SismaY*fy.
Le ultime quattro sono assenti quando non è richiesto il contributo del sisma in direzione verticale. Le combinazioni delle azioni sismiche così ottenute vengono combinate con i carichi verticali (come da scenario).	
Sez	Sezione di verifica [Sinistra/Destra]
Td [kg]	Taglio di verifica ⁽²⁾
VRdns [kg]	Resistenza a taglio in assenza di armature
VRcd [kg]	Resistenza taglio-compressione calcestruzzo
VRsd [kg]	Resistenza taglio-trazione acciaio
VRd [kg]	Resistenza a taglio =min(VRcd,VRsd)
VRd,f [kg]	Resistenza a taglio dovuta alla resistenza a trazione del calcestruzzo ad alte prestazioni (quando presente)(cfr. eq 4.2 CNR204/2006), oppure resistenza rinforzo del composito (quando presente)(cfr. eq 4.19 CNR200/2013), oppure resistenza rinforzo della camicia in acciaio (quando presente)(cfr. eq C8.7.4.5 Circolare NTC)
Mt [kg*m]	Momento torcente
Tpl [kg]	Taglio dovuto ai momenti resistenti alle estremità della trave
Mr [kg*m]	Momento resistente (ultimo) utilizzato per il calcolo di Tpl quando richiesto
Dx [cm]	Distanza dall'estremo da armare con staffe
Staffe [cmq]	Area delle staffe
cot(θ)	cot(θ) secondo il punto 4.1.2.3.5 delle Norme Tecniche
F.Par. [cmq]	Area armatura longitudinale di parete ⁽³⁾
Cs	Coefficiente di sicurezza definito dal rapporto Fr/Fd (Fr=resistenza,Fd=azione)
ζs	Livello di sicurezza sismico definito come rapporto tra l'accelerazione sopportabile e l'accelerazione di progetto, quando richiesto dal criterio di verifica
Verifiche duttilità (quando richieste):	
Zona	Sezione di verifica dell'elemento
Comb.	Combinazione di verifica
Nmax [kg]	Sforzo Normale massimo
Dir	Direzione di flessione (pilastri=Y o Z, travi =Z, pareti= ortogonale alla base)
Mry [kg*m]	Momento di snervamento corrispondente a Nmax

MrU [kg*m]	Momento ultimo (resistente) corrispondente a Nmax sulla sezione depurata del calcestruzzo non confinato, considerando il confinamento
ϕ_y [1/m]	Curvatura allo snervamento ($\phi_y = MrU / M_{ry} * \phi'_y$)
ϕ_u [1/m]	Curvatura allo corrispondente a MrU
μ	Capacità in duttilità della sezione
F.Conf	Fattore di confinamento adottato (= fck, c/fck)
μ_d	Richiesta in duttilità della sezione
Cs	Livello di sicurezza ($Cs = \mu / \mu_d$)

Note Verifica travi:

- (¹) il valore del momento di verifica è dato da $M + \Delta M$
- (²) Td è il valore di verifica a taglio esso è calcolato in funzione della somma tra taglio da carichi verticali il valore di Tpl ovvero quando la trave è tozza amplificando il taglio di calcolo dovuto al sisma per il fattore di comportamento
- (³) armatura necessaria per la sola verifica a torsione
- (⁴) le deformazioni sono stampate a meno del fattore 10^{-3}
- (⁵) distanza tra la fibra di cls compressa più lontana e l'asse neutro in direzione ortogonale all'asse neutro
- (⁶) distanza tra le fibre sollecitate più lontane dall'asse neutro: nel caso di sezione parzializzata le due fibre sono quella di cls compresso e quella dell'acciaio teso più lontane da n-n, mentre nel caso di sezione completamente compressa le due fibre sono le due di cls compresso più lontane da n-n
- (⁷) Indica lo stato della sezione se: completamente compressa (Compr.), completamente tesa (Tesa), parzializzata (Parz.)



$M_z=0$ per presso-flessione retta e z asse di simmetria
 $d = d_p$ per sezione parzializzata
 $d = d_c$ per sezione completamente compressa ($x \geq d_c$)

Schema geometrico verifica della sezione

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Trave: 301 [3071,3072], Pilastrate [--,--] Sez. R: By=70.00 cm Bz=25.00 cm L=410.00 cm Ln=410.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_e=6.952$ [(4+5)-VII-3] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3000	--	--	--	6.03	6.03	5128	5128	1	1	1.7
41.00	1339	--	861	--	6.03	6.03	5128	5128	1	1	2.3
CAMP	26	1826	681	--	6.03	6.03	5128	5128	1	1	2.8
369.00	617	-572	767	581	6.03	6.03	5128	5128	3	1	3.7
FLN	2097	--	--	--	6.03	6.03	5128	5128	3	1	2.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	5.22	18.90	0.276	--	--	--	5128	5128	1	1	Parz.	--
41.00	5.17	18.90	0.274	--	--	--	5128	5128	1	1	Parz.	--
CAMP	5.09	18.90	0.269	5.15	18.90	0.272	5128	5128	1	1	Parz.	Parz.
369.00	5.12	18.90	0.271	5.05	18.90	0.267	5128	5128	3	1	Parz.	Parz.
FLN	5.16	18.90	0.273	--	--	--	5128	5128	3	1	Parz.	--

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=1 Cen=1 Des=3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4475	--	43694	40149	40149	0	0	25.00	24.13	9.0
Cen	3627	--	43694	18743	18743	--	--	--	11.26	5.2
Des	4033	--	43694	40149	40149	0	0	25.00	24.13	10.0

Trave: 401 [4001,4002], Pilastrate [2001,2002] Sez. R: By=30.00 cm Bz=50.00 cm L=782.00 cm Ln=782.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.033$ [(4+5)-III-4] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	12738	3918	--	1052	8.04	6.03	13013	10008	(4+5)-III-4	(4+5)-III-1	1.0
78.20	7616	5585	3235	521	8.04	6.03	13013	10008	(4+5)-III-4	(4+5)-III-1	1.2
CAMP	6297	6410	3196	--	6.03	6.03	10001	10001	(4+5)-III-1	(4+5)-III-1	1.1
703.80	11357	3092	3727	1013	14.07	6.03	21944	10019	(4+5)-III-1	(4+5)-III-4	1.5
FLN	17259	647	--	1544	14.07	6.03	21944	10019	(4+5)-III-1	(4+5)-III-4	1.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	8.37	43.90	0.191	10.68	43.90	0.243	13013	10008	(4+5)-III-4	(4+5)-III-1	Parz.	Parz.
78.20	12.57	43.90	0.286	10.73	43.90	0.244	13013	10008	(4+5)-III-4	(4+5)-III-1	Parz.	Parz.
CAMP	9.45	43.90	0.215	10.97	43.90	0.250	10001	10001	(4+5)-III-1	(4+5)-III-1	Parz.	Parz.
703.80	15.92	43.90	0.363	10.09	43.90	0.230	21944	10019	(4+5)-III-1	(4+5)-III-4	Parz.	Parz.
FLN	16.04	43.90	0.365	10.03	43.90	0.229	21944	10019	(4+5)-III-1	(4+5)-III-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(4+5)-III-4 Cen=(4+5)-III-4 Des=1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7088	--	43253	38856	38856	0	0	50.00	10.05	5.5
Cen	7009	--	43253	17972	17972	--	--	--	4.65	2.6
Des	8503	--	43253	38856	38856	0	0	50.00	10.05	4.6

Trave: 401 [4002,4003], Pilastrate [2002,2003] Sez. R: By=30.00 cm Bz=50.00 cm L=678.00 cm Ln=678.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.128$ [(4+5)-III-1] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	17346	2153	--	1048	14.07	6.03	21944	10019	(4+5)-III-4	(4+5)-III-1	1.3
67.80	12219	3592	3735	588	14.07	6.03	21944	10019	(4+5)-III-4	(4+5)-III-1	1.4
CAMP	7723	5976	3275	52	8.04	6.03	13013	10008	(4+5)-III-4	(4+5)-III-4	1.2
610.20	7648	6047	3095	--	8.04	6.03	13013	10008	(4+5)-III-1	(4+5)-III-4	1.2
FLN	11897	5486	--	409	8.04	6.03	13013	10008	(4+5)-III-1	(4+5)-III-4	1.1

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X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	16.05	43.90	0.366	10.06	43.90	0.229	21944	10019	(4+5)-III-4	(4+5)-III-1	Parz.	Parz.
67.80	15.97	43.90	0.364	10.09	43.90	0.230	21944	10019	(4+5)-III-4	(4+5)-III-1	Parz.	Parz.
CAMP	12.58	43.90	0.287	10.73	43.90	0.244	13013	10008	(4+5)-III-4	(4+5)-III-4	Parz.	Parz.
610.20	12.57	43.90	0.286	10.73	43.90	0.244	13013	10008	(4+5)-III-1	(4+5)-III-4	Parz.	Parz.
FLN	12.63	43.90	0.288	10.72	43.90	0.244	13013	10008	(4+5)-III-1	(4+5)-III-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500 Comb: Sin=(4+5)-III-4 Cen=(4+5)-III-4 Des=(4+5)-III-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8029	--	43253	38856	38856	0	0	50.00	10.05	4.8
Cen	7097	--	43253	17831	17831	--	--	--	4.61	2.5
Des	6734	--	43253	38856	38856	0	0	50.00	10.05	5.8

Trave: 402 [4003,4006], Pilastrate [2003,2006] Sez. R: By=30.00 cm Bz=50.00 cm L=465.00 cm Ln=465.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.297$ [(4+5)-IV-4] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	10389	1411	--	1993	8.04	6.03	13013	10008	(4+5)-IV-4	(4+5)-IV-1	1.3
46.50	6436	3327	3953	1272	8.04	6.03	13013	10008	(4+5)-IV-4	(4+5)-IV-1	1.3
CAMP	3161	5394	3521	--	6.03	6.03	10001	10001	(4+5)-IV-4		2 1.5
418.50	6332	201	4352	1673	8.04	6.03	13013	10008	(4+5)-IV-1	(4+5)-IV-4	1.2
FLN	10684	-2113	--	2415	8.04	6.03	13013	10008	(4+5)-IV-1	(4+5)-IV-4	1.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	12.55	43.90	0.286	10.62	43.90	0.242	13013	10008	(4+5)-IV-4	(4+5)-IV-1	Parz.	Parz.
46.50	12.55	43.90	0.286	10.67	43.90	0.243	13013	10008	(4+5)-IV-4	(4+5)-IV-1	Parz.	Parz.
CAMP	10.99	43.90	0.250	10.93	43.90	0.249	10001	10001	(4+5)-IV-4	2	Parz.	Parz.
418.50	12.57	43.90	0.286	10.56	43.90	0.241	13013	10008	(4+5)-IV-1	(4+5)-IV-4	Parz.	Parz.
FLN	12.57	43.90	0.286	10.50	43.90	0.239	13013	10008	(4+5)-IV-1	(4+5)-IV-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500 Comb: Sin=2 Cen=3 Des=3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	11001	--	43253	38856	38856	0	0	50.00	10.05	3.5
Cen	7967	--	43253	17662	17662	--	--	--	4.57	2.2
Des	12831	--	43253	38856	38856	0	0	50.00	10.05	3.0

Trave: 402 [4006,4009], Pilastrate [2006,2009] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.224$ [(4+5)-IV-4] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	8548	76	--	1456	6.03	6.03	10001	10001	(4+5)-IV-4	(4+5)-IV-1	1.2
40.00	5511	1354	3037	818	6.03	6.03	10001	10001	(4+5)-IV-4	(4+5)-IV-1	1.2
CAMP	4180	2358	3651	--	6.03	6.03	10001	10001	(4+5)-IV-1	(4+5)-IV-1	1.3
360.00	7038	174	3376	1236	10.05	6.03	16013	10013	(4+5)-IV-1	(4+5)-IV-4	1.5
FLN	10414	-1442	--	1874	10.05	6.03	16013	10013	(4+5)-IV-1	(4+5)-IV-4	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	11.08	43.90	0.252	10.75	43.90	0.245	10001	10001	(4+5)-IV-4	(4+5)-IV-1	Parz.	Parz.
40.00	11.08	43.90	0.252	10.78	43.90	0.246	10001	10001	(4+5)-IV-4	(4+5)-IV-1	Parz.	Parz.
CAMP	11.04	43.90	0.252	10.79	43.90	0.246	10001	10001	(4+5)-IV-1	(4+5)-IV-1	Parz.	Parz.
360.00	13.72	43.90	0.313	10.35	43.90	0.236	16013	10013	(4+5)-IV-1	(4+5)-IV-4	Parz.	Parz.
FLN	13.72	43.90	0.313	10.32	43.90	0.235	16013	10013	(4+5)-IV-1	(4+5)-IV-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500 Comb: Sin=3 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	9804	--	43253	38856	38856	0	0	50.00	10.05	4.0
Cen	6934	--	43253	17662	17662	--	--	--	4.57	2.5

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Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
Des	11117	--	43253	38856	38856	0	0	50.00	10.05	3.5

Trave: 402 [4009,4012], Pilastrate [2009,2012] Sez. R: By=30.00 cm Bz=50.00 cm L=500.00 cm Ln=525.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.019$ [(4+5)-IV-4] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	10134	-2258	--	2801	12.06	6.03	18992	10016	(4+5)-IV-4	(4+5)-IV-1	1.9
52.50	5537	720	4324	1963	6.03	6.03	10001	10001	(4+5)-IV-4	(4+5)-IV-1	1.0
CAMP	3373	6264	3902	--	6.03	6.03	10001	10001	(4+5)-IV-1	3	1.4
472.50	6633	-831	6324	2379	8.04	6.03	13013	10008	2	(4+5)-IV-4	1.0
FLN	13356	--	--	--	10.05	6.03	16013	10013	2	1	1.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.74	43.90	0.336	10.15	43.90	0.231	18992	10016	(4+5)-IV-4	(4+5)-IV-1	Parz.	Parz.
52.50	5.96	43.90	0.136	10.80	43.90	0.246	10001	10001	(4+5)-IV-4	(4+5)-IV-1	Parz.	Parz.
CAMP	11.02	43.90	0.251	10.97	43.90	0.250	10001	10001	(4+5)-IV-1	3	Parz.	Parz.
472.50	6.51	43.90	0.148	10.55	43.90	0.240	13013	10008	2	(4+5)-IV-4	Parz.	Parz.
FLN	13.88	43.90	0.316	--	--	--	16013	10013	2	1	Parz.	--

Verifica a taglio: cot(0) Sin=2.500, cot(0) Cen=2.500, cot(0) Des=2.500 Comb: Sin=2 Cen=3 Des=3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	13084	--	43253	38856	38856	0	0	50.00	10.05	3.0
Cen	11629	--	43253	17763	17763	--	--	--	4.60	1.5
Des	13564	--	43253	38856	38856	0	0	50.00	10.05	2.9

Trave: 402 [4012,4015], Pilastrate [2012,2015] Sez. R: By=30.00 cm Bz=50.00 cm L=460.00 cm Ln=485.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.285$ [(4+5)-VIII-2] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	10812	-2202	--	2614	8.04	8.04	13013	13013	(4+5)-VIII-2	(4+5)-VIII-3	1.2
48.50	6554	378	4258	1840	8.04	8.04	13013	13013	(4+5)-VIII-2	(4+5)-VIII-3	1.2
CAMP	3056	4597	3576	--	6.03	6.03	10001	10001	(4+5)-VIII-2	3	1.5
436.50	6344	147	4203	1846	10.05	6.03	16013	10013	(4+5)-VIII-3	(4+5)-IV-4	1.5
FLN	10546	-2375	--	2558	10.05	6.03	16013	10013	(4+5)-VIII-3	(4+5)-VIII-2	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	12.29	43.90	0.280	11.85	43.90	0.270	13013	13013	(4+5)-VIII-2	(4+5)-VIII-3	Parz.	Parz.
48.50	12.29	43.90	0.280	11.92	43.90	0.272	13013	13013	(4+5)-VIII-2	(4+5)-VIII-3	Parz.	Parz.
CAMP	10.98	43.90	0.250	10.89	43.90	0.248	10001	10001	(4+5)-VIII-2	3	Parz.	Parz.
436.50	13.73	43.90	0.313	10.37	43.90	0.236	16013	10013	(4+5)-VIII-3	(4+5)-IV-4	Parz.	Parz.
FLN	13.73	43.90	0.313	10.31	43.90	0.235	16013	10013	(4+5)-VIII-3	(4+5)-VIII-2	Parz.	Parz.

Verifica a taglio: cot(0) Sin=2.500, cot(0) Cen=2.500, cot(0) Des=2.500 Comb: Sin=2 Cen=2 Des=3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	12235	--	43253	38856	38856	0	0	50.00	10.05	3.2
Cen	7365	--	43253	17662	17662	--	--	--	4.57	2.4
Des	11402	--	43253	38856	38856	0	0	50.00	10.05	3.4

Trave: 402 [4015,4018], Pilastrate [2015,2018] Sez. R: By=30.00 cm Bz=50.00 cm L=435.00 cm Ln=435.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.312$ [(4+5)-VIII-3] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	10607	-1207	--	2006	10.05	6.03	16013	10013	(4+5)-VIII-2	(4+5)-VIII-3	1.5
43.50	6598	633	4009	1312	10.05	6.03	16013	10013	(4+5)-VIII-2	(4+5)-VIII-3	1.5
CAMP	3609	4613	3545	--	6.03	6.03	10001	10001	(4+5)-VIII-3	(4+5)-VIII-2	1.4
391.50	6661	3458	3642	920	8.04	6.03	13013	10008	(4+5)-VIII-3	(4+5)-VIII-2	1.3
FLN	10303	1985	--	1593	8.04	6.03	13013	10008	(4+5)-VIII-3	(4+5)-VIII-2	1.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	13.73	43.90	0.313	10.33	43.90	0.235	16013	10013	(4+5)-VIII-2	(4+5)-VIII-3	Parz.	Parz.
43.50	13.73	43.90	0.313	10.37	43.90	0.236	16013	10013	(4+5)-VIII-2	(4+5)-VIII-3	Parz.	Parz.
CAMP	11.01	43.90	0.251	10.89	43.90	0.248	10001	10001	(4+5)-VIII-3	(4+5)-VIII-2	Parz.	Parz.
391.50	12.54	43.90	0.286	10.66	43.90	0.243	13013	10008	(4+5)-VIII-3	(4+5)-VIII-2	Parz.	Parz.
FLN	12.54	43.90	0.286	10.63	43.90	0.242	13013	10008	(4+5)-VIII-3	(4+5)-VIII-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500 Comb: Sin=2 Cen=2 Des=3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	11590	--	43253	38856	38856	0	0	50.00	10.05	3.4
Cen	7222	--	43253	17934	17934	--	--	--	4.64	2.5
Des	9838	--	43253	38856	38856	0	0	50.00	10.05	3.9

Trave: 403 [4011,4010], Pilastrate [2011,2010] Sez. R: By=50.00 cm Bz=30.00 cm L=797.00 cm Ln=767.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.080$ [(4+5)-VII-2] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5505	2788	--	--	6.03	6.03	5839	5839	(4+5)-VII-2	(4+5)-VII-3	1.1
76.70	3817	2771	592	6	6.03	6.03	5839	5839	(4+5)-VII-2	(4+5)-VII-3	1.3
CAMP	3526	2533	625	83	6.03	6.03	5839	5839	(4+5)-VII-3	(4+5)-VII-3	1.4
690.30	5308	1751	702	27	10.05	6.03	8776	5905	(4+5)-VII-3	(4+5)-VII-2	1.5
FLN	7310	1454	--	104	10.05	6.03	8776	5905	(4+5)-VII-3	(4+5)-VII-2	1.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	4.71	23.90	0.197	6.57	23.90	0.275	5839	5839	(4+5)-VII-2	(4+5)-VII-3	Parz.	Parz.
76.70	6.67	23.90	0.279	6.57	23.90	0.275	5839	5839	(4+5)-VII-2	(4+5)-VII-3	Parz.	Parz.
CAMP	6.66	23.90	0.278	6.56	23.90	0.274	5839	5839	(4+5)-VII-3	(4+5)-VII-3	Parz.	Parz.
690.30	8.12	23.90	0.340	6.47	23.90	0.271	8776	5905	(4+5)-VII-3	(4+5)-VII-2	Parz.	Parz.
FLN	8.21	23.90	0.343	6.46	23.90	0.270	8776	5905	(4+5)-VII-3	(4+5)-VII-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500 Comb: Sin=(4+5)-VII-3 Cen=(4+5)-VII-3 Des=(4+5)-VII-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2345	--	39246	36790	36790	0	0	30.00	17.48	16
Cen	2467	--	39246	16272	16272	--	--	--	7.73	6.6
Des	2755	--	39246	36790	36790	0	0	30.00	17.48	13

Trave: 403 [4012,4011], Pilastrate [2012,2011] Sez. R: By=50.00 cm Bz=30.00 cm L=663.00 cm Ln=678.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.018$ [(4+5)-VII-2] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7228	1840	--	20	8.04	6.03	7310	5877	(4+5)-VII-2	(4+5)-VII-3	1.0
67.80	5404	1889	723	--	8.04	6.03	7310	5877	(4+5)-VII-2	(4+5)-VII-3	1.2
CAMP	3753	2533	655	176	6.03	6.03	5839	5839	(4+5)-VII-2	(4+5)-VII-2	1.3
610.20	3919	2978	596	108	6.03	6.03	5839	5839	(4+5)-VII-3	(4+5)-VII-2	1.3
FLN	5420	3250	--	--	6.03	6.03	5839	5839	(4+5)-VII-3	(4+5)-VII-2	1.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	4.95	23.90	0.207	6.50	23.90	0.272	7310	5877	(4+5)-VII-2	(4+5)-VII-3	Parz.	Parz.
67.80	7.51	23.90	0.314	6.50	23.90	0.272	7310	5877	(4+5)-VII-2	(4+5)-VII-3	Parz.	Parz.
CAMP	6.67	23.90	0.279	6.56	23.90	0.275	5839	5839	(4+5)-VII-2	(4+5)-VII-2	Parz.	Parz.
610.20	6.68	23.90	0.279	6.59	23.90	0.276	5839	5839	(4+5)-VII-3	(4+5)-VII-2	Parz.	Parz.
FLN	4.89	23.90	0.205	6.60	23.90	0.276	5839	5839	(4+5)-VII-3	(4+5)-VII-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500 Comb: Sin=(4+5)-VII-3 Cen=(4+5)-VII-3 Des=(4+5)-VII-3

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Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2817	--	39246	36790	36790	0	0	30.00	17.48	13
Cen	2562	--	39246	16272	16272	--	--	--	7.73	6.4
Des	2342	--	39246	36790	36790	0	0	30.00	17.48	16

Trave: 404 [4004,4001], Pilastrate [2004,2001] Sez. R: By=30.00 cm Bz=50.00 cm L=465.00 cm Ln=465.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_E=1.551$ [(4+5)-II-2] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	10990	-2491	--	2670	10.18	7.63	16197	12404	(4+5)-II-3	(4+5)-II-2	1.5
46.50	6405	68	4584	1861	10.18	7.63	16197	12404	(4+5)-II-3	(4+5)-II-2	1.5
CAMP	3353	5533	3801	--	7.63	7.63	12403	12403	(4+5)-II-2	2	1.7
418.50	6888	2849	4273	1556	10.18	7.63	16197	12404	(4+5)-II-2	(4+5)-II-3	1.5
FLN	11161	603	--	2340	10.18	7.63	16197	12404	(4+5)-II-2	(4+5)-II-3	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	13.58	43.90	0.309	11.36	43.90	0.259	16197	12404	(4+5)-II-3	(4+5)-II-2	Parz.	Parz.
46.50	13.58	43.90	0.309	11.42	43.90	0.260	16197	12404	(4+5)-II-3	(4+5)-II-2	Parz.	Parz.
CAMP	11.92	43.90	0.272	11.85	43.90	0.270	12403	12403	(4+5)-II-2	2	Parz.	Parz.
418.50	13.59	43.90	0.310	11.51	43.90	0.262	16197	12404	(4+5)-II-2	(4+5)-II-3	Parz.	Parz.
FLN	13.59	43.90	0.310	11.46	43.90	0.261	16197	12404	(4+5)-II-2	(4+5)-II-3	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500 Comb: Sin=2 Cen=2 Des=3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	13298	--	43253	38856	38856	0	0	51.00	10.05	2.9
Cen	8186	--	43253	17662	17662	--	--	--	4.57	2.2
Des	11750	--	43253	38856	38856	0	0	51.00	10.05	3.3

Trave: 404 [4007,4004], Pilastrate [2007,2004] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_E=1.493$ [(4+5)-II-2] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	10668	-1796	--	2097	12.72	15.27	19966	23729	(4+5)-II-3	(4+5)-II-2	1.9
40.00	7118	10	3550	1401	12.72	7.63	19968	12405	(4+5)-II-3	(4+5)-II-2	1.9
CAMP	4131	2387	3820	--	7.63	7.63	12403	12403	(4+5)-II-3	2	1.6
360.00	5838	995	3267	1051	7.63	7.63	12403	12403	(4+5)-II-2	(4+5)-II-3	1.4
FLN	9105	-527	--	1747	7.63	7.63	12403	12403	(4+5)-II-2	(4+5)-II-3	1.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	13.80	43.90	0.314	14.84	43.90	0.338	19966	23729	(4+5)-II-3	(4+5)-II-2	Parz.	Parz.
40.00	14.83	43.90	0.338	11.15	43.90	0.254	19968	12405	(4+5)-II-3	(4+5)-II-2	Parz.	Parz.
CAMP	11.96	43.90	0.272	11.72	43.90	0.267	12403	12403	(4+5)-II-3	2	Parz.	Parz.
360.00	12.01	43.90	0.274	11.70	43.90	0.267	12403	12403	(4+5)-II-2	(4+5)-II-3	Parz.	Parz.
FLN	12.01	43.90	0.274	11.67	43.90	0.266	12403	12403	(4+5)-II-2	(4+5)-II-3	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500 Comb: Sin=2 Cen=2 Des=3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	11572	--	43253	38856	38856	0	0	51.00	10.05	3.4
Cen	7175	--	43253	17662	17662	--	--	--	4.57	2.5
Des	10439	--	43253	38856	38856	0	0	51.00	10.05	3.7

Trave: 404 [4010,4007], Pilastrate [2010,2007] Sez. R: By=30.00 cm Bz=50.00 cm L=500.00 cm Ln=525.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_E=1.420$ [(4+5)-II-3] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	13937	--	--	--	10.18	7.63	16197	12404		2	1.2
52.50	6897	-966	6623	2609	10.18	7.63	16197	12404		2	(4+5)-II-2 1.2

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X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
CAMP	3281	6566	4146	--	7.63	7.63	12403	12403	(4+5)-II-3	3	1.7
472.50	5963	384	4698	2248	15.27	7.63	23703	12405	(4+5)-II-2	(4+5)-II-3	2.2
FLN	10956	-2976	--	3161	15.27	7.63	23703	12405	(4+5)-II-2	(4+5)-II-3	2.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	13.73	43.90	0.313	--	--	--	16197	12404	2	1	Parz.	--
52.50	13.71	43.90	0.312	11.41	43.90	0.260	16197	12404	2	(4+5)-II-2	Parz.	Parz.
CAMP	11.93	43.90	0.272	11.89	43.90	0.271	12403	12403	(4+5)-II-3	3	Parz.	Parz.
472.50	15.93	43.90	0.363	10.96	43.90	0.250	23703	12405	(4+5)-II-2	(4+5)-II-3	Parz.	Parz.
FLN	15.94	43.90	0.363	10.89	43.90	0.248	23703	12405	(4+5)-II-2	(4+5)-II-3	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500 Comb: Sin=2 Cen=2 Des=3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	14185	--	43253	38856	38856	0	0	51.00	10.05	2.7
Cen	12176	--	43253	17763	17763	--	--	--	4.60	1.5
Des	13826	--	43253	38856	38856	0	0	51.00	10.05	2.8

Trave: 404 [4013,4010], Pilastrate [2013,2010] Sez. R: By=30.00 cm Bz=50.00 cm L=460.00 cm Ln=485.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, ζ_e=1.588 [(4+5)-VI-4] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	11281	-2836	--	2850	12.72	7.63	19968	12405	(4+5)-VI-1	(4+5)-VI-4	1.8
48.50	6734	-24	4548	2073	12.72	7.63	19968	12405	(4+5)-VI-1	(4+5)-VI-4	1.8
CAMP	3068	5164	3833	--	7.63	7.63	12403	12403	(4+5)-VI-4	3	1.8
436.50	6818	356	4578	2036	10.18	10.18	16194	16194	(4+5)-VI-4	(4+5)-VI-1	1.4
FLN	11396	-2486	--	2879	10.18	10.18	16194	16194	(4+5)-VI-4	(4+5)-VI-1	1.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.86	43.90	0.338	11.11	43.90	0.253	19968	12405	(4+5)-VI-1	(4+5)-VI-4	Parz.	Parz.
48.50	14.86	43.90	0.338	11.17	43.90	0.255	19968	12405	(4+5)-VI-1	(4+5)-VI-4	Parz.	Parz.
CAMP	11.91	43.90	0.271	11.83	43.90	0.270	12403	12403	(4+5)-VI-4	3	Parz.	Parz.
436.50	13.25	43.90	0.302	12.90	43.90	0.294	16194	16194	(4+5)-VI-4	(4+5)-VI-1	Parz.	Parz.
FLN	13.25	43.90	0.302	12.82	43.90	0.292	16194	16194	(4+5)-VI-4	(4+5)-VI-1	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500 Comb: Sin=3 Cen=3 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	12504	--	43253	38856	38856	0	0	51.00	10.05	3.1
Cen	8050	--	43253	17662	17662	--	--	--	4.57	2.2
Des	13285	--	43253	38856	38856	0	0	51.00	10.05	2.9

Trave: 404 [4016,4013], Pilastrate [2016,2013] Sez. R: By=30.00 cm Bz=50.00 cm L=435.00 cm Ln=435.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, ζ_e=1.572 [(4+5)-VI-1] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	11034	1351	--	1898	10.18	7.63	16197	12404	(4+5)-VI-1	(4+5)-VI-4	1.5
43.50	7110	3099	3924	1165	10.18	7.63	16197	12404	(4+5)-VI-1	(4+5)-VI-4	1.5
CAMP	3829	4643	3813	--	7.63	7.63	12403	12403	(4+5)-VI-1	(4+5)-VI-4	1.6
391.50	6722	480	4227	1481	12.72	7.63	19968	12405	(4+5)-VI-4	(4+5)-VI-1	1.8
FLN	10949	-1571	--	2238	12.72	7.63	19968	12405	(4+5)-VI-4	(4+5)-VI-1	1.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	13.59	43.90	0.309	11.47	43.90	0.261	16197	12404	(4+5)-VI-1	(4+5)-VI-4	Parz.	Parz.
43.50	13.59	43.90	0.309	11.51	43.90	0.262	16197	12404	(4+5)-VI-1	(4+5)-VI-4	Parz.	Parz.
CAMP	11.94	43.90	0.272	11.81	43.90	0.269	12403	12403	(4+5)-VI-1	(4+5)-VI-4	Parz.	Parz.
391.50	14.84	43.90	0.338	11.17	43.90	0.254	19968	12405	(4+5)-VI-4	(4+5)-VI-1	Parz.	Parz.
FLN	14.84	43.90	0.338	11.13	43.90	0.254	19968	12405	(4+5)-VI-4	(4+5)-VI-1	Parz.	Parz.

Verifica a taglio: cot(0) Sin=2.500,cot(0) Cen=2.500,cot(0) Des=2.500 Comb: Sin=3 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10862	--	43253	38856	38856	0	0	51.00	10.05	3.6
Cen	7783	--	43253	17934	17934	--	--	--	4.64	2.3
Des	12565	--	43253	38856	38856	0	0	51.00	10.05	3.1

Trave: 405 [4005,4004], Pilastrate [2005,2004] Sez. R: By=50.00 cm Bz=30.00 cm L=797.00 cm Ln=767.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_E=1.029$ [(4+5)-III-4] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6032	2896	--	1	12.06	6.03	10234	5925	(4+5)-III-1	(4+5)-III-4	1.7
76.70	4223	2900	634	--	6.03	6.03	5839	5839	(4+5)-III-1	(4+5)-III-4	1.2
CAMP	3256	2682	618	76	6.03	6.03	5839	5839	(4+5)-III-4	(4+5)-III-4	1.5
690.30	5017	2301	695	--	6.03	6.03	5839	5839	(4+5)-III-4	(4+5)-III-1	1.0
FLN	7000	2124	--	62	8.04	6.03	7310	5877	(4+5)-III-4	(4+5)-III-1	1.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	8.66	23.90	0.362	6.52	23.90	0.273	10234	5925	(4+5)-III-1	(4+5)-III-4	Parz.	Parz.
76.70	6.70	23.90	0.280	6.58	23.90	0.275	5839	5839	(4+5)-III-1	(4+5)-III-4	Parz.	Parz.
CAMP	6.64	23.90	0.278	6.57	23.90	0.275	5839	5839	(4+5)-III-4	(4+5)-III-4	Parz.	Parz.
690.30	4.50	23.90	0.188	6.54	23.90	0.274	5839	5839	(4+5)-III-4	(4+5)-III-1	Parz.	Parz.
FLN	5.44	23.90	0.228	6.51	23.90	0.273	7310	5877	(4+5)-III-4	(4+5)-III-1	Parz.	Parz.

Verifica a taglio: cot(0) Sin=2.500,cot(0) Cen=2.500,cot(0) Des=2.500 Comb: Sin=(4+5)-III-4 Cen=(4+5)-III-4 Des=(4+5)-III-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2501	--	39246	36790	36790	0	0	30.00	17.48	15
Cen	2441	--	39246	16272	16272	--	--	--	7.73	6.7
Des	2728	--	39246	36790	36790	0	0	30.00	17.48	13

Trave: 405 [4005,4006], Pilastrate [2005,2006] Sez. R: By=50.00 cm Bz=30.00 cm L=663.00 cm Ln=678.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_E=1.004$ [(4+5)-III-1] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6306	3247	--	--	12.06	6.03	10234	5925	(4+5)-III-4	(4+5)-III-1	1.6
67.80	4631	3008	664	95	6.03	6.03	5839	5839	(4+5)-III-4	(4+5)-III-1	1.1
CAMP	3491	2597	642	163	6.03	6.03	5839	5839	(4+5)-III-1	(4+5)-III-1	1.4
610.20	5109	2565	710	49	6.03	6.03	5839	5839	(4+5)-III-1	(4+5)-III-4	1.0
FLN	6899	2689	--	--	8.04	6.03	7310	5877	(4+5)-III-1	(4+5)-III-4	1.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	8.68	23.90	0.363	6.53	23.90	0.273	10234	5925	(4+5)-III-4	(4+5)-III-1	Parz.	Parz.
67.80	5.28	23.90	0.221	6.59	23.90	0.276	5839	5839	(4+5)-III-4	(4+5)-III-1	Parz.	Parz.
CAMP	6.65	23.90	0.278	6.57	23.90	0.275	5839	5839	(4+5)-III-1	(4+5)-III-1	Parz.	Parz.
610.20	4.52	23.90	0.189	6.56	23.90	0.274	5839	5839	(4+5)-III-1	(4+5)-III-4	Parz.	Parz.
FLN	5.82	23.90	0.244	6.54	23.90	0.274	7310	5877	(4+5)-III-1	(4+5)-III-4	Parz.	Parz.

Verifica a taglio: cot(0) Sin=2.500,cot(0) Cen=2.500,cot(0) Des=2.500 Comb: Sin=(4+5)-III-4 Cen=(4+5)-III-4 Des=(4+5)-III-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2598	--	39246	36790	36790	0	0	30.00	17.48	14
Cen	2513	--	39246	16272	16272	--	--	--	7.73	6.5
Des	2768	--	39246	36790	36790	0	0	30.00	17.48	13

Trave: 406 [4008,4007], Pilastrate [2008,2007] Sez. R: By=50.00 cm Bz=30.00 cm L=797.00 cm Ln=767.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_E=1.025$ [(4+5)-III-4] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5660	2865	--	--	6.03	6.03	5839	5839	(4+5)-III-1	(4+5)-III-4	1.0
76.70	3939	2851	603	5	6.03	6.03	5839	5839	(4+5)-III-1	(4+5)-III-4	1.3
CAMP	3422	2617	623	82	6.03	6.03	5839	5839	(4+5)-III-4	(4+5)-III-4	1.4
690.30	5200	1891	701	15	8.04	6.03	7310	5877	(4+5)-III-4	(4+5)-III-1	1.2
FLN	7200	1627	--	93	8.04	6.03	7310	5877	(4+5)-III-4	(4+5)-III-1	1.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	4.52	23.90	0.189	6.57	23.90	0.275	5839	5839	(4+5)-III-1	(4+5)-III-4	Parz.	Parz.
76.70	6.68	23.90	0.280	6.57	23.90	0.275	5839	5839	(4+5)-III-1	(4+5)-III-4	Parz.	Parz.
CAMP	6.65	23.90	0.278	6.56	23.90	0.275	5839	5839	(4+5)-III-4	(4+5)-III-4	Parz.	Parz.
690.30	7.49	23.90	0.313	6.50	23.90	0.272	7310	5877	(4+5)-III-4	(4+5)-III-1	Parz.	Parz.
FLN	4.98	23.90	0.209	6.49	23.90	0.271	7310	5877	(4+5)-III-4	(4+5)-III-1	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500 Comb: Sin=(4+5)-III-4 Cen=(4+5)-III-4 Des=(4+5)-III-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2388	--	39246	36790	36790	0	0	30.00	17.48	15
Cen	2463	--	39246	16272	16272	--	--	--	7.73	6.6
Des	2750	--	39246	36790	36790	0	0	30.00	17.48	13

Trave: 406 [4008,4009], Pilastrate [2008,2009] Sez. R: By=50.00 cm Bz=30.00 cm L=663.00 cm Ln=678.00 cm Criterio : CLS_TraviAlte - Verifica a flessione, $\zeta_E=1.004$ [(4+5)-III-4] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5818	3267	--	--	6.03	6.03	5839	5839	(4+5)-III-4	(4+5)-III-1	1.0
67.80	4245	3005	624	104	6.03	6.03	5839	5839	(4+5)-III-4	(4+5)-III-1	1.2
CAMP	3653	2571	651	172	6.03	6.03	5839	5839	(4+5)-III-1	(4+5)-III-1	1.4
610.20	5294	2135	719	9	8.04	6.03	7310	5877	(4+5)-III-1	(4+5)-III-4	1.2
FLN	7107	2156	--	--	8.04	6.03	7310	5877	(4+5)-III-1	(4+5)-III-4	1.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	4.52	23.90	0.189	6.60	23.90	0.276	5839	5839	(4+5)-III-4	(4+5)-III-1	Parz.	Parz.
67.80	6.70	23.90	0.281	6.59	23.90	0.276	5839	5839	(4+5)-III-4	(4+5)-III-1	Parz.	Parz.
CAMP	6.67	23.90	0.279	6.57	23.90	0.275	5839	5839	(4+5)-III-1	(4+5)-III-1	Parz.	Parz.
610.20	7.50	23.90	0.314	6.51	23.90	0.272	7310	5877	(4+5)-III-1	(4+5)-III-4	Parz.	Parz.
FLN	5.15	23.90	0.216	6.51	23.90	0.272	7310	5877	(4+5)-III-1	(4+5)-III-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500 Comb: Sin=(4+5)-III-4 Cen=(4+5)-III-4 Des=(4+5)-III-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2447	--	39246	36790	36790	0	0	30.00	17.48	15
Cen	2547	--	39246	16272	16272	--	--	--	7.73	6.4
Des	2801	--	39246	36790	36790	0	0	30.00	17.48	13

Trave: 407 [4002,4005], Pilastrate [2002,2005] Sez. R: By=30.00 cm Bz=50.00 cm L=465.24 cm Ln=465.00 cm Criterio : CLS_TraviAlte - Verifica a flessione, $\zeta_E=1.480$ [(4+5)-VI-3] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	12317	--	--	--	10.18	7.63	16197	12404	3	1	1.3
46.50	5432	-1169	6886	2672	10.18	7.63	16197	12404	3	(4+5)-VI-3	1.3
CAMP	3056	6764	4368	--	7.63	7.63	12403	12403	(4+5)-VI-3	3	1.7
418.50	6102	-129	7129	2658	10.18	7.63	16197	12404	2	(4+5)-VI-2	1.2
FLN	13232	-3634	--	3664	10.18	7.63	16197	12404	2	(4+5)-VI-2	1.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	13.65	43.90	0.311	--	--	--	16197	12404	3	1	Parz.	--
46.50	13.65	43.90	0.311	11.41	43.90	0.260	16197	12404	3	(4+5)-VI-3	Parz.	Parz.
CAMP	11.93	43.90	0.272	11.90	43.90	0.271	12403	12403	(4+5)-VI-3	3	Parz.	Parz.
418.50	13.70	43.90	0.312	11.44	43.90	0.261	16197	12404	2	(4+5)-VI-2	Parz.	Parz.
FLN	13.70	43.90	0.312	11.36	43.90	0.259	16197	12404	2	(4+5)-VI-2	Parz.	Parz.

Verifica a taglio: cot(0) Sin=2.500, cot(0) Cen=2.500, cot(0) Des=2.500 Comb: Sin=3 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	15642	--	43253	38856	38856	0	0	51.00	10.05	2.5
Cen	10282	--	43253	17662	17662	--	--	--	4.57	1.7
Des	17014	--	43253	38856	38856	0	0	51.00	10.05	2.3

Trave: 407 [4005,4008], Pilastrate [2005,2008] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm Criterio : CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.301$ [(4+5)-II-1] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	11652	128	--	2064	10.18	7.63	16197	12404	(4+5)-II-4	(4+5)-II-1	1.4
40.00	7515	1933	4137	1199	10.18	7.63	16197	12404	(4+5)-II-4	(4+5)-II-1	1.4
CAMP	5050	3441	4857	--	7.63	7.63	12403	12403	(4+5)-II-1	(4+5)-II-1	1.3
360.00	8851	360	4501	1648	12.72	7.63	19968	12405	(4+5)-II-1	(4+5)-II-4	1.5
FLN	13352	-1809	--	2513	12.72	12.72	19968	19968	(4+5)-II-1	(4+5)-II-4	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	13.62	43.90	0.310	11.43	43.90	0.260	16197	12404	(4+5)-II-4	(4+5)-II-1	Parz.	Parz.
40.00	13.62	43.90	0.310	11.47	43.90	0.261	16197	12404	(4+5)-II-4	(4+5)-II-1	Parz.	Parz.
CAMP	12.05	43.90	0.274	11.76	43.90	0.268	12403	12403	(4+5)-II-1	(4+5)-II-1	Parz.	Parz.
360.00	14.96	43.90	0.341	11.17	43.90	0.254	19968	12405	(4+5)-II-1	(4+5)-II-4	Parz.	Parz.
FLN	14.22	43.90	0.324	13.78	43.90	0.314	19968	19968	(4+5)-II-1	(4+5)-II-4	Parz.	Parz.

Verifica a taglio: cot(0) Sin=2.500, cot(0) Cen=2.500, cot(0) Des=2.500 Comb: Sin=3 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	13757	--	43253	38856	38856	0	0	51.00	10.05	2.8
Cen	9450	--	43253	17662	17662	--	--	--	4.57	1.9
Des	15241	--	43253	38856	38856	0	0	51.00	10.05	2.5

Trave: 407 [4008,4011], Pilastrate [2008,2011] Sez. R: By=30.00 cm Bz=50.00 cm L=500.00 cm Ln=525.00 cm Criterio : CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.422$ [(4+5)-II-1] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	14416	-3904	--	3981	15.27	7.63	23703	12405	3	(4+5)-II-1	1.6
52.50	5781	328	8124	2845	15.27	7.63	23703	12405	3	(4+5)-II-1	1.7
CAMP	3846	8811	5103	--	7.63	7.63	12403	12403	(4+5)-II-1	3	1.4
472.50	8623	-1105	8591	3240	12.72	7.63	19968	12405	2	(4+5)-II-4	1.2
FLN	17756	--	--	--	12.72	7.63	19968	12405	2	1	1.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	16.11	43.90	0.367	10.88	43.90	0.248	23703	12405	3	(4+5)-II-1	Parz.	Parz.
52.50	16.09	43.90	0.366	10.97	43.90	0.250	23703	12405	3	(4+5)-II-1	Parz.	Parz.
CAMP	12.00	43.90	0.273	12.00	43.90	0.273	12403	12403	(4+5)-II-1	3	Parz.	Parz.
472.50	15.16	43.90	0.345	11.18	43.90	0.255	19968	12405	2	(4+5)-II-4	Parz.	Parz.
FLN	15.19	43.90	0.346	--	--	--	19968	12405	2	1	Parz.	--

Verifica a taglio: cot(0) Sin=2.500, cot(0) Cen=2.500, cot(0) Des=2.500 Comb: Sin=3 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	18349	--	43253	38856	38856	0	0	51.00	10.05	2.1
Cen	15897	--	43253	17763	17763	--	--	--	4.60	1.1
Des	18009	--	43253	38856	38856	0	0	51.00	10.05	2.2

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

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Trave: 407 [4011,4014], Pilastrate [2011,2014] Sez. R: By=30.00 cm Bz=50.00 cm L=460.00 cm Ln=485.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.206$ [(4+5)-VI-2] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	14094	-2945	--	3536	10.18	10.18	16194	16194	(4+5)-VI-2	(4+5)-VI-3	1.1
48.50	8371	546	5724	2487	10.18	10.18	16194	16194	(4+5)-VI-2	(4+5)-VI-3	1.1
CAMP	3859	6708	4853	--	7.63	7.63	12403	12403	(4+5)-VI-3	3	1.4
436.50	8609	336	5654	2544	12.72	7.63	19968	12405	(4+5)-VI-3	(4+5)-VI-2	1.4
FLN	14263	-3086	--	3468	12.72	7.63	19968	12405	(4+5)-VI-3	(4+5)-VI-2	1.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	13.37	43.90	0.305	12.83	43.90	0.292	16194	16194	(4+5)-VI-2	(4+5)-VI-3	Parz.	Parz.
48.50	13.37	43.90	0.305	12.92	43.90	0.294	16194	16194	(4+5)-VI-2	(4+5)-VI-3	Parz.	Parz.
CAMP	11.99	43.90	0.273	11.90	43.90	0.271	12403	12403	(4+5)-VI-3	3	Parz.	Parz.
436.50	15.01	43.90	0.342	11.20	43.90	0.255	19968	12405	(4+5)-VI-3	(4+5)-VI-2	Parz.	Parz.
FLN	15.01	43.90	0.342	11.12	43.90	0.253	19968	12405	(4+5)-VI-3	(4+5)-VI-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=2 Cen=3 Des=3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	16992	--	43253	38856	38856	0	0	51.00	10.05	2.3
Cen	10292	--	43253	17662	17662	--	--	--	4.57	1.7
Des	15476	--	43253	38856	38856	0	0	51.00	10.05	2.5

Trave: 407 [4014,4017], Pilastrate [2014,2017] Sez. R: By=30.00 cm Bz=50.00 cm L=435.26 cm Ln=435.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.603$ [(4+5)-VI-2] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	11803	-2208	--	3116	12.72	7.63	19968	12405	(4+5)-VI-2	(4+5)-VI-3	1.7
43.50	7322	635	4480	2175	12.72	7.63	19968	12405	(4+5)-VI-2	(4+5)-VI-3	1.7
CAMP	3671	5031	4258	--	7.63	7.63	12403	12403	(4+5)-VI-2	3	1.6
391.50	5744	-1309	5946	2327	10.18	7.63	16197	12404	3	(4+5)-VI-2	1.4
FLN	11690	--	--	--	10.18	7.63	16197	12404	3	1	1.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.88	43.90	0.339	11.14	43.90	0.254	19968	12405	(4+5)-VI-2	(4+5)-VI-3	Parz.	Parz.
43.50	14.88	43.90	0.339	11.20	43.90	0.255	19968	12405	(4+5)-VI-2	(4+5)-VI-3	Parz.	Parz.
CAMP	11.95	43.90	0.272	11.83	43.90	0.269	12403	12403	(4+5)-VI-2	3	Parz.	Parz.
391.50	13.62	43.90	0.310	11.39	43.90	0.259	16197	12404	3	(4+5)-VI-2	Parz.	Parz.
FLN	13.62	43.90	0.310	--	--	--	16197	12404	3	1	Parz.	--

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=2 Cen=3 Des=3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	15263	--	43253	38856	38856	0	0	51.00	10.05	2.5
Cen	9251	--	43253	18040	18040	--	--	--	4.67	2.0
Des	14385	--	43253	38856	38856	0	0	51.00	10.05	2.7

Trave: 408 [4014,4013], Pilastrate [2014,2013] Sez. R: By=50.00 cm Bz=30.00 cm L=797.00 cm Ln=767.00 cm Criterio :
CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.002$ [(4+5)-VII-3] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6111	2970	--	--	12.06	6.03	10234	5925	(4+5)-VII-2	(4+5)-VII-3	1.7
76.70	4295	2952	637	6	6.03	6.03	5839	5839	(4+5)-VII-2	(4+5)-VII-3	1.2
CAMP	3347	2714	625	83	6.03	6.03	5839	5839	(4+5)-VII-3	(4+5)-VII-3	1.5
690.30	5130	2293	702	--	6.03	6.03	5839	5839	(4+5)-VII-3	(4+5)-VII-2	1.0
FLN	7133	2124	--	59	8.04	6.03	7310	5877	(4+5)-VII-3	(4+5)-VII-2	1.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	8.67	23.90	0.363	6.52	23.90	0.273	10234	5925	(4+5)-VII-2	(4+5)-VII-3	Parz.	Parz.
76.70	6.71	23.90	0.281	6.58	23.90	0.275	5839	5839	(4+5)-VII-2	(4+5)-VII-3	Parz.	Parz.
CAMP	6.64	23.90	0.278	6.57	23.90	0.275	5839	5839	(4+5)-VII-3	(4+5)-VII-3	Parz.	Parz.
690.30	4.53	23.90	0.190	6.54	23.90	0.274	5839	5839	(4+5)-VII-3	(4+5)-VII-2	Parz.	Parz.
FLN	5.10	23.90	0.213	6.51	23.90	0.273	7310	5877	(4+5)-VII-3	(4+5)-VII-2	Parz.	Parz.

Verifica a taglio: cot(0) Sin=2.500, cot(0) Cen=2.500, cot(0) Des=2.500 Comb: Sin=(4+5)-VII-3 Cen=(4+5)-VII-3 Des=(4+5)-VII-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2512	--	39246	36790	36790	0	0	30.00	17.48	15
Cen	2468	--	39246	16272	16272	--	--	--	7.73	6.6
Des	2755	--	39246	36790	36790	0	0	30.00	17.48	13

Trave: 408 [4015,4014], Pilastrate [2015,2014] Sez. R: By=50.00 cm Bz=30.00 cm L=663.00 cm Ln=678.00 cm Criterio : CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.052$ [(4+5)-VII-2] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7062	2541	--	--	8.04	6.03	7310	5877	(4+5)-VII-2	(4+5)-VII-3	1.0
67.80	5238	2447	723	37	8.04	6.03	7310	5877	(4+5)-VII-2	(4+5)-VII-3	1.2
CAMP	3587	2699	655	176	6.03	6.03	5839	5839	(4+5)-VII-2	(4+5)-VII-2	1.4
610.20	4511	3143	653	108	6.03	6.03	5839	5839	(4+5)-VII-3	(4+5)-VII-2	1.1
FLN	6157	3415	--	--	12.06	6.03	10234	5925	(4+5)-VII-3	(4+5)-VII-2	1.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	5.26	23.90	0.220	6.53	23.90	0.273	7310	5877	(4+5)-VII-2	(4+5)-VII-3	Parz.	Parz.
67.80	7.50	23.90	0.314	6.53	23.90	0.273	7310	5877	(4+5)-VII-2	(4+5)-VII-3	Parz.	Parz.
CAMP	6.66	23.90	0.279	6.57	23.90	0.275	5839	5839	(4+5)-VII-2	(4+5)-VII-2	Parz.	Parz.
610.20	5.95	23.90	0.249	6.60	23.90	0.276	5839	5839	(4+5)-VII-3	(4+5)-VII-2	Parz.	Parz.
FLN	8.67	23.90	0.363	6.54	23.90	0.274	10234	5925	(4+5)-VII-3	(4+5)-VII-2	Parz.	Parz.

Verifica a taglio: cot(0) Sin=2.500, cot(0) Cen=2.500, cot(0) Des=2.500 Comb: Sin=(4+5)-VII-3 Cen=(4+5)-VII-3 Des=(4+5)-VII-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2816	--	39246	36790	36790	0	0	30.00	17.48	13
Cen	2562	--	39246	16272	16272	--	--	--	7.73	6.4
Des	2554	--	39246	36790	36790	0	0	30.00	17.48	14

Trave: 409 [4017,4016], Pilastrate [2017,2016] Sez. R: By=30.00 cm Bz=50.00 cm L=782.00 cm Ln=782.00 cm Criterio : CLS_TraviAlte - Verifica a flessione, $\zeta_e=1.027$ [(4+5)-VII-3] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	17356	695	--	1538	14.07	6.03	21944	10019	(4+5)-VII-2	(4+5)-VII-3	1.3
78.20	11435	3131	3739	1007	14.07	6.03	21944	10019	(4+5)-VII-2	(4+5)-VII-3	1.4
CAMP	6356	6465	3208	--	6.03	6.03	10001	10001	(4+5)-VII-2	(4+5)-VII-2	1.0
703.80	7652	5658	3241	509	8.04	6.03	13013	10008	(4+5)-VII-3	(4+5)-VII-2	1.2
FLN	12784	4011	--	1040	8.04	6.03	13013	10008	(4+5)-VII-3	(4+5)-VII-2	1.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	16.05	43.90	0.366	10.03	43.90	0.229	21944	10019	(4+5)-VII-2	(4+5)-VII-3	Parz.	Parz.
78.20	15.92	43.90	0.363	10.09	43.90	0.230	21944	10019	(4+5)-VII-2	(4+5)-VII-3	Parz.	Parz.
CAMP	8.50	43.90	0.194	10.98	43.90	0.250	10001	10001	(4+5)-VII-2	(4+5)-VII-2	Parz.	Parz.
703.80	12.58	43.90	0.286	10.74	43.90	0.245	13013	10008	(4+5)-VII-3	(4+5)-VII-2	Parz.	Parz.
FLN	7.93	43.90	0.181	10.69	43.90	0.243	13013	10008	(4+5)-VII-3	(4+5)-VII-2	Parz.	Parz.

Verifica a taglio: cot(0) Sin=2.500, cot(0) Cen=2.500, cot(0) Des=2.500 Comb: Sin=1 Cen=(4+5)-VII-3 Des=(4+5)-VII-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8533	--	43253	38856	38856	0	0	50.00	10.05	4.6
Cen	7033	--	43253	17972	17972	--	--	--	4.65	2.6
Des	7100	--	43253	38856	38856	0	0	50.00	10.05	5.5

Trave: 409 [4018,4017], Pilastrate [2018,2017] Sez. R: By=30.00 cm Bz=50.00 cm L=678.00 cm Ln=678.00 cm Criterio : CLS_TraviAlte - Verifica a flessione, $\zeta_E=1.124$ [(4+5)-VII-2] : **Verificato**

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	11931	5473	--	420	8.04	6.03	13013	10008	(4+5)-VII-2	(4+5)-VII-3	1.1
67.80	7669	6049	3105	--	8.04	6.03	13013	10008	(4+5)-VII-2	(4+5)-VII-3	1.2
CAMP	7617	5993	3264	41	8.04	6.03	13013	10008	(4+5)-VII-3	(4+5)-VII-3	1.2
610.20	12098	3675	3724	579	14.07	6.03	21944	10019	(4+5)-VII-3	(4+5)-VII-2	1.4
FLN	17211	2249	--	1039	14.07	6.03	21944	10019	(4+5)-VII-3	(4+5)-VII-2	1.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	12.63	43.90	0.288	10.72	43.90	0.244	13013	10008	(4+5)-VII-2	(4+5)-VII-3	Parz.	Parz.
67.80	12.57	43.90	0.286	10.73	43.90	0.244	13013	10008	(4+5)-VII-2	(4+5)-VII-3	Parz.	Parz.
CAMP	12.58	43.90	0.286	10.73	43.90	0.244	13013	10008	(4+5)-VII-3	(4+5)-VII-3	Parz.	Parz.
610.20	15.96	43.90	0.364	10.10	43.90	0.230	21944	10019	(4+5)-VII-3	(4+5)-VII-2	Parz.	Parz.
FLN	16.04	43.90	0.365	10.07	43.90	0.229	21944	10019	(4+5)-VII-3	(4+5)-VII-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500 Comb: Sin=(4+5)-VII-3 Cen=(4+5)-VII-3 Des=(4+5)-VII-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6753	--	43253	38856	38856	0	0	50.00	10.05	5.8
Cen	7075	--	43253	17831	17831	--	--	--	4.61	2.5
Des	8007	--	43253	38856	38856	0	0	50.00	10.05	4.9

Verifica dei Pilastri

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Simbologia

L [cm] Lunghezza teorica elemento (distanza tra i nodi)
Ln [cm] Lunghezza netta elemento (tiene conto dei conci rigidi)
L2,L3 [cm] Lunghezze libere di inflessione
Sez. R: Sezione Rettangolare
By[cm]: Larghezza (asse locale y)
Bz[cm]: Larghezza (asse locale z)
Sez. T: Sezione a T (rovescia e non)
Ba[cm]: Larghezza base inferiore
Ha[cm]: Altezza inferiore
Bs[cm]: Larghezza superiore
Hs[cm]: Altezza superiore
Sez. L: Sezione ad L (rovescia e non)
Ba[cm]: Larghezza base inferiore
Ha[cm]: Altezza inferiore
Bs[cm]: Larghezza superiore
Hs[cm]: Altezza superiore
Sez. C: Sezione circolare
R[cm]: Raggio
Sez. G: Sezione generica
B[cm]: Larghezza
H[cm]: Altezza
Aspigholi Area di ferro negli spigholi
Afy Area di ferro sul lato Y
Afz Area di ferro sul lato Z
Zona Punto di verifica
1/N Distanza dall'inizio della lunghezza netta
Piede Inizio lunghezza netta
Testa Fine lunghezza netta
Comb Combinazione di carico: quando Comb non è sismica è individuata dal codice [(+/-)C], quando è sismica è individuata dal codice [(+/-)(Cx+Cy) Cm Sc], (+/-) rappresenta la eventuale traslazione del diagramma del momento dovuta al taglio, come specificato nel criterio di verifica [positiva (+) o negativa (-)]
- C Individua la Combinazione di Carico non sismica (1, 2, ecc. come da scenario);
- Cx Individua la Combinazione di Carico sismica in direzione x (SismaX, come da scenario);

- Cy Individua la Combinazione di Carico sismica in direzione y (SismaY, come da scenario);
- Cm Individua la Combinazione spostamento masse (I, II, III, IV, V, ecc. come da Combinazioni Sisma in Spostamento masse impalcato);
- Sc Individua la sottocombinazione ottenuta mediante la permutazione dei segni (1, 2, 3, 4, 5, 6, 7, 8):
 - 1) $Sc = + SismaZ*fx + SismaX*fy + SismaY*fy$
 - 2) $Sc = + SismaZ*fx + SismaX*fy - SismaY*fy$
 - 3) $Sc = + SismaZ*fx - SismaX*fy + SismaY*fy$
 - 4) $Sc = + SismaZ*fx - SismaX*fy - SismaY*fy$
 - 5) $Sc = - SismaZ*fx + SismaX*fy + SismaY*fy$
 - 6) $Sc = - SismaZ*fx + SismaX*fy - SismaY*fy$
 - 7) $Sc = - SismaZ*fx - SismaX*fy + SismaY*fy$
 - 8) $Sc = - SismaZ*fx - SismaX*fy - SismaY*fy$

Le ultime quattro sono assenti quando non è richiesto il contributo del sisma in direzione verticale. Le combinazioni delle azioni sismiche così ottenute vengono combinate con i carichi verticali (come da scenario).

N [kg] Sforzo Normale
 N*y [kg] Sforzo Normale x Omega2
 N*z [kg] Sforzo Normale x Omega3
 My [kg*m] Momento flettente dir Y
 M'y [kg*m] Momento flettente dir Y x cy
 cy [kg*m] Coefficiente moltiplicativo momento flettente dir Y per verifica a carico di punta
 cz [kg*m] Coefficiente moltiplicativo momento flettente dir Z per verifica a carico di punta
 Mz [kg*m] Momento flettente dir Z
 M'z [kg*m] Momento flettente dir Z x cz
 εcmax Deformazione massima cls (1)
 εfmax Deformazione massima acciaio (1)
 εcMy Deformazione massima cls int direzione Y per pressoflessione retta (1)
 εfMy Deformazione massima acciaio int direzione Y per pressoflessione retta (1)
 εcMz Deformazione massima cls int direzione Z per pressoflessione retta (1)
 εfMz Deformazione massima acciaio int direzione Z per pressoflessione retta (1)
 ΣMrtY Somma dei momenti resistenti delle travi in direzione Y(2)
 ΣMrtZ Somma dei momenti resistenti delle travi in direzione Z(2)
 ΣMyRich. Momento resistente richiesto direzione Y per rispettare la gerarchia(2)
 ΣMzRich. Momento resistente richiesto direzione Z per rispettare la gerarchia(2)
 T [kg] Valore del taglio
 Dir[Y-Z] Direzione della componente di taglio
 VRdns [kg] Resistenza a taglio in assenza di armature
 VRdns [kg] Resistenza a taglio in assenza di armature
 VRcd [kg] Resistenza taglio-compressione calcestruzzo
 VRsd [kg] Resistenza taglio-trazione acciaio
 VRd [kg] Resistenza a taglio =min(VRcd,VRsd)
 VRd,f [kg] Resistenza a taglio dovuta alla resistenza a trazione del calcestruzzo ad alte prestazioni (quando presente)(cfr. eq 4.2 CNR204/2006), oppure resistenza rinforzo del composito (quando presente)(cfr. eq 4.19 CNR200/2013), oppure resistenza rinforzo della camicia in acciaio (quando presente)(cfr. eq C8.7.4.5 Circolare NTC)
 Ast/m [cmq] Armatura staffe
 Min.Norm. Valore minimo di norma dell' area delle staffe
 cot(θ) secondo il punto 4.1.2.3.5 delle Norme Tecniche
 Fatt.Ampl.Sisma Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)
 Cs Coefficiente di sicurezza definito dal rapporto |Fr|/|Fd| (Fr=punto sul dominio di resistenza ottenuto aumentando proporzionalmente Fd,Fd=azione), quando richiesto dal criterio di verifica
 ζs Livello di sicurezza sismico definito come rapporto tra l'accelerazione sopportabile e l'accelerazione di progetto(valore stampato quando richiesto dal criterio di verifica)

Verifiche duttilità (quando richieste):

Zona Sezione di verifica dell'elemento
 Comb. Combinazione di verifica
 Nmax [kg] Sforzo Normale massimo
 Dir Direzione di flessione (pilastri=Y o Z, travi =Z, pareti= ortogonale alla base)
 Mry [kg*m] Momento di snervamento corrispondente a Nmax
 MrU [kg*m] Momento ultimo (resistente) corrispondente a Nmax sulla sezione depurata del calcestruzzo non confinato, considerando il confinamento
 φy[1/m] Curvatura allo snervamento (φy= MrU/Mry * φ'y)
 φu[1/m] Curvatura allo corrispondente a MrU
 μ Capacità in duttilità della sezione
 F.Conf Fattore di confinamento adottato (= fck,c/fck)
 μd Richiesta in duttilità della sezione
 Cs Livello di sicurezza (Cs=μ/μd)

Note Verifica pilastri:

(1) le deformazioni sono stampate a meno del fattore 10⁻³

(2) I momenti resistenti richiesti sono quelli dovuti alla ripartizione della somma dei momenti resistenti delle travi quando nella tabella dei momenti appare '-' significa che la gerarchia in quella direzione non è applicabile a seconda che il pilastro sia al piano terra o all'ultimo piano, oppure, la combinazione corrente non è sismica, oppure, la combinazione è sismica ma la sua direzione non è nella direzione del pilastro considerata. Un valore nullo dei momenti resistenti è relativo a piede o testa di pilastri in fondazione o copertura

Pilastro: 2001 [2001,4001] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.055$ [(4+5)-III-1] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

$$v_{max}=N/(fcd \cdot A)=0.054 \leq 0.65 \quad [\text{Comb. (4+5)-VI-4(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-III-1(-)	-12189	-334	8982	17332	9496	17332	9496	1.1
Testa	(4+5)-I-3(+)	-13452	4751	7904	17560	9615	17560	9615	1.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-III-4	--	--	3002	--	41320	8814	8814	4.19	2.500	2.9
Z	(4+5)-II-2	--	--	2926	--	45452	16190	16190	4.19	2.500	5.5

Pilastro: 2002 [2002,4002] Sez. R: By=50.00 cm Bz=30.00 cm L=545.00 cm Ln=545.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.023$ [(4+5)-III-1] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 3.14	Afz = 3.14
Testa	AfSpigolo = 3.14	Afy = 3.14	Afz = 3.14

$$v_{max}=N/(fcd \cdot A)=0.079 \leq 0.65 \quad [\text{Comb. (4+5)-II-4(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-III-1(-)	-21698	-1567	22781	12589	23621	12589	23621	1.0
Testa	(4+5)-III-1(+)	-19654	1471	-19162	12412	23264	12412	23264	1.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-III-4	--	--	7696	--	46516	16190	16190	4.19	2.500	2.1
Z	(4+5)-II-4	--	--	1239	--	42355	8814	8814	4.19	2.500	7.1

Pilastro: 2003 [2003,4003] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.219$ [(4+5)-III-4] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

$$v_{max}=N/(fcd \cdot A)=0.05 \leq 0.65 \quad [\text{Comb. (4+5)-V-2(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-III-4(-)	-11316	3042	-9473	21390	11649	21390	11649	1.2
Testa	(4+5)-III-4(+)	-9272	-2459	7980	21061	11461	21061	11461	1.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-III-1	--	--	3202	--	41033	8814	8814	4.19	2.500	2.8
Z	(4+5)-IV-4	--	--	2974	--	45199	16190	16190	4.19	2.500	5.4

Pilastro: 2004 [2004,4004] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.195$ [(4+5)-I-2] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

$$v_{max}=N/(fcd \cdot A)=0.064 \leq 0.65 \quad [\text{Comb. (4+5)-III-4(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-I-2(-)	-17419	4223	8273	18267	9985	18267	9985	1.2
Testa	(4+5)-I-2(+)	-15375	-3427	-6441	17904	9795	17904	9795	1.6

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot (θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-III-4	--	--	2724	--	41760	8814	8814	4.19	2.500	3.2
Z	(4+5)-II-3	--	--	3912	--	45846	16190	16190	4.19	2.500	4.1

Pilastro: 2005 [2005,3005] Sez. R: By=30.00 cm Bz=50.00 cm L=145.00 cm Ln=145.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=2.562$ [(4+5)-II-1] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

$v_{max}=N/(fcd*A)=0.098 \leq 0.65$ [Comb. (4+5)-I-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-I-3(+)	-6960	1679	3352	20683	11247	20683	11247	3.7
Testa	(4+5)-I-3(+)	-5268	-1406	-3307	20403	11091	20403	11091	3.7

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot (θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-III-1	--	--	3439	--	42401	8814	8814	4.19	2.500	2.6
Z	(4+5)-II-1	--	--	6645	--	44806	16190	16190	4.19	2.500	2.4

Pilastro: 2005 [3005,4005] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.102$ [(4+5)-III-1] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

$v_{max}=N/(fcd*A)=0.075 \leq 0.65$ [Comb. (4+5)-II-4(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-III-1(-)	-21846	-5001	11103	22637	12608	22637	12608	1.1
Testa	(4+5)-III-1(+)	-20346	5277	-9992	22465	12472	22465	12472	1.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot (θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-III-4	--	--	5274	--	42104	8814	8814	4.19	2.500	1.7
Z	(4+5)-VI-2	--	--	6388	--	46525	16190	16190	4.19	2.500	2.5

Pilastro: 2006 [2006,4006] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.125$ [(4+5)-III-4] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

$v_{max}=N/(fcd*A)=0.06 \leq 0.65$ [Comb. (4+5)-I-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-III-4(-)	-15790	3642	-8681	17978	9833	17978	9833	1.1
Testa	(4+5)-III-4(+)	-13746	-2918	7139	17613	9642	17613	9642	1.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot (θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-III-1	--	--	2903	--	41586	8814	8814	4.19	2.500	3.0
Z	(4+5)-IV-1	--	--	4029	--	45651	16190	16190	4.19	2.500	4.0

Pilastro: 2007 [2007,4007] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.258$ [(4+5)-I-2] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
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Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
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$v_{max}=N/(fcd \cdot A)=0.068 \leq 0.65$ [Comb. (4+5)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-I-2(-)	-18261	5997	7766	18416	10064	18416	10064	1.3
Testa	(4+5)-I-2(+)	-16217	-5986	-6244	18054	9873	18054	9873	1.6

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-III-4	--	--	2581	--	41880	8814	8814	4.19	2.500	3.4
Z	(4+5)-II-3	--	--	3433	--	46113	16190	16190	4.19	2.500	4.7

Pilastro: 2008 [2008,3008] Sez. R: By=30.00 cm Bz=50.00 cm L=145.00 cm Ln=145.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=2.691$ [(4+5)-III-1] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

$v_{max}=N/(fcd \cdot A)=0.106 \leq 0.65$ [Comb. (4+5)-III-1(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-I-3(-)	-10826	1519	2999	21311	11604	21311	11604	4.8
Testa	(4+5)-III-4(+)	-9779	958	-3007	21143	11507	21143	11507	4.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-III-1	--	--	3318	--	43418	8814	8814	4.19	2.500	2.7
Z	(4+5)-II-2	--	--	5872	--	45722	16190	16190	4.19	2.500	2.8

Pilastro: 2008 [3008,4008] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.188$ [(4+5)-III-1] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

$v_{max}=N/(fcd \cdot A)=0.079 \leq 0.65$ [Comb. (4+5)-VI-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-III-1(-)	-24300	-3755	10594	22896	12829	22896	12829	1.2
Testa	(4+5)-I-2(+)	-22212	-4066	-9301	22679	12641	22679	12641	1.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-III-1	--	--	4987	--	42250	8814	8814	4.19	2.500	1.8
Z	(4+5)-II-1	--	--	5938	--	46673	16190	16190	4.19	2.500	2.7

Pilastro: 2009 [2009,4009] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.211$ [(4+5)-III-4] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

$v_{max}=N/(fcd \cdot A)=0.064 \leq 0.65$ [Comb. (4+5)-III-1(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-III-4(-)	-16483	5144	-8075	18101	9898	18101	9898	1.2
Testa	(4+5)-III-4(+)	-14439	-5197	6757	17737	9707	17737	9707	1.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
Y	(4+5)-III-1	--	--	2722	--	41768	8814	8814	4.19	2.500	3.2
Z	(4+5)-IV-1	--	--	3294	--	45922	16190	16190	4.19	2.500	4.9

Pilastro: 2010 [2010,4010] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.297$ [(4+5)-V-1] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

$v_{max}=N/(fcd*A)=0.071 \leq 0.65$ [Comb. (4+5)-VII-4(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-V-1(-)	-19748	-5164	7741	18677	10202	18677	10202	1.3
Testa	(4+5)-V-1(+)	-17704	4342	-6393	18318	10012	18318	10012	1.6

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-VII-3	--	--	2601	--	42047	8814	8814	4.19	2.500	3.4
Z	(4+5)-II-3	--	--	3347	--	46175	16190	16190	4.19	2.500	4.8

Pilastro: 2011 [2011,3011] Sez. R: By=30.00 cm Bz=50.00 cm L=145.00 cm Ln=145.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.937$ [(4+5)-VII-2] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

$v_{max}=N/(fcd*A)=0.09 \leq 0.65$ [Comb. (4+5)-VI-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-V-1(-)	-12921	882	-4873	17464	9565	17464	9565	2.3
Testa	(4+5)-V-1(+)	-19154	-882	4873	18573	10147	18573	10147	2.6

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-VII-2	--	--	4784	--	42158	26443	26443	12.57	2.500	5.5
Z	(4+5)-VI-2	--	--	6147	--	47749	47749	47749	12.57	2.458	7.8

Pilastro: 2011 [3011,4011] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.086$ [(4+5)-VII-2] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

$v_{max}=N/(fcd*A)=0.08 \leq 0.65$ [Comb. (4+5)-II-4(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-VII-2(-)	-25269	4136	9642	19631	10711	19631	10711	1.1
Testa	(4+5)-VII-2(+)	-23769	-3647	-9016	19374	10573	19374	10573	1.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-VII-2	--	--	4665	--	42370	8814	8814	4.19	2.500	1.9
Z	(4+5)-II-4	--	--	5837	--	46741	16190	16190	4.19	2.500	2.8

Pilastro: 2012 [2012,4012] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.234$ [(4+5)-VII-3] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

$v_{max}=N/(fcd*A)=0.067 \leq 0.65$ [Comb. (4+5)-V-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-VII-3 (-)	-18146	-4988	-8082	18396	10053	18396	10053	1.2
Testa	(4+5)-VII-3 (+)	-16103	4233	6827	18034	9863	18034	9863	1.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot (θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-VII-2	--	--	2736	--	41905	8814	8814	4.19	2.500	3.2
Z	(4+5)-IV-1	--	--	3274	--	45983	16190	16190	4.19	2.500	4.9

Pilastro: 2013 [2013,4013] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.172$ [(4+5)-V-1] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

$v_{max}=N/(fcd*A)=0.067 \leq 0.65$ [Comb. (4+5)-V-4 (+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-V-1 (-)	-17801	-4573	8435	18335	10021	18335	10021	1.2
Testa	(4+5)-V-1 (+)	-15757	3994	-6652	17972	9830	17972	9830	1.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot (θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-VII-3	--	--	2792	--	41858	8814	8814	4.19	2.500	3.2
Z	(4+5)-VI-4	--	--	3712	--	46074	16190	16190	4.19	2.500	4.4

Pilastro: 2014 [2014,3014] Sez. R: By=30.00 cm Bz=50.00 cm L=145.00 cm Ln=145.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.482$ [(4+5)-VII-3] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

$v_{max}=N/(fcd*A)=0.094 \leq 0.65$ [Comb. (4+5)-VI-3 (+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-VII-2 (-)	-14775	-1462	-5948	21823	11965	21823	11965	2.3
Testa	(4+5)-VII-2 (+)	-16200	1462	5948	21988	12096	21988	12096	2.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot (θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-VII-3	--	--	6025	--	42054	8814	8814	4.19	2.500	1.5
Z	(4+5)-VI-3	--	--	6133	--	47336	16190	16190	4.19	2.500	2.6

Pilastro: 2014 [3014,4014] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.078$ [(4+5)-VII-2] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

$v_{max}=N/(fcd*A)=0.074 \leq 0.65$ [Comb. (4+5)-VI-3 (-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-VII-2 (-)	-22635	4255	11527	22725	12679	22725	12679	1.1
Testa	(4+5)-VII-2 (+)	-21135	-3923	-10367	22556	12544	22556	12544	1.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot (θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-VII-3	--	--	5474	--	42135	8814	8814	4.19	2.500	1.6
Z	(4+5)-VI-3	--	--	5750	--	46488	16190	16190	4.19	2.500	2.8

Pilastro: 2015 [2015,4015] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.117$ [(4+5)-VII-3] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

$v_{max}=N/(fcd \cdot A)=0.064 \leq 0.65$ [Comb. (4+5)-VII-2(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-VII-3(-)	-16170	-4122	-8730	18046	9869	18046	9869	1.1
Testa	(4+5)-VII-3(+)	-14126	3564	7219	17681	9678	17681	9678	1.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-VII-2	--	--	2926	--	41759	8814	8814	4.19	2.500	3.0
Z	(4+5)-VIII-2	--	--	3698	--	45912	16190	16190	4.19	2.500	4.4

Pilastro: 2016 [2016,4016] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.047$ [(4+5)-VII-2] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

$v_{max}=N/(fcd \cdot A)=0.053 \leq 0.65$ [Comb. (4+5)-II-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-VII-2(-)	-11712	411	8981	17246	9452	17246	9452	1.1
Testa	(4+5)-V-4(+)	-12718	-5149	7959	17428	9546	17428	9546	1.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-VII-3	--	--	3033	--	41244	8814	8814	4.19	2.500	2.9
Z	(4+5)-VI-1	--	--	3054	--	45416	16190	16190	4.19	2.500	5.3

Pilastro: 2017 [2017,4017] Sez. R: By=50.00 cm Bz=30.00 cm L=545.00 cm Ln=545.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.000$ [(4+5)-VII-2] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 3.14	Afz = 3.14
Testa	AfSpigolo = 3.14	Afy = 3.14	Afz = 3.14

$v_{max}=N/(fcd \cdot A)=0.078 \leq 0.65$ [Comb. (4+5)-VI-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-VII-2(-)	-21095	1623	23079	12537	23516	12537	23516	1.0
Testa	(4+5)-VII-2(+)	-19052	-1670	-19296	12359	23158	12359	23158	1.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-VII-3	--	--	7775	--	46453	16190	16190	4.19	2.500	2.1
Z	(4+5)-VI-3	--	--	1304	--	42314	8814	8814	4.19	2.500	6.8

Pilastro: 2018 [2018,4018] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm Criterio: CLS_Pilastri - Verifica a presso-flessione deviata, $\zeta_e=1.227$ [(4+5)-VII-3] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

$v_{max}=N/(fcd \cdot A)=0.048 \leq 0.65$ [Comb. (4+5)-I-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(4+5)-VII-3(-)	-11020	-3046	-9430	21343	11621	21343	11621	1.2
Testa	(4+5)-VII-3(+)	-8977	2274	7873	21013	11433	21013	11433	1.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot (θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(4+5)-VII-2	--	--	3175	--	40958	8814	8814	4.19	2.500	2.8
Z	(4+5)-VIII-3	--	--	3066	--	45173	16190	16190	4.19	2.500	5.3

Verifica dei Muri in calcestruzzo

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Simbologia:

Muro	Indice del muro in verifica
Nodi	[n1-n2-n3-n4...] Indici dei nodi di attacco del muro
Pann.X	Numero di pannelli in direzione locale X del muro(per muri a pannelli)
Pann.Y	Numero di pannelli in direzione locale Y del muro(per muri a pannelli)
Pann	Numero totale di pannelli (per muri a mesh)
Spess [cm]	Spessore del muro
Criterio	Criterio di verifica adottato per la verifica
Pannello	Indice del pannello
Nx [kg]	Sforzo in direzione x locale per metro lineare (Nx=xxx*spessore)
Ny [kg]	Sforzo in direzione y locale per metro lineare (Ny=syy*spessore)
Nxy [kg]	Sforzo tagliante locale per metro lineare (Nxy=sxy*spessore)
Mx [kg*m]	Momento in direzione x locale per metro lineare
My [kg*m]	Momento in direzione y locale per metro lineare
Mxy [kg*m]	Momento torcente locale per metro lineare
Ax [mq]	Armatura totale pannello in direzione x locale ⁽¹⁾
Ay [mq]	Armatura totale pannello in direzione y locale ⁽¹⁾
εc	Deformazione nel cls ⁽²⁾
εf	Deformazione nell'acciaio ⁽²⁾
Massimi	Armature massime riscontrate nel muro
Massimo	massima sigma ideale riscontrata nel muro
σid+,σid- [N/mmq]	$(\sigma_x^2 + \sigma_y^2 - \sigma_x \sigma_y + 3 \tau_{xy}^2)^{1/2}$ Tensioni ideali ai lembi della lastra (Acciaio)
σid+,σid- [kg/cmq]	$(\sigma_x^2 + \sigma_y^2 - \sigma_x \sigma_y + 3 \tau_{xy}^2)^{1/2}$ Tensioni ideali ai lembi della lastra (Legno)
Fatt.Ampl.Sisma	Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)
Cs	Coefficiente di sicurezza definito dal rapporto Mr(N) / Md (Mr(N)=Momento resistente corrispondente allo sforzo normale N,Md=momento agente), quando richiesto dal criterio di verifica
ξs	Livello di sicurezza sismico definito come rapporto tra l'accelerazione sopportabile e l'accelerazione di progetto, quando richiesto dal criterio di verifica

Note Verifica muri:

⁽¹⁾: Le armature Ax ed Ay vanno intese come a metro lineare di pannello.

⁽²⁾:Le deformazioni sono stampate a meno del fattore 10⁻³; esse si riferiscono alla verifica considerando quali sollecitazioni di progetto Mx,d=Mx +/- |Mxy|,My,d=My +/- |Mxy| scegliendo il segno in modo tale da rendere massimo in valore assoluto il relativo momento flettente,le sollecitazioni stampate si riferiscono alle sollecitazioni in una data combinazione riferite al sistema locale del pannello

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Muro [Platea]: 1 - Nodi: [2024-2027-2003-2023]Pann=4Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=12.826$ [(4+5)-I-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	3202	1381	-2902	-192	-147	254	31.42	31.42	(4+5)-VIII-3	56
2	-122	9898	-5377	109	-918	463	31.42	31.42	3	17
3	10482	623	-5011	-1012	81	441	31.42	31.42	3	16
4	-6826	-2074	-14730	607	101	1207	31.42	31.42	(4+5)-VIII-3	15
Massimi/minimi										
1							31.42			
1								31.42		
4										15

Muro [Platea]: 2 - Nodi: [2023-2003-2002-2022]Pann=28Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=2.062$ [(4+5)-I-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	1112	17531	-4606	70	-2050	-130	31.42	31.42	(4+5)-III-4	10
2	47	13951	-5741	149	-1136	-600	31.42	31.42	(4+5)-III-4	13
3	328	-19928	-3163	64	1692	-390	31.42	31.42	(4+5)-I-2	14
4	314	-22862	-4202	46	1996	-635	31.42	31.42	2	11
5	183	-30753	-3916	34	2673	-522	31.42	31.42	3	9.9
6	169	-36548	-3378	30	3163	-388	31.42	31.42	3	9.2
7	153	-40007	-2814	28	3455	-245	31.42	31.42	3	9.0
8	93	-41165	-2171	25	3556	-102	31.42	31.42	3	9.1
9	37	-40112	-1444	21	3472	39	31.42	31.42	3	9.5
10	-23	-36807	-669	16	3200	182	31.42	31.42	3	9.6
11	-64	-31122	112	19	2727	326	31.42	31.42	3	10
12	118	-22754	783	2	2030	483	31.42	31.42	3	12
13	819	-22626	-2500	-98	1938	282	31.42	31.42	(4+5)-III-4	13
14	-371	16164	1765	98	-1937	413	31.42	31.42	(4+5)-III-1	9.4
15	2380	29912	-9179	-514	-3157	1366	31.42	31.42	(4+5)-III-4	4.3
16	-692	14176	764	-97	-1225	919	31.42	31.42	(4+5)-III-4	11
17	281	-16338	-1426	-17	1394	979	31.42	31.42	(4+5)-VII-2	12
18	411	-22517	309	-85	1953	899	31.42	31.42	3	10
19	247	-30409	-370	-44	2634	818	31.42	31.42	3	9.1
20	188	-36041	-1020	-32	3114	711	31.42	31.42	3	8.5
21	131	-39377	-1652	-22	3397	591	31.42	31.42	3	8.3
22	38	-40518	-2139	-5	3497	452	31.42	31.42	3	8.4
23	-23	-39542	-2531	10	3419	300	31.42	31.42	3	8.9
24	-29	-36377	-2942	21	3159	142	31.42	31.42	3	9.9
25	85	-30822	-3459	12	2694	-9	31.42	31.42	3	12
26	1019	-25023	-1262	-81	2105	110	31.42	31.42	(4+5)-III-4	14
27	3702	-23965	-3851	-294	2088	254	31.42	31.42	(4+5)-I-3	13
28	2798	38034	7732	-504	-3886	-1277	31.42	31.42	(4+5)-I-2	3.4
Massimi/minimi										
1							31.42			
1								31.42		
28										3.4

Muro [Platea]: 3 - Nodi: [2022-2002-2026-2021]Pann=12Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=1.779$ [(4+5)-III-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-135	19838	-4341	55	-2472	-427	31.42	31.42	(4+5)-III-4	7.4
2	903	-26542	694	-97	2254	-388	31.42	31.42	(4+5)-I-2	12
3	-58	-23283	-3172	4	2080	-698	31.42	31.42	3	11
4	-279	-32755	-2095	15	2864	-576	31.42	31.42	3	9.3
5	-246	-40527	-1088	20	3517	-449	31.42	31.42	3	8.4
6	569	-46108	32	42	4088	-242	31.42	31.42	3	7.9

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
7	3059	41686	-10324	-520	-4409	1679	31.42	31.42	(4+5)-III-4	2.8
8	-1487	16053	3715	-60	-1232	818	31.42	31.42	(4+5)-III-4	11
9	-58	-22694	2502	43	2044	670	31.42	31.42		3
10	-263	-32335	2307	62	2814	466	31.42	31.42		9.7
11	-19	-40191	2513	35	3478	247	31.42	31.42		3
12	-609	-44878	1962	24	4000	51	31.42	31.42		8.4
Massimi/minimi										
1							31.42			
1								31.42		
7										2.8

Muro [Platea]: 4 - Nodi: [2021-2026-2001-2020]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=2.856$ [(4+5)-I-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-347	-50475	938	6	4202	-112	31.42	31.42		3
2	325	-52505	1228	26	4502	-33	31.42	31.42		7.8
3	292	-52498	1759	34	4499	133	31.42	31.42		7.7
4	318	-49994	2168	34	4287	304	31.42	31.42		7.6
5	273	-44901	2543	35	3862	471	31.42	31.42		7.9
6	218	-37236	3012	36	3217	623	31.42	31.42		2
7	278	-27263	3442	44	2365	749	31.42	31.42		3
8	281	-22669	2616	65	1922	448	31.42	31.42	(4+5)-III-4	13
9	934	13260	3484	125	-1071	667	31.42	31.42	(4+5)-III-1	13
10	997	17217	4679	52	-2120	172	31.42	31.42	(4+5)-I-2	9.6
11	292	-49808	2117	-4	4133	-164	31.42	31.42		3
12	98	-51452	1880	-30	4412	-249	31.42	31.42		2
13	262	-51399	1166	-50	4406	-365	31.42	31.42		2
14	385	-48993	301	-64	4198	-468	31.42	31.42		2
15	364	-44119	-640	-60	3788	-560	31.42	31.42		2
16	292	-36738	-1459	-52	3165	-657	31.42	31.42		2
17	300	-26991	-2077	-70	2331	-748	31.42	31.42		3
18	150	-18812	514	7	1616	-931	31.42	31.42	(4+5)-V-4	11
19	-924	13169	-1602	-59	-1122	-918	31.42	31.42	(4+5)-I-2	11
20	2223	29717	8798	-498	-3182	-1373	31.42	31.42	(4+5)-I-2	4.2
Massimi/minimi										
1							31.42			
1								31.42		
20										4.2

Muro [Platea]: 5 - Nodi: [2020-2001-2025-2019]Pann=4Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=13.329$ [(4+5)-III-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-172	10496	5613	104	-998	-499	31.42	31.42		2
2	3383	1630	2993	-198	-141	-271	31.42	31.42	(4+5)-VI-1	53
3	-6865	-1477	15290	607	22	-1245	31.42	31.42	(4+5)-VI-1	14
4	10718	817	5271	-1024	97	-453	31.42	31.42		2
Massimi/minimi										
1							31.42			
1								31.42		
3										14

Muro [Platea]: 6 - Nodi: [2001-2004-2035-2025]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=3.094$ [(4+5)-II-3] : **Verificato**

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	28395	5854	16344	-3234	-1004	-2130	31.42	31.42	(4+5)-I-3	3.7
2	18643	61	2694	-2090	91	211	31.42	31.42	(4+5)-VI-1	9.4
3	12541	-2245	2457	-1020	200	-1400	31.42	31.42	(4+5)-I-3	9.5
4	15992	-386	6259	-1247	146	556	31.42	31.42	(4+5)-II-3	12
5	-12236	-176	1773	1117	48	-897	31.42	31.42	(4+5)-VI-4	14
6	-12310	-296	4738	1136	9	328	31.42	31.42	(4+5)-VI-4	19
7	-16619	-537	1611	1508	75	-702	31.42	31.42	(4+5)-VI-4	13
8	-14165	-201	4194	1346	3	474	31.42	31.42	3	16
9	-20329	-356	311	1877	90	-595	31.42	31.42	3	12
10	-20740	-176	3003	1904	-1	309	31.42	31.42	3	13
11	-23764	-187	801	2163	69	-374	31.42	31.42	3	12
12	-24379	-116	1900	2210	2	126	31.42	31.42	3	13
13	-24222	52	1519	2194	36	-178	31.42	31.42	3	13
14	-24934	-74	937	2256	10	-71	31.42	31.42	3	13
15	-21136	447	2881	1953	-4	-21	31.42	31.42	3	15
16	-22230	106	102	2029	4	-281	31.42	31.42	3	13
17	-14113	756	1708	1314	-6	217	31.42	31.42	(4+5)-I-3	18
18	-15037	1885	539	1430	14	-649	31.42	31.42	3	14
19	-15606	-639	13262	1161	81	-999	31.42	31.42	(4+5)-VI-1	13
20	2211	-2919	4323	-395	67	-617	31.42	31.42	(4+5)-I-2	25
Massimi/minimi										
1							31.42			
1								31.42		
1										3.7

Muro [Platea]: 7 - Nodi: [2004-2007-2041-2035]Pann=16Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_s=3.735$ [(4+5)-II-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	19427	2245	5303	-2222	-424	-990	31.42	31.42	(4+5)-II-3	6.7
2	9388	-509	726	-1247	55	381	31.42	31.42	(4+5)-VI-1	14
3	-13828	766	1025	1275	-32	-694	31.42	31.42	(4+5)-V-4	14
4	-18925	1726	-339	1664	-30	248	31.42	31.42	(4+5)-II-2	15
5	-18354	411	198	1697	-4	-550	31.42	31.42	3	13
6	-19041	25	3012	1750	9	249	31.42	31.42	3	15
7	-21624	288	1739	1946	1	-426	31.42	31.42	3	13
8	-22048	-30	2278	1991	15	47	31.42	31.42	3	15
9	-20914	298	2803	1884	-6	-292	31.42	31.42	3	14
10	-21413	3	1592	1932	17	-144	31.42	31.42	3	14
11	-16377	545	4336	1520	-50	-187	31.42	31.42	3	17
12	-17263	335	1041	1577	13	-342	31.42	31.42	3	15
13	-9402	2337	4930	897	-280	-396	31.42	31.42	(4+5)-VI-1	21
14	-8093	1736	1346	847	45	-685	31.42	31.42	3	18
15	13774	2311	-375	-1602	-332	439	31.42	31.42	(4+5)-VI-4	11
16	6788	-921	3845	-906	43	-716	31.42	31.42	2	15
Massimi/minimi										
1							31.42			
1								31.42		
1										6.7

Muro [Platea]: 8 - Nodi: [2007-2010-2061-2041]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_s=3.629$ [(4+5)-II-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	20066	1916	5702	-2370	-421	-1107	31.42	31.42	(4+5)-II-3	6.1
2	11983	-381	1412	-1557	41	372	31.42	31.42	(4+5)-VI-1	12
3	-11353	841	1926	1045	-27	-910	31.42	31.42	(4+5)-V-4	14
4	-16989	1450	-358	1491	-39	253	31.42	31.42	(4+5)-II-2	17
5	-15255	499	1608	1425	-24	-856	31.42	31.42	3	12
6	-16254	104	4506	1508	12	312	31.42	31.42	3	16

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
7	-19321	60	2579	1750	17	-703	31.42	31.42		12
8	-19182	-89	3649	1733	13	218	31.42	31.42		15
9	-20774	-369	2321	1868	75	-521	31.42	31.42		12
10	-21059	-174	2709	1889	4	77	31.42	31.42		15
11	-20541	-644	2112	1853	118	-284	31.42	31.42		14
12	-19452	-259	1552	1768	-1	-154	31.42	31.42		15
13	-18498	-813	1605	1689	153	-11	31.42	31.42		17
14	-18455	-515	71	1684	-6	-145	31.42	31.42		16
15	-14195	-855	1108	1363	196	302	31.42	31.42		17
16	-14445	-719	-1725	1372	-21	-242	31.42	31.42		18
17	9825	-46	2410	-684	-105	554	31.42	31.42	(4+5)-II-2	19
18	8997	2247	-1083	-656	10	-652	31.42	31.42	(4+5)-I-2	18
19	22325	1145	-5317	-2505	-287	1030	31.42	31.42	(4+5)-VI-4	5.9
20	19348	-2568	1675	-2043	54	-560	31.42	31.42	(4+5)-I-2	8.3
Massimi/minimi										
1							31.42			
1								31.42		
19										5.9

Muro [Platea]: 9 - Nodi: [2010-2013-2080-2061]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=3.193$ [(4+5)-VI-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	20044	1871	-659	-2461	-280	-514	31.42	31.42	(4+5)-II-3	7.2
2	18505	-3153	-5125	-1817	68	759	31.42	31.42	(4+5)-V-1	8.4
3	-16542	1996	-9744	1595	-300	227	31.42	31.42		16
4	-17782	2220	-1743	1666	-1	1002	31.42	31.42		11
5	-28787	849	-6222	2606	-44	158	31.42	31.42		11
6	-29885	354	-1077	2659	-10	589	31.42	31.42		9.6
7	-35351	696	-3454	3122	-27	193	31.42	31.42		9.8
8	-36157	183	-1325	3181	-3	325	31.42	31.42		9.3
9	-37149	415	-1517	3265	2	266	31.42	31.42		9.3
10	-37894	95	-1639	3324	-3	81	31.42	31.42		9.6
11	-35243	110	-266	3086	26	383	31.42	31.42		9.3
12	-35810	-43	-2217	3136	6	-122	31.42	31.42		10.0
13	-30373	63	292	2655	11	534	31.42	31.42		9.8
14	-30902	-40	-2961	2710	19	-277	31.42	31.42		11
15	-23134	259	1067	2050	-16	658	31.42	31.42		11
16	-23729	46	-3664	2107	22	-415	31.42	31.42		12
17	-20930	1747	208	1827	-162	387	31.42	31.42	(4+5)-II-3	13
18	-20465	307	-1494	1792	-2	-249	31.42	31.42	(4+5)-II-3	14
19	23878	2868	-6090	-2660	-542	1081	31.42	31.42	(4+5)-VI-4	5.5
20	14166	198	-1448	-1694	61	-295	31.42	31.42	(4+5)-II-2	11
Massimi/minimi										
1							31.42			
1								31.42		
19										5.5

Muro [Platea]: 10 - Nodi: [2013-2016-2091-2080]Pann=16Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=3.339$ [(4+5)-VI-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-9975	490	-11629	722	13	874	31.42	31.42	(4+5)-II-2	17
2	1785	-2687	-4509	-266	44	560	31.42	31.42	(4+5)-VII-2	30
3	-14515	1287	-2200	1389	-225	-115	31.42	31.42		19
4	-15731	1626	228	1484	26	396	31.42	31.42		15
5	-18073	-249	-1052	1646	48	27	31.42	31.42		17
6	-18823	-180	-159	1704	22	121	31.42	31.42		16
7	-18900	-183	-1048	1699	48	264	31.42	31.42		15
8	-18885	-228	-1486	1707	18	1	31.42	31.42		17
9	-17298	-264	-2349	1547	61	499	31.42	31.42	(4+5)-II-3	14

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
10	-16337	-103	-2528	1495	18	-137	31.42	31.42	1	18
11	-15252	104	-2278	1365	10	690	31.42	31.42	(4+5)-II-3	14
12	-15450	-244	-3798	1394	16	-117	31.42	31.42	(4+5)-II-3	19
13	-10661	1241	-1344	993	-182	797	31.42	31.42	(4+5)-II-3	15
14	-12307	1945	-1539	1117	38	-295	31.42	31.42	(4+5)-VI-1	20
15	25812	4732	-12752	-2827	-863	1746	31.42	31.42	(4+5)-V-4	4.4
16	16637	108	-1347	-1781	69	-280	31.42	31.42	(4+5)-II-2	11
Massimi/minimi										
1							31.42			
1								31.42		
15										4.4

Muro [Platea]: 11 - Nodi: [2016-2095-2094-2091]Pann=4Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=14.449$ [(4+5)-VI-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-7405	-2482	-12356	659	132	1014	31.42	31.42	(4+5)-II-2	16
2	9059	325	-3912	-901	89	348	31.42	31.42	1	19
3	129	9054	-3640	79	-818	283	31.42	31.42	(4+5)-VII-2	21
4	3100	1093	-2653	-171	-134	226	31.42	31.42	(4+5)-II-2	63
Massimi/minimi										
1							31.42			
1								31.42		
1										16

Muro [Platea]: 12 - Nodi: [2092-2096-2095-2016]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=3.101$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-483	-42935	-193	45	3607	41	31.42	31.42	1	9.3
2	-298	-43104	-854	15	3660	180	31.42	31.42	1	8.8
3	-106	-42392	-1002	-15	3602	311	31.42	31.42	1	8.6
4	-2	-40416	-915	-28	3437	422	31.42	31.42	1	8.6
5	60	-37033	-752	-38	3153	526	31.42	31.42	1	8.9
6	126	-31782	-936	-46	2721	666	31.42	31.42	2	9.3
7	407	-25738	-647	-89	2213	764	31.42	31.42	2	10
8	545	-18866	-2610	-39	1624	998	31.42	31.42	(4+5)-I-3	11
9	2047	-13816	-1559	-255	1170	950	31.42	31.42	(4+5)-III-3	13
10	2459	25748	-7015	-517	-2784	1168	31.42	31.42	(4+5)-V-1	5.1
11	-108	-42921	-190	12	3610	-10	31.42	31.42	1	9.3
12	-27	-42983	-937	30	3656	-20	31.42	31.42	1	9.2
13	89	-42279	-1667	34	3600	-64	31.42	31.42	1	9.2
14	130	-40354	-2265	36	3440	-126	31.42	31.42	1	9.3
15	133	-37018	-2830	40	3165	-194	31.42	31.42	1	9.7
16	147	-32287	-3382	45	2774	-264	31.42	31.42	1	10
17	257	-26187	-3813	55	2265	-346	31.42	31.42	1	12
18	363	-22799	-3174	70	1943	-195	31.42	31.42	(4+5)-VII-3	14
19	2248	-19434	-1794	41	1626	-383	31.42	31.42	(4+5)-VII-3	15
20	1258	13223	-3791	62	-1733	-192	31.42	31.42	(4+5)-V-1	12
Massimi/minimi										
1							31.42			
1								31.42		
10										5.1

Muro [Platea]: 13 - Nodi: [2017-2097-2096-2092]Pann=12Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=1.890$ [(4+5)-VII-3] : **Verificato**

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Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	3578	38782	9566	-608	-4044	-1520	31.42	31.42	(4+5)-VII-3	3.1
2	3064	-29303	2787	-198	2532	-721	31.42	31.42	(4+5)-V-1	9.6
3	152	-23774	1519	10	2108	-969	31.42	31.42		2 9.8
4	-377	-32570	787	46	2804	-639	31.42	31.42		1 9.2
5	-668	-37115	143	83	3203	-415	31.42	31.42		1 9.0
6	-448	-40734	-179	90	3595	-160	31.42	31.42		1 8.9
7	631	16045	3925	66	-2047	360	31.42	31.42	(4+5)-VII-3	9.2
8	644	-28257	2092	-91	2404	199	31.42	31.42	(4+5)-V-1	12
9	-15	-26999	4358	13	2372	356	31.42	31.42		1 11
10	-218	-32596	3400	27	2818	269	31.42	31.42		1 10
11	-198	-37140	2222	17	3207	211	31.42	31.42		1 9.6
12	-273	-40587	742	20	3587	95	31.42	31.42		1 9.1
Massimi/minimi										
1							31.42			
1								31.42		
1										3.1

Muro [Platea]: 14 - Nodi: [2093-2099-2098-2018]Pann=4Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=17.798$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	6550	365	2294	-627	27	-190	31.42	31.42	(4+5)-IV-4	30
2	-4403	-1615	7962	385	87	-650	31.42	31.42	(4+5)-IV-4	25
3	1408	1278	1809	-104	-111	-150	31.42	31.42	(4+5)-III-4	97
4	91	5997	2439	41	-543	-187	31.42	31.42	(4+5)-VII-4	33
Massimi/minimi										
1							31.42			
1								31.42		
2										25

Muro [Platea]: 15 - Nodi: [2018-2098-2097-2017]Pann=28Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=2.469$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	2183	16805	4792	-406	-1836	-798	31.42	31.42	(4+5)-VII-3	8.4
2	1358	-14712	-303	-207	1241	-608	31.42	31.42	(4+5)-I-1	15
3	481	-19203	763	-73	1721	-697	31.42	31.42	(4+5)-III-1	12
4	302	-24522	1362	-67	2071	-652	31.42	31.42	(4+5)-III-1	11
5	604	-32071	-141	-124	2715	-448	31.42	31.42		3 10
6	365	-36078	594	-81	3064	-419	31.42	31.42		3 9.3
7	175	-38298	1106	-49	3259	-354	31.42	31.42		3 9.1
8	36	-38845	1418	-25	3312	-259	31.42	31.42		3 9.2
9	-33	-38306	1281	-13	3271	-122	31.42	31.42		2 9.7
10	-51	-36362	749	1	3110	102	31.42	31.42		1 10
11	154	-32813	973	-22	2814	217	31.42	31.42		1 11
12	587	-26975	1890	-60	2341	289	31.42	31.42		1 12
13	3288	-25186	1595	-226	2210	38	31.42	31.42	(4+5)-VII-3	14
14	4294	31167	-4401	-622	-3173	882	31.42	31.42	(4+5)-V-1	4.7
15	660	10475	2335	70	-1230	128	31.42	31.42	(4+5)-VII-3	17
16	1069	-18800	-1860	-1	1618	390	31.42	31.42	(4+5)-VII-2	15
17	617	-23958	1531	46	2030	230	31.42	31.42	(4+5)-V-1	13
18	553	-26372	2348	71	2249	346	31.42	31.42		3 12
19	372	-32066	2380	56	2736	265	31.42	31.42		3 11
20	256	-36020	2188	46	3075	184	31.42	31.42		3 10.0
21	165	-38227	1809	39	3266	105	31.42	31.42		3 9.8
22	101	-38876	1166	36	3324	47	31.42	31.42		2 9.8
23	47	-38207	538	33	3273	-25	31.42	31.42		2 10.0
24	-15	-36262	-666	26	3113	-90	31.42	31.42		1 10
25	-18	-32732	-1310	32	2825	-173	31.42	31.42		1 11

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
26	114	-27377	-1850	26	2383	-274	31.42	31.42		12
27	1835	-18824	-1284	62	1716	-564	31.42	31.42		13
28	-179	9565	-61	114	-1238	-452	31.42	31.42	(4+5)-VII-2	14
Massimi/minimi										
1							31.42			
1								31.42		
14										4.7

Muro [Platea]: 16 - Nodi: [2027-2040-2006-2003]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=3.029$ [(4+5)-IV-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	19128	-34	-2531	-2063	93	-175	31.42	31.42	(4+5)-VIII-3	9.6
2	33492	3064	-11528	-3450	-593	1540	31.42	31.42	(4+5)-IV-1	3.7
3	17472	-417	-5988	-1380	144	-509	31.42	31.42	(4+5)-IV-1	12
4	13520	-2174	-2708	-1111	184	1340	31.42	31.42	(4+5)-III-1	9.3
5	8402	-338	-3409	-597	-20	-494	31.42	31.42	(4+5)-IV-1	22
6	-6399	-752	-2200	654	157	1044	31.42	31.42	(4+5)-VII-2	16
7	-13363	-324	-3221	1224	12	-229	31.42	31.42	(4+5)-VIII-2	19
8	-11144	-879	-1673	1071	159	784	31.42	31.42	(4+5)-VII-2	15
9	-15497	-212	-1863	1452	-4	-326	31.42	31.42		2
10	-14049	-800	-1316	1326	153	547	31.42	31.42	(4+5)-V-2	15
11	-18760	-239	-654	1726	-1	-180	31.42	31.42		2
12	-18376	-553	384	1700	110	177	31.42	31.42		3
13	-19751	-330	794	1800	14	-65	31.42	31.42		1
14	-19467	-511	927	1767	94	-109	31.42	31.42		1
15	-19320	-229	2045	1754	18	45	31.42	31.42		1
16	-18567	-49	1072	1679	40	-337	31.42	31.42		1
17	-16822	1423	1920	1534	34	290	31.42	31.42		1
18	-15897	2153	81	1452	-300	-429	31.42	31.42		1
19	-9168	383	-1129	417	29	379	31.42	31.42		1
20	-18449	-215	-9607	1444	-1	725	31.42	31.42	(4+5)-VIII-3	13
Massimi/minimi										
1							31.42			
1								31.42		
2										3.7

Muro [Platea]: 17 - Nodi: [2040-2046-2009-2006]Pann=16Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=4.079$ [(4+5)-IV-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-12296	-766	2890	862	-0	-383	31.42	31.42	(4+5)-IV-4	22
2	15227	3753	-5576	-1791	-571	946	31.42	31.42	(4+5)-IV-1	8.2
3	-19350	992	-1929	1715	-10	-122	31.42	31.42	(4+5)-VIII-2	16
4	-17471	1762	-2192	1570	-165	683	31.42	31.42	(4+5)-VI-2	13
5	-18425	-216	-2423	1630	9	83	31.42	31.42	(4+5)-VIII-2	17
6	-15748	144	-3358	1439	1	739	31.42	31.42		3
7	-15420	-404	-1514	1388	5	148	31.42	31.42	(4+5)-VIII-2	19
8	-15965	-516	-3567	1462	105	541	31.42	31.42		3
9	-14302	-614	-678	1330	0	115	31.42	31.42		1
10	-13799	-895	-2922	1290	165	266	31.42	31.42		3
11	-10966	-558	1085	1043	4	169	31.42	31.42		1
12	-10837	-725	-1144	1031	135	-159	31.42	31.42		1
13	-6251	1122	1720	657	33	352	31.42	31.42		1
14	-5443	1118	-1183	587	-186	-350	31.42	31.42		1
15	4843	3	-1344	-744	39	436	31.42	31.42		3
16	13079	1806	3647	-1499	-335	-678	31.42	31.42	(4+5)-VIII-2	10
Massimi/minimi										
1							31.42			
1								31.42		
2										8.2

Muro [Platea]: 18 - Nodi: [2046-2063-2012-2009]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=3.949$ [(4+5)-IV-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	9689	-493	-162	-1263	36	-428	31.42	31.42	(4+5)-VIII-3	14
2	18320	2983	-3068	-2117	-464	790	31.42	31.42	(4+5)-IV-1	7.5
3	-11810	2004	-1959	1133	34	-533	31.42	31.42		17
4	-12251	740	-514	1143	-34	608	31.42	31.42	(4+5)-VII-2	16
5	-17609	53	-2271	1567	30	-261	31.42	31.42		16
6	-15710	223	-906	1416	-23	634	31.42	31.42		14
7	-20422	-267	-2013	1816	21	-194	31.42	31.42		15
8	-19631	-296	-1071	1735	51	471	31.42	31.42		13
9	-22565	-260	-849	1997	12	-115	31.42	31.42		14
10	-21652	-474	-590	1913	76	260	31.42	31.42		14
11	-23382	-213	289	2065	13	-30	31.42	31.42		14
12	-23209	-366	796	2035	59	-132	31.42	31.42		14
13	-22709	-167	1305	2007	25	64	31.42	31.42		14
14	-22500	-77	994	1966	18	-306	31.42	31.42		13
15	-20400	169	2060	1808	29	177	31.42	31.42		15
16	-19668	504	437	1736	-63	-420	31.42	31.42		14
17	-14596	2104	1446	1383	39	502	31.42	31.42		15
18	-14517	976	-631	1342	-65	-360	31.42	31.42	(4+5)-III-1	17
19	6331	-602	-737	-888	52	432	31.42	31.42	(4+5)-IV-4	18
20	13888	2899	1462	-1650	-441	-572	31.42	31.42	(4+5)-VIII-2	10
Massimi/minimi										
1							31.42			
1								31.42		
2										7.5

Muro [Platea]: 19 - Nodi: [2063-2081-2015-2012]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=4.568$ [(4+5)-VIII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	4623	-588	-995	-845	53	-311	31.42	31.42	(4+5)-VIII-3	21
2	12212	2200	-5025	-1609	-411	918	31.42	31.42	(4+5)-IV-1	9.1
3	-10696	1516	-2441	990	44	-507	31.42	31.42		18
4	-10391	372	-1178	954	14	639	31.42	31.42	(4+5)-VII-2	17
5	-16477	-272	-2407	1485	15	-319	31.42	31.42		16
6	-15482	-318	320	1413	74	533	31.42	31.42		15
7	-20726	-257	-1299	1847	11	-247	31.42	31.42		14
8	-20289	-487	361	1819	91	335	31.42	31.42		14
9	-23499	-156	-335	2081	3	-149	31.42	31.42		13
10	-21795	-450	74	1956	92	221	31.42	31.42		14
11	-24354	-25	459	2148	5	-32	31.42	31.42		14
12	-24307	-122	417	2147	37	-68	31.42	31.42		14
13	-22942	-206	1198	2023	16	73	31.42	31.42		14
14	-23133	-164	-244	2033	41	-182	31.42	31.42		14
15	-19563	186	2050	1766	3	187	31.42	31.42		15
16	-18051	-410	1088	1646	152	-512	31.42	31.42	(4+5)-I-1	13
17	-18909	-112	865	1680	-10	178	31.42	31.42	(4+5)-IV-1	16
18	-17999	952	-328	1594	-45	-394	31.42	31.42	(4+5)-II-1	15
19	8256	269	603	-1009	63	256	31.42	31.42	(4+5)-IV-4	19
20	15198	3244	4207	-1741	-531	-766	31.42	31.42	(4+5)-VIII-2	8.9
Massimi/minimi										
1							31.42			
1								31.42		
20										8.9

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Muro [Platea]: 20 - Nodi: [2081-2093-2018-2015]Pann=16Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=4.659$ [(4+5)-VIII-2] : **Verificato**

Armatura a maglia doppia

Animaletta a maglia doppia										
Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-7980	8	675	364	8	-374	31.42	31.42		1
2	-10037	41	6083	677	-10	-360	31.42	31.42	(4+5)-IV-4	26
3	-17015	960	-909	1554	42	-381	31.42	31.42		1
4	-16288	1160	2189	1486	-186	209	31.42	31.42		1
5	-20906	273	-1303	1874	14	-91	31.42	31.42		1
6	-20430	443	-760	1838	-40	253	31.42	31.42		1
7	-20178	-312	-224	1829	15	70	31.42	31.42		1
8	-19701	-287	-1211	1786	71	42	31.42	31.42		1
9	-16570	90	887	1525	5	241	31.42	31.42		1
10	-16386	-122	1056	1472	30	-332	31.42	31.42	(4+5)-IV-1	16
11	-13699	-507	2631	1234	12	178	31.42	31.42	(4+5)-IV-1	20
12	-14132	-194	686	1255	53	-493	31.42	31.42	(4+5)-IV-1	16
13	10319	-604	3083	-788	112	342	31.42	31.42	(4+5)-VIII-2	21
14	6449	-1316	2210	-485	150	-1057	31.42	31.42	(4+5)-VII-2	16
15	13104	-342	1480	-1352	64	141	31.42	31.42	(4+5)-IV-4	15
16	17465	4757	10654	-2001	-821	-1446	31.42	31.42	(4+5)-VII-2	6.4
Massimi/minimi										
1							31.42			
1								31.42		
16										6.4

Muro [Platea]: 21 - Nodi: [2018-2017-2089-2090]Pann=28Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=2.581$ [(4+5)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-21687	1934	-629	1493	-123	225	31.42	31.42	(4+5)-V-1	17
2	-27888	-3598	-2672	1976	1500	757	31.42	31.42	3	11
3	-22730	2439	-498	1824	-293	-235	31.42	31.42	(4+5)-VII-2	15
4	-33368	-3959	17	2625	1332	631	31.42	31.42	3	9.8
5	-24229	-2496	-1453	1954	-564	-473	31.42	31.42	1	12
6	-35453	-4429	-435	3099	1329	493	31.42	31.42	3	9.0
7	-30075	-3989	-2045	2487	-598	-389	31.42	31.42	1	11
8	-36941	-4930	-984	3344	1393	403	31.42	31.42	3	8.7
9	-34319	-4858	-2038	2855	-558	-285	31.42	31.42	1	10
10	-37859	-5556	-1385	3462	1463	324	31.42	31.42	3	8.7
11	-37129	-5490	-1602	3093	-519	-199	31.42	31.42	1	9.9
12	-38235	-6142	-1602	3504	1520	239	31.42	31.42	3	8.8
13	-38624	-6011	-838	3220	-493	-138	31.42	31.42	1	9.8
14	-38098	-6566	-1704	3485	1553	156	31.42	31.42	3	9.0
15	-38950	-6412	162	3245	-483	-97	31.42	31.42	1	9.9
16	-37838	-6779	-1193	3447	1559	53	31.42	31.42	2	9.4
17	-38112	-6724	1273	3173	-482	-72	31.42	31.42	1	10
18	-36807	-7310	-35	3338	1620	-130	31.42	31.42	1	9.4
19	-36087	-6952	2436	3005	-504	-59	31.42	31.42	1	11
20	-35130	-7361	-64	3190	1633	-208	31.42	31.42	1	9.5
21	-32840	-6917	3571	2744	-604	-42	31.42	31.42	1	11
22	-32828	-7218	-179	3030	1678	-299	31.42	31.42	1	9.6
23	-27306	-6113	2996	2275	-812	170	31.42	31.42	2	13
24	-29890	-6353	-406	2860	1684	-394	31.42	31.42	1	9.6
25	-163	-3617	-2931	-199	-1179	769	31.42	31.42	(4+5)-VII-2	13
26	-26320	-5414	-822	2448	1722	-418	31.42	31.42	1	11
27	24325	3623	-14111	-2825	-406	1470	31.42	31.42	(4+5)-VII-2	4.8
28	-24022	-4228	361	1331	1639	-174	31.42	31.42	1	15
Massimi/minimi										
1							31.42			
1								31.42		
27										4.8

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Muro [Platea]: 22 - Nodi: [2090-2015-2018]Pann=13Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=6.573$ [(4+5)-III-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-16188	-14291	4912	634	-653	-1417	31.42	31.42		14
2	-10583	-17463	3869	542	-1453	-1547	31.42	31.42		9.6
3	-6718	-17809	1598	199	-2814	-1068	31.42	31.42		7.5
4	-4859	-14011	-832	-201	-1628	-446	31.42	31.42		14
5	3868	5799	-8593	-420	-1399	1013	31.42	31.42	(4+5)-IV-4	10
6	-14280	-18774	-2698	1191	2478	541	31.42	31.42		9.7
7	-17926	-11398	-422	2034	2910	42	31.42	31.42		9.4
8	-16917	-11649	6568	1614	2656	723	31.42	31.42		8.2
9	-12695	-3274	5299	914	455	-320	31.42	31.42	(4+5)-VIII-2	23
10	-15059	-8522	6278	962	494	-1253	31.42	31.42		13
11	-16942	-10969	4628	1009	468	-1155	31.42	31.42		13
12	-13726	-13310	2762	1271	589	-970	31.42	31.42		13
13	-12131	-14940	1064	1150	920	-896	31.42	31.42		14
Massimi/minimi										
1							31.42			
1								31.42		
3										7.5

Muro [Platea]: 23 - Nodi: [2012-2062-2054]Pann=31Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=5.011$ [(4+5)-III-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-29307	-22516	4527	5798	2056	646	31.42	31.42		4.8
2	-26776	-19928	2430	6439	2403	377	31.42	31.42		4.5
3	-25358	-18177	1029	6423	2451	248	31.42	31.42		4.6
4	-23409	-15811	917	6177	2405	-48	31.42	31.42		4.8
5	-22054	-13990	-198	5394	2418	-144	31.42	31.42		5.4
6	-23554	-15851	-4690	5550	3038	628	31.42	31.42		4.9
7	-21853	-14514	-726	5664	2470	-130	31.42	31.42		5.1
8	-23353	-16581	71	6231	2529	-29	31.42	31.42		4.8
9	-25254	-19279	-36	6315	2652	215	31.42	31.42		4.7
10	-26468	-21069	856	5982	2648	271	31.42	31.42		4.9
11	-27612	-22053	1751	5342	2523	211	31.42	31.42		5.6
12	-28815	-21722	1963	4547	2201	99	31.42	31.42		6.7
13	-29546	-19091	2381	3786	1671	-52	31.42	31.42		8.1
14	-27774	-18209	-834	2814	1151	139	31.42	31.42		10
15	-23636	-15510	-3010	1940	766	158	31.42	31.42		14
16	-15237	-11105	-3600	747	405	196	31.42	31.42	(4+5)-I-1	30
17	18711	-2878	2775	-1969	-942	-1604	31.42	31.42	(4+5)-III-4	6.1
18	-12292	-12604	-7963	1148	-106	-1761	31.42	31.42		9.6
19	-25465	-14642	-6652	2686	664	-1094	31.42	31.42		8.1
20	-34635	-15873	-2392	3372	841	-855	31.42	31.42		7.6
21	-39197	-17686	3049	3913	979	-588	31.42	31.42		7.3
22	-39044	-21052	6952	4193	1406	86	31.42	31.42		7.7
23	-26839	-20872	1816	6145	2473	366	31.42	31.42		4.7
24	-25821	-19585	827	6340	2562	289	31.42	31.42		4.6
25	-26648	-21249	1416	6014	2572	302	31.42	31.42		4.9
26	-30791	-18329	1454	3814	1226	-226	31.42	31.42		7.8
27	-31647	-21717	3206	5048	1924	69	31.42	31.42		6.2
28	-29644	-21937	2676	4816	2125	79	31.42	31.42		6.4
29	-33296	-19614	3587	4410	1462	-221	31.42	31.42		6.9
30	-27940	-22362	2369	5489	2427	231	31.42	31.42		5.4
31	-28737	-22444	3299	5555	2244	246	31.42	31.42		5.4
Massimi/minimi										
1							31.42			
1								31.42		
2										4.5

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Muro [Platea]: 24 - Nodi: [2062-2014-2011]Pann=15Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=20.855$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-15813	-17130	-3099	2019	3625	1731	31.42	31.42	3	5.4
2	-19517	-15879	-2102	2913	5311	2067	31.42	31.42	3	3.9
3	-23231	-14921	-1309	3242	6054	2098	31.42	31.42	3	3.5
4	-27695	-14810	-1419	3291	6234	2357	31.42	31.42	3	3.3
5	-25263	-11889	1886	2671	6605	2284	31.42	31.42	3	3.1
6	-19836	-7945	6671	2524	6764	2026	31.42	31.42	3	3.1
7	-13083	-1443	10815	1709	6390	1545	31.42	31.42	3	3.2
8	-5049	1387	11047	1080	5702	1320	31.42	31.42	3	3.6
9	-608	-1108	6256	-477	4295	319	31.42	31.42	2	5.6
10	-8295	-41	6453	-810	2248	-596	31.42	31.42	2	9.0
11	-13548	-5843	5682	416	1107	-239	31.42	31.42	1	20
12	-11057	-19973	83	81	-2483	27	31.42	31.42	3	12
13	-16152	-20464	-526	1025	1899	737	31.42	31.42	1	11
14	-12394	-8691	4500	1555	3818	909	31.42	31.42	3	5.8
15	-16772	-13797	1716	2396	5337	1641	31.42	31.42	3	4.0
Massimi/minimi										
1							31.42			
1								31.42		
6										3.1

Muro [Platea]: 25 - Nodi: [2015-2062-2012]Pann=35Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=5.226$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-22093	-19682	3092	2300	4452	-727	31.42	31.42	3	5.7
2	-20751	-28782	6472	2086	4681	-1099	31.42	31.42	3	5.4
3	-19374	-38045	10319	1812	3598	-1145	31.42	31.42	3	6.9
4	-15836	-37859	7960	1872	3410	-1190	31.42	31.42	3	7.1
5	-12292	-34120	3510	1924	2923	-1394	31.42	31.42	3	7.4
6	-9004	-32784	-905	2010	1116	-1195	31.42	31.42	2	8.5
7	-17	-10841	-4629	44	-1124	-276	31.42	31.42	(4+5)-VII-3	20
8	3870	10455	-3986	-551	-3269	271	31.42	31.42	(4+5)-VII-3	6.6
9	-6311	-20493	-1241	-791	-2234	1521	31.42	31.42	2	7.9
10	-11277	-22853	-1575	8	-2077	1725	31.42	31.42	2	7.9
11	-15887	-21951	-2569	373	-1715	1867	31.42	31.42	2	8.3
12	-20322	-18753	-3905	621	-1326	1902	31.42	31.42	1	9.0
13	-22665	-15436	-4442	661	-969	1887	31.42	31.42	1	10.0
14	-23257	-11937	-4959	532	-671	1808	31.42	31.42	1	11
15	-19152	-10107	-5970	1044	192	1124	31.42	31.42	(4+5)-IV-1	13
16	-19027	-6692	-5874	1132	420	972	31.42	31.42	(4+5)-IV-1	14
17	9388	1889	5081	-1152	-165	-671	31.42	31.42	(4+5)-IV-4	13
18	-18050	-10985	-4703	1902	2467	-217	31.42	31.42	3	10
19	-20963	-14950	-1002	2221	3562	-272	31.42	31.42	3	7.4
20	-10933	-24750	844	789	1876	-533	31.42	31.42	3	13
21	-7886	-19722	506	417	1098	-67	31.42	31.42	(4+5)-V-2	25
22	-14254	-21375	918	799	1480	46	31.42	31.42	2	19
23	-15108	-19149	472	711	656	662	31.42	31.42	1	21
24	-7829	-20063	1815	-299	35	836	31.42	31.42	3	24
25	-13846	-19792	-106	303	-386	1292	31.42	31.42	1	17
26	-22227	-12406	-3717	1367	590	1274	31.42	31.42	1	11
27	-19777	-16887	-532	1675	2153	714	31.42	31.42	3	10
28	-21366	-16070	-2924	1252	498	1339	31.42	31.42	1	11
29	-19811	-18326	-1403	1118	324	1302	31.42	31.42	1	12
30	-16979	-19619	-673	759	3	1286	31.42	31.42	1	14
31	-16705	-19961	1313	1092	1307	565	31.42	31.42	2	16
32	-19533	-18410	729	1669	1928	517	31.42	31.42	2	12
33	-14856	-21253	1974	1152	2210	-91	31.42	31.42	3	13
34	-18727	-20986	2950	1836	3331	-320	31.42	31.42	3	8.1
35	-14792	-26242	2314	1519	2863	-704	31.42	31.42	3	8.6
Massimi/minimi										
1							31.42			
1								31.42		

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
2										5.4

Muro [Platea]: 26 - Nodi: [2013-2087-2016]Pann=14Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=2.855$ [(4+5)-VI-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-16817	-2051	-6024	1411	38	472	31.42	31.42	(4+5)-II-3	15
2	-18703	-3207	-4835	1533	-2	392	31.42	31.42	1	15
3	-18201	-5218	-3606	1496	89	463	31.42	31.42	1	15
4	-15381	-4473	-3838	1134	-433	404	31.42	31.42	1	19
5	-1848	-765	-13101	99	-763	1002	31.42	31.42	(4+5)-V-2	15
6	-13794	9767	-3731	1233	164	182	31.42	31.42	1	20
7	-17499	1592	-4243	1533	249	232	31.42	31.42	1	16
8	-18392	-792	-4911	1563	366	438	31.42	31.42	1	15
9	-16738	-2224	-5981	1431	347	557	31.42	31.42	(4+5)-II-3	14
10	-13752	-2564	-6264	1191	410	728	31.42	31.42	(4+5)-II-3	15
11	8280	-3925	-3965	-813	512	656	31.42	31.42	(4+5)-V-4	16
12	38232	2939	10554	-3280	-312	-942	31.42	31.42	(4+5)-II-2	4.2
13	10739	1345	188	-822	-213	-364	31.42	31.42	(4+5)-II-2	20
14	-14261	-1581	-7020	1214	-11	423	31.42	31.42	(4+5)-II-3	17
Massimi/minimi										
1							31.42			
1								31.42		
12										4.2

Muro [Platea]: 27 - Nodi: [2004-2036-2007]Pann=51Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=4.341$ [(4+5)-VI-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-27057	-14632	-767	7749	1968	494	31.42	31.42	2	3.7
2	-26884	-14528	-726	7570	2031	553	31.42	31.42	3	3.8
3	-27110	-14281	-746	6917	2033	568	31.42	31.42	3	4.1
4	-27379	-14057	-795	5732	1999	525	31.42	31.42	3	4.9
5	-27551	-14014	-924	4054	1881	408	31.42	31.42	3	6.9
6	-18276	-10682	-1909	2384	1198	399	31.42	31.42	(4+5)-III-4	10
7	-16224	-8191	749	-1561	590	-159	31.42	31.42	(4+5)-III-1	17
8	-26308	-11241	-1507	-4327	-19	-92	31.42	31.42	1	6.9
9	-25543	-3247	-1886	-8538	-1490	1085	31.42	31.42	2	3.2
10	-27689	-12536	2820	-6893	376	783	31.42	31.42	2	4.0
11	-27951	-18452	3142	-5806	811	612	31.42	31.42	2	4.8
12	-28029	-20199	592	-5720	1024	497	31.42	31.42	1	5.0
13	-28475	-20512	-1630	-5873	1051	355	31.42	31.42	1	5.0
14	-29726	-18189	-3184	-6229	770	176	31.42	31.42	1	4.9
15	-30190	-14847	-2431	-7139	15	200	31.42	31.42	2	4.3
16	-25791	-4805	3564	-8824	-1670	-186	31.42	31.42	2	3.4
17	-11906	-12490	3011	-2423	-223	577	31.42	31.42	(4+5)-I-2	9.3
18	-20431	-12432	-1742	2163	993	798	31.42	31.42	(4+5)-V-4	10.0
19	-27949	-15736	167	4558	1587	619	31.42	31.42	3	6.0
20	-28481	-15462	-25	6384	2062	630	31.42	31.42	3	4.4
21	-28731	-15285	-111	7474	2306	668	31.42	31.42	3	3.8
22	-28803	-15150	-164	7928	2330	702	31.42	31.42	3	3.6
23	-28873	-14882	-350	7766	2114	630	31.42	31.42	2	3.7
24	-29001	-14543	-239	6951	1809	510	31.42	31.42	2	4.2
25	-28780	-14153	-600	5234	1315	438	31.42	31.42	1	5.5
26	-27998	-14398	-144	6632	1751	366	31.42	31.42	2	4.4
27	-27623	-14752	-583	7425	1875	459	31.42	31.42	2	3.9
28	-28228	-14833	-374	7827	2052	574	31.42	31.42	2	3.7
29	-27556	-14857	-270	7779	2082	604	31.42	31.42	3	3.7
30	-28342	-15132	-67	7499	2203	679	31.42	31.42	3	3.8
31	-28329	-15050	-155	7864	2223	663	31.42	31.42	3	3.6
32	-28013	-14990	-93	7637	2138	669	31.42	31.42	3	3.7

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
33	-27395	-14768	-262	7370	2056	647	31.42	31.42		3.8
34	-27821	-15005	38	7030	2045	707	31.42	31.42		4.0
35	-28167	-15244	111	6683	2028	706	31.42	31.42		4.2
36	-27920	-15339	493	5145	1720	790	31.42	31.42		5.2
37	-29397	-15516	-986	-3437	1253	746	31.42	31.42		7.5
38	-29087	-13102	333	-3055	709	989	31.42	31.42		7.7
39	-28736	-15352	970	-379	1450	1000	31.42	31.42		12
40	-20073	-11490	-1759	2787	1121	822	31.42	31.42	(4+5) -III-4	8.1
41	-27960	-14425	-140	4850	1989	684	31.42	31.42		5.6
42	-27560	-14595	-178	6415	2017	691	31.42	31.42		4.3
43	-27798	-14954	289	5781	1906	789	31.42	31.42		4.7
44	-28197	-14855	489	3775	1810	859	31.42	31.42		6.7
45	-19002	-11130	-2036	2927	1445	612	31.42	31.42	(4+5) -III-4	8.2
46	-28879	-15039	380	1192	1821	791	31.42	31.42		11
47	-28942	-17006	-521	-3403	1469	482	31.42	31.42		8.0
48	-29229	-17009	-1027	-3389	1516	597	31.42	31.42		7.8
49	-29064	-15949	53	-1058	1967	617	31.42	31.42		11
50	-28531	-14869	-295	423	1849	403	31.42	31.42		13
51	-28508	-14574	-798	-2672	1302	277	31.42	31.42		11
Massimi/minimi										
1							31.42			
1								31.42		
9										3.2

Muro [Platea]: 28 - Nodi: [2001-2026-2028] Pann=44 Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=2.819$ [(4+5) -III-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-35844	-20568	-3629	5068	2236	692	31.42	31.42		5.6
2	-33153	-20748	-5376	5524	3964	975	31.42	31.42		4.9
3	-32691	-20177	-6898	5701	5277	1398	31.42	31.42		4.4
4	-33957	-20140	-10523	7305	7738	2857	31.42	31.42		2.8
5	-34128	-19251	-7293	6447	5109	1374	31.42	31.42		4.1
6	-34147	-19214	-5476	6339	4380	856	31.42	31.42		4.5
7	-34630	-18792	-4598	6106	3538	437	31.42	31.42		4.9
8	-34697	-18281	-4318	5712	2788	85	31.42	31.42		5.6
9	-33973	-17446	-4633	5044	1996	-216	31.42	31.42		6.1
10	-32649	-16555	-5426	4245	1146	-465	31.42	31.42		6.8
11	-29945	-15433	-6949	3229	266	-642	31.42	31.42		8.1
12	-25355	-13849	-9356	2033	-824	-714	31.42	31.42		11
13	-8356	-4203	-2997	294	-1445	-937	31.42	31.42	(4+5) -VI-1	11
14	-7210	-9976	-11676	-745	-2606	-800	31.42	31.42		8.1
15	30458	-5587	-1725	-3201	-2550	-1854	31.42	31.42	(4+5) -III-1	3.8
16	-5423	-9028	-15989	8	-3505	-2234	31.42	31.42		4.7
17	-17463	-12955	-17330	1358	-2903	-1810	31.42	31.42		5.9
18	-28902	-13826	-16482	1894	-2955	-1633	31.42	31.42		6.1
19	-37163	-15137	-15085	2929	-3070	-1487	31.42	31.42		6.2
20	-41781	-15510	-12904	3516	-3004	-1061	31.42	31.42		7.0
21	-47242	-15828	-9946	4009	-2939	-609	31.42	31.42		7.5
22	-49486	-16170	-6721	4236	-2869	-186	31.42	31.42		7.9
23	-49298	-16473	-3446	4307	-2644	229	31.42	31.42		7.7
24	-47663	-16259	-242	4071	-2573	561	31.42	31.42		7.5
25	-40165	-19752	-2113	4683	6	514	31.42	31.42		6.4
26	-31907	-15924	-8720	3480	-553	-592	31.42	31.42		7.8
27	-28391	-15053	-11153	2617	-1585	-779	31.42	31.42		9.1
28	-34305	-16031	-11271	3400	-1690	-656	31.42	31.42		7.9
29	-34936	-16997	-7116	4318	190	-417	31.42	31.42		6.8
30	-38319	-16650	-9517	4138	-1190	-409	31.42	31.42		7.2
31	-41465	-17491	-7775	4628	-970	-170	31.42	31.42		7.0
32	-36182	-18531	-5062	5490	1928	26	31.42	31.42		5.9
33	-35767	-18122	-5815	4931	1074	-220	31.42	31.42		6.3
34	-38012	-18398	-5946	5043	551	-109	31.42	31.42		6.4
35	-39818	-19138	-4901	5286	811	286	31.42	31.42		6.0
36	-42744	-18468	-4524	4903	-657	284	31.42	31.42		6.5
37	-40139	-19145	-3689	5045	473	445	31.42	31.42		6.1
38	-43320	-17977	-6034	4844	-950	59	31.42	31.42		6.9
39	-39501	-18619	-5601	5233	645	123	31.42	31.42		6.2
40	-37305	-19819	-4793	5577	1938	377	31.42	31.42		5.5

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
41	-35617	-19559	-4789	5899	2860	399	31.42	31.42	2	5.1
42	-36939	-19086	-4946	5606	1928	212	31.42	31.42	2	5.6
43	-36826	-20089	-4307	5461	2167	531	31.42	31.42	2	5.4
44	-34696	-20311	-5213	5963	3584	693	31.42	31.42	2	4.8
Massimi/minimi										
1							31.42			
1								31.42		
4										2.8

Muro [Platea]: 29 - Nodi: [2009-2044-2006]Pann=56Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45,ζ_e=4.295 [(4+5)-VIII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-47251	-8577	3016	4256	938	-268	31.42	31.42	3	7.6
2	-43109	-10658	5544	4693	1320	-101	31.42	31.42	3	7.1
3	-37174	-13326	6341	4882	1640	229	31.42	31.42	1	6.4
4	-31471	-14616	8605	4911	1782	403	31.42	31.42	1	5.9
5	-25649	-15849	9319	4630	1795	483	31.42	31.42	1	6.0
6	-19431	-16640	9191	3884	1657	497	31.42	31.42	1	6.7
7	-12096	-17340	8048	2433	1343	294	31.42	31.42	1	10
8	-7358	-11480	8357	1380	711	-383	31.42	31.42	(4+5)-I-2	15
9	5377	13404	-5233	-884	-1787	840	31.42	31.42	(4+5)-VIII-3	8.7
10	-7842	-13223	7314	-1818	1310	46	31.42	31.42	2	14
11	-13938	-15759	7094	-1856	1276	-216	31.42	31.42	3	14
12	-17806	-15835	4074	-2391	1128	-280	31.42	31.42	3	11
13	-19757	-14180	440	-2775	868	-317	31.42	31.42	3	9.5
14	-20112	-10810	-2953	-2734	466	-271	31.42	31.42	3	9.8
15	-17781	-5628	-5617	-2795	-41	-71	31.42	31.42	3	10
16	11488	4105	2511	-2530	-1230	-1185	31.42	31.42	(4+5)-III-4	6.2
17	-15625	-7564	-10316	559	-724	-953	31.42	31.42	3	16
18	-27582	-9716	-11602	2318	-177	-1114	31.42	31.42	3	9.0
19	-37088	-9519	-10404	3443	62	-913	31.42	31.42	3	7.5
20	-43900	-8464	-7885	4138	262	-542	31.42	31.42	3	7.3
21	-47638	-7971	-4678	4520	421	-106	31.42	31.42	3	7.5
22	-48167	-8607	-3973	4479	668	379	31.42	31.42	1	7.2
23	-47628	-7929	-1846	4159	592	524	31.42	31.42	1	7.4
24	-44371	-7761	-1113	4014	470	698	31.42	31.42	1	7.2
25	-41573	-7592	-1690	2719	427	151	31.42	31.42	1	12
26	-47347	-5667	-35	3035	349	-715	31.42	31.42	3	9.2
27	-49408	-6557	1026	3705	476	-443	31.42	31.42	3	8.4
28	-45234	-9998	-3397	4834	749	197	31.42	31.42	1	6.8
29	-47557	-7635	-119	4594	484	-125	31.42	31.42	3	7.3
30	-45517	-9129	638	4852	795	-75	31.42	31.42	3	7.0
31	-40219	-9819	-4946	4686	580	37	31.42	31.42	2	7.0
32	-42955	-10752	-4637	4836	772	198	31.42	31.42	1	6.7
33	-38751	-12181	-2937	4810	1072	209	31.42	31.42	1	6.6
34	-39701	-12004	240	4865	1259	140	31.42	31.42	1	6.6
35	-34576	-10688	-4995	4132	524	-69	31.42	31.42	3	7.7
36	-33270	-11093	-809	4424	1064	72	31.42	31.42	2	7.1
37	-30672	-13727	5093	4460	1863	188	31.42	31.42	1	6.8
38	-31867	-12593	1891	4358	1543	157	31.42	31.42	1	7.0
39	-35381	-13017	3104	4775	1637	164	31.42	31.42	1	6.5
40	-27645	-10581	309	3240	948	-38	31.42	31.42	3	9.4
41	-27038	-9970	-3947	2894	389	-83	31.42	31.42	3	10
42	-23787	-10735	-365	879	1113	63	31.42	31.42	1	23
43	-19212	-7733	261	899	608	-192	31.42	31.42	(4+5)-I-2	27
44	-22985	-8353	70	-510	836	-120	31.42	31.42	3	28
45	-24808	-9949	-632	1873	1105	124	31.42	31.42	1	15
46	-18605	-6504	-2078	1012	312	-34	31.42	31.42	(4+5)-I-2	28
47	-25468	-11418	1394	2426	1370	119	31.42	31.42	1	12
48	-28281	-11200	2706	3630	1399	50	31.42	31.42	2	8.4
49	-26684	-12437	3444	3182	1692	164	31.42	31.42	1	9.2
50	-26454	-13830	5718	3800	1956	186	31.42	31.42	1	7.7
51	-23624	-11415	1069	1226	1345	75	31.42	31.42	1	20
52	-22356	-11061	1883	-561	1187	-144	31.42	31.42	3	21
53	-17678	-13421	6695	845	1798	-175	31.42	31.42	3	14
54	-21008	-12530	4431	-9	1502	-171	31.42	31.42	3	17
55	-21869	-14179	5865	2664	1943	137	31.42	31.42	1	11

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
56	-19578	-9366	4682	1722	1102	-194	31.42	31.42	(4+5)-I-2	15
Massimi/minimi										
1							31.42			
1								31.42		
4										5.9

Muro [Platea]: 30 - Nodi: [2003-2029-2002]Pann=56Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45,ζ_e=3.991 [(4+5)-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-25366	-5878	146	1322	114	1176	31.42	31.42	(4+5)-I-2	12
2	-29529	-12381	637	1995	932	1348	31.42	31.42	2	9.3
3	-30386	-15243	-114	2880	1638	1188	31.42	31.42	2	7.7
4	-30868	-17276	-274	3581	2253	933	31.42	31.42	2	7.0
5	-31910	-18648	119	4102	2800	649	31.42	31.42	3	6.7
6	-32294	-19110	619	4443	3245	249	31.42	31.42	3	6.8
7	-33056	-18857	1156	4722	3698	-219	31.42	31.42	3	6.5
8	-33821	-17932	2118	4967	4006	-696	31.42	31.42	3	5.7
9	-34741	-18196	4600	5741	4746	-2011	31.42	31.42	3	4.2
10	-30540	-18408	3266	3883	4254	-1178	31.42	31.42	3	5.4
11	-27390	-18273	2260	2346	2914	-709	31.42	31.42	2	8.0
12	-15770	-15645	-937	638	1103	501	31.42	31.42	(4+5)-III-4	18
13	-20507	-17756	2481	-975	-1451	1340	31.42	31.42	3	10
14	-10320	-15209	8226	-2287	-6466	2043	31.42	31.42	3	3.3
15	-15442	-24063	1251	-369	-4389	2387	31.42	31.42	3	4.5
16	-21673	-26424	-2953	479	-3315	2130	31.42	31.42	3	5.6
17	-27290	-26374	-5381	1251	-2888	2306	31.42	31.42	3	5.9
18	-32594	-24640	-6371	1572	-2557	2535	31.42	31.42	3	5.9
19	-36947	-22052	-6187	1654	-2221	2716	31.42	31.42	3	6.0
20	-40019	-18906	-5049	1552	-1906	2848	31.42	31.42	3	6.1
21	-41548	-15364	-3113	1296	-1637	2929	31.42	31.42	3	6.2
22	-41420	-11785	-673	879	-1393	3008	31.42	31.42	3	6.3
23	-39584	-8040	1935	195	-1215	2986	31.42	31.42	3	6.4
24	-35170	-3865	4754	-512	-1137	2652	31.42	31.42	3	6.9
25	-27899	209	8531	-974	-951	2568	31.42	31.42	3	7.2
26	-17487	4710	10460	-2421	-1182	2552	31.42	31.42	3	5.8
27	18183	2832	7426	-4046	-1092	1266	31.42	31.42	(4+5)-VII-3	4.1
28	-15920	616	7846	-1615	-1674	1199	31.42	31.42	3	8.8
29	-23717	-2948	4600	-234	-830	1428	31.42	31.42	3	12
30	-34797	-11107	1381	1515	-588	2144	31.42	31.42	2	8.8
31	-30990	-8819	2751	1009	-514	1917	31.42	31.42	2	11
32	-31686	-12231	991	1919	291	1705	31.42	31.42	2	8.7
33	-36965	-16923	-1271	2485	-248	2079	31.42	31.42	3	7.2
34	-35904	-14023	-294	2163	-274	2063	31.42	31.42	2	7.7
35	-33955	-18312	-357	3090	1055	1533	31.42	31.42	3	6.9
36	-32301	-17458	-91	3206	1533	1284	31.42	31.42	2	7.1
37	-32637	-18734	47	3702	2145	1012	31.42	31.42	3	6.8
38	-32571	-15135	18	2636	866	1569	31.42	31.42	2	7.6
39	-36437	-19385	-2286	2577	-384	2089	31.42	31.42	3	7.0
40	-34652	-21355	-2743	2554	-451	2016	31.42	31.42	3	7.0
41	-32593	-20138	458	3663	2165	850	31.42	31.42	3	7.0
42	-32761	-19502	177	3712	2111	958	31.42	31.42	3	6.8
43	-32246	-19660	776	4090	2840	545	31.42	31.42	3	6.8
44	-34139	-19554	-700	3188	1011	1475	31.42	31.42	3	6.9
45	-33271	-20686	-608	3168	1082	1365	31.42	31.42	3	7.0
46	-31078	-19965	1970	3594	2783	246	31.42	31.42	3	8.2
47	-32413	-19168	2564	4282	3700	-295	31.42	31.42	3	6.9
48	-30465	-19773	2625	3831	3360	-365	31.42	31.42	3	7.5
49	-31978	-20217	1195	3662	2483	583	31.42	31.42	3	7.5
50	-32143	-19650	1644	4228	3297	125	31.42	31.42	3	7.3
51	-31764	-21257	-51	3085	1274	1152	31.42	31.42	3	7.5
52	-31939	-22752	-2459	2407	-431	1862	31.42	31.42	3	7.4
53	-25796	-21366	825	1448	46	1199	31.42	31.42	3	12
54	-28854	-23114	-1338	2082	-332	1612	31.42	31.42	3	8.4
55	-28703	-20210	2012	2668	2186	199	31.42	31.42	3	11
56	-30059	-21020	1032	2906	1588	805	31.42	31.42	3	8.4
Massimi/minimi										
1							31.42			

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1								31.42		
14										3.3

Muro [Platea]: 31 - Nodi: [2084-2085-2088]Pann=21Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45,ζ_e=12.249 [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-18278	-32779	-2013	1124	3598	213	31.42	31.42	3	8.4
2	-27621	-36374	641	1901	3061	-332	31.42	31.42	1	9.6
3	-31554	-33377	945	2373	2538	-361	31.42	31.42	1	11
4	-34896	-28662	907	2837	2018	-320	31.42	31.42	1	10
5	-38523	-22489	1453	3213	1630	-147	31.42	31.42	1	9.8
6	-35973	-27515	3474	3116	2411	-131	31.42	31.42	1	10.0
7	-32461	-32336	4913	3084	2855	-281	31.42	31.42	1	9.4
8	-28910	-36190	6498	2995	3267	-531	31.42	31.42	1	8.6
9	-24201	-39116	7946	2663	3471	-797	31.42	31.42	1	7.7
10	-18538	-45874	11374	1793	3522	-939	31.42	31.42	1	7.7
11	-13456	-44571	3385	931	3045	-95	31.42	31.42	1	11
12	-10818	-42473	-3144	804	2626	454	31.42	31.42	1	11
13	-11987	-40012	-9825	877	3054	993	31.42	31.42	1	8.2
14	-13370	-32720	-7261	831	3349	757	31.42	31.42	2	7.8
15	-14574	-32751	-3695	830	3564	514	31.42	31.42	3	7.8
16	-26901	-36701	2364	2198	3370	-410	31.42	31.42	1	8.6
17	-30012	-34339	2469	2603	3019	-394	31.42	31.42	1	9.4
18	-27515	-36508	4054	2545	3454	-495	31.42	31.42	1	8.2
19	-23314	-40241	4335	2086	3817	-578	31.42	31.42	1	7.6
20	-19558	-40208	1645	1376	3663	-275	31.42	31.42	1	8.4
21	-23356	-38705	2187	1846	3658	-324	31.42	31.42	1	8.3
Massimi/minimi										
1							31.42			
1								31.42		
19										7.6

Muro [Platea]: 32 - Nodi: [2002-2028-2026]Pann=25Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45,ζ_e=2.616 [(4+5)-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-25468	-29491	-7015	2717	3836	1231	31.42	31.42	2	6.2
2	-30243	-27538	-9197	1680	2343	2222	31.42	31.42	2	6.8
3	-34739	-26339	-12850	-24	1109	3175	31.42	31.42	2	7.1
4	-34850	-21790	-8827	-389	847	2947	31.42	31.42	2	7.8
5	-34432	-17270	-5811	-847	439	2867	31.42	31.42	3	8.7
6	-18466	-2843	6980	-2578	-1081	1647	31.42	31.42	(4+5)-I-3	6.9
7	-10315	-341	14723	-3874	-1587	1919	31.42	31.42	(4+5)-I-3	4.7
8	17384	1772	29265	-7308	-2949	828	31.42	31.42	(4+5)-I-3	2.7
9	-23447	-14725	1749	-897	-2305	1700	31.42	31.42	3	7.1
10	-22726	-12619	-5032	1490	331	748	31.42	31.42	(4+5)-I-2	13
11	-24088	-22572	-2466	2242	1665	-96	31.42	31.42	3	13
12	-22517	-26174	-2831	2918	3173	-615	31.42	31.42	3	8.1
13	-20316	-29718	-3012	3313	4684	-889	31.42	31.42	3	5.6
14	-17808	-32641	-2680	3425	5828	-1043	31.42	31.42	3	4.6
15	-13683	-35296	-5945	3655	8666	-1515	31.42	31.42	3	3.2
16	-18898	-32620	-4448	3818	6522	-239	31.42	31.42	3	4.7
17	-22212	-30825	-5429	3291	5203	353	31.42	31.42	2	5.7
18	-29144	-21230	-4721	939	923	1709	31.42	31.42	2	11
19	-22847	-14223	-7020	1169	716	1169	31.42	31.42	(4+5)-I-2	13
20	-26087	-22271	-3481	1767	1484	796	31.42	31.42	3	12
21	-25897	-27261	-6173	2366	3240	1088	31.42	31.42	2	7.1
22	-29410	-25190	-8000	1400	2000	2017	31.42	31.42	2	7.6
23	-28083	-24187	-5346	1645	2106	1374	31.42	31.42	2	8.7
24	-24544	-25400	-4120	2401	2809	366	31.42	31.42	2	9.6

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
25	-23048	-28525	-4716	2952	4196	131	31.42	31.42	2	7.2
Massimi/minimi										
1							31.42			
1								31.42		
8										2.7

Muro [Platea]: 33 - Nodi: [2037-2043-2042-2036]Pann=8Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=9.218$ [(4+5)-II-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-14801	-15749	2460	1306	-2889	-748	31.42	31.42	(4+5)-III-4	13
2	-25991	-27776	2528	2649	-439	-372	31.42	31.42	3	17
3	-15716	-14237	4175	940	-3301	-62	31.42	31.42	(4+5)-III-4	14
4	-26233	-23654	3210	2496	-602	197	31.42	31.42	3	19
5	-16248	-14194	5825	866	-3614	750	31.42	31.42	(4+5)-V-4	11
6	-26468	-22327	5705	2302	-1295	939	31.42	31.42	3	16
7	-18852	-17863	12196	-144	-6289	2247	31.42	31.42	(4+5)-V-4	5.8
8	-15320	-18674	8297	919	-3595	964	31.42	31.42	(4+5)-V-4	11
Massimi/minimi										
1							31.42			
1								31.42		
7										5.8

Muro [Platea]: 34 - Nodi: [2032-2031-2028-2029]Pann=16Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=7.932$ [(4+5)-III-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-4316	-27613	3164	-1106	-945	-1910	31.42	31.42	(4+5)-II-4	15
2	-20333	-30885	7573	51	2019	-1447	31.42	31.42	3	15
3	-26604	-28644	8324	590	2808	-1620	31.42	31.42	3	12
4	-33117	-27275	8538	1563	3344	-1848	31.42	31.42	3	10
5	-6254	-27570	-4506	-709	-1362	-1963	31.42	31.42	(4+5)-II-4	16
6	-20324	-30532	-830	-212	1472	-988	31.42	31.42	3	22
7	-22832	-28405	1151	-87	2345	-970	31.42	31.42	3	16
8	-23944	-29119	1812	96	2763	-933	31.42	31.42	3	14
9	-11581	-28417	-10556	-67	-1630	-2445	31.42	31.42	(4+5)-VI-4	13
10	-13277	-21036	-8771	-865	156	-603	31.42	31.42	(4+5)-III-4	33
11	-15523	-15948	-3503	-92	1362	-506	31.42	31.42	(4+5)-II-3	26
12	-25963	-30438	-3799	216	2192	-506	31.42	31.42	3	20
13	-32425	-36623	-19687	-88	-3097	-4562	31.42	31.42	3	7.2
14	-23007	-24324	-13528	-1775	78	-273	31.42	31.42	(4+5)-I-4	25
15	-35839	-28751	-12001	857	1918	651	31.42	31.42	1	21
16	-39784	-25380	-11153	2296	2810	1356	31.42	31.42	3	12
Massimi/minimi										
1							31.42			
1								31.42		
13										7.2

Muro [Platea]: 35 - Nodi: [2033-2038-2005-2032]Pann=16Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=9.056$ [(4+5)-I-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-23538	-16941	-7845	3528	2700	1487	31.42	31.42	3	10
2	-22822	-14941	-9769	3838	2222	2324	31.42	31.42	3	8.3
3	-21723	-12066	-10623	4614	1674	2421	31.42	31.42	3	7.2

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
4	-22202	-8353	-11389	4254	902	1674	31.42	31.42		8.6
5	-22324	-15674	-7615	3052	3009	1174	31.42	31.42		12
6	-21853	-14734	-10695	3170	2296	1836	31.42	31.42		10
7	-21152	-12302	-11892	3485	1460	2254	31.42	31.42		8.8
8	-20704	-9079	-13633	3244	324	1500	31.42	31.42		11
9	-20544	-15950	-8048	2675	2966	1031	31.42	31.42		12
10	-20797	-15039	-11347	2477	2292	1460	31.42	31.42		13
11	-20627	-12653	-13278	2163	1570	1948	31.42	31.42		12
12	-18504	-9699	-15090	2014	109	1450	31.42	31.42		14
13	-18655	-17651	-7840	2404	2699	740	31.42	31.42		14
14	-19377	-15982	-12415	1940	2182	949	31.42	31.42		16
15	-19278	-13493	-14563	719	1582	1120	31.42	31.42		18
16	-11661	-12126	-9309	699	1384	1008	31.42	31.42	(4+5)-I-3	20
Massimi/minimi										
1							31.42			
1								31.42		
3										7.2

Muro [Platea]: 36 - Nodi: [2033-2032-2029]Pann=9Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=14.877$ [(4+5)-VI-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-17155	-32895	13948	1068	792	-1230	31.42	31.42		21
2	-8605	-18775	4807	717	1254	-958	31.42	31.42	(4+5)-II-3	22
3	-21598	-30538	11931	623	1901	-1511	31.42	31.42		16
4	-27843	-30338	11806	854	2829	-1648	31.42	31.42		12
5	-31970	-37089	11005	1343	4927	-1842	31.42	31.42		8.2
6	-28603	-33077	11508	384	3682	-1105	31.42	31.42		11
7	-26209	-31399	13403	194	2116	-404	31.42	31.42		21
8	-19821	-31207	14216	1275	851	1160	31.42	31.42		21
9	-11517	-16744	7664	833	1386	-362	31.42	31.42	(4+5)-IV-3	28
Massimi/minimi										
1							31.42			
1								31.42		
5										8.2

Muro [Platea]: 37 - Nodi: [2032-2005-2037-2031]Pann=16Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=6.736$ [(4+5)-III-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-20792	-8358	-9501	4943	-60	-17	31.42	31.42		10
2	-14630	-11178	-12356	7040	1275	-2598	31.42	31.42		5.0
3	-12080	-14950	-14055	7726	2263	-4055	31.42	31.42		4.0
4	-9622	-19792	-16089	9800	2923	-5215	31.42	31.42		3.1
5	-12166	1153	-7120	2340	-3694	636	31.42	31.42	(4+5)-III-4	9.9
6	-13117	-14205	-11197	5909	101	-1187	31.42	31.42		6.7
7	-10174	-17854	-12452	6846	1412	-2020	31.42	31.42		5.3
8	-5516	-25458	-11090	7543	1677	-2595	31.42	31.42		4.5
9	-11187	-794	-6507	1558	-4994	1296	31.42	31.42	(4+5)-III-4	6.9
10	-11563	-16227	-10271	4615	-586	-370	31.42	31.42		9.5
11	-9497	-20237	-10588	5606	806	-876	31.42	31.42		7.2
12	-7470	-26515	-7565	5816	791	-1410	31.42	31.42		6.3
13	-8806	-1483	-4865	857	-5935	1707	31.42	31.42	(4+5)-III-4	5.7
14	-11693	-17847	-8777	3363	-1076	234	31.42	31.42		13
15	-10002	-21621	-8908	4384	340	-269	31.42	31.42		10
16	-8952	-26337	-5709	4630	113	-874	31.42	31.42		8.4
Massimi/minimi										
1							31.42			
1								31.42		
4										3.1

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Muro [Platea]: 38 - Nodi: [2038-2044-2008-2005]Pann=16Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=9.850$ [(4+5)-III-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-14511	-15048	-6115	2146	3394	1156	31.42	31.42	3	11
2	-12964	-15104	-7793	2191	2498	1744	31.42	31.42	3	11
3	-10602	-14801	-8586	2226	1277	1757	31.42	31.42	3	12
4	-7793	-13870	-8583	2330	-432	1453	31.42	31.42	3	12
5	-10107	-14832	-6430	1614	4377	1159	31.42	31.42	3	8.7
6	-10421	-15688	-7250	1444	2683	1639	31.42	31.42	3	11
7	-11058	-16318	-7195	1260	504	1659	31.42	31.42	3	16
8	-9193	-12191	-7322	435	-3555	1407	31.42	31.42	(4+5)-I-2	9.6
9	-8734	-9875	-6612	1559	5020	1213	31.42	31.42	3	7.5
10	-10853	-10779	-6160	1437	3096	1941	31.42	31.42	3	9.3
11	-13071	-11287	-5262	1284	397	2132	31.42	31.42	3	14
12	-10977	-7516	-6387	367	-3537	1294	31.42	31.42	(4+5)-I-2	9.5
13	-10654	-1076	-5109	2022	8440	860	31.42	31.42	3	4.7
14	-15513	-846	-1346	1248	3989	2253	31.42	31.42	3	7.0
15	-9310	-3526	-2170	-39	-1531	2131	31.42	31.42	(4+5)-III-1	12
16	-9801	-6102	-2593	-164	-4602	1826	31.42	31.42	(4+5)-III-1	7.1
Massimi/minimi										
1							31.42			
1								31.42		
13										4.7

Muro [Platea]: 39 - Nodi: [2044-2050-2049-2008]Pann=16Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=5.762$ [(4+5)-IV-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-19408	3947	13451	778	6363	4638	31.42	31.42	3	3.8
2	-17510	-3906	7894	1072	3075	2735	31.42	31.42	3	7.7
3	-9617	-5954	2418	-503	-1974	1683	31.42	31.42	(4+5)-III-1	12
4	-8769	-6902	650	-1060	-5332	1780	31.42	31.42	(4+5)-III-1	6.4
5	-16746	-17849	8251	1456	869	2943	31.42	31.42	3	11
6	-14779	-14112	9156	1718	776	2554	31.42	31.42	3	11
7	-7827	-10761	3456	104	-2544	1676	31.42	31.42	(4+5)-III-1	11
8	-7689	-11413	2274	-45	-5170	1932	31.42	31.42	(4+5)-III-1	6.6
9	-17821	-21961	6082	2128	-418	2616	31.42	31.42	3	10
10	-14992	-20274	6823	2325	-727	2425	31.42	31.42	3	10
11	-7097	-14362	3382	709	-2729	1904	31.42	31.42	(4+5)-III-1	10
12	-6812	-14607	2947	604	-4710	2262	31.42	31.42	(4+5)-III-1	6.9
13	-18933	-24411	4617	2617	-1349	2731	31.42	31.42	3	9.3
14	-15247	-23019	5297	3171	-1524	2753	31.42	31.42	3	8.2
15	-13447	-21944	5374	3719	-2350	2322	31.42	31.42	3	7.9
16	-6725	-16505	2422	1341	-3761	2575	31.42	31.42	(4+5)-III-1	7.7
Massimi/minimi										
1							31.42			
1								31.42		
1										3.8

Muro [Platea]: 40 - Nodi: [2005-2008-2043-2037]Pann=16Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=10.164$ [(4+5)-III-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-5282	-9379	-1275	570	-6280	1442	31.42	31.42	(4+5)-III-4	6.0
2	-7029	-10323	-1855	695	-3706	836	31.42	31.42	(4+5)-III-4	10
3	-8092	-12802	-1389	1035	-2583	193	31.42	31.42	(4+5)-III-4	17

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
4	-9876	-15368	232	1214	-2645	-465	31.42	31.42	(4+5)-III-4	16
5	-8829	-9517	-625	43	-6052	1071	31.42	31.42	(4+5)-III-4	6.5
6	-8832	-11792	769	180	-4798	906	31.42	31.42	(4+5)-III-4	8.3
7	-10472	-12909	1898	286	-4022	545	31.42	31.42	(4+5)-III-4	10
8	-12807	-13803	2582	486	-3814	159	31.42	31.42	(4+5)-I-4	12
9	-10543	-8300	2014	-97	-6339	1128	31.42	31.42	(4+5)-III-4	6.2
10	-11080	-9837	3230	45	-5160	779	31.42	31.42	(4+5)-I-4	7.9
11	-12118	-10736	3895	135	-4446	729	31.42	31.42	(4+5)-III-4	9.1
12	-14787	-10061	3966	293	-4540	626	31.42	31.42	(4+5)-I-4	9.0
13	-10731	-5343	4557	-255	-7731	1041	31.42	31.42	(4+5)-I-4	5.1
14	-12265	-4741	5437	-102	-5156	731	31.42	31.42	(4+5)-III-4	7.6
15	-13658	-4369	6065	238	-3366	1047	31.42	31.42	(4+5)-I-4	10
16	-15611	-4832	7623	182	-1944	1510	31.42	31.42	(4+5)-III-4	13
Massimi/minimi										
1							31.42			
1								31.42		
13										5.1

Muro [Platea]: 41 - Nodi: [2029-2028-2002]Pann=25Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=6.069$ [(4+5)-III-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-25064	-21704	-2252	1924	4522	-73	31.42	31.42		3
2	-24587	-21142	-733	1340	2923	-492	31.42	31.42		3
3	-19785	-13759	3955	1180	1018	-828	31.42	31.42	(4+5)-I-2	15
4	-18856	-18616	1699	-820	-1264	-843	31.42	31.42		3
5	-291	-6672	-14549	-2626	-4448	1922	31.42	31.42	(4+5)-I-3	4.2
6	-12558	-7963	6550	-1121	-303	-591	31.42	31.42	(4+5)-III-1	16
7	-21691	-18769	3519	190	2547	166	31.42	31.42		2
8	-22261	-20075	3886	812	5112	-201	31.42	31.42		3
9	-22330	-22172	5648	1146	6114	-630	31.42	31.42		3
10	-21526	-23803	9215	1507	7166	-799	31.42	31.42		3
11	-19405	-22484	2853	792	6576	-410	31.42	31.42		3
12	-19756	-24210	-3652	916	6291	-253	31.42	31.42		3
13	-23196	-25699	-10325	2015	6850	983	31.42	31.42		3
14	-25116	-23694	-7277	2680	6194	679	31.42	31.42		3
15	-25288	-22960	-4659	2443	5727	521	31.42	31.42		3
16	-16125	-13038	3723	50	1462	-1105	31.42	31.42	(4+5)-I-2	11
17	-22506	-18896	2236	287	4606	-469	31.42	31.42		3
18	-23097	-22008	-1278	1015	4754	-554	31.42	31.42		3
19	-21510	-21827	-2415	939	5602	-544	31.42	31.42		3
20	-22581	-20318	-128	612	4985	-609	31.42	31.42		3
21	-22930	-22294	-3544	1353	5532	-217	31.42	31.42		3
22	-24620	-23525	-5174	1952	6013	284	31.42	31.42		3
23	-22669	-19414	544	380	3163	-817	31.42	31.42		3
24	-23652	-20712	-863	1118	3978	-530	31.42	31.42		3
25	-24234	-22466	-2815	1534	4545	-326	31.42	31.42		3
Massimi/minimi										
1							31.42			
1								31.42		
10										3.8

Muro [Platea]: 42 - Nodi: [2001-2028-2036-2004]Pann=100Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=4.188$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-37830	-16333	8196	8703	1854	-608	31.42	31.42		2
2	-33787	-15175	6698	6441	1681	-1007	31.42	31.42		1
3	-29979	-16539	7274	5392	1818	-1235	31.42	31.42		1
4	-27187	-16804	7051	4779	1766	-1341	31.42	31.42		1
5	-27076	-17632	6570	6338	2513	-1728	31.42	31.42		2

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
6	-26931	-17901	6146	7183	2910	-1896	31.42	31.42	2	3.4
7	-26750	-18072	5988	7332	3115	-1894	31.42	31.42	2	3.3
8	-26397	-18319	5821	6857	3070	-1717	31.42	31.42	3	3.6
9	-26221	-18367	5572	5759	2726	-1411	31.42	31.42	3	4.3
10	-25943	-18400	5147	4045	2013	-913	31.42	31.42	3	6.2
11	-20466	-12810	3654	2233	934	-320	31.42	31.42	(4+5) -I-4	12
12	-11915	-9571	-265	-2249	-842	737	31.42	31.42	(4+5) -III-1	9.3
13	-23484	-14197	4574	-6511	-3128	3438	31.42	31.42	2	3.0
14	-26535	-22686	5068	-5036	-1672	3348	31.42	31.42	2	3.7
15	-27714	-25176	3719	-4314	-882	3392	31.42	31.42	2	4.0
16	-29501	-24364	1398	-4082	-279	3185	31.42	31.42	2	4.3
17	-31396	-20910	-449	-3988	85	2846	31.42	31.42	2	4.6
18	-32634	-15498	-1294	-3919	199	2419	31.42	31.42	2	5.0
19	-32556	-8631	-1092	-3782	61	1899	31.42	31.42	2	5.6
20	-30061	-741	-1	-3561	-402	1299	31.42	31.42	2	6.4
21	-24050	9000	2416	-3609	-752	1029	31.42	31.42	2	6.5
22	13326	11949	11152	-4497	-1401	-795	31.42	31.42	(4+5) -V-1	4.3
23	-772	-99	1912	-2231	-989	-281	31.42	31.42	(4+5) -V-1	10
24	-8975	-3272	3566	-1042	-286	-623	31.42	31.42	(4+5) -VI-1	16
25	-27174	-10397	2339	673	1157	-880	31.42	31.42	3	14
26	-29598	-14096	3630	1983	2077	-1101	31.42	31.42	2	8.9
27	-30971	-16382	4587	3286	2908	-1147	31.42	31.42	2	7.1
28	-31972	-17762	4970	4410	3468	-1095	31.42	31.42	2	5.8
29	-32848	-18338	4881	5450	3862	-953	31.42	31.42	2	5.0
30	-33614	-18136	4584	6300	4123	-684	31.42	31.42	2	4.6
31	-34534	-17520	4327	7096	4220	-303	31.42	31.42	2	4.3
32	-36092	-16220	4296	7835	4322	152	31.42	31.42	3	4.1
33	-40606	-15476	6410	9821	3324	278	31.42	31.42	3	3.3
34	-30207	-18097	6292	6463	4063	-891	31.42	31.42	2	4.3
35	-31041	-17963	6193	7187	3986	-824	31.42	31.42	2	3.9
36	-31846	-18028	5740	6895	4163	-681	31.42	31.42	2	4.2
37	-32583	-18123	5098	6605	4207	-625	31.42	31.42	2	4.4
38	-31726	-18245	5341	5828	4110	-813	31.42	31.42	2	4.8
39	-30957	-18156	5889	6176	4169	-790	31.42	31.42	2	4.5
40	-35686	-16719	7094	8095	2972	-340	31.42	31.42	2	3.8
41	-32648	-17589	5758	7332	4093	-546	31.42	31.42	2	4.0
42	-33196	-17145	5584	7654	3973	-459	31.42	31.42	2	3.9
43	-33563	-17733	5275	7286	4157	-451	31.42	31.42	2	4.1
44	-32154	-17586	6265	7652	3881	-644	31.42	31.42	2	3.8
45	-34414	-17029	6194	8043	3567	-283	31.42	31.42	2	3.9
46	-32678	-17082	7153	7402	2544	-974	31.42	31.42	2	3.8
47	-32000	-17454	6939	7881	3109	-867	31.42	31.42	2	3.6
48	-30910	-17818	6553	7792	3504	-953	31.42	31.42	2	3.6
49	-29340	-18037	6626	7694	3209	-1371	31.42	31.42	2	3.4
50	-28054	-18036	6525	7466	3024	-1689	31.42	31.42	2	3.4
51	-30074	-17272	7304	6752	2426	-1398	31.42	31.42	2	3.8
52	-28701	-17687	6948	6955	2642	-1633	31.42	31.42	2	3.6
53	-29984	-17644	7001	7557	2890	-1330	31.42	31.42	2	3.5
54	-29972	-18005	6460	7389	3746	-1086	31.42	31.42	2	3.7
55	-29356	-18062	6461	6644	3844	-1106	31.42	31.42	2	4.0
56	-28396	-18090	6351	6750	3564	-1351	31.42	31.42	2	3.8
57	-27462	-18132	6113	6813	3290	-1585	31.42	31.42	2	3.7
58	-27704	-18141	6296	7413	3264	-1689	31.42	31.42	2	3.4
59	-28776	-18095	6470	7450	3478	-1405	31.42	31.42	2	3.5
60	-28140	-18078	6217	5490	3409	-1107	31.42	31.42	3	4.7
61	-27182	-18200	5862	5651	3044	-1307	31.42	31.42	3	4.4
62	-28883	-18082	6490	5479	3750	-920	31.42	31.42	3	4.9
63	-29732	-18657	5350	-342	1997	1205	31.42	31.42	3	9.1
64	-29775	-19652	3880	-2285	887	2211	31.42	31.42	1	7.0
65	-15126	-8812	1481	-1625	82	723	31.42	31.42	(4+5) -III-1	12
66	-28041	-17988	5902	-2718	340	1805	31.42	31.42	1	6.8
67	-28629	-18245	5469	-425	1501	803	31.42	31.42	3	13
68	-29226	-18675	5469	-470	1787	1072	31.42	31.42	3	10
69	-28859	-19683	4797	-2605	638	2187	31.42	31.42	1	6.5
70	-20729	-13253	3761	2189	1385	-324	31.42	31.42	(4+5) -I-4	12
71	-27152	-18008	5463	3916	2493	-870	31.42	31.42	3	6.4
72	-29389	-17829	6150	1448	2730	378	31.42	31.42	3	9.3
73	-21220	-13436	3808	2175	1741	-173	31.42	31.42	(4+5) -I-4	13
74	-29121	-17867	6009	1493	2546	224	31.42	31.42	3	10
75	-29202	-17558	6521	2902	3255	-210	31.42	31.42	2	8.3
76	-28922	-17890	6555	4228	3589	-620	31.42	31.42	3	6.4
77	-21757	-13138	3992	3277	2258	-374	31.42	31.42	(4+5) -I-4	8.1
78	-28228	-17792	5952	3777	2978	-688	31.42	31.42	3	6.9
79	-29040	-16801	6141	2933	3316	-512	31.42	31.42	2	7.5

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
80	-29586	-16658	5514	3136	3236	-810	31.42	31.42	2	7.1
81	-29790	-17391	5893	3928	3679	-756	31.42	31.42	2	6.5
82	-30742	-17975	5635	4817	3873	-876	31.42	31.42	2	5.5
83	-30150	-18036	6155	5248	4062	-787	31.42	31.42	2	5.2
84	-29612	-18007	6462	5468	3999	-823	31.42	31.42	2	5.0
85	-29471	-17711	6405	4207	3832	-647	31.42	31.42	2	6.4
86	-29089	-17145	6523	3010	3437	-337	31.42	31.42	2	7.6
87	-29227	-17426	6651	2988	3413	-243	31.42	31.42	2	7.9
88	-29193	-17876	6654	4344	3800	-598	31.42	31.42	3	6.3
89	-30463	-17704	3162	-1980	1063	2028	31.42	31.42	1	7.8
90	-29852	-17732	5259	-99	2138	1103	31.42	31.42	3	8.9
91	-29326	-17427	6287	1559	2883	333	31.42	31.42	3	9.0
92	-30374	-14499	2983	-1670	1104	1674	31.42	31.42	1	9.4
93	-29366	-16050	5287	164	2174	809	31.42	31.42	3	9.6
94	-28914	-16701	6298	1703	2919	138	31.42	31.42	3	9.4
95	-28507	-15742	5986	1791	2795	-184	31.42	31.42	2	9.6
96	-28344	-14989	5038	1908	2540	-598	31.42	31.42	2	9.1
97	-29040	-10768	3208	-1411	948	1189	31.42	31.42	1	12
98	-11260	-5147	2021	-1404	479	475	31.42	31.42	(4+5)-III-1	15
99	-28185	-14086	5270	375	2041	377	31.42	31.42	3	12
100	-27104	-12301	4333	546	1690	-200	31.42	31.42	3	15
Massimi/minimi										
1							31.42			
1								31.42		
13										3.0

Muro [Platea]: 43 - Nodi: [2003-2006-2029]Pann=69Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=3.386$ [(4+5)-VIII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-15108	-29607	2765	2281	3519	686	31.42	31.42	3	7.4
2	-15754	-33255	691	2704	4367	737	31.42	31.42	3	6.3
3	-17041	-34669	-1480	3069	4834	813	31.42	31.42	3	5.7
4	-18627	-34544	-3516	3390	4968	904	31.42	31.42	3	5.5
5	-19959	-33440	-5351	3769	4851	1069	31.42	31.42	3	5.4
6	-21103	-32564	-6951	3934	4482	1166	31.42	31.42	3	5.6
7	-20072	-34758	-9278	4940	4802	2127	31.42	31.42	3	4.2
8	-21703	-31468	-7472	4706	4451	1069	31.42	31.42	3	5.1
9	-21821	-30245	-6154	4283	4532	770	31.42	31.42	3	5.9
10	-21635	-29347	-5490	3731	4583	492	31.42	31.42	3	6.1
11	-20620	-28259	-4839	3088	4434	279	31.42	31.42	2	6.6
12	-19371	-27646	-4782	2423	4144	74	31.42	31.42	2	7.3
13	-17756	-26458	-5119	1657	3576	-126	31.42	31.42	2	8.3
14	-15880	-24618	-5574	877	2805	-304	31.42	31.42	2	9.7
15	-12672	-21364	-5754	56	1592	-487	31.42	31.42	1	14
16	-1125	-8695	-831	-1060	-17	-569	31.42	31.42	(4+5)-VIII-3	16
17	4223	-6312	322	-1673	-1003	-595	31.42	31.42	(4+5)-VIII-3	11
18	30176	-2974	4634	-3397	-2187	-1476	31.42	31.42	(4+5)-VIII-3	4.0
19	4334	-16535	-11806	-630	-3408	-652	31.42	31.42	3	7.1
20	-5568	-20207	-12028	-415	-3479	-720	31.42	31.42	3	7.0
21	-11244	-22316	-11047	416	-3905	-788	31.42	31.42	3	6.4
22	-15352	-23449	-8383	1085	-3867	-600	31.42	31.42	3	6.7
23	-18193	-23445	-5452	1245	-3806	-409	31.42	31.42	3	7.1
24	-19129	-22555	-1819	1330	-3750	-239	31.42	31.42	3	7.5
25	-17933	-20511	1549	1255	-3477	-54	31.42	31.42	3	8.4
26	-15481	-15866	4254	1031	-3236	48	31.42	31.42	3	8.7
27	-1597	8004	-4289	-361	-2612	992	31.42	31.42	(4+5)-III-4	6.6
28	-14970	-14906	6653	1164	292	384	31.42	31.42	1	18
29	-15085	-23381	4590	1781	2198	626	31.42	31.42	3	11
30	-3923	-10517	-1421	510	-819	-465	31.42	31.42	(4+5)-I-3	21
31	-3094	-8081	-603	164	-803	-493	31.42	31.42	(4+5)-I-3	21
32	-10111	-22510	-4839	885	557	-339	31.42	31.42	1	22
33	-1447	-9970	-2164	208	-1407	-548	31.42	31.42	(4+5)-I-3	14
34	-9894	-23341	-7993	867	-2193	-288	31.42	31.42	3	12
35	-12369	-24789	-6411	1417	-1709	-181	31.42	31.42	3	16
36	-10633	-23998	-5851	1287	-627	-240	31.42	31.42	2	18
37	-11762	-24995	-4444	1709	866	-242	31.42	31.42	2	14
38	-13251	-27147	-3155	2470	1975	36	31.42	31.42	2	11

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
39	-12802	-25811	-3299	2028	783	-154	31.42	31.42	1	13
40	-13272	-26894	-3145	2274	970	6	31.42	31.42	2	12
41	-13874	-25676	-2862	2059	-136	-102	31.42	31.42	1	13
42	-13003	-25306	-4282	1718	-832	-188	31.42	31.42	1	15
43	-14951	-24695	-3548	1773	-1739	-166	31.42	31.42	1	15
44	-13429	-27246	-2591	2380	1365	144	31.42	31.42	3	11
45	-13819	-27807	-1691	2564	2171	323	31.42	31.42	3	9.8
46	-13978	-28023	-2574	2692	2529	213	31.42	31.42	3	9.7
47	-14484	-28258	-126	2540	3000	453	31.42	31.42	2	9.0
48	-15677	-24309	-1786	1847	-1584	-78	31.42	31.42	1	15
49	-13899	-26040	-2290	2162	187	73	31.42	31.42	2	13
50	-13664	-26038	-1226	2186	783	201	31.42	31.42	3	12
51	-13936	-24988	872	2060	1543	340	31.42	31.42	3	12
52	-14713	-23532	-286	1830	-1133	35	31.42	31.42	3	15
53	-13677	-20408	1784	1653	-448	57	31.42	31.42	3	16
54	-12472	-22986	-4163	957	1593	-379	31.42	31.42	1	15
55	-13510	-25116	-3287	1920	2171	-203	31.42	31.42	1	13
56	-14957	-27478	-3764	1634	2740	-250	31.42	31.42	1	10
57	-18551	-27558	-4092	2873	4187	154	31.42	31.42	2	7.1
58	-16849	-26525	-4148	2251	3542	-50	31.42	31.42	2	8.5
59	-16880	-27337	-3462	2886	3813	160	31.42	31.42	2	7.8
60	-14663	-27065	-3226	2589	2941	49	31.42	31.42	2	10
61	-15713	-30129	-1239	2958	3980	550	31.42	31.42	2	6.9
62	-15337	-28536	-2486	2996	3537	319	31.42	31.42	2	8.0
63	-17539	-31379	-2565	3394	4620	666	31.42	31.42	3	6.0
64	-17412	-28917	-3055	3308	4296	408	31.42	31.42	2	6.6
65	-19642	-28425	-4223	3351	4487	350	31.42	31.42	2	6.4
66	-19163	-29200	-3720	3581	4604	510	31.42	31.42	2	6.1
67	-20623	-29724	-4757	3784	4695	559	31.42	31.42	3	6.0
68	-19274	-31503	-3821	3709	4850	757	31.42	31.42	3	5.6
69	-20618	-31257	-5047	4030	4765	829	31.42	31.42	3	5.6
Massimi/minimi										
1							31.42			
1								31.42		
18										4.0

Muro [Platea]: 44 - Nodi: [2006-2033-2029]Pann=23Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45,ζ_e=3.300 [(4+5)-III-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-34560	-12154	-7548	3422	1984	-2218	31.42	31.42	3	5.7
2	-40909	-12255	-3238	4056	2073	-1839	31.42	31.42	3	5.7
3	-44059	-13589	1723	4385	2060	-1522	31.42	31.42	3	5.8
4	-46006	-14756	6150	4223	1869	-1275	31.42	31.42	3	6.2
5	-44633	-16631	10365	4064	1588	-1015	31.42	31.42	3	6.7
6	-40078	-18842	13519	3693	1320	-711	31.42	31.42	3	7.5
7	-34099	-21118	16802	3049	876	-491	31.42	31.42	3	9.1
8	-30500	-21947	11303	3447	1819	-1112	31.42	31.42	3	6.9
9	-31040	-21173	9298	3705	2700	-1558	31.42	31.42	3	6.0
10	-32439	-19489	9644	3915	3085	-2062	31.42	31.42	3	5.3
11	-31907	-21780	8493	4143	3767	-1435	31.42	31.42	3	5.7
12	-34262	-20855	8258	4413	3202	-1260	31.42	31.42	3	5.7
13	-37432	-18603	6327	4662	2962	-1182	31.42	31.42	3	5.6
14	-39044	-16249	3384	4606	2718	-1133	31.42	31.42	3	5.8
15	-37201	-14356	-464	4218	2503	-1128	31.42	31.42	3	6.1
16	-32799	-12773	-4150	3472	2221	-1193	31.42	31.42	3	6.8
17	-24768	-12391	-7778	2360	1778	-1351	31.42	31.42	3	8.2
18	-12331	-14187	-9681	786	1055	-1617	31.42	31.42	3	11
19	28368	-9880	-8236	-2686	-353	-1878	31.42	31.42	(4+5)-III-4	4.3
20	-10124	-13052	-12982	906	924	-2813	31.42	31.42	3	7.4
21	-25035	-12246	-10877	2432	1701	-2606	31.42	31.42	3	6.0
22	-36635	-20067	10610	4198	2318	-1175	31.42	31.42	3	6.1
23	-40931	-17765	8178	4524	2235	-1192	31.42	31.42	3	5.8
Massimi/minimi										
1							31.42			
1								31.42		
19										4.3

Muro [Platea]: 45 - Nodi: [2006-2038-2033]Pann=22Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=4.178$ [(4+5)-III-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-48463	-12406	5826	4341	1235	-736	31.42	31.42	3	6.9
2	-50657	-11935	5470	4393	1146	-393	31.42	31.42	3	7.4
3	-49820	-11858	5240	4195	1139	-64	31.42	31.42	3	8.2
4	-44756	-12630	3802	3662	1192	286	31.42	31.42	1	8.6
5	-37523	-13592	3632	2956	1243	444	31.42	31.42	1	9.6
6	-26778	-14774	3378	2035	1282	522	31.42	31.42	1	12
7	-11263	-15505	1325	669	1028	497	31.42	31.42	1	19
8	25910	-7882	3863	-2144	657	-336	31.42	31.42	(4+5)-III-4	8.1
9	-14725	-9667	4238	1204	759	-756	31.42	31.42	(4+5)-V-2	14
10	-26995	-12118	1862	2274	919	-994	31.42	31.42	3	9.4
11	-38288	-12588	2586	3212	910	-1012	31.42	31.42	3	7.8
12	-45874	-12201	3165	3905	869	-916	31.42	31.42	3	7.1
13	-50185	-11727	4229	4307	847	-752	31.42	31.42	3	6.9
14	-51417	-11558	5686	4446	853	-576	31.42	31.42	3	7.0
15	-49745	-11779	7335	4321	841	-427	31.42	31.42	3	7.4
16	-43715	-11734	9230	3838	893	-215	31.42	31.42	3	8.4
17	-37240	-12059	8435	2780	929	-257	31.42	31.42	3	11
18	-39651	-11876	7678	2328	1040	-457	31.42	31.42	3	12
19	-39462	-13275	7238	1247	854	-382	31.42	31.42	3	20
20	-38452	-12415	7659	2927	907	-1493	31.42	31.42	3	7.4
21	-42033	-12610	5218	3776	1124	-818	31.42	31.42	3	7.3
22	-41900	-11372	7306	3625	1037	-725	31.42	31.42	3	7.7
Massimi/minimi										
1							31.42			
1								31.42		
1										6.9

Muro [Platea]: 46 - Nodi: [2006-2044-2038]Pann=42Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=5.073$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-38124	-20765	-17349	3859	1552	1474	31.42	31.42	3	6.2
2	-40677	-19650	-17350	3810	1888	1590	31.42	31.42	3	6.2
3	-42523	-17185	-15943	3423	2146	1588	31.42	31.42	3	6.7
4	-41566	-14012	-13618	2826	2135	1470	31.42	31.42	2	7.8
5	-39734	-10803	-9687	2240	1979	1295	31.42	31.42	2	8.4
6	-33146	-8820	-5155	1376	1446	837	31.42	31.42	1	12
7	-22647	-5884	1290	469	1078	652	31.42	31.42	1	15
8	12563	-2	10454	-1706	-235	-1149	31.42	31.42	(4+5)-I-3	8.0
9	-18381	-10816	-5161	1629	-778	-837	31.42	31.42	3	12
10	-28134	-15028	-11013	2105	-268	-130	31.42	31.42	3	14
11	-32794	-18674	-14115	2802	249	244	31.42	31.42	3	10
12	-36138	-19698	-15201	3190	704	663	31.42	31.42	3	8.4
13	-38192	-19850	-15139	3399	1118	997	31.42	31.42	3	7.5
14	-38726	-19390	-14586	3555	1583	1316	31.42	31.42	3	6.8
15	-38033	-18350	-14067	3517	1959	1616	31.42	31.42	3	6.4
16	-36649	-17145	-13962	3309	2183	1798	31.42	31.42	3	6.4
17	-35554	-15487	-14603	2732	2000	1599	31.42	31.42	3	7.5
18	-32219	-13463	-13378	2772	1852	1523	31.42	31.42	3	7.4
19	-30490	-11561	-12084	1768	808	664	31.42	31.42	3	13
20	-35931	-14388	-15250	1726	410	559	31.42	31.42	3	14
21	-37094	-16200	-15418	2023	745	705	31.42	31.42	3	12
22	-35020	-17095	-14457	2400	891	728	31.42	31.42	3	10
23	-36304	-19865	-16281	3345	1255	1228	31.42	31.42	3	7.1
24	-36696	-14887	-11020	3211	1384	1260	31.42	31.42	3	7.3
25	-31449	-13898	-8977	2663	673	886	31.42	31.42	3	8.9
26	-34425	-17292	-12411	3211	1022	1119	31.42	31.42	3	7.4

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
27	-39741	-18137	-14431	3859	1992	1629	31.42	31.42		3 6.0
28	-38865	-16533	-13169	3567	1772	1470	31.42	31.42		3 6.6
29	-37430	-18457	-13459	3833	1865	1542	31.42	31.42		3 6.1
30	-36283	-19172	-13694	3637	1488	1377	31.42	31.42		3 6.5
31	-39059	-19055	-15286	4035	2025	1698	31.42	31.42		3 5.8
32	-37606	-19204	-14334	4037	2078	1678	31.42	31.42		3 5.7
33	-37515	-19552	-14678	3895	1859	1608	31.42	31.42		3 6.0
34	-37044	-19518	-14484	4004	2027	1667	31.42	31.42		3 5.8
35	-37180	-19895	-14344	3843	1660	1507	31.42	31.42		3 6.1
36	-35956	-17351	-14667	3438	1985	1651	31.42	31.42		3 6.4
37	-37146	-18659	-14841	3828	2052	1707	31.42	31.42		3 5.9
38	-37432	-18952	-14760	4031	2061	1700	31.42	31.42		3 5.7
39	-38125	-19165	-15490	4016	1938	1685	31.42	31.42		3 5.8
40	-37011	-17358	-15753	3375	1755	1542	31.42	31.42		3 6.6
41	-37160	-18930	-14868	3926	2092	1722	31.42	31.42		3 5.8
42	-36943	-18562	-14935	3728	1732	1565	31.42	31.42		3 6.2
Massimi/minimi										
1							31.42			
1								31.42		
38										5.7

Muro [Platea]: 47 - Nodi: [2009-2050-2044]Pann=27Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=3.802$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-33607	-12591	-4541	3270	668	1025	31.42	31.42		2 7.5
2	-35183	-16756	-8607	4120	990	1250	31.42	31.42		2 6.0
3	-33276	-19234	-10458	4708	1265	1250	31.42	31.42		3 5.4
4	-29480	-20944	-11515	5037	1527	1136	31.42	31.42		3 5.1
5	-25324	-21419	-11102	5050	1483	837	31.42	31.42		3 5.2
6	-22830	-22163	-10630	4832	1602	712	31.42	31.42		1 5.4
7	-21526	-18960	-9558	4618	1172	350	31.42	31.42		1 6.0
8	-21618	-20594	-10623	4403	795	299	31.42	31.42		1 6.3
9	-19582	-23364	-13336	4128	622	275	31.42	31.42		1 6.7
10	-20085	-25157	-23211	3983	-704	-629	31.42	31.42		3 6.4
11	-29105	-23378	-22084	4051	-764	-73	31.42	31.42		3 7.6
12	-36074	-24017	-20081	4134	-224	706	31.42	31.42		1 6.7
13	-40253	-18998	-17555	4363	16	910	31.42	31.42		3 6.3
14	-41828	-15828	-13207	4061	395	1328	31.42	31.42		3 6.2
15	-40447	-13447	-8351	3632	666	1640	31.42	31.42		2 6.3
16	-37843	-9563	-2653	2709	885	1834	31.42	31.42		2 7.2
17	-29691	-8351	2559	1364	1119	1992	31.42	31.42		1 8.7
18	-16002	-6109	6552	-349	759	2092	31.42	31.42		1 9.4
19	24040	-280	4374	-3301	-198	1330	31.42	31.42	(4+5)-VII-3	4.4
20	-18745	-2802	217	799	-181	650	31.42	31.42	(4+5)-III-1	20
21	-28412	-9223	-326	2071	317	873	31.42	31.42		2 11
22	-27000	-21726	-14425	4797	987	880	31.42	31.42		3 5.4
23	-27244	-25572	-16178	4292	588	906	31.42	31.42		1 5.9
24	-31729	-22044	-16939	4559	424	960	31.42	31.42		3 5.7
25	-34947	-20560	-15714	4652	566	1183	31.42	31.42		3 5.5
26	-35581	-19382	-13224	4686	823	1309	31.42	31.42		3 5.4
27	-31488	-20813	-13490	4871	1083	1157	31.42	31.42		3 5.2
Massimi/minimi										
1							31.42			
1								31.42		
19										4.4

Muro : 48 - Nodi: [4-3-2-5], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45, $\zeta_e=32.650$ [(4+5)-III-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
1	-1386	3792	9155	86	317	-92	20.11	20.11		16
2	-8317	3807	10272	170	453	65	20.11	20.11		13
3	-10975	3007	10779	200	342	33	20.11	20.11		18
4	-11228	1908	10850	202	167	31	20.11	20.11		35
5	-3674	3670	9393	58	281	-26	20.11	20.11		22
6	-8962	3452	10998	151	423	139	20.11	20.11		12
7	-11062	2951	11468	193	324	98	20.11	20.11		16
8	-11318	2630	11352	196	163	78	20.11	20.11		28
9	-6047	1729	9394	-52	278	10	20.11	20.11		24
10	-9963	1713	11273	-22	376	173	20.11	20.11		13
11	-11280	2266	11591	-16	266	116	20.11	20.11		18
12	-11252	2621	11505	-23	117	78	20.11	20.11		35
13	-3851	-4087	6939	-83	-215	-136	20.11	20.11		21
14	-9936	-1972	10147	-345	247	-33	20.11	20.11		21
15	-11202	280	10841	-438	160	-119	20.11	20.11		15
16	-11305	2459	11043	-475	40	-158	20.11	20.11		13
Massimi/minimi										
1							20.11			
1								20.11		
6										12

Muro : 49 - Nodi: [6-4-5-7], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=13.887$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	1531	3595	6792	-10	455	-193	20.11	20.11		10
2	-7891	1781	6754	-215	382	-89	20.11	20.11		15
3	-11071	226	6932	-372	219	-99	20.11	20.11		17
4	-11333	-1180	6976	-462	48	-96	20.11	20.11		15
5	-373	4447	8006	89	339	-166	20.11	20.11		13
6	-7312	3492	8318	65	405	-1	20.11	20.11		17
7	-10721	1916	8050	19	277	29	20.11	20.11		23
8	-8119	552	6848	2	121	48	20.11	20.11	(4+5)-II-2	42
9	-1501	4737	8555	100	309	-140	20.11	20.11		15
10	-7671	4105	9172	165	439	20	20.11	20.11		15
11	-10810	2984	9235	190	320	31	20.11	20.11		19
12	-11574	1482	9146	179	153	56	20.11	20.11		33
13	-3167	4419	8758	104	259	-118	20.11	20.11		18
14	-8086	3528	9673	150	426	32	20.11	20.11		15
15	-10839	2820	10087	189	329	8	20.11	20.11		20
16	-11762	2233	10173	192	167	18	20.11	20.11		37
Massimi/minimi										
1							20.11			
1								20.11		
1										10

Muro : 50 - Nodi: [8-6-7-9], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=34.707$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	5464	-1210	4688	-82	-386	63	20.11	20.11		16
2	-6829	2097	5195	100	422	123	20.11	20.11		13
3	-11716	805	5168	172	446	74	20.11	20.11		13
4	-13471	-335	4458	224	318	6	20.11	20.11		22
5	3600	-1272	4875	-148	-351	62	20.11	20.11		17
6	-7154	2196	6266	70	400	190	20.11	20.11		12
7	-11288	1158	6128	144	394	137	20.11	20.11		13
8	-12750	75	5297	190	261	65	20.11	20.11		22
9	1676	-1944	5173	-147	-276	54	20.11	20.11		22
10	-7783	892	6800	-53	368	224	20.11	20.11		12
11	-11024	604	6761	-38	315	161	20.11	20.11		15

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
12	-12101	-138	6125	-31	178	85	20.11	20.11	3	27
13	-113	-2885	5106	-33	-278	-43	20.11	20.11	1	23
14	-7610	-2115	6401	-266	281	50	20.11	20.11	3	22
15	-10615	-1191	6797	-400	215	-26	20.11	20.11	3	19
16	-11623	-630	6649	-467	85	-81	20.11	20.11	3	15
Massimi/minimi										
1							20.11			
1								20.11		
6										12

Muro : 51 - Nodi: [10-8-9-11], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_s=14.887$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	6992	-3813	380	260	-415	47	20.11	20.11	1	16
2	-5731	-5765	-676	107	429	-92	20.11	20.11	3	15
3	-10262	-9266	-297	183	550	-76	20.11	20.11	3	13
4	-12986	-19200	3631	621	1214	-254	20.11	20.11	1	6.0
5	6239	-4233	2062	14	-485	57	20.11	20.11	1	14
6	-6079	-1572	1529	225	465	-80	20.11	20.11	3	13
7	-11567	-4019	2259	351	577	-53	20.11	20.11	3	12
8	-11802	-8593	3118	409	589	-111	20.11	20.11	1	11
9	5306	-3235	3194	-77	-504	91	20.11	20.11	1	12
10	-6351	720	3021	216	462	26	20.11	20.11	3	14
11	-11697	-721	3341	349	562	-2	20.11	20.11	3	13
12	-14080	-1755	3186	416	476	-70	20.11	20.11	3	13
13	4284	-1715	3889	-85	-476	92	20.11	20.11	1	13
14	-6676	1524	4054	140	429	92	20.11	20.11	3	13
15	-11587	132	4258	230	502	36	20.11	20.11	3	13
16	-13567	-813	3821	293	397	-38	20.11	20.11	3	16
Massimi/minimi										
1							20.11			
1								20.11		
4										6.0

Muro : 52 - Nodi: [12-10-11-13], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_s=13.020$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	1983	-2341	-8367	-37	-441	-64	20.11	20.11	1	14
2	-7493	909	-10079	103	574	-230	20.11	20.11	3	8.7
3	-10908	-1011	-10761	115	687	-190	20.11	20.11	3	8.2
4	-7740	-6402	-11606	79	1137	-5	20.11	20.11	1	6.7
5	4749	-3483	-7285	-5	-449	-43	20.11	20.11	1	15
6	-6373	54	-8988	212	579	-196	20.11	20.11	3	9.1
7	-10686	-1988	-9751	281	724	-216	20.11	20.11	3	7.7
8	-8659	-7851	-10553	259	1266	-77	20.11	20.11	1	5.8
9	7103	-3988	-5889	102	-430	16	20.11	20.11	1	17
10	-5496	-1925	-6990	240	534	-111	20.11	20.11	3	11
11	-10454	-5564	-7714	341	690	-214	20.11	20.11	3	8.4
12	-9421	-12373	-9098	463	1466	-178	20.11	20.11	1	5.0
13	8729	-2838	-4113	290	-321	56	20.11	20.11	1	18
14	-5470	-5359	-3738	117	468	-25	20.11	20.11	3	15
15	-9636	-10346	-3831	145	568	-118	20.11	20.11	3	12
16	-10051	-22358	-6150	691	1666	-196	20.11	20.11	1	4.9
Massimi/minimi										
1							20.11			
1								20.11		
16										4.9

Muro : 53 - Nodi: [14-12-13-15], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=---,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=20.844$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-5275	-5111	-9454	-112	-301	106	20.11	20.11	1	19
2	-10088	-1804	-10450	-404	307	-25	20.11	20.11	2	19
3	-11661	1514	-11174	-509	316	49	20.11	20.11	3	15
4	-5334	892	-11368	-338	774	191	20.11	20.11	1	7.3
5	-5036	989	-10586	-114	289	-51	20.11	20.11	3	21
6	-9757	810	-12773	-118	460	-240	20.11	20.11	3	10
7	-7486	-1355	-11908	-95	374	-159	20.11	20.11	1	14
8	-8494	-927	-11406	-98	740	91	20.11	20.11	1	8.6
9	1428	-2761	-9999	-120	-306	-56	20.11	20.11	1	20
10	-8689	1933	-12617	18	517	-236	20.11	20.11	3	9.2
11	-11449	890	-13104	4	512	-135	20.11	20.11	3	11
12	-10389	-2416	-11398	-12	814	55	20.11	20.11	1	8.4
13	4459	-3062	-9574	-71	-345	-48	20.11	20.11	1	19
14	-7608	750	-11344	50	556	-218	20.11	20.11	3	9.1
15	-11879	-404	-11828	12	576	-155	20.11	20.11	3	9.7
16	-12663	-4616	-11680	27	907	37	20.11	20.11	1	8.0
Massimi/minimi										
1							20.11			
1								20.11		
4										7.3

Muro : 54 - Nodi: [16-14-15-17], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=---,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=35.869$ [(4+5)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-7964	5495	-13072	131	475	277	20.11	20.11	3	8.7
2	-10509	5488	-14214	130	478	85	20.11	20.11	3	12
3	-10902	5601	-13955	99	316	121	20.11	20.11	3	15
4	-3620	2529	-10372	-177	131	89	20.11	20.11	1	28
5	-5357	5175	-13240	141	554	292	20.11	20.11	3	7.8
6	-9915	4749	-14392	128	492	66	20.11	20.11	3	12
7	-11919	4556	-14284	49	283	55	20.11	20.11	3	20
8	-8301	599	-10183	-201	96	10	20.11	20.11	1	37
9	-3288	4373	-12628	104	585	293	20.11	20.11	3	7.6
10	-9437	3239	-13409	-17	447	32	20.11	20.11	3	14
11	-12562	997	-13633	-152	222	1	20.11	20.11	3	31
12	-15097	1297	-11015	-221	-77	-87	20.11	20.11	3	27
13	99	2780	-10859	-126	710	319	20.11	20.11	3	6.6
14	-9604	190	-10989	-360	406	119	20.11	20.11	3	13
15	-12649	-2369	-10924	-571	87	103	20.11	20.11	3	12
16	-21669	-4284	-12242	-428	-312	55	20.11	20.11	3	19
Massimi/minimi										
1							20.11			
1								20.11		
13										6.6

Muro : 55 - Nodi: [18-16-17-19], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=---,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=13.944$ [(4+5)-III-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-8367	-1510	-8604	-155	-259	212	20.11	20.11	1	15
2	-11795	3394	-9916	-302	184	108	20.11	20.11	3	20
3	-11372	7522	-10176	-297	109	174	20.11	20.11	3	17

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
4	-6889	8929	-6327	-258	15	101	20.11	20.11	(4+5)-III-1	22
5	-10314	4317	-10990	-6	341	115	20.11	20.11	3	15
6	-11952	5939	-12474	69	322	-20	20.11	20.11	3	19
7	-11010	8573	-12882	120	183	67	20.11	20.11	3	25
8	-142	5560	-10418	203	-30	101	20.11	20.11	1	23
9	-8044	5486	-12071	121	409	176	20.11	20.11	3	11
10	-11166	6901	-13468	219	402	23	20.11	20.11	3	15
11	-10995	7855	-13993	256	252	111	20.11	20.11	3	18
12	-7748	8469	-13336	282	55	132	20.11	20.11	3	19
13	-5465	4381	-12677	109	488	251	20.11	20.11	3	9.0
14	-10521	6002	-13814	181	457	74	20.11	20.11	3	12
15	-11485	7209	-13795	152	263	136	20.11	20.11	3	16
16	-11207	7590	-13423	163	42	189	20.11	20.11	3	23
Massimi/minimi										
1							20.11			
1								20.11		
13										9.0

Muro : 56 - Nodi: [20-18-19-21], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\xi_e=31.384$ [(4+5)-IV-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-11658	4405	-7376	209	427	123	20.11	20.11	3	12
2	-12241	4651	-7725	275	400	-8	20.11	20.11	3	16
3	-11878	5619	-8155	303	278	3	20.11	20.11	3	23
4	-10479	6587	-7891	289	153	-21	20.11	20.11	3	26
5	-11028	5244	-7151	271	465	183	20.11	20.11	3	10
6	-11961	6022	-8281	325	402	15	20.11	20.11	3	16
7	-11881	6443	-8539	341	261	-16	20.11	20.11	3	23
8	-11081	6965	-8118	314	121	-61	20.11	20.11	3	22
9	-8683	5213	-7948	146	456	240	20.11	20.11	3	9.5
10	-11291	6171	-8486	188	337	34	20.11	20.11	3	18
11	-11838	6528	-8597	151	202	-21	20.11	20.11	3	29
12	-11974	7399	-8636	124	59	-67	20.11	20.11	3	43
13	-6893	5448	-8017	-173	546	313	20.11	20.11	3	7.7
14	-11912	6239	-8300	-254	275	146	20.11	20.11	3	15
15	-11691	6806	-8390	-288	101	133	20.11	20.11	3	19
16	-12741	7741	-9677	-285	-89	69	20.11	20.11	3	23
Massimi/minimi										
1							20.11			
1								20.11		
13										7.7

Muro : 57 - Nodi: [22-20-21-23], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\xi_e=33.056$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-15108	-1079	-5016	-312	226	42	20.11	20.11	3	24
2	-13398	1329	-5112	-425	176	33	20.11	20.11	3	18
3	-12403	3809	-5499	-460	111	93	20.11	20.11	3	15
4	-10694	6337	-5717	-424	56	119	20.11	20.11	3	15
5	-13062	2417	-5515	15	386	-30	20.11	20.11	3	16
6	-13435	3315	-6521	18	298	-88	20.11	20.11	3	18
7	-12393	4926	-6616	-6	204	-21	20.11	20.11	3	29
8	-10299	6364	-6738	-24	122	8	20.11	20.11	3	50
9	-11649	3460	-6057	170	430	7	20.11	20.11	3	15
10	-12867	4367	-7011	236	370	-85	20.11	20.11	3	15
11	-12100	5259	-7306	230	263	-32	20.11	20.11	3	22
12	-10053	6242	-7339	192	157	-15	20.11	20.11	3	38
13	-10107	3162	-6549	163	463	80	20.11	20.11	3	13
14	-12445	4574	-7322	257	413	-42	20.11	20.11	3	15

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
15	-11981	5330	-7660	265	285	-4	20.11	20.11	3	23
16	-9970	5822	-7640	241	157	-8	20.11	20.11	3	32
Massimi/minimi										
1							20.11			
1								20.11		
13										13

Muro : 58 - Nodi: [24-22-23-25], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=33.340$ [(4+5)-I-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-13252	3822	-2252	194	494	58	20.11	20.11	3	12
2	-13568	5209	-2429	260	414	29	20.11	20.11	3	15
3	-12438	6668	-2460	259	290	18	20.11	20.11	3	21
4	-10001	8065	-2375	220	181	10	20.11	20.11	3	33
5	-12809	4468	-2949	233	513	113	20.11	20.11	3	11
6	-13461	5629	-3179	273	393	38	20.11	20.11	3	15
7	-12487	6827	-3152	244	270	-6	20.11	20.11	3	23
8	-10108	8021	-2997	184	169	-35	20.11	20.11	3	31
9	-12375	4239	-3502	104	487	150	20.11	20.11	3	10
10	-13323	5200	-3719	81	320	32	20.11	20.11	3	19
11	-12511	6275	-3730	25	213	-28	20.11	20.11	3	27
12	-10233	7563	-3663	-23	126	-62	20.11	20.11	3	34
13	-11385	2938	-3652	-311	467	180	20.11	20.11	3	11
14	-13602	4100	-4068	-386	251	78	20.11	20.11	3	18
15	-12651	5207	-4372	-443	140	74	20.11	20.11	3	16
16	-10237	6559	-4547	-417	67	63	20.11	20.11	3	17
Massimi/minimi										
1							20.11			
1								20.11		
9										10

Muro : 59 - Nodi: [26-24-25-27], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=26.070$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-13236	2225	834	-298	390	-125	20.11	20.11	3	13
2	-13885	4238	1155	-382	211	-39	20.11	20.11	3	20
3	-12697	6167	1179	-406	112	-8	20.11	20.11	3	20
4	-10320	8220	1122	-345	46	18	20.11	20.11	3	22
5	-13257	4227	329	120	468	-123	20.11	20.11	3	11
6	-13715	5499	124	123	315	-40	20.11	20.11	3	19
7	-12598	7084	68	92	208	32	20.11	20.11	3	27
8	-10174	8710	-74	69	124	75	20.11	20.11	3	32
9	-13119	4566	-516	256	505	-69	20.11	20.11	3	12
10	-13622	5963	-666	321	398	-34	20.11	20.11	3	15
11	-12487	7328	-799	309	275	17	20.11	20.11	3	22
12	-9975	8670	-946	261	172	52	20.11	20.11	3	26
13	-12932	3894	-1388	204	505	9	20.11	20.11	3	13
14	-13583	5496	-1507	285	426	-1	20.11	20.11	3	15
15	-12441	6992	-1604	288	297	18	20.11	20.11	3	20
16	-9916	8333	-1675	251	186	30	20.11	20.11	3	28
Massimi/minimi										
1							20.11			
1								20.11		
5										11

Muro : 60 - Nodi: [28-26-27-29], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=---,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=24.806$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-11632	3899	5328	197	510	-95	20.11	20.11		3
2	-13229	5623	5852	286	433	-9	20.11	20.11		3
3	-12487	7010	6113	294	297	-41	20.11	20.11		3
4	-10038	6572	5963	265	177	-47	20.11	20.11		2
5	-12644	4485	4525	230	482	-11	20.11	20.11		3
6	-13471	5896	5094	309	395	35	20.11	20.11		3
7	-12551	7332	5292	310	275	-24	20.11	20.11		3
8	-10357	8914	5322	276	170	-54	20.11	20.11		3
9	-13495	3804	3604	78	432	47	20.11	20.11		3
10	-13832	5227	4213	103	312	49	20.11	20.11		3
11	-12680	7155	4223	89	209	-27	20.11	20.11		3
12	-10440	9082	4204	84	126	-68	20.11	20.11		3
13	-10207	1727	-274	-231	282	70	20.11	20.11	(4+5)-II-4	20
14	-13824	3542	2678	-392	193	-3	20.11	20.11		3
15	-12675	6182	2763	-408	113	-48	20.11	20.11		3
16	-10577	8929	2720	-338	60	-68	20.11	20.11		3
Massimi/minimi										
1							20.11			
1								20.11		
1										11

Muro : 61 - Nodi: [30-28-29-31], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=---,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=23.557$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-8339	4330	7044	-240	588	-291	20.11	20.11		3
2	-12957	4779	7637	-357	308	-154	20.11	20.11		3
3	-12599	5240	8086	-436	151	-173	20.11	20.11		3
4	-10413	5943	8266	-436	41	-167	20.11	20.11		3
5	-10393	5034	7310	137	531	-238	20.11	20.11		3
6	-12463	5738	7824	105	352	-48	20.11	20.11		3
7	-11806	4963	7229	39	212	-12	20.11	20.11		2
8	-10602	7210	7693	-16	107	32	20.11	20.11		3
9	-11466	5002	6878	237	534	-198	20.11	20.11		3
10	-12819	6054	7455	281	415	-50	20.11	20.11		3
11	-12436	7022	7476	257	272	-19	20.11	20.11		3
12	-10554	7844	7324	203	154	13	20.11	20.11		3
13	-12699	4321	6160	199	489	-146	20.11	20.11		3
14	-13103	5472	6716	262	423	-43	20.11	20.11		3
15	-12428	6875	6908	270	291	-47	20.11	20.11		3
16	-10392	6676	6541	239	176	-37	20.11	20.11		2
Massimi/minimi										
1							20.11			
1								20.11		
1										7.6

Muro : 62 - Nodi: [32-30-31-33], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=---,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=24.748$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-7047	3468	9613	123	466	-127	20.11	20.11		3
2	-11365	4461	10793	205	456	26	20.11	20.11		3
3	-11971	4830	11373	211	317	-34	20.11	20.11		3
4	-10607	4942	11554	191	164	-52	20.11	20.11		3
5	-9296	3563	9387	119	417	-58	20.11	20.11		3
6	-11932	4193	10807	185	401	84	20.11	20.11		3

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
7	-12062	4820	11199	189	283	17	20.11	20.11	3	22
8	-10843	5766	11197	168	151	-14	20.11	20.11	3	40
9	-11368	2015	8932	-29	373	-26	20.11	20.11	3	17
10	-12730	2842	10418	-20	328	90	20.11	20.11	3	16
11	-12327	4508	10523	-34	217	15	20.11	20.11	3	29
12	-10923	5986	10512	-39	108	-25	20.11	20.11	3	49
13	-7575	-3818	6703	-154	-216	-163	20.11	20.11	1	20
14	-12538	226	8683	-420	191	-92	20.11	20.11	3	16
15	-12174	3222	9229	-470	116	-174	20.11	20.11	3	13
16	-11191	6152	9394	-447	40	-208	20.11	20.11	3	12
Massimi/minimi										
1							20.11			
1								20.11		
1										11

Muro : 63 - Nodi: [3-32-33-2], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=29.956$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-3000	4565	9178	-98	631	-294	20.11	20.11	3	7.2
2	-10502	3734	9731	-266	397	-140	20.11	20.11	3	13
3	-11694	2918	10227	-394	210	-162	20.11	20.11	3	15
4	-10642	2337	10476	-461	46	-159	20.11	20.11	3	13
5	-5477	5074	10131	157	506	-237	20.11	20.11	3	8.9
6	-9911	4887	10832	132	421	-16	20.11	20.11	3	15
7	-11500	4261	10791	67	270	19	20.11	20.11	3	23
8	-10854	3806	10777	-7	114	50	20.11	20.11	3	41
9	-6968	4984	10211	197	484	-195	20.11	20.11	3	9.7
10	-10465	5181	11134	258	466	-6	20.11	20.11	3	14
11	-11621	5049	11367	255	316	1	20.11	20.11	3	21
12	-10934	4603	11329	211	158	24	20.11	20.11	3	35
13	-8920	4239	9883	156	413	-153	20.11	20.11	3	12
14	-11008	4250	10980	208	441	0	20.11	20.11	3	15
15	-11707	4643	11522	230	315	-39	20.11	20.11	3	19
16	-11103	5222	11669	210	168	-40	20.11	20.11	3	32
Massimi/minimi										
1							20.11			
1								20.11		
1										7.2

Muro : 64 - Nodi: [5-2-2079-2077], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=5.354$ [(4+5)-VI-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-10827	954	9422	181	-7	43	20.11	20.11	2	36
2	-11485	899	8866	174	-28	36	20.11	20.11	2	39
3	-13799	-319	6814	186	477	8	20.11	20.11	1	15
4	-12140	50	6185	350	1649	-214	20.11	20.11	1	3.8
5	-10756	2348	10965	181	10	70	20.11	20.11	3	32
6	-9273	-200	7273	131	-62	98	20.11	20.11	1	35
7	-12823	1520	6353	237	414	1	20.11	20.11	1	17
8	-10874	2676	6155	360	1594	-237	20.11	20.11	1	3.7
9	-5907	-213	8225	-61	-114	116	20.11	20.11	1	31
10	-8383	493	6806	-35	-95	125	20.11	20.11	1	32
11	-12005	1950	5191	89	279	33	20.11	20.11	1	22
12	-11253	4127	6560	241	1548	-272	20.11	20.11	1	3.7
13	-10122	4114	10410	-471	-61	-142	20.11	20.11	3	13
14	-9402	4981	7952	-467	-103	-87	20.11	20.11	2	14
15	-10079	5649	6156	-393	79	-41	20.11	20.11	2	18
16	-12352	587	5578	-160	1482	-257	20.11	20.11	1	4.0
Massimi/minimi										

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
1							20.11			
1								20.11		
12										3.7

Muro : 65 - Nodi: [7-5-2077-2075], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=8.071$ [(4+5)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-10530	-2747	6785	-478	-79	-87	20.11	20.11		3 14
2	-10336	-5753	6085	-447	-57	-82	20.11	20.11		2 15
3	-13015	-12572	5897	-305	505	-67	20.11	20.11		1 14
4	-17784	-16996	6456	81	2183	-201	20.11	20.11		1 3.6
5	-6955	-3301	6354	-103	-127	27	20.11	20.11		1 48
6	-7084	-3531	7576	-41	24	52	20.11	20.11	(4+5)-VIII-4	83
7	-13898	-6767	8060	74	597	3	20.11	20.11		1 13
8	-12372	-5839	5778	303	2092	-165	20.11	20.11		1 3.4
9	-11234	-197	9251	161	9	71	20.11	20.11		3 35
10	-11259	-1660	9448	164	28	67	20.11	20.11		3 35
11	-13695	-2577	7513	247	607	21	20.11	20.11		1 12
12	-10422	-938	6370	303	1944	-193	20.11	20.11		1 3.4
13	-11452	1141	10021	180	21	34	20.11	20.11		3 38
14	-11424	278	8722	175	22	41	20.11	20.11		2 38
15	-12832	-1082	6783	206	583	23	20.11	20.11		1 12
16	-9275	-234	6490	295	1818	-222	20.11	20.11		1 3.5
Massimi/minimi										
1							20.11			
1								20.11		
12										3.4

Muro : 66 - Nodi: [9-7-2075-2073], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=8.373$ [(4+5)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-13166	-1355	3331	293	158	-66	20.11	20.11		3 23
2	-11528	-2171	2559	396	167	-111	20.11	20.11		3 16
3	-9025	-4543	1682	442	788	-130	20.11	20.11		1 8.2
4	-3504	-5669	4165	504	2131	-49	20.11	20.11		1 3.5
5	-12487	-1263	4055	247	116	-9	20.11	20.11		3 32
6	-11479	-2474	3028	343	147	-64	20.11	20.11		3 20
7	-10652	-4158	1846	422	780	-136	20.11	20.11		1 8.1
8	-3966	-4354	5272	496	2279	-126	20.11	20.11		1 3.1
9	-7877	-3034	2960	-62	-29	45	20.11	20.11		1 73
10	-11063	-3139	3652	90	96	-30	20.11	20.11		3 59
11	-11638	-5918	1523	236	698	-111	20.11	20.11		1 9.4
12	-5797	-5283	6107	406	2423	-202	20.11	20.11		1 2.9
13	-11233	-1307	5833	-463	-24	-108	20.11	20.11		3 14
14	-11124	-3497	4161	-406	28	-108	20.11	20.11		2 16
15	-12532	-9778	2305	-231	614	-95	20.11	20.11		1 11
16	-8690	-12589	5690	51	2521	-231	20.11	20.11		1 3.0
Massimi/minimi										
1							20.11			
1								20.11		
12										2.9

Muro : 67 - Nodi: [11-9-2073-2071], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=10.467$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-12976	-9700	5070	432	128	-478	20.11	20.11	1	9.1
2	-10751	-2675	6261	119	127	-230	20.11	20.11	1	21
3	-8020	3229	5556	-337	309	-288	20.11	20.11	1	11
4	4035	9418	2097	1	1455	-73	20.11	20.11	1	4.1
5	-12113	-7281	2093	421	329	-261	20.11	20.11	1	12
6	-10293	-2900	2852	340	167	-255	20.11	20.11	1	14
7	-7622	2202	2203	348	420	-166	20.11	20.11	1	12
8	2111	3999	1849	532	1744	192	20.11	20.11	1	3.5
9	-13967	-2318	2283	456	267	-146	20.11	20.11	2	14
10	-10219	-2958	752	443	187	-262	20.11	20.11	1	11
11	-7779	-503	827	549	599	-117	20.11	20.11	1	10.0
12	617	-511	2441	567	1860	158	20.11	20.11	1	3.5
13	-13310	-1340	2905	360	218	-116	20.11	20.11	3	17
14	-11816	-1639	1636	447	181	-154	20.11	20.11	2	14
15	-8818	-3454	682	497	719	-122	20.11	20.11	1	8.8
16	-1301	-5096	3624	503	1984	47	20.11	20.11	1	3.7
Massimi/minimi										
1							20.11			
1								20.11		
8										3.5

Muro : 68 - Nodi: [13-11-2071-2068], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=13.078$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-10278	-757	-3334	-184	-228	-227	20.11	20.11	1	16
2	-10614	1147	-2458	-196	26	-176	20.11	20.11	1	22
3	-12703	4767	-63	-154	146	-143	20.11	20.11	3	23
4	-5832	10889	1529	-77	123	79	20.11	20.11	1	30
5	-9372	-1442	-3769	-13	-300	-233	20.11	20.11	1	14
6	-13412	1735	-3131	147	180	-173	20.11	20.11	3	20
7	-13983	4573	-2283	204	240	-115	20.11	20.11	3	19
8	-8726	6694	649	165	277	132	20.11	20.11	1	16
9	-8081	-3062	-4162	187	-349	-185	20.11	20.11	1	14
10	-11602	-809	-4949	424	189	-77	20.11	20.11	1	16
11	-14869	2486	-3466	530	313	-108	20.11	20.11	3	13
12	-14152	2871	1321	445	448	85	20.11	20.11	1	13
13	-5755	-6052	-4872	602	-104	52	20.11	20.11	1	12
14	-11372	-2771	-5812	791	218	273	20.11	20.11	1	7.6
15	-15492	-351	-4168	976	322	214	20.11	20.11	1	7.1
16	-25668	1166	1622	928	649	155	20.11	20.11	1	8.7
Massimi/minimi										
1							20.11			
1								20.11		
15										7.1

Muro : 69 - Nodi: [15-13-2068-2066], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=12.217$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-16069	-2525	-6142	-558	47	-43	20.11	20.11	3	14
2	-6451	-3691	-1876	-705	38	65	20.11	20.11	3	10.0
3	-3008	-6096	1675	-861	67	-6	20.11	20.11	3	8.5
4	-3137	-11552	6665	-1534	-26	75	20.11	20.11	3	4.6
5	-12804	-236	-3902	-290	116	-91	20.11	20.11	3	22
6	-5614	-2418	-1176	-467	-67	16	20.11	20.11	1	16
7	-5058	-2250	3223	-672	-38	8	20.11	20.11	1	11
8	-12636	-1894	4472	-1003	-26	-26	20.11	20.11	3	8.0
9	-9534	-672	-2623	-215	-44	-104	20.11	20.11	1	25

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
10	-8325	-512	-1163	-375	-53	-66	20.11	20.11		1
11	-7983	965	3315	-519	-15	-65	20.11	20.11		1
12	-8451	381	3889	-605	-15	-115	20.11	20.11		3
13	-8796	-875	-2688	-197	-120	-169	20.11	20.11		1
14	-9724	441	-1445	-347	-36	-139	20.11	20.11		1
15	-10374	3579	1668	-402	10	-102	20.11	20.11		1
16	-9643	8403	5896	-305	-21	-129	20.11	20.11		3
Massimi/minimi										
1							20.11			
1								20.11		
4										4.6

Muro : 70 - Nodi: [17-15-2066-2064], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=20.574$ [(4+5)-III-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-3854	142	-8583	-235	-264	153	20.11	20.11		1
2	201	-272	-4808	-75	-91	192	20.11	20.11		1
3	2634	857	-5217	138	-255	263	20.11	20.11		3
4	2269	87	630	168	-344	276	20.11	20.11		3
5	-5012	-1766	-7724	-288	-176	195	20.11	20.11		1
6	-902	-3420	-4563	-244	-102	253	20.11	20.11		1
7	-507	-4180	-4646	-144	-246	310	20.11	20.11		3
8	-2616	-4975	1071	-90	-431	320	20.11	20.11		3
9	-6476	-3349	-6073	-275	-60	173	20.11	20.11		1
10	-2485	-5318	-3631	-437	-132	224	20.11	20.11		1
11	-1911	-7889	-1427	-539	-194	288	20.11	20.11		1
12	-7125	-11031	1323	-448	-533	394	20.11	20.11		3
13	-6418	-3854	-7795	-386	127	-8	20.11	20.11		3
14	-5526	-7575	-3554	-719	-112	99	20.11	20.11		3
15	-5853	-11999	-154	-942	-243	115	20.11	20.11		3
16	-14621	-18227	2048	-1031	-657	340	20.11	20.11		3
Massimi/minimi										
1							20.11			
1								20.11		
16										6.1

Muro : 71 - Nodi: [19-17-2064-2059], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=11.104$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	7497	10887	-5970	403	59	60	20.11	20.11		1
2	5059	11585	-2907	454	-112	2	20.11	40.21		1
3	5668	15171	-263	517	-331	-40	20.11	40.21		1
4	20710	35299	-8634	276	-1140	432	20.11	40.21		3
5	4789	6247	-7200	310	-42	57	20.11	20.11		1
6	4417	8927	-3858	389	-136	20	20.11	20.11		1
7	6290	18358	-7445	348	-548	74	20.11	20.11		3
8	13751	15364	-3209	466	-576	382	20.11	20.11		3
9	-1396	7453	-10451	278	-77	64	20.11	20.11		2
10	1143	9097	-7987	289	-177	53	20.11	20.11		2
11	5258	10529	-6907	374	-442	166	20.11	20.11		3
12	8546	8165	-1071	431	-436	365	20.11	20.11		3
13	2367	1305	-8324	-66	-227	125	20.11	20.11		1
14	832	5405	-8886	179	-159	93	20.11	20.11		3
15	2495	5254	-5867	296	-366	213	20.11	20.11		3
16	3422	3872	-32	315	-406	304	20.11	20.11		3
Massimi/minimi										
1							20.11			
2								40.21		
8										5.9

Muro : 72 - Nodi: [21-19-2059-2065], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=6.322$ [(4+5)-VIII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-7208	6526	-6465	232	17	-72	20.11	20.11	3	25
2	-1386	3857	-4204	138	-185	-152	20.11	20.11	3	20
3	2007	-2084	-2622	-93	-544	-223	20.11	20.11	3	9.5
4	-7490	-11286	2599	-445	-974	193	20.11	20.11	3	7.0
5	-8646	7101	-5845	260	-24	-127	20.11	20.11	3	20
6	-2934	4839	-2016	193	-227	-196	20.11	20.11	3	16
7	103	-324	1106	122	-578	-281	20.11	20.11	3	8.3
8	-13935	-1168	415	60	-367	-225	20.11	20.11	3	12
9	-8342	4642	-5516	41	-150	-112	20.11	20.11	1	25
10	-5514	7703	-519	154	-263	-195	20.11	20.11	3	14
11	-2427	6875	3736	247	-603	-231	20.11	20.11	3	7.7
12	-10328	985	684	442	-378	-372	20.11	20.11	3	9.3
13	-15493	8812	-5407	-203	-212	-43	20.11	20.11	2	25
14	-7251	10688	-481	44	-327	-114	20.11	20.11	3	14
15	-3892	15206	2154	249	-673	-175	20.11	20.11	3	6.6
16	-11366	24615	7522	795	-1138	-684	20.11	20.11	3	2.6
Massimi/minimi										
1							20.11			
1								20.11		
16										2.6

Muro : 73 - Nodi: [23-21-2065-2067], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=3.971$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-7378	8503	-4940	-359	-23	106	20.11	20.11	2	17
2	-2100	14022	-6195	-261	-208	116	20.11	20.11	3	18
3	1702	21595	-6240	-262	-797	116	20.11	20.11	3	5.5
4	-2429	28586	-3801	-303	-1886	139	20.11	20.11	3	2.1
5	-2693	5499	-5339	-89	-65	-6	20.11	20.11	1	77
6	-2187	9030	-6890	-154	-208	14	20.11	20.11	2	28
7	1382	11443	-9042	-261	-798	84	20.11	20.11	3	6.8
8	-7668	14953	-4571	-409	-1886	203	20.11	20.11	3	2.7
9	-6354	6873	-7465	110	38	-24	20.11	20.11	3	57
10	-1003	4551	-5497	-127	-212	-60	20.11	20.11	1	24
11	771	3445	-8519	-275	-703	51	20.11	20.11	3	9.0
12	-11518	3279	-7568	-546	-1856	204	20.11	20.11	3	3.3
13	-6267	5893	-7075	172	21	-46	20.11	20.11	3	35
14	-1040	3938	-6331	39	-204	-99	20.11	20.11	3	22
15	-131	-198	-5433	-230	-621	-82	20.11	20.11	3	10
16	-14005	-9105	-7146	-686	-1752	192	20.11	20.11	3	4.1
Massimi/minimi										
1							20.11			
1								20.11		
4										2.1

Muro : 74 - Nodi: [25-23-2067-2069], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=4.023$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-6099	8315	-1341	149	34	8	20.11	20.11	2	49

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
2	-341	10322	-1697	30	-288	4	20.11	20.11		21
3	2251	10065	-1195	-71	-981	-35	20.11	20.11		6.0
4	-4290	7037	166	-261	-2179	38	20.11	20.11	(4+5)-VII-3	2.9
5	-5982	9317	-2577	87	31	-48	20.11	20.11		57
6	-396	10167	-1586	-40	-294	-40	20.11	20.11		18
7	2860	9631	-246	-131	-1001	-34	20.11	20.11		6.0
8	-5773	8001	-1758	-273	-2198	81	20.11	20.11	(4+5)-VII-3	2.8
9	-6326	9239	-3210	-75	9	-80	20.11	20.11		50
10	-1157	11276	-1890	-150	-292	-60	20.11	20.11		17
11	1923	13041	-182	-206	-991	1	20.11	20.11		5.9
12	-5190	10130	-2703	-297	-2224	131	20.11	20.11	(4+5)-VII-3	2.6
13	-6896	8191	-3404	-360	-44	38	20.11	20.11		19
14	-2009	12704	-3346	-274	-304	48	20.11	20.11		17
15	779	18837	-1714	-266	-988	94	20.11	20.11		4.9
16	-5676	24502	-1533	-329	-2183	115	20.11	20.11		2.1
Massimi/minimi										
1							20.11			
1								20.11		
16										2.1

Muro : 75 - Nodi: [27-25-2069-2072], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=---,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=2.440$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-6646	11040	689	-215	-28	45	20.11	20.11		30
2	681	15864	-1164	6	-208	67	20.11	20.11	(4+5)-VII-3	20
3	5394	21636	-1972	44	-776	2	20.11	20.11	(4+5)-VII-3	6.4
4	3932	26171	-497	-129	-2106	-126	20.11	20.11	(4+5)-VII-3	2.0
5	-6090	10595	-562	46	19	100	20.11	20.11		51
6	1610	12917	-2893	-27	-223	90	20.11	20.11	(4+5)-VII-3	19
7	5669	14608	-3637	-120	-863	-22	20.11	20.11	(4+5)-VII-3	6.4
8	824	15474	-889	-227	-2170	-110	20.11	20.11	(4+5)-VII-3	2.5
9	-6019	8627	-507	186	41	63	20.11	20.11		31
10	1984	10571	-3323	-31	-247	60	20.11	20.11	(4+5)-VII-3	20
11	5430	10213	-3480	-157	-949	-22	20.11	20.11	(4+5)-VII-3	6.3
12	-1525	10430	-1405	-234	-2178	-63	20.11	20.11	(4+5)-VII-3	2.7
13	-5956	8385	-903	182	41	32	20.11	20.11		36
14	248	10230	-1774	60	-273	23	20.11	20.11		21
15	3748	9880	-1510	-72	-955	-33	20.11	20.11		6.2
16	-3604	8288	-1647	-197	-2201	6	20.11	20.11	(4+5)-VII-3	2.9
Massimi/minimi										
1							20.11			
1								20.11		
4										2.0

Muro : 76 - Nodi: [29-27-2072-2074], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=---,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=2.538$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-6989	7913	5788	206	51	-38	20.11	20.11		32
2	566	12033	3746	7	-207	-16	20.11	20.11	(4+5)-V-4	27
3	3793	13196	2538	-111	-777	-32	20.11	20.11	(4+5)-V-4	7.2
4	58	14515	1341	-199	-1765	-126	20.11	20.11	(4+5)-V-4	3.0
5	-6953	8856	5226	217	58	-59	20.11	20.11		28
6	1094	12906	3342	5	-198	-54	20.11	20.11	(4+5)-V-4	23
7	4994	13487	2458	-122	-786	-46	20.11	20.11	(4+5)-V-4	7.0
8	463	13877	741	-217	-1852	-107	20.11	20.11	(4+5)-V-4	2.9
9	-6609	11501	4259	79	33	-89	20.11	20.11		46
10	1191	14534	2542	5	-191	-84	20.11	20.11	(4+5)-V-4	21
11	5675	16507	2569	-85	-771	-54	20.11	20.11	(4+5)-V-4	6.7
12	1961	16766	234	-181	-1928	-68	20.11	20.11	(4+5)-V-4	2.7

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
13	-7031	10244	2777	-205	4	-74	20.11	20.11	2	28
14	-1376	16677	2352	-38	-163	-64	20.11	20.11	3	24
15	5900	22267	1019	44	-736	-27	20.11	20.11	(4+5)-V-4	6.5
16	5394	27476	1106	-66	-1934	-50	20.11	20.11	(4+5)-VII-3	2.2
Massimi/minimi										
1							20.11			
1								20.11		
16										2.2

Muro : 77 - Nodi: [31-29-2074-2076], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=3.602$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-7587	7431	7761	-383	-70	-130	20.11	20.11	3	15
2	-5375	6988	6014	-334	-222	-82	20.11	20.11	2	18
3	526	13657	3905	-142	-590	-68	20.11	20.11	(4+5)-V-4	8.8
4	-2833	16483	3290	-218	-1421	-254	20.11	20.11	(4+5)-V-4	3.3
5	-4888	9149	6412	-55	0	73	20.11	20.11	(4+5)-V-4	59
6	-1033	10782	5204	-112	-178	70	20.11	20.11	(4+5)-V-4	24
7	1933	11797	3559	-198	-598	-17	20.11	20.11	(4+5)-V-4	9.7
8	-1358	12433	2678	-251	-1484	-227	20.11	20.11	(4+5)-V-4	3.5
9	-7513	7021	6622	132	33	29	20.11	20.11	2	48
10	-128	11002	4820	-46	-181	48	20.11	20.11	(4+5)-V-4	26
11	3030	11689	3586	-159	-673	-23	20.11	20.11	(4+5)-V-4	8.6
12	-328	12191	2408	-227	-1547	-194	20.11	20.11	(4+5)-V-4	3.4
13	-7427	7699	6269	181	54	-17	20.11	20.11	2	39
14	554	11749	4341	-0	-180	8	20.11	20.11	(4+5)-V-4	32
15	4151	13053	3230	-112	-711	-21	20.11	20.11	(4+5)-V-4	8.0
16	786	14740	2387	-178	-1627	-151	20.11	20.11	(4+5)-V-4	3.2
Massimi/minimi										
1							20.11			
1								20.11		
16										3.2

Muro : 78 - Nodi: [33-31-2076-2078], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=3.493$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-8441	5608	11362	144	14	-43	20.11	20.11	3	42
2	-3011	7358	8214	16	-121	-18	20.11	20.11	(4+5)-VI-4	46
3	-2256	8288	7054	-53	-353	-12	20.11	20.11	(4+5)-VI-4	17
4	-5612	8894	7051	-225	-732	-68	20.11	20.11	(4+5)-VI-4	7.8
5	-8800	5432	9912	131	18	-18	20.11	20.11	2	53
6	-2631	9079	7953	10	-107	-22	20.11	20.11	(4+5)-VI-4	48
7	-576	10166	7114	-71	-359	-30	20.11	20.11	(4+5)-VI-4	16
8	-3660	12597	4878	-179	-763	-125	20.11	20.11	(4+5)-VI-4	6.6
9	-5828	7411	5372	-44	5	-43	20.11	20.11	(4+5)-VI-2	88
10	-2172	11055	7124	-44	-107	-39	20.11	20.11	(4+5)-VI-4	41
11	437	13764	6400	-76	-382	-45	20.11	20.11	(4+5)-VI-4	14
12	607	16281	4648	-149	-739	-229	20.11	20.11	(4+5)-V-4	5.7
13	-8605	9058	8956	-369	-22	-193	20.11	20.11	3	14
14	-4899	12931	7948	-263	-91	-148	20.11	20.11	3	18
15	1491	18081	4500	-108	-350	-69	20.11	20.11	(4+5)-VI-4	13
16	5095	24076	4726	-135	-814	-241	20.11	20.11	(4+5)-V-4	4.5
Massimi/minimi										
1							20.11			
1								20.11		
16										4.5

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

R.37.12

Maggio 2021

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Muro : 79 - Nodi: [2-33-2078-2079], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=5.909$ [(4+5)-VI-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-9052	2216	10080	-490	-111	-124	20.11	20.11		3
2	-8609	1061	8157	-525	-234	-79	20.11	20.11		2
3	-10855	-595	7032	-503	-156	-27	20.11	20.11		2
4	-22779	-6437	6867	-160	1000	-142	20.11	20.11		1
5	-9300	3206	10675	-81	-37	73	20.11	20.11		3
6	-8166	2308	10117	-140	-148	82	20.11	20.11		3
7	-3052	4481	6273	-119	-233	38	20.11	20.11	(4+5)-VI-2	25
8	-17750	-52	4810	114	999	-42	20.11	20.11		1
9	-9106	4112	11252	138	2	47	20.11	20.11		3
10	-7449	3547	10774	65	-113	68	20.11	20.11		3
11	-2306	4430	7624	-45	-273	32	20.11	20.11	(4+5)-VI-4	22
12	-14562	1263	3917	192	926	-18	20.11	20.11		1
13	-9190	5355	11467	158	22	-21	20.11	20.11		3
14	-7621	4418	9597	106	-81	14	20.11	20.11		2
15	-734	6723	7546	-52	-283	16	20.11	20.11	(4+5)-VI-4	22
16	-11455	749	3649	131	867	3	20.11	20.11		1
Massimi/minimi										
1							20.11			
1								20.11		
4										6.7

Muro : 80 - Nodi: [53-1-2058-2070], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=6.343$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-89	-12076	633	-5	678	387	20.11	20.11		1
2	-2248	-17307	776	203	-90	483	20.11	20.11		1
3	-5601	-23032	2957	245	-1334	216	20.11	20.11		1
4	-11649	-19815	2931	-201	-4739	-290	20.11	20.11		1
5	-364	-8707	4393	-67	1062	289	20.11	20.11		1
6	-4029	-9811	4833	-509	-237	381	20.11	20.11		1
7	-6815	-8726	4073	-863	-2010	168	20.11	20.11		1
8	-4170	-8667	2001	-928	-4693	-12	20.11	20.11		1
9	-1799	-8586	5287	63	1310	-41	20.11	20.11		1
10	-3004	-7999	4491	-420	-276	19	20.11	20.11		1
11	-4518	-6691	2917	-823	-1980	185	20.11	20.11		1
12	-3354	-6440	2237	-983	-4885	494	20.11	20.11		1
13	938	-11290	4625	728	1197	227	20.11	20.11		1
14	-1386	-8565	3222	493	-274	-327	20.11	20.11		1
15	-2012	-7954	1516	697	-1175	-81	20.11	20.11		1
16	-3915	1766	2232	114	-4590	680	20.11	20.11		3
Massimi/minimi										
1							20.11			
1								20.11		
16										1.7

Muro [Platea]: 81 - Nodi: [10-12-34-35]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=11.067$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	13868	-9899	-11171	-1512	-2986	-609	20.11	20.11		3
2	11155	-8730	-10945	-1765	-2908	-711	20.11	20.11		3
3	14449	-6114	-8893	-830	-1854	-563	20.11	20.11		1
4	18141	-5768	-7868	-1431	-1453	-461	20.11	20.11		3

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
5	15803	-5020	-6595	-635	-1934	-699	20.11	20.11	1	5.1
6	20656	-6730	-6191	-937	-1319	-709	20.11	20.11	3	5.6
7	13723	-9191	-7492	-1601	-2761	-566	20.11	20.11	3	4.3
8	16196	-6508	-10375	-1589	-2014	-569	20.11	20.11	3	4.7
Massimi/minimi										
1							20.11			
1								20.11		
2										3.9

Muro [Platea]: 82 - Nodi: [6-8-36-37]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=10.230$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	13404	-12371	1735	-1262	-3278	-9	20.11	20.11		3
2	13455	-12656	-254	-1270	-3057	-188	20.11	20.11		3
3	16298	-5815	-453	-831	-1127	432	20.11	20.11		3
4	19806	-5413	1377	-906	-1155	517	20.11	20.11		3
5	19025	-4722	2838	-1098	-1175	479	20.11	20.11		3
6	19784	-5500	4184	-1305	-1449	318	20.11	20.11		3
7	14889	-11041	2079	-1430	-3020	21	20.11	20.11		3
8	15918	-8088	1896	-1405	-1963	112	20.11	20.11		3
Massimi/minimi										
1							20.11			
1								20.11		
1										4.5

Muro [Platea]: 83 - Nodi: [18-20-38-39]Pann=9Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=14.582$ [(4+5)-VIII-3] : **Verificato**

Armatura a maglia doppia

Armatura a maglia doppia											
Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs	
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq			
1	-11080	964	-5895	-375	369	-188	20.11	20.11		3	23
2	-12086	148	-7152	361	108	-475	20.11	20.11		1	18
3	-8068	3995	-8956	456	789	-437	20.11	20.11		1	9.8
4	-11965	6911	-7789	178	730	-386	20.11	20.11		1	10
5	-9815	3636	-4240	-524	535	-215	20.11	20.11		3	16
6	-12383	-1121	-6785	-350	629	-672	20.11	20.11		3	9.9
7	-10450	649	-6669	2	383	-318	20.11	20.11		3	18
8	-5825	650	-6050	-549	93	-203	20.11	20.11	(4+5)-I-4	18	
9	-13570	658	-5755	-273	590	-518	20.11	20.11		3	11
Massimi/minimi											
1							20.11				
1								20.11			
3											9.

Muro [Platea]: 84 - Nodi: [4-6-37-40]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=13.805$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Animaletta a maglia doppia										
Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	11645	-4938	7309	-802	-849	667	20.11	20.11		3
2	10353	-9189	9303	-998	-2549	499	20.11	20.11		3
3	11582	-4152	8334	-921	-808	584	20.11	20.11		3
4	9404	-8009	9928	-1106	-2602	532	20.11	20.11		3
5	11651	-3293	9146	-1013	-721	491	20.11	20.11		3
6	8417	-7072	10450	-1244	-2662	567	20.11	20.11		3
7	10997	-1752	9436	-1116	-596	407	20.11	20.11		3

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
8	7101	-6427	10956	-1402	-2731	607	20.11	20.11		4.1
Massimi/minimi										
1							20.11			
1								20.11		
8										4.1

Muro [Platea]: 85 - Nodi: [3-4-40-41]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=14.464$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	7015	-4181	5652	-493	-478	737	20.11	20.11	3	9.4
2	9214	-9739	7422	-719	-2029	368	20.11	20.11	3	6.0
3	8082	-3591	7557	-728	-583	800	20.11	20.11	3	7.5
4	8349	-8494	8386	-831	-2097	412	20.11	20.11	3	5.6
5	9297	-3530	8455	-846	-637	790	20.11	20.11	3	6.8
6	7696	-7446	9398	-909	-2182	489	20.11	20.11	3	5.2
7	9714	-2918	9117	-924	-628	736	20.11	20.11	3	6.7
8	6689	-6726	10391	-1000	-2283	571	20.11	20.11	3	4.8
Massimi/minimi										
1							20.11			
1								20.11		
8										4.8

Muro [Platea]: 86 - Nodi: [12-42-34]Pann=3Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=12.646$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-10712	10020	10666	-2908	-1203	357	20.11	20.11	3	4.4
2	-7572	17218	5908	-1602	-1253	629	20.11	20.11	3	5.2
3	-12028	14497	9613	-2908	-1173	475	20.11	20.11	3	4.3
Massimi/minimi										
1							20.11			
1								20.11		
3										4.3

Muro [Platea]: 87 - Nodi: [14-16-43-44]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=15.983$ [(4+5)-VIII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	3983	1814	-10656	-1052	138	-395	20.11	20.11	3	8.3
2	350	-593	-13716	-1257	-1742	-557	20.11	20.11	3	5.6
3	4460	-581	-11808	-856	-8	-465	20.11	20.11	3	9.1
4	2772	-1988	-13789	-1019	-1700	-518	20.11	20.11	3	5.9
5	3634	-1992	-11741	-689	-123	-554	20.11	20.11	3	9.8
6	4301	-3735	-13683	-832	-1662	-490	20.11	20.11	3	6.2
7	3058	-3280	-11205	-516	-193	-640	20.11	20.11	3	11
8	5661	-5595	-13403	-687	-1630	-466	20.11	20.11	3	6.5
Massimi/minimi										
1							20.11			
1								20.11		
2										5.6

Muro [Platea]: 88 - Nodi: [8-10-35-36]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=10.765$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	20441	-6653	1023	-1188	-1688	213	20.11	20.11	3	6.7
2	15223	-12959	172	-1434	-3330	-116	20.11	20.11	3	4.3
3	16170	-5646	2544	-666	-1828	277	20.11	20.11	1	6.5
4	15738	-12708	1525	-1450	-3352	-56	20.11	20.11	3	4.3
5	16100	-6227	3732	-683	-1943	275	20.11	20.11	1	6.2
6	16115	-12797	2830	-1473	-3381	9	20.11	20.11	3	4.4
7	16407	-7012	5897	-678	-2020	275	20.11	20.11	1	6.0
8	16613	-13047	4181	-1458	-3426	61	20.11	20.11	3	4.2
Massimi/minimi										
1							20.11			
1								20.11		
8										4.2

Muro [Platea]: 89 - Nodi: [16-18-39-43]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=11.105$ [(4+5)-IV-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	26	-712	-11509	-599	-27	-642	20.11	20.11	3	10
2	541	-2452	-13537	-620	-1405	-510	20.11	20.11	3	6.8
3	-194	-1815	-11350	-496	-76	-691	20.11	20.11	3	11
4	1801	-3814	-12915	-507	-1346	-455	20.11	20.11	3	7.4
5	-1230	-2001	-10846	-378	-69	-711	20.11	20.11	3	12
6	2789	-5378	-12168	-423	-1296	-400	20.11	20.11	3	8.0
7	-2450	-2527	-9627	-175	-6	-677	20.11	20.11	3	15
8	4092	-6959	-11258	-330	-1259	-376	20.11	20.11	3	8.5
Massimi/minimi										
1							20.11			
1								20.11		
2										6.8

Muro [Platea]: 90 - Nodi: [12-14-44-42]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=12.351$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	15868	-3958	-9162	-1257	-1007	-794	20.11	20.11	3	4.9
2	13097	-9867	-9700	-1271	-2612	-461	20.11	20.11	3	4.7
3	15401	-4384	-8319	-1135	-916	-821	20.11	20.11	3	5.2
4	13199	-10501	-8277	-1182	-2483	-344	20.11	20.11	3	5.1
5	14119	-4700	-7052	-956	-784	-817	20.11	20.11	3	5.9
6	13213	-11486	-7053	-1109	-2380	-245	20.11	20.11	3	5.5
7	13606	-5675	-4583	-651	-631	-762	20.11	20.11	3	7.4
8	13518	-12731	-5966	-1006	-2300	-193	20.11	20.11	3	5.9
Massimi/minimi										
1							20.11			
1								20.11		
2										4.7

Muro [Platea]: 91 - Nodi: [30-32-45-46]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=11.430$ [(4+5)-VIII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-6815	-395	9074	-15	295	623	20.11	20.11	(4+5)-V-4	14
2	861	-2904	10215	-349	-728	468	20.11	20.11	3	11
3	-4141	-794	9555	-397	113	749	20.11	20.11	3	12
4	-293	-1797	10758	-443	-763	500	20.11	20.11	3	10
5	-3453	-799	9310	-488	65	737	20.11	20.11	3	11
6	-1104	-657	11221	-516	-803	549	20.11	20.11	3	9.5
7	-3599	-163	8968	-567	67	691	20.11	20.11	3	11
8	-2169	460	11570	-596	-849	600	20.11	20.11	3	8.7
Massimi/minimi										
1							20.11			
1								20.11		
8										8.7

Muro [Platea]: 92 - Nodi: [20-22-47-38]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=9.427$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-11256	653	-6284	-284	251	-512	20.11	20.11	3	17
2	-10958	5065	-8806	454	1032	-457	20.11	20.11	1	8.0
3	-10504	170	-7024	-251	269	-564	20.11	20.11	3	15
4	-9812	4043	-9151	529	1050	-434	20.11	20.11	1	8.1
5	-10409	416	-7757	-199	334	-583	20.11	20.11	3	14
6	-8842	3141	-9342	604	1066	-420	20.11	20.11	1	8.2
7	-10798	769	-8378	-87	437	-546	20.11	20.11	3	13
8	-7839	2360	-9445	676	1082	-422	20.11	20.11	1	8.2
Massimi/minimi										
1							20.11			
1								20.11		
2										8.0

Muro [Platea]: 93 - Nodi: [22-24-48-49]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=15.972$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-15083	3159	2081	-226	719	46	20.11	20.11	3	16
2	-12348	5809	-843	542	1420	-122	20.11	20.11	1	7.6
3	-12387	1878	-2734	-88	498	-129	20.11	20.11	(4+5)-V-4	20
4	-11105	5406	-1619	619	1401	-136	20.11	20.11	1	7.7
5	-12963	1004	-3943	-24	432	-183	20.11	20.11	(4+5)-V-4	20
6	-10383	4994	-2198	657	1385	-144	20.11	20.11	1	7.8
7	-13591	453	-4621	36	404	-236	20.11	20.11	(4+5)-V-4	20
8	-9869	4816	-2813	680	1375	-146	20.11	20.11	1	7.8
Massimi/minimi										
1							20.11			
1								20.11		
2										7.6

Muro [Platea]: 94 - Nodi: [22-49-47]Pann=3Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=13.232$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	2944	-6367	8893	1175	801	459	20.11	20.11	1	7.5
2	1973	-11825	6745	475	-250	405	20.11	20.11	3	14

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
3	1702	-4946	8377	1154	700	357	20.11	20.11	1	8.2
Massimi/minimi										
1							20.11			
1								20.11		
1										7.5

Muro [Platea]: 95 - Nodi: [24-26-50-48]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=15.794$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-14608	1300	-2750	1	480	-202	20.11	20.11	(4+5)-V-4	18
2	-10956	5592	-1224	659	1432	-108	20.11	20.11	1	7.7
3	-13918	1293	-3836	15	526	-250	20.11	20.11	(4+5)-V-4	16
4	-11008	5504	-1843	647	1388	-114	20.11	20.11	1	7.9
5	-13696	2022	-4721	16	615	-280	20.11	20.11	(4+5)-V-4	14
6	-11032	5634	-2319	619	1346	-118	20.11	20.11	1	8.1
7	-14604	3045	-5750	32	731	-275	20.11	20.11	(4+5)-V-4	12
8	-10900	5899	-2711	567	1307	-113	20.11	20.11	1	8.3
Massimi/minimi										
1							20.11			
1								20.11		
2										7.7

Muro [Platea]: 96 - Nodi: [26-28-51-50]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=14.020$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-14152	1574	7695	-93	604	432	20.11	20.11	3	12
2	-8606	3759	6285	587	1240	220	20.11	20.11	1	8.3
3	-13888	1452	5367	45	564	370	20.11	20.11	(4+5)-VII-3	13
4	-8960	3981	5884	545	1222	208	20.11	20.11	1	8.4
5	-13942	1055	4322	26	510	341	20.11	20.11	(4+5)-VII-3	15
6	-9252	4421	5462	498	1205	203	20.11	20.11	1	8.5
7	-14410	1404	3495	-10	503	292	20.11	20.11	(4+5)-VII-3	16
8	-9525	5131	4901	451	1188	201	20.11	20.11	1	8.6
Massimi/minimi										
1							20.11			
1								20.11		
2										8.3

Muro [Platea]: 97 - Nodi: [28-30-46-51]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=10.025$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-14177	715	4587	49	484	263	20.11	20.11	(4+5)-V-4	17
2	-7607	3995	5958	423	1089	244	20.11	20.11	1	9.1
3	-13092	1354	3819	-24	546	203	20.11	20.11	(4+5)-V-4	17
4	-8616	4737	5310	347	1052	224	20.11	20.11	1	9.4
5	-12221	2516	2790	-118	640	140	20.11	20.11	(4+5)-V-4	16
6	-9405	5728	4695	257	1017	205	20.11	20.11	1	9.6
7	-12848	4546	849	-257	751	96	20.11	20.11	(4+5)-V-4	14
8	-10314	6785	4084	136	985	202	20.11	20.11	1	9.8
Massimi/minimi										
1							20.11			
1								20.11		

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
2										9.1

Muro [Platea]: 98 - Nodi: [52-41-40]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=66.609$ [(4+5)-VIII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	6341	6097	-808	-395	-422	57	20.11	20.11	3	24
2	7105	5588	-909	-474	-249	70	20.11	20.11	3	21
3	6650	5397	-36	-452	-352	-25	20.11	20.11	3	24
4	5985	6121	-1214	-410	-566	64	20.11	20.11	3	19
5	6380	6106	-824	-357	-323	114	20.11	20.11	3	25
6	6351	6111	-782	-380	-277	57	20.11	20.11	3	27
7	6307	6103	-787	-407	-524	62	20.11	20.11	3	20
8	6330	6081	-823	-394	-436	113	20.11	20.11	3	21
Massimi/minimi										
1							20.11			
1								20.11		
4										19

Muro [Platea]: 99 - Nodi: [32-3-41-45]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=10.878$ [(4+5)-VI-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-1593	-2427	9213	-452	-137	689	20.11	20.11	3	11
2	2158	-2379	11539	-599	-1122	605	20.11	20.11	3	7.6
3	-971	-1491	9319	-577	-67	594	20.11	20.11	3	11
4	521	-848	11543	-743	-1158	619	20.11	20.11	3	7.2
5	-274	-280	8995	-701	57	475	20.11	20.11	3	11
6	-1046	733	11404	-924	-1197	637	20.11	20.11	3	6.9
7	-713	2166	7546	-864	215	365	20.11	20.11	3	10
8	-3137	2117	11207	-1156	-1237	665	20.11	20.11	3	6.5
Massimi/minimi										
1							20.11			
1								20.11		
8										6.5

Muro [Platea]: 100 - Nodi: [52-40-37]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=54.765$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	7107	6900	-1284	-441	-476	79	20.11	20.11	3	21
2	7745	6420	-1206	-525	-338	99	20.11	20.11	3	18
3	7155	5616	-499	-485	-364	7	20.11	20.11	3	23
4	6726	6936	-1404	-454	-577	71	20.11	20.11	3	18
5	7184	6947	-1289	-407	-402	137	20.11	20.11	3	21
6	7094	6911	-1177	-434	-363	87	20.11	20.11	3	22
7	7011	6968	-1194	-447	-551	78	20.11	20.11	3	18
8	7065	6863	-1268	-428	-474	126	20.11	20.11	3	19
Massimi/minimi										
1							20.11			
1								20.11		
4										18

Muro [Platea]: 101 - Nodi: [52-43-39]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=88.372$ [(4+5)-II-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	4735	4869	1939	-275	-310	-126	20.11	20.11	3	27
2	3745	5341	2157	-288	-489	-87	20.11	20.11	3	21
3	5494	5256	1276	-405	-361	-58	20.11	20.11	3	26
4	5142	4664	2352	-301	-155	-231	20.11	20.11	3	22
5	4605	4879	1980	-246	-397	-169	20.11	20.11	3	21
6	4717	4862	1923	-309	-448	-91	20.11	20.11	3	22
7	4788	4866	1899	-243	-186	-168	20.11	20.11	3	29
8	4708	4861	1908	-193	-270	-185	20.11	20.11	3	26
Massimi/minimi										
1							20.11			
1								20.11		
2										21

Muro [Platea]: 102 - Nodi: [52-44-43]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=78.062$ [(4+5)-VI-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	4713	6243	2295	-283	-400	-141	20.11	20.11	3	22
2	3839	6890	2201	-288	-577	-103	20.11	20.11	3	17
3	5321	6454	1457	-388	-442	-67	20.11	20.11	3	23
4	5246	6204	2487	-310	-271	-238	20.11	20.11	3	22
5	4549	6214	2335	-253	-477	-191	20.11	20.11	3	18
6	4704	6225	2200	-314	-528	-110	20.11	20.11	3	18
7	4834	6192	2196	-254	-285	-180	20.11	20.11	3	25
8	4730	6272	2271	-206	-371	-202	20.11	20.11	3	20
Massimi/minimi										
1							20.11			
1								20.11		
2										17

Muro [Platea]: 103 - Nodi: [52-39-38]Pann=3Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=70.115$ [(4+5)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	3401	3585	1837	-249	-337	-64	20.11	20.11	3	30
2	5447	4638	780	-403	-306	-31	20.11	20.11	3	27
3	-1728	-4000	1935	134	369	-138	20.11	20.11	1	26
Massimi/minimi										
1							20.11			
1								20.11		
3										26

Muro [Platea]: 104 - Nodi: [52-42-44]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=71.694$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	4813	8107	1535	-288	-530	-111	20.11	20.11	3	18
2	3930	8513	1906	-297	-693	-78	20.11	20.11	3	15

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
3	5239	7504	939	-376	-509	-41	20.11	20.11		3
4	5042	8001	2177	-301	-379	-201	20.11	20.11		3
5	4769	8148	1580	-274	-617	-140	20.11	20.11		3
6	4774	8097	1610	-319	-657	-78	20.11	20.11		3
7	4785	8174	1588	-260	-419	-145	20.11	20.11		3
8	4769	8093	1561	-222	-488	-161	20.11	20.11		3
Massimi/minimi										
1							20.11			
1								20.11		
2										15

Muro [Platea]: 105 - Nodi: [52-37-36]Pann=3Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=48.925$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	7198	8641	-1660	-466	-612	91	20.11	20.11		3
2	7718	8394	-1621	-503	-517	128	20.11	20.11		3
3	7235	5886	-829	-489	-391	43	20.11	20.11		3
Massimi/minimi										
1							20.11			
1								20.11		
1										16

Muro [Platea]: 106 - Nodi: [52-36-35]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=47.480$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	6954	9454	-1577	-443	-635	97	20.11	20.11		3
2	7124	9024	-1444	-490	-600	118	20.11	20.11		3
3	6803	6910	-1006	-459	-454	59	20.11	20.11		3
4	6908	9179	-1416	-452	-606	67	20.11	20.11		3
5	7025	9479	-1570	-425	-629	118	20.11	20.11		3
6	6932	9446	-1501	-451	-625	115	20.11	20.11		3
7	6890	9517	-1497	-436	-634	83	20.11	20.11		3
8	6943	9454	-1518	-415	-621	100	20.11	20.11		3
Massimi/minimi										
1							20.11			
1								20.11		
5										15

Muro [Platea]: 107 - Nodi: [52-35-34]Pann=3Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=50.374$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	5992	10823	-1002	-406	-740	85	20.11	20.11		3
2	6097	7384	-504	-413	-483	44	20.11	20.11		3
3	6328	10608	-869	-400	-677	38	20.11	20.11		3
Massimi/minimi										
1							20.11			
1								20.11		
1										13

Muro [Platea]: 108 - Nodi: [52-34-42]Pann=3Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=39.571$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	5416	10561	252	-323	-736	-53	20.11	20.11	3	14
2	4345	11985	221	-292	-765	-21	20.11	20.11	3	14
3	5325	7496	655	-380	-477	6	20.11	20.11	3	24
Massimi/minimi										
1							20.11			
1								20.11		
2										14

Muro [Platea]: 109 - Nodi: [52-38-47]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=43.704$ [(4+5)-I-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-2309	-4417	1202	145	310	-72	20.11	20.11	1	35
2	2971	3115	1051	-231	-321	-20	20.11	20.11	3	36
3	5138	4105	246	-384	-289	10	20.11	20.11	3	30
4	-1806	-4497	1240	139	435	-95	20.11	20.11	1	25
5	-2488	-4445	1227	139	236	-133	20.11	20.11	1	36
6	2617	2651	483	-173	-272	-12	20.11	20.11	(4+5)-II-4	43
7	-2189	-4497	1081	158	401	-85	20.11	20.11	1	28
8	-2309	-4415	1115	166	319	-122	20.11	20.11	1	30
Massimi/minimi										
1							20.11			
1								20.11		
4										25

Muro [Platea]: 110 - Nodi: [52-47-49]Pann=3Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=50.284$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-2406	-6276	953	168	430	-64	20.11	20.11	1	28
2	-2875	-5784	581	184	353	-50	20.11	20.11	1	34
3	4515	4621	-189	-351	-308	36	20.11	20.11	3	31
Massimi/minimi										
1							20.11			
1								20.11		
1										28

Muro [Platea]: 111 - Nodi: [52-51-46]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=38.250$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	3842	2598	-763	-213	-190	42	20.11	20.11	3	47
2	4239	2860	-597	-291	-111	68	20.11	20.11	3	33
3	4339	5410	-193	-307	-361	-15	20.11	20.11	3	32
4	3406	3389	-1026	-231	-336	50	20.11	20.11	3	32
5	-2729	-3405	-691	170	267	65	20.11	20.11	1	40
6	-2748	-3418	-591	198	301	17	20.11	20.11	1	42
7	3739	2656	-694	-224	-266	46	20.11	20.11	3	39

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
8	3708	2486	-888	-208	-187	96	20.11	20.11		40
Massimi/minimi										
1							20.11			
1								20.11		
4										32

Muro [Platea]: 112 - Nodi: [52-50-51]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=32.341$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-3133	-4407	-611	210	285	31	20.11	20.11	1	42
2	-2781	-4199	-625	195	313	34	20.11	20.11	1	39
3	3924	5168	-434	-286	-348	11	20.11	20.11	3	33
4	2360	3034	-732	-157	-260	32	20.11	20.11	(4+5)-V-1	42
5	-3135	-4352	-602	199	313	50	20.11	20.11	1	37
6	-3139	-4379	-505	223	337	15	20.11	20.11	1	38
7	-3210	-4353	-546	196	241	48	20.11	20.11	1	46
8	-3209	-4466	-656	177	280	60	20.11	20.11	1	39
Massimi/minimi										
1							20.11			
1								20.11		
3										33

Muro [Platea]: 113 - Nodi: [52-48-50]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=30.690$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-3154	-5461	-517	215	361	27	20.11	20.11	1	35
2	-3096	-5050	-480	210	334	32	20.11	20.11	1	37
3	3833	4867	-616	-287	-331	32	20.11	20.11	3	33
4	-3362	-4880	-643	220	318	57	20.11	20.11	1	36
5	-3198	-5405	-501	206	363	30	20.11	20.11	1	35
6	-3163	-5434	-428	222	373	16	20.11	20.11	1	35
7	-3208	-5418	-477	208	348	37	20.11	20.11	1	35
8	-3231	-5524	-577	195	363	40	20.11	20.11	1	34
Massimi/minimi										
1							20.11			
1								20.11		
3										33

Muro [Platea]: 114 - Nodi: [52-46-45]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=50.298$ [(4+5)-VI-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	4557	4032	-745	-265	-287	44	20.11	20.11	3	36
2	5183	3891	-648	-348	-147	60	20.11	20.11	3	29
3	5015	5442	25	-346	-356	-32	20.11	20.11	3	30
4	4088	4480	-1070	-284	-452	60	20.11	20.11	3	23
5	4569	4104	-746	-233	-195	105	20.11	20.11	3	35
6	4557	4073	-615	-250	-144	39	20.11	20.11	3	41
7	4454	4091	-669	-281	-387	54	20.11	20.11	3	27
8	4465	3948	-813	-272	-291	108	20.11	20.11	3	30
Massimi/minimi										
1							20.11			
1								20.11		

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
4										23

Muro [Platea]: 115 - Nodi: [52-49-48]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45,ζ_e=31.091 [(4+5)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-3210	-6411	128	222	430	-11	20.11	20.11	1	31
2	-3257	-5575	66	214	331	4	20.11	20.11	1	41
3	4069	4625	-586	-313	-318	44	20.11	20.11	3	33
4	-3171	-5597	-151	218	411	8	20.11	20.11	1	32
5	-3397	-6352	179	225	407	-30	20.11	20.11	1	31
6	-3221	-6380	188	221	400	-17	20.11	20.11	1	33
7	-3204	-6392	111	222	454	-10	20.11	20.11	1	30
8	-3321	-6490	2	224	440	-14	20.11	20.11	1	30
Massimi/minimi										
1							20.11			
1								20.11		
7										30

Muro [Platea]: 116 - Nodi: [52-45-41]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45,ζ_e=62.553 [(4+5)-II-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	5458	4988	-797	-331	-352	49	20.11	20.11	3	30
2	6147	4711	-695	-411	-194	61	20.11	20.11	3	25
3	5870	5441	123	-401	-358	-40	20.11	20.11	3	27
4	5024	5316	-1119	-347	-508	63	20.11	20.11	3	21
5	5455	5045	-798	-292	-254	109	20.11	20.11	3	29
6	5464	5027	-689	-315	-203	46	20.11	20.11	3	33
7	5374	5031	-738	-346	-456	57	20.11	20.11	3	23
8	5372	4914	-872	-333	-359	112	20.11	20.11	3	25
Massimi/minimi										
1							20.11			
1								20.11		
4										21

Muro : 117 - Nodi: [1-19-2059-2058], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45,ζ_e=8.759 [(4+5)-VIII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	31422	5506	12294	197	183	-54	40.21	20.11	(4+5)-IV-4	35
2	-348	930	12875	387	255	153	40.21	20.11	3	22
3	-14508	-9027	13388	335	567	384	20.11	20.11	3	10
4	-17553	-503	6063	300	1048	593	20.11	20.11	(4+5)-IV-1	5.5
5	8014	593	5277	197	63	71	20.11	20.11	(4+5)-VIII-3	30
6	1633	4813	18340	125	395	111	20.11	20.11	3	17
7	-8168	9385	15635	110	944	225	20.11	20.11	3	6.7
8	-8640	9502	9303	122	1698	537	20.11	20.11	3	3.5
9	-6980	-1019	2735	221	66	8	20.11	20.11	(4+5)-IV-1	42
10	-6196	2984	10955	205	493	9	20.11	20.11	3	17
11	-2769	6569	12993	231	1265	41	20.11	20.11	3	6.3
12	-1197	9292	11283	228	2259	284	20.11	20.11	3	3.1
13	-20521	-4160	1460	-35	104	-50	20.11	20.11	3	61
14	-10528	6799	2203	-11	495	-16	20.11	20.11	3	16
15	-7538	14270	4725	37	1231	-52	20.11	20.11	3	5.7

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
16	894	18016	11714	200	2867	112	20.11	20.11	3	2.3
Massimi/minimi										
1							40.21			
1								20.11		
16										2.3

Muro [Platea]: 118 - Nodi: [2062-2011-2057] Pann=19 Spess.=50 cm, Terreno=DefTerr_70882, , Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=11.936$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-22976	-12095	1434	3789	1419	-690	31.42	31.42	3	6.7
2	-23320	-13070	1922	5447	1557	-279	31.42	31.42	3	5.2
3	-23685	-16396	1837	6290	1952	200	31.42	31.42	2	4.6
4	-24010	-18678	3168	6794	2293	489	31.42	31.42	2	4.1
5	-23630	-21407	5950	6941	2288	592	31.42	31.42	2	4.0
6	-23199	-18316	3148	6885	2270	574	31.42	31.42	2	4.0
7	-22691	-16320	1676	6183	1793	247	31.42	31.42	2	4.7
8	-22681	-11982	1389	4327	856	-352	31.42	31.42	3	6.4
9	-24099	-11944	1943	1281	-112	-848	31.42	31.42	3	14
10	-28051	-12412	8481	-3589	-845	-1688	31.42	31.42	3	5.9
11	-19993	-14213	6734	-4023	-214	-1500	31.42	31.42	3	5.3
12	-17129	-17048	2630	-3761	406	-1475	31.42	31.42	3	5.5
13	-16805	-19536	-3099	-2747	1402	-1458	31.42	31.42	3	6.8
14	-20297	-16554	-1106	-474	1520	-1382	31.42	31.42	2	9.9
15	-21767	-11839	1171	1836	1282	-1136	31.42	31.42	3	10
16	-22744	-12721	1809	3890	1178	-506	31.42	31.42	3	6.8
17	-22119	-12453	2218	1642	715	-1169	31.42	31.42	3	11
18	-21249	-16625	1407	91	460	-1060	31.42	31.42	2	19
19	-21204	-16453	245	-747	842	-1319	31.42	31.42	2	13
Massimi/minimi										
1							31.42			
1								31.42		
5										4.0

Muro [Platea]: 119 - Nodi: [2062-2057-2054] Pann=17 Spess.=50 cm, Terreno=DefTerr_70882, , Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=23.354$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-20365	-17002	4130	4926	2975	-1503	31.42	31.42	3	4.6
2	-21156	-19249	4414	5673	2903	-1659	31.42	31.42	3	4.0
3	-21338	-21796	4588	5980	2742	-1557	31.42	31.42	3	3.9
4	-19068	-26324	6480	6285	2554	-1608	31.42	31.42	3	3.7
5	-20268	-22321	4949	6121	2721	-1581	31.42	31.42	3	3.8
6	-20362	-19288	4906	5653	2784	-1716	31.42	31.42	3	4.0
7	-20220	-17087	5040	4760	2734	-1624	31.42	31.42	3	4.6
8	-19636	-15426	4888	3193	2614	-1327	31.42	31.42	3	6.5
9	-19450	-13373	3827	1359	2690	-761	31.42	31.42	3	8.1
10	-25489	-14397	-1371	169	2738	396	31.42	31.42	1	9.0
11	-24820	-14548	-7019	-1198	3547	796	31.42	31.42	1	6.5
12	-23593	-12059	-3268	41	3485	692	31.42	31.42	1	6.7
13	-23919	-11749	-808	1579	2992	600	31.42	31.42	1	7.7
14	-24375	-11705	325	3803	2571	299	31.42	31.42	1	7.4
15	-19541	-14142	3436	4024	3013	-1132	31.42	31.42	3	5.7
16	-18586	-13261	3365	2522	2772	-788	31.42	31.42	3	7.9
17	-19943	-15801	4437	4125	2880	-1463	31.42	31.42	3	5.3
Massimi/minimi										
1							31.42			
1								31.42		
4										3.7

Muro [Platea]: 120 - Nodi: [2086-2014-2062]Pann=16Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=24.694$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-44607	-14596	7566	2674	912	-1018	31.42	31.42	3	9.2
2	-43471	-17172	10000	3095	1486	-753	31.42	31.42	3	8.8
3	-40469	-20092	9932	3528	2031	-947	31.42	31.42	3	7.4
4	-41886	-17274	8812	4348	1623	-1308	31.42	31.42	3	5.9
5	-41829	-15312	6117	4865	1501	-1091	31.42	31.42	3	5.6
6	-40540	-15967	2782	5328	1521	-663	31.42	31.42	3	5.6
7	-41010	-17467	936	5442	1728	-222	31.42	31.42	3	5.9
8	-45691	-17807	1913	4719	1545	41	31.42	31.42	3	7.2
9	-44432	-16762	1671	4340	1305	616	31.42	31.42	2	6.9
10	-39857	-11545	4	3130	573	831	31.42	31.42	2	8.4
11	-34416	-8431	-2905	1620	470	576	31.42	31.42	1	15
12	-42223	-10099	-1395	1030	226	-425	31.42	31.42	1	23
13	-45941	-11042	2647	2098	759	-867	31.42	31.42	2	12
14	-41498	-12453	-1052	3529	591	17	31.42	31.42	2	9.4
15	-41844	-13478	1003	4166	903	-531	31.42	31.42	3	7.1
16	-41971	-15645	-509	4742	1318	89	31.42	31.42	2	7.0
Massimi/minimi										
1							31.42			
1								31.42		
6										5.6

Muro : 121 - Nodi: [53-2070-2071-11], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=7.288$ [(4+5)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-2980	4222	6676	-101	70	26	20.11	20.11	1	73
2	-5130	-338	6542	54	1	18	20.11	20.11	(4+5)-VI-3	>100
3	-8038	-6679	14582	-9	-60	108	20.11	20.11	1	58
4	-14952	-10346	16865	234	-271	455	20.11	20.11	1	14
5	-19546	-1742	9132	35	500	70	20.11	20.11	1	16
6	-14955	-5750	16905	32	152	-66	20.11	20.11	1	44
7	-11232	-6848	19890	27	-62	-84	20.11	20.11	1	67
8	-6139	-8656	17307	-28	-177	468	20.11	20.11	1	15
9	-41478	-10772	9052	-158	597	205	20.11	20.11	1	13
10	-25068	-11792	19397	-236	-21	-6	20.11	20.11	1	49
11	-7530	-11328	18581	-267	-250	-88	20.11	20.11	1	28
12	4711	-10219	13845	-469	41	232	20.11	20.11	1	12
13	-66968	-32177	13381	-2430	603	226	20.11	20.11	1	6.1
14	-20182	-16035	7171	-2227	-172	327	20.11	20.11	1	4.4
15	-3022	-4660	4678	-1830	-439	341	20.11	20.11	1	4.3
16	11541	5412	5409	-1790	-180	220	20.11	20.11	1	3.8
Massimi/minimi										
1							20.11			
1								20.11		
16										3.8

Muro [Platea]: 122 - Nodi: [2007-2036-2042]Pann=42Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=5.032$ [(4+5)-I-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-12426	-15440	-4263	2066	2319	1167	31.42	31.42	(4+5)-III-4	8.2
2	-20082	-20319	-6651	3500	3444	1725	31.42	31.42	3	5.6
3	-20256	-20444	-6820	4206	4065	2281	31.42	31.42	2	4.5

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
4	-20348	-20493	-6574	4693	4502	2666	31.42	31.42	2	4.0
5	-20339	-20493	-6355	4925	4639	2858	31.42	31.42	2	3.8
6	-20316	-20475	-6115	4894	4535	2845	31.42	31.42	2	3.8
7	-19657	-20913	-5904	4433	4011	2586	31.42	31.42	1	4.2
8	-20070	-20498	-6075	3962	3502	2226	31.42	31.42	1	4.8
9	-20991	-20149	-6361	2838	2812	1645	31.42	31.42	1	6.6
10	-17988	-20632	-5443	3270	2742	1687	31.42	31.42	1	5.9
11	-15960	-21813	-6185	3444	2751	1819	31.42	31.42	1	5.4
12	-15476	-22351	-8559	3153	2363	1571	31.42	31.42	1	6.0
13	-16647	-21657	-8232	3971	3165	2253	31.42	31.42	1	4.6
14	-17069	-20492	-8022	4561	3710	2510	31.42	31.42	2	4.1
15	-17934	-19832	-7436	4732	4053	2717	31.42	31.42	2	3.9
16	-18546	-19401	-6803	4424	4035	2654	31.42	31.42	2	4.1
17	-18745	-18975	-5926	3678	3692	2335	31.42	31.42	3	4.8
18	-18831	-18654	-5283	2471	2832	1794	31.42	31.42	3	6.3
19	-12549	-14369	-3507	1135	1791	1130	31.42	31.42	(4+5)-V-4	9.7
20	-9590	-8647	225	-1575	-1151	-445	31.42	31.42	(4+5)-III-1	14
21	923	-7598	1534	-5429	-2971	-2131	31.42	31.42	(4+5)-I-2	3.3
22	-10439	-10605	-2675	-1227	-1369	-963	31.42	31.42	(4+5)-VII-1	12
23	-12554	-14804	-3593	1136	1405	718	31.42	31.42	(4+5)-VII-4	13
24	-12380	-14981	-3610	1736	2066	1265	31.42	31.42	(4+5)-VII-4	8.5
25	-19015	-20016	-6144	3132	2905	1679	31.42	31.42	3	6.1
26	-18789	-19667	-6153	3782	3566	2338	31.42	31.42	2	4.8
27	-18677	-19267	-5671	2920	2918	1883	31.42	31.42	3	6.1
28	-18725	-19713	-6037	3663	3386	2133	31.42	31.42	3	5.0
29	-19302	-20473	-6712	4079	3734	2243	31.42	31.42	2	4.6
30	-18550	-19897	-6655	4450	3978	2642	31.42	31.42	2	4.1
31	-18780	-20263	-6636	4387	3915	2540	31.42	31.42	2	4.2
32	-17998	-20304	-7173	4793	4100	2780	31.42	31.42	2	3.8
33	-18296	-20690	-6893	4817	4206	2785	31.42	31.42	2	3.8
34	-19522	-20655	-6555	4833	4444	2741	31.42	31.42	2	3.9
35	-18798	-20793	-6703	4843	4313	2767	31.42	31.42	2	3.8
36	-19491	-20542	-6741	4549	4161	2566	31.42	31.42	2	4.1
37	-19195	-20631	-6232	4664	4102	2669	31.42	31.42	2	4.0
38	-19297	-20699	-6360	4929	4468	2830	31.42	31.42	2	3.8
39	-18341	-20842	-6515	4902	4264	2791	31.42	31.42	2	3.8
40	-17528	-21317	-6341	4437	3732	2533	31.42	31.42	1	4.1
41	-17561	-21264	-7097	4713	3908	2673	31.42	31.42	2	3.9
42	-17050	-21038	-7490	4621	3776	2602	31.42	31.42	2	4.0
Massimi/minimi										
1							31.42			
1								31.42		
21										3.3

Muro [Platea]: 123 - Nodi: [2043-2008-2049-2048]Pann=16Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45,ζ=7.852 [(4+5)-I-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-2332	-19261	3098	2308	2120	-838	31.42	31.42	2	14
2	-9628	-18200	4355	848	2450	-903	31.42	31.42	2	15
3	-15429	-17164	5729	-254	3001	-626	31.42	31.42	2	14
4	-10628	-12097	7414	-1253	3875	879	31.42	31.42	(4+5)-VI-4	10.0
5	-126	-14098	-2848	-2263	946	-1127	31.42	31.42	(4+5)-I-4	13
6	-11126	-17595	2709	-1216	2415	-2140	31.42	31.42	3	11
7	-16371	-14502	3679	-1801	3778	-2154	31.42	31.42	3	8.1
8	-19441	-10975	2281	-2295	5700	-2385	31.42	31.42	3	5.8
9	-2225	-10918	-3336	-4942	54	-944	31.42	31.42	(4+5)-III-3	7.5
10	-4026	-9277	-1941	-4698	840	-1144	31.42	31.42	(4+5)-III-3	7.7
11	-16140	-13904	-496	-3077	3540	-2749	31.42	31.42	3	7.6
12	-19034	-11071	-447	-2934	5122	-2892	31.42	31.42	3	5.9
13	-4070	-7929	-3987	-8254	-533	-432	31.42	31.42	(4+5)-III-3	5.1
14	-5043	-9106	-3312	-7476	244	-668	31.42	31.42	(4+5)-I-3	5.5
15	-6710	-8243	-1973	-6503	1163	-915	31.42	31.42	(4+5)-V-3	6.1
16	-11566	-12161	-3384	-253	4906	-2524	31.42	31.42	(4+5)-II-2	6.4
Massimi/minimi										
1							31.42			
1								31.42		
13										5.1

Muro [Platea]: 124 - Nodi: [2042-2043-2048-2047]Pann=8Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=5.333$ [(4+5)-III-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-21526	-12437	-6338	-4368	719	-1256	31.42	31.42	(4+5)-V-4	9.0
2	-21756	-11673	-4559	-4528	1072	-1282	31.42	31.42	(4+5)-V-4	8.7
3	-21229	-11118	-3546	-4468	1767	-1198	31.42	31.42	(4+5)-V-4	8.9
4	-26828	-18649	-2333	-2789	4487	-1637	31.42	31.42	3	8.1
5	-26653	-13599	-6882	-8259	446	-1753	31.42	31.42	(4+5)-V-4	5.2
6	-23338	-13139	-5728	-7246	769	-1754	31.42	31.42	(4+5)-V-4	5.7
7	-21717	-11924	-5894	-6383	1367	-1900	31.42	31.42	(4+5)-V-4	6.1
8	-21848	-8586	-7222	-5646	2375	-2169	31.42	31.42	(4+5)-V-4	6.5
Massimi/minimi										
1							31.42			
1								31.42		
5										5.2

Muro [Platea]: 125 - Nodi: [2015-2086-2062]Pann=15Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=7.164$ [(4+5)-IV-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-43232	-18550	-6176	4523	1702	775	31.42	31.42	2	6.4
2	-45008	-17640	-4536	4197	1534	594	31.42	31.42	2	7.1
3	-45679	-17526	-1868	3919	1545	127	31.42	31.42	2	8.5
4	-44315	-18580	-4053	3426	1506	507	31.42	31.42	2	8.7
5	-42362	-20101	-5280	2867	1731	802	31.42	31.42	2	9.2
6	-39220	-18594	-5217	2035	1563	783	31.42	31.42	3	12
7	-30896	-16517	-3789	798	1491	817	31.42	31.42	1	12
8	511	-2350	927	-994	-135	-479	31.42	31.42	(4+5)-V-4	17
9	-26392	-20375	-9906	2519	1005	311	31.42	31.42	3	11
10	-37586	-22288	-10743	3582	1551	506	31.42	31.42	3	8.0
11	-41124	-23629	-10782	4097	1863	874	31.42	31.42	2	6.7
12	-38496	-23056	-8436	4657	2284	1060	31.42	31.42	2	5.8
13	-40132	-20259	-6988	4715	2082	929	31.42	31.42	2	5.9
14	-40629	-20088	-6105	4319	1992	943	31.42	31.42	2	6.3
15	-36985	-20006	-5019	4113	2052	808	31.42	31.42	3	6.6
Massimi/minimi										
1							31.42			
1								31.42		
12										5.8

Muro [Platea]: 126 - Nodi: [2015-2090-2086]Pann=9Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=9.029$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-24225	-21149	-4448	1650	2361	659	31.42	31.42	3	9.8
2	-4822	-13380	1962	24	796	-455	31.42	31.42	(4+5)-IV-1	22
3	-21796	-25945	-5303	2016	367	-31	31.42	31.42	1	15
4	-23997	-31319	-4255	1963	871	210	31.42	31.42	1	14
5	-21967	-29176	-6324	1830	1787	715	31.42	31.42	1	12
6	-22566	-31448	-5626	2510	3200	780	31.42	31.42	3	7.9
7	-23907	-34643	-4431	2605	3553	915	31.42	31.42	3	7.2
8	-25119	-38069	-8670	2302	3928	913	31.42	31.42	2	6.8
9	-27389	-30292	-9582	2077	3175	667	31.42	31.42	3	8.2
Massimi/minimi										

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
1							31.42			
1								31.42		
8										6.8

Muro [Platea]: 127 - Nodi: [2090-2089-2086]Pann=42Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=18.058$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-40384	-17531	-3706	3228	-115	56	31.42	31.42	3	10
2	-40478	-18473	-2879	3231	-173	84	31.42	31.42	3	10
3	-40079	-19067	-2124	3221	-186	151	31.42	31.42	3	9.9
4	-39305	-19558	-1412	3156	-207	232	31.42	31.42	3	9.8
5	-38314	-19742	-604	3045	-295	327	31.42	31.42	3	9.8
6	-36975	-19847	76	2884	-328	454	31.42	31.42	3	9.8
7	-35160	-19754	344	2695	-241	518	31.42	31.42	3	10
8	-34994	-19201	331	2606	-26	359	31.42	31.42	2	11
9	-34558	-19055	4	2564	616	330	31.42	31.42	2	11
10	-32545	-18989	73	2664	835	363	31.42	31.42	2	11
11	-30301	-17746	-1251	2126	1701	296	31.42	31.42	2	13
12	-36113	-19496	-2356	2830	2497	385	31.42	31.42	2	10
13	-39933	-21059	-3974	3526	2446	531	31.42	31.42	2	8.2
14	-44345	-20560	-6182	3811	2117	535	31.42	31.42	2	7.8
15	-42304	-20266	-5424	3735	2300	299	31.42	31.42	3	8.3
16	-41402	-17200	-4899	3339	1867	48	31.42	31.42	3	9.9
17	-38957	-13861	-2190	2916	1203	-99	31.42	31.42	1	11
18	-40010	-16247	-3656	3112	427	34	31.42	31.42	3	11
19	-39830	-17493	-2940	3141	2	-111	31.42	31.42	1	10
20	-39802	-19074	-2909	3367	329	154	31.42	31.42	3	9.4
21	-39290	-19473	-2932	3463	711	178	31.42	31.42	3	9.1
22	-40042	-20186	-4910	3726	2012	304	31.42	31.42	3	8.2
23	-39335	-19531	-3384	3540	1137	173	31.42	31.42	3	8.9
24	-39867	-18952	-3722	3557	1395	152	31.42	31.42	3	8.9
25	-39938	-18509	-3299	3394	537	157	31.42	31.42	3	9.3
26	-39775	-17231	-4082	3368	726	151	31.42	31.42	3	9.4
27	-39426	-19438	-2496	3359	305	186	31.42	31.42	3	9.3
28	-36174	-20008	-646	2999	62	328	31.42	31.42	3	9.8
29	-36108	-20065	-961	3107	743	328	31.42	31.42	2	9.5
30	-37181	-19888	-1544	3385	1017	218	31.42	31.42	2	9.1
31	-38730	-20347	-3640	3604	1716	295	31.42	31.42	3	8.5
32	-37381	-20539	-2418	3493	1429	214	31.42	31.42	2	8.8
33	-38444	-20723	-3461	3598	1973	286	31.42	31.42	2	8.5
34	-37388	-20527	-1580	3284	671	254	31.42	31.42	3	9.2
35	-37742	-20227	-1205	3159	130	266	31.42	31.42	3	9.6
36	-36745	-20035	-1104	3098	286	281	31.42	31.42	3	9.6
37	-38158	-20145	-2248	3347	754	235	31.42	31.42	3	9.2
38	-38805	-19978	-2289	3360	529	218	31.42	31.42	3	9.2
39	-38533	-20037	-1812	3270	266	221	31.42	31.42	3	9.4
40	-38900	-19933	-3173	3543	1327	249	31.42	31.42	3	8.7
41	-38783	-19966	-2750	3460	900	228	31.42	31.42	3	8.9
42	-38090	-20403	-2667	3422	1087	247	31.42	31.42	3	9.0
Massimi/minimi										
1							31.42			
1								31.42		
14										7.8

Muro [Platea]: 128 - Nodi: [2089-2085-2086]Pann=12Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=22.056$ [(4+5)-II-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-37312	-22118	8273	3306	1039	-592	31.42	31.42	2	8.4
2	-41767	-21228	12135	3392	1451	-904	31.42	31.42	1	7.8

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
3	-35384	-26206	12158	2809	2140	-860	31.42	31.42	1	8.8
4	-31314	-32149	14750	2594	3027	-1119	31.42	31.42	2	7.7
5	-27597	-37668	12450	2420	3566	-1123	31.42	31.42	3	7.0
6	-30556	-30866	7975	2922	3246	-1037	31.42	31.42	3	7.4
7	-31149	-26224	5490	2482	2587	-613	31.42	31.42	3	9.6
8	-27321	-22520	2900	1866	1548	-326	31.42	31.42	3	14
9	-34022	-24653	3691	2896	1175	-418	31.42	31.42	2	9.7
10	-31817	-25476	7673	3249	2096	-614	31.42	31.42	3	8.2
11	-33688	-26110	10425	3322	2051	-816	31.42	31.42	2	7.7
12	-30970	-28048	10366	3175	2583	-972	31.42	31.42	3	7.6
Massimi/minimi										
1							31.42			
1								31.42		
5										7.0

Muro [Platea]: 129 - Nodi: [2050-2054-2049]Pann=10Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=16.739$ [(4+5)-II-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-18882	-25661	4263	3048	-1640	2812	31.42	31.42	3	8.5
2	-17848	-26416	4099	2787	-1226	2804	31.42	31.42	3	8.8
3	-14619	-25262	4451	4089	-2121	3775	31.42	31.42	3	6.1
4	-12600	-24005	5023	4780	-2392	3354	31.42	31.42	3	5.8
5	-12996	-21206	5124	5109	-3173	2659	31.42	31.42	3	6.1
6	-14003	-22738	4417	4399	-2415	3028	31.42	31.42	3	6.5
7	-16094	-24175	4348	3790	-1881	3203	31.42	31.42	3	7.0
8	-19230	-24778	4447	3029	-1733	2826	31.42	31.42	3	8.5
9	-19267	-25566	4183	3118	-1759	2826	31.42	31.42	3	8.4
10	-17205	-25041	4182	3684	-1914	3458	31.42	31.42	3	6.9
Massimi/minimi										
1							31.42			
1								31.42		
4										5.8

Muro [Platea]: 130 - Nodi: [2049-2054-2057]Pann=12Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=16.467$ [(4+5)-II-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-21468	-11499	4490	-3652	7500	2460	31.42	31.42	3	4.7
2	-21155	-11702	3682	-3334	6482	2589	31.42	31.42	3	5.2
3	-23310	-12881	3366	-3691	6418	1939	31.42	31.42	3	5.7
4	-24546	-15047	3578	-4200	6376	1177	31.42	31.42	3	6.4
5	-27352	-15480	4347	-3208	5185	-365	31.42	31.42	3	8.7
6	-21629	-16732	4052	-4700	5936	179	31.42	31.42	3	8.0
7	-21036	-17630	3283	-4539	6556	817	31.42	31.42	2	6.7
8	-25901	-17432	1949	-2172	10032	2463	31.42	31.42	1	3.9
9	-20202	-10927	3964	-4162	8498	2551	31.42	31.42	3	4.3
10	-22106	-13008	3891	-4114	7289	2036	31.42	31.42	3	5.1
11	-22273	-15274	3996	-4661	7098	1352	31.42	31.42	3	5.7
12	-20829	-14479	3735	-4654	7897	1840	31.42	31.42	3	4.9
Massimi/minimi										
1							31.42			
1								31.42		
8										3.9

Muro [Platea]: 131 - Nodi: [2048-2049-2057]Pann=12Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=14.081$ [(4+5)-IV-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-22122	-6761	983	-3141	7848	-3258	31.42	31.42	3	4.1
2	-22467	-6625	1899	-2518	7697	-2638	31.42	31.42	3	4.4
3	-22472	-4693	5292	-2297	8820	-500	31.42	31.42	3	4.8
4	-22495	-7359	1253	-2636	6717	-2731	31.42	31.42	3	4.8
5	-22156	-8849	-576	-2898	6593	-3148	31.42	31.42	3	4.8
6	-22971	-7853	-2792	-2836	6456	-3369	31.42	31.42	3	4.7
7	-23037	-7271	-1852	-2874	7215	-3711	31.42	31.42	3	4.2
8	-22382	-6720	-2198	-2751	8095	-4215	31.42	31.42	3	3.7
9	-18761	-10418	-4880	-1403	10274	-3571	31.42	31.42	2	3.4
10	-22493	-3852	-2807	-2454	8490	-4075	31.42	31.42	3	3.6
11	-21682	-7102	17	-3100	8155	-3880	31.42	31.42	3	3.8
12	-22132	-7465	-724	-2942	7579	-3525	31.42	31.42	3	4.1
Massimi/minimi										
1							31.42			
1								31.42		
9										3.4

Muro [Platea]: 132 - Nodi: [2048-2057-2056]Pann=10Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=4.854$ [(4+5)-I-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-11894	-14762	9111	-1260	5626	6103	31.42	31.42	3	4.1
2	-12067	-15517	8915	-1319	6897	5685	31.42	31.42	3	3.9
3	-10943	-4371	6123	-314	8166	4860	31.42	31.42	3	3.4
4	-14655	-20570	5791	-4142	7671	4629	31.42	31.42	3	4.1
5	-13930	-14196	5799	-1417	4840	6361	31.42	31.42	3	4.3
6	-15019	-17632	11064	186	4779	6168	31.42	31.42	3	4.5
7	-4078	-12058	16903	4415	5562	7355	31.42	31.42	3	3.7
8	-15181	-12227	8794	454	4616	5593	31.42	31.42	3	4.6
9	-13336	-12406	6879	-419	5570	5763	31.42	31.42	3	4.2
10	-13815	-17302	7485	144	5120	5594	31.42	31.42	3	4.6
Massimi/minimi										
1							31.42			
1								31.42		
3										3.4

Muro [Platea]: 133 - Nodi: [2048-2056-2053]Pann=9Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=5.018$ [(4+5)-III-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-11948	-20512	10311	7042	-1402	3557	31.42	31.42	3	4.5
2	-351	-19331	14819	9988	-390	5062	31.42	31.42	3	2.9
3	-8214	-22421	7420	7329	-2303	3674	31.42	31.42	3	4.2
4	-11241	-19387	7000	6744	-2906	3935	31.42	31.42	3	4.4
5	-13892	-17878	6614	2455	-5677	6750	31.42	31.42	3	4.0
6	-13951	-17458	10078	5453	-2151	3048	31.42	31.42	3	5.6
7	-13534	-18979	10759	5228	-1281	2526	31.42	31.42	3	6.2
8	-12237	-24237	8880	4584	431	1897	31.42	31.42	3	7.3
9	-13626	-21595	10023	6050	-1359	2359	31.42	31.42	3	5.7
Massimi/minimi										
1							31.42			
1								31.42		
2										2.9

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Muro [Platea]: 134 - Nodi: [2047-2048-2053]Pann=7Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=5.651$ [(4+5)-III-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-26220	-16435	-2348	-2275	5455	-693	31.42	31.42	3	7.9
2	-26472	-16889	-2467	-2597	4960	-1061	31.42	31.42	3	8.1
3	-23097	-13644	-6335	-1698	8013	-3042	31.42	31.42	3	4.3
4	-25368	-12643	-5638	-1875	6405	-1684	31.42	31.42	3	5.9
5	-25048	-13722	-3481	-1775	6000	-950	31.42	31.42	3	6.9
6	-27835	-11934	-1444	-933	5675	-929	31.42	31.42	3	7.2
7	-27033	-14097	-2272	-1665	5728	-348	31.42	31.42	3	7.9
Massimi/minimi										
1							31.42			
1								31.42		
3										4.3

Muro [Platea]: 135 - Nodi: [2056-2057-2011-2060]Pann=8Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=6.896$ [(4+5)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-33970	-3527	-15375	554	7011	-3781	31.42	31.42	3	4.1
2	-12057	-2585	-15902	1957	5389	-3050	31.42	31.42	2	5.2
3	-9337	319	-14104	2475	4788	-1626	31.42	31.42	1	6.7
4	-13313	-4308	-9449	1921	4219	-1890	31.42	31.42	1	7.3
5	-9702	880	-11427	959	8074	-2096	31.42	31.42	2	4.2
6	-10218	876	-15509	1745	5063	-3190	31.42	31.42	2	5.2
7	-12977	-2121	-9829	2279	4000	-2588	31.42	31.42	1	6.7
8	-31320	-11262	-19826	690	-1688	-4121	31.42	31.42	3	8.1
Massimi/minimi										
1							31.42			
1								31.42		
1										4.1

Muro [Platea]: 136 - Nodi: [2088-2085-2089]Pann=27Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=9.842$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-4966	-28174	1726	-112	1272	430	31.42	31.42	(4+5)-V-1	18
2	-7235	-28646	-574	394	1624	469	31.42	31.42	(4+5)-V-1	15
3	-10983	-26886	-2620	848	1730	542	31.42	31.42	(4+5)-V-1	14
4	-24780	-31120	-2537	1715	1837	852	31.42	31.42	1	12
5	-27766	-26695	-6468	2076	2085	900	31.42	31.42	1	10
6	-30934	-26845	-9586	2536	2406	904	31.42	31.42	1	9.2
7	-29723	-26582	-4611	2542	3230	459	31.42	31.42	1	8.3
8	-29276	-25964	-248	2566	3634	-77	31.42	31.42	1	8.2
9	-29227	-25906	3891	2674	3900	-561	31.42	31.42	1	6.8
10	-27691	-27622	6978	2551	3695	-865	31.42	31.42	1	6.8
11	-24780	-31972	8228	2240	3463	-1061	31.42	31.42	1	7.0
12	-20682	-36490	8843	2002	3288	-1059	31.42	31.42	1	7.5
13	-16960	-41865	10018	1311	3422	-936	31.42	31.42	1	7.7
14	-14336	-36822	7298	1448	3434	-809	31.42	31.42	3	7.7
15	-14385	-33178	4909	1969	2815	-807	31.42	31.42	3	8.8
16	-17803	-26855	1774	1785	1444	45	31.42	31.42	1	16
17	-5185	-25754	3064	-200	1146	111	31.42	31.42	(4+5)-V-1	24
18	-17940	-29864	6971	1747	3194	-1173	31.42	31.42	3	7.2
19	-16419	-30269	6183	1551	2850	-1065	31.42	31.42	3	8.0
20	-17723	-29051	6247	1377	2836	-886	31.42	31.42	3	8.4
21	-14819	-29558	6019	601	2016	-480	31.42	31.42	3	13
22	-16614	-29533	5403	804	2267	-424	31.42	31.42	3	12
23	-26504	-28173	5002	2368	3482	-842	31.42	31.42	1	7.2

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
24	-19438	-28134	5703	1538	3007	-772	31.42	31.42	3	8.2
25	-22911	-28127	4493	1990	3356	-629	31.42	31.42	2	7.8
26	-18459	-29105	4281	1145	2538	-267	31.42	31.42	3	11
27	-21507	-27663	2848	1689	2910	-186	31.42	31.42	3	10.0
Massimi/minimi										
1							31.42			
1								31.42		
10										6.8

Muro [Platea]: 137 - Nodi: [2009-2052-2050]Pann=28Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=4.724$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-21602	-24094	-11161	1799	1001	53	31.42	31.42	3	16
2	-23791	-25486	-9160	2415	1974	178	31.42	31.42	3	12
3	-24733	-26233	-6721	2563	3067	380	31.42	31.42	2	8.9
4	-23430	-25895	-5137	3160	3768	853	31.42	31.42	2	6.6
5	-20667	-27778	-4562	3496	4213	1433	31.42	31.42	2	5.5
6	-18582	-28334	-4348	3712	4347	1697	31.42	31.42	2	5.1
7	-16414	-27206	-4714	3937	4065	1844	31.42	31.42	3	5.0
8	-13966	-26066	-4868	3882	3566	1803	31.42	31.42	3	5.0
9	-12062	-24681	-5573	3696	2484	1644	31.42	31.42	3	5.2
10	-13893	-27634	-5026	3789	3306	1840	31.42	31.42	3	5.0
11	-15768	-29401	-5595	3717	3782	1906	31.42	31.42	3	5.1
12	-17931	-30689	-6955	3391	3839	1901	31.42	31.42	3	5.5
13	-19641	-31138	-8221	2870	3592	1807	31.42	31.42	2	5.8
14	-20916	-28835	-9478	2456	3067	1637	31.42	31.42	2	6.6
15	-21267	-24777	-9802	1978	2114	1332	31.42	31.42	2	8.8
16	-19834	-18026	-9023	1470	929	903	31.42	31.42	3	12
17	-14925	-9494	-7029	707	188	464	31.42	31.42	(4+5)-I-2	24
18	18252	-900	2887	-2009	-1119	-1185	31.42	31.42	(4+5)-VII-3	6.8
19	-10674	-13408	-8916	893	-1151	-1051	31.42	31.42	3	13
20	-17470	-20449	-11653	1731	197	-227	31.42	31.42	3	15
21	-20520	-28423	-8368	2656	3054	1361	31.42	31.42	2	7.0
22	-20804	-25788	-9480	2331	2097	1026	31.42	31.42	3	8.8
23	-21653	-26907	-8318	2708	2639	1045	31.42	31.42	3	7.9
24	-18998	-29509	-5501	3406	4088	1668	31.42	31.42	2	5.4
25	-19909	-29681	-7060	3012	3646	1524	31.42	31.42	2	6.0
26	-20471	-28291	-5491	3322	3953	1391	31.42	31.42	2	5.8
27	-21011	-28284	-6788	2998	3474	1213	31.42	31.42	2	6.6
28	-22325	-27281	-6074	3138	3465	1013	31.42	31.42	2	6.9
Massimi/minimi										
1							31.42			
1								31.42		
7										5.0

Muro [Platea]: 138 - Nodi: [2052-2054-2050]Pann=14Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=27.018$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-26685	-19282	-3948	5902	2501	298	31.42	31.42	2	4.9
2	-28290	-20508	-2826	5433	2551	320	31.42	31.42	2	5.4
3	-28394	-21130	-1695	4219	2472	428	31.42	31.42	2	6.7
4	-27840	-19427	-2620	5419	2581	354	31.42	31.42	2	5.4
5	-26313	-19177	-3338	5964	2598	308	31.42	31.42	2	4.9
6	-26330	-19354	-4898	5874	2624	383	31.42	31.42	1	4.9
7	-24608	-17456	-5500	5718	2660	328	31.42	31.42	1	5.0
8	-23195	-15231	-6287	5695	1984	443	31.42	31.42	1	4.9
9	-21198	-10759	-4748	5171	1639	-452	31.42	31.42	3	5.3
10	-22215	-10910	-4896	4837	1416	-691	31.42	31.42	3	5.4
11	-22881	-11362	-5561	4685	1378	-732	31.42	31.42	3	5.5

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
12	-23754	-14248	-5119	5539	2060	-169	31.42	31.42	3	5.3
13	-26878	-19122	-5741	5804	2477	362	31.42	31.42	1	5.0
14	-24913	-15768	-6337	5573	2188	231	31.42	31.42	1	5.2
Massimi/minimi										
1							31.42			
1								31.42		
5										4.9

Muro [Platea]: 139 - Nodi: [2012-2054-2052]Pann=31Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=4.974$ [(4+5)-III-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-24510	-20055	5565	2319	1251	-267	31.42	31.42	3	12
2	-25118	-23049	5014	3190	2019	-546	31.42	31.42	3	8.1
3	-24743	-24153	4503	3934	2521	-771	31.42	31.42	3	6.4
4	-24330	-23835	3682	4735	2925	-1023	31.42	31.42	3	5.3
5	-24008	-22247	2980	5331	3152	-1240	31.42	31.42	3	4.6
6	-23626	-20049	2449	5584	3288	-1402	31.42	31.42	3	4.3
7	-22918	-17812	2118	5471	3343	-1465	31.42	31.42	3	4.3
8	-21657	-15277	1847	5031	3256	-1373	31.42	31.42	3	4.6
9	-26222	-13426	635	5630	3008	-905	31.42	31.42	1	4.7
10	-22752	-14690	1581	5035	3280	-1433	31.42	31.42	3	4.6
11	-24158	-17107	1614	5448	3348	-1435	31.42	31.42	3	4.4
12	-25482	-18924	1898	5436	3244	-1340	31.42	31.42	3	4.5
13	-26533	-20644	2322	4996	3028	-1084	31.42	31.42	3	5.0
14	-27132	-22617	2820	4110	2576	-680	31.42	31.42	3	6.4
15	-28736	-23614	2011	2976	2161	-154	31.42	31.42	3	9.9
16	-31775	-22497	2265	2249	1532	597	31.42	31.42	1	11
17	-30117	-19848	4059	1610	1143	839	31.42	31.42	1	13
18	-25844	-16084	5847	946	896	1172	31.42	31.42	2	14
19	-5418	-3369	5784	-1052	-16	1174	31.42	31.42	(4+5)-III-4	12
20	16444	-1521	6726	-3018	-390	1001	31.42	31.42	(4+5)-III-4	5.5
21	-17401	-9915	908	743	182	479	31.42	31.42	(4+5)-III-1	24
22	-23640	-16234	2412	1521	495	387	31.42	31.42	1	16
23	-24732	-22048	2908	5125	3101	-1152	31.42	31.42	3	4.8
24	-24710	-20421	2404	5439	3241	-1292	31.42	31.42	3	4.5
25	-25613	-21574	2707	5009	3041	-1082	31.42	31.42	3	5.0
26	-27841	-21978	3625	2713	1418	140	31.42	31.42	1	11
27	-26055	-22968	3086	4383	2750	-796	31.42	31.42	3	5.9
28	-25011	-23385	3442	4600	2856	-913	31.42	31.42	3	5.5
29	-26729	-23287	4091	3214	1979	-229	31.42	31.42	3	8.9
30	-25393	-23755	4018	3912	2473	-630	31.42	31.42	3	6.7
31	-26764	-23405	3458	3770	2390	-438	31.42	31.42	3	7.3
Massimi/minimi										
1							31.42			
1								31.42		
6										4.3

Muro [Platea]: 140 - Nodi: [2009-2012-2052]Pann=29Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=4.067$ [(4+5)-VIII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-23308	-11412	2543	2123	3050	273	31.42	31.42	3	8.3
2	-23398	-16020	2871	2541	3311	207	31.42	31.42	3	8.1
3	-25360	-21109	2813	2378	3194	-146	31.42	31.42	1	8.9
4	-23795	-16736	455	2295	3256	-308	31.42	31.42	1	8.1
5	-22704	-12463	-257	1741	2978	-365	31.42	31.42	1	8.4
6	-20213	-7417	-278	1048	1918	-303	31.42	31.42	1	12
7	-8620	-4607	-2303	-106	1118	336	31.42	31.42	(4+5)-III-1	18
8	16756	5275	6841	-2098	-699	-875	31.42	31.42	(4+5)-VIII-3	7.4
9	-12257	-4980	-3308	1069	-1637	-667	31.42	31.42	2	11

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
10	-18478	-9351	-2704	1329	-1566	-453	31.42	31.42	1	14
11	-21271	-12360	-1479	1604	-1778	-387	31.42	31.42	1	13
12	-22742	-13324	568	1756	-1838	-290	31.42	31.42	1	13
13	-23392	-12905	2721	1823	-1801	-197	31.42	31.42	1	14
14	-21945	-11508	2811	1725	-1676	72	31.42	31.42	3	16
15	-19710	-8311	3756	1539	-1417	227	31.42	31.42	3	16
16	-14699	-3711	2718	1301	-1425	544	31.42	31.42	3	13
17	12901	5074	-6623	-1645	-563	777	31.42	31.42	(4+5)-IV-4	9.4
18	-11763	-3998	2051	553	1136	-276	31.42	31.42	(4+5)-VII-2	19
19	-21387	-6737	1680	1427	2031	215	31.42	31.42	3	12
20	-22023	-12533	3892	2208	-37	-91	31.42	31.42	1	13
21	-19978	-10102	1915	2086	393	138	31.42	31.42	3	13
22	-21264	-13027	2005	2382	1455	171	31.42	31.42	3	12
23	-20693	-13820	209	2153	1290	-275	31.42	31.42	1	12
24	-18799	-11101	-397	1852	233	-215	31.42	31.42	1	14
25	-20344	-13513	-228	1962	-148	-189	31.42	31.42	1	14
26	-22524	-15341	3549	2530	1821	-104	31.42	31.42	1	11
27	-21792	-15909	1376	2385	1768	-211	31.42	31.42	1	11
28	-21874	-14228	2773	2202	104	-139	31.42	31.42	1	13
29	-21240	-14659	1263	2111	65	-171	31.42	31.42	1	13
Massimi/minimi										
1							31.42			
1								31.42		
8										7.4

Muro [Platea]: 141 - Nodi: [2079-2078-2084]Pann=8Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=6.072$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-12263	2339	8748	-2055	-729	-487	31.42	31.42	(4+5)-V-4	11
2	-12339	3716	7352	-4237	-1161	-1233	31.42	31.42	(4+5)-V-4	5.1
3	-15294	2350	7370	-5109	-1169	-1965	31.42	31.42	(4+5)-V-4	4.0
4	-12684	168	7617	-4032	-851	-1856	31.42	31.42	(4+5)-V-4	4.7
5	-9151	-1322	8606	-2383	-484	-1650	31.42	31.42	(4+5)-V-4	6.8
6	-50302	-7854	1832	3124	1360	-486	31.42	31.42	1	9.7
7	-49143	-4833	6330	2021	1110	-164	31.42	31.42	1	16
8	-15448	3898	5771	-2835	-929	-1491	31.42	31.42	(4+5)-V-4	6.6
Massimi/minimi										
1							31.42			
1								31.42		
3										4.0

Muro [Platea]: 142 - Nodi: [2083-2079-2084]Pann=8Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=10.014$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-35143	-18708	-7685	6244	1199	188	31.42	31.42	1	5.0
2	-31738	-18829	-14331	6504	1816	326	31.42	31.42	1	4.6
3	-38344	-19142	-14287	3839	1593	193	31.42	31.42	1	8.2
4	-42424	-13026	-5598	5326	650	-195	31.42	31.42	1	6.1
5	-36670	-19549	-8556	6907	1130	423	31.42	31.42	1	4.4
6	-37173	-17679	-8875	6306	1621	513	31.42	31.42	1	4.8
7	-21164	-11192	-3145	5036	291	-452	31.42	31.42	3	5.4
8	-19404	-11796	-2446	6075	169	-228	31.42	31.42	3	4.6
Massimi/minimi										
1							31.42			
1								31.42		
5										4.4

Muro [Platea]: 143 - Nodi: [2083-2077-2079]Pann=8Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=11.172$ [(4+5)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-193	-47794	-472	3605	2834	361	31.42	31.42	1	6.4
2	-3762	-55895	-9307	3534	3339	488	31.42	31.42	1	6.5
3	-3494	-45132	-3086	3735	4746	2191	31.42	31.42	1	4.4
4	2508	-46137	-616	3650	3868	820	31.42	31.42	1	5.6
5	15	-51277	54	4258	2458	-946	31.42	31.42	1	4.9
6	2875	-50467	-3257	3808	2251	482	31.42	31.42	1	5.8
7	2180	-49586	-1752	3781	3588	189	31.42	31.42	1	6.3
8	2215	-43145	-800	4132	1834	-432	31.42	31.42	1	5.5
Massimi/minimi										
1							31.42			
1								31.42		
3										4.4

Muro [Platea]: 144 - Nodi: [2088-2083-2084]Pann=13Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=13.518$ [(4+5)-VI-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-27822	-40761	-7428	2393	3290	754	31.42	31.42	1	8.3
2	-28877	-39108	-3100	2357	3254	383	31.42	31.42	1	9.1
3	-26751	-39038	203	2021	3283	163	31.42	31.42	1	9.6
4	-21621	-40324	2825	1661	3253	-308	31.42	31.42	1	9.3
5	-25116	-40937	-1151	2144	3322	-112	31.42	31.42	1	9.7
6	-24854	-34844	-4465	2236	3139	441	31.42	31.42	3	9.0
7	-21988	-35587	-6572	2049	3694	814	31.42	31.42	3	7.2
8	-16007	-36837	-7740	1335	4134	835	31.42	31.42	3	6.6
9	-14504	-50613	-4452	1218	4600	298	31.42	31.42	1	7.2
10	-18051	-49741	-8740	1380	3876	636	31.42	31.42	1	7.8
11	-20143	-47610	-11972	1498	3986	903	31.42	31.42	1	7.1
12	-24583	-49024	-17865	2019	3597	1520	31.42	31.42	1	6.8
13	-27928	-42853	-13124	2368	3353	1139	31.42	31.42	1	7.5
Massimi/minimi										
1							31.42			
1								31.42		
8										6.6

Muro [Platea]: 145 - Nodi: [2082-2075-2077]Pann=8Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=15.425$ [(4+5)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	517	-36954	-3574	4401	4107	1621	31.42	31.42	1	4.2
2	-1093	-39381	-8635	4633	3531	1617	31.42	31.42	1	4.1
3	-4789	-39615	-7940	3839	4574	1692	31.42	31.42	1	4.8
4	2379	-37262	-3358	4459	5150	1133	31.42	31.42	1	4.5
5	1121	-40097	-3748	4964	3742	383	31.42	31.42	1	4.7
6	2150	-37526	-6742	4310	3141	1721	31.42	31.42	1	4.1
7	2081	-38980	-4970	4667	4997	1252	31.42	31.42	1	4.2
8	2625	-34152	-3077	5148	3453	688	31.42	31.42	1	4.3
Massimi/minimi										
1							31.42			
1								31.42		
2										4.1

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Muro [Platea]: 146 - Nodi: [2082-2077-2083]Pann=3Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=15.306$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-26335	-23504	-22280	6261	1937	321	31.42	31.42	1	4.7
2	-24977	-24283	-22745	5660	2123	793	31.42	31.42	1	4.7
3	-21167	-23374	-21053	5843	2841	735	31.42	31.42	1	4.5
Massimi/minimi										
1							31.42			
1								31.42		
3										4.5

Muro [Platea]: 147 - Nodi: [2013-2082-2087]Pann=31Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=5.147$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-17959	-20530	6323	4191	2066	279	31.42	31.42	1	6.5
2	-14680	-20295	5131	3517	1900	253	31.42	31.42	1	7.5
3	-11522	-19158	3932	2282	1483	184	31.42	31.42	1	11
4	-8770	-11888	6206	1259	898	-452	31.42	31.42	(4+5)-VII-3	16
5	-4512	-16187	6375	178	1099	-387	31.42	31.42	(4+5)-II-3	19
6	-9879	-17585	5067	-713	1366	232	31.42	31.42	1	18
7	-10047	-17441	4512	-796	1492	-171	31.42	31.42	(4+5)-II-3	17
8	-14863	-16532	2251	-1722	1333	-186	31.42	31.42	3	15
9	-13938	-12104	90	-2347	820	-165	31.42	31.42	3	11
10	13900	-2045	6311	-2688	-516	-1298	31.42	31.42	(4+5)-V-1	5.7
11	-15067	-9201	-1226	940	201	-658	31.42	31.42	(4+5)-III-3	18
12	-22721	-11710	-4605	1718	271	-1002	31.42	31.42	3	11
13	-30413	-12115	-2874	3041	748	-1085	31.42	31.42	2	7.6
14	-37337	-13883	-176	3842	1307	-779	31.42	31.42	1	7.1
15	-41911	-14007	5441	4228	1251	-595	31.42	31.42	1	7.0
16	-31968	-18319	6228	4661	1740	-139	31.42	31.42	1	6.6
17	-23596	-20286	6497	4590	2016	175	31.42	31.42	1	6.3
18	-16890	-17269	3692	454	1901	152	31.42	31.42	1	14
19	-16913	-17697	4185	1993	2166	260	31.42	31.42	1	12
20	-14588	-18063	3965	775	1999	228	31.42	31.42	1	13
21	-18926	-18218	4845	2872	2156	253	31.42	31.42	1	9.3
22	-16118	-15627	1400	612	1413	247	31.42	31.42	1	17
23	-20744	-14547	3716	2860	1371	-106	31.42	31.42	3	10.0
24	-18420	-10897	4590	2037	977	-307	31.42	31.42	(4+5)-I-3	12
25	-19008	-17085	2465	2544	1821	190	31.42	31.42	1	11
26	-19113	-13743	1615	2726	899	-253	31.42	31.42	3	9.8
27	-22432	-14377	4513	3314	1503	-135	31.42	31.42	3	8.7
28	-24354	-18098	3979	3825	2104	46	31.42	31.42	1	7.8
29	-21298	-18229	4125	3337	2098	99	31.42	31.42	1	8.6
30	-25360	-13129	1860	3426	1016	-312	31.42	31.42	3	8.1
31	-28512	-13856	4492	3945	1335	-329	31.42	31.42	3	7.3
Massimi/minimi										
1							31.42			
1								31.42		
10										5.7

Muro [Platea]: 148 - Nodi: [2082-2083-2088]Pann=14Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=19.036$ [(4+5)-III-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-41421	-28114	9761	3469	2437	-792	31.42	31.42	1	7.9
2	-40181	-28928	7079	3242	2520	-659	31.42	31.42	1	8.5

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
3	-41121	-25854	4974	3219	2239	-510	31.42	31.42	1	9.0
4	-40673	-20525	3589	3441	1658	-331	31.42	31.42	1	8.8
5	-39142	-24594	4613	3427	1904	-324	31.42	31.42	1	8.8
6	-39751	-27947	6486	3388	2210	-464	31.42	31.42	1	8.6
7	-41291	-27444	8061	3431	2299	-612	31.42	31.42	1	8.3
8	-43235	-25349	9487	3577	2237	-791	31.42	31.42	1	7.7
9	-40506	-18485	10420	3481	2008	-1172	31.42	31.42	3	7.2
10	-40511	-15780	10729	3837	1579	-1292	31.42	31.42	3	6.5
11	-49201	-13989	9149	4092	1178	-819	31.42	31.42	1	7.1
12	-48109	-18259	12555	3996	1411	-1063	31.42	31.42	1	6.9
13	-44348	-24348	12109	3677	2042	-1002	31.42	31.42	1	7.3
14	-44930	-21391	9708	3865	1933	-890	31.42	31.42	1	7.2
Massimi/minimi										
1							31.42			
1								31.42		
10										6.5

Muro [Platea]: 149 - Nodi: [2082-2088-2087]Pann=43Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=11.424$ [(4+5)-V-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-18652	-42379	6003	1106	2594	-1436	31.42	31.42	1	8.4
2	-16301	-41714	4626	1065	2257	-1438	31.42	31.42	1	9.1
3	-13072	-39112	2941	989	1985	-1225	31.42	31.42	2	10
4	-10857	-36200	1439	834	1593	-1056	31.42	31.42	2	12
5	-4766	-27676	2231	369	1472	-633	31.42	31.42	(4+5)-VII-3	15
6	-2371	-24025	264	112	1318	-528	31.42	31.42	(4+5)-VII-3	16
7	-4204	-17293	-5047	168	856	518	31.42	31.42	(4+5)-II-3	21
8	-7308	-21569	-924	444	1386	624	31.42	31.42	(4+5)-II-3	15
9	-9730	-25426	1633	645	1576	438	31.42	31.42	(4+5)-II-3	15
10	-15094	-32884	7232	801	1857	399	31.42	31.42	3	14
11	-16764	-35253	7833	971	2704	312	31.42	31.42	3	11
12	-17458	-37602	8151	1069	3242	-101	31.42	31.42	3	9.8
13	-20331	-41280	10993	1247	3470	-451	31.42	31.42	1	8.5
14	-17836	-43139	12523	1321	3808	-967	31.42	31.42	1	7.1
15	-18539	-42518	9597	1638	4534	-813	31.42	31.42	1	6.3
16	-20447	-41406	6742	1931	4755	-616	31.42	31.42	1	6.2
17	-21971	-40178	4842	2206	4844	-424	31.42	31.42	1	6.3
18	-23145	-39215	4651	2275	4718	-272	31.42	31.42	1	6.6
19	-23589	-38500	5494	2208	4426	-252	31.42	31.42	1	7.0
20	-23407	-38191	7417	1982	3931	-434	31.42	31.42	1	7.5
21	-22961	-37665	9676	1682	3238	-862	31.42	31.42	1	8.0
22	-22300	-40217	8596	1307	3067	-1210	31.42	31.42	1	7.8
23	-20564	-41933	7328	1146	2850	-1356	31.42	31.42	1	8.0
24	-20683	-39214	6998	2149	4302	-542	31.42	31.42	1	6.8
25	-21568	-39147	5704	2324	4522	-471	31.42	31.42	1	6.6
26	-20654	-38590	6241	2257	4134	-491	31.42	31.42	1	7.1
27	-21922	-39195	5082	2267	4346	-489	31.42	31.42	1	6.8
28	-20577	-38838	5393	2148	3942	-611	31.42	31.42	1	7.2
29	-19857	-40073	5257	1711	3494	-906	31.42	31.42	1	7.6
30	-22382	-39620	6723	1768	3753	-801	31.42	31.42	1	7.3
31	-21184	-40285	5979	1713	3656	-903	31.42	31.42	1	7.3
32	-22231	-39257	5450	2076	4134	-596	31.42	31.42	1	7.0
33	-16234	-33677	6276	1265	2848	-103	31.42	31.42	3	11
34	-20255	-37504	6460	2135	3780	-478	31.42	31.42	1	7.7
35	-19588	-36062	7013	1834	3274	-393	31.42	31.42	1	8.9
36	-20467	-37716	7850	1902	3771	-418	31.42	31.42	1	7.8
37	-18168	-39032	4671	1558	3106	-912	31.42	31.42	1	8.2
38	-19558	-37660	5411	2001	3504	-623	31.42	31.42	1	7.9
39	-13746	-34121	3206	1122	2417	-593	31.42	31.42	2	11
40	-8155	-26242	3494	583	2043	-379	31.42	31.42	(4+5)-VII-3	13
41	-15606	-33371	4942	1355	2680	-321	31.42	31.42	2	11
42	-15267	-36562	3667	1358	2794	-719	31.42	31.42	2	9.3
43	-17064	-35355	4961	1718	3108	-448	31.42	31.42	2	9.1
Massimi/minimi										
1							31.42			
1								31.42		
16										6.2

Muro [Platea]: 150 - Nodi: [2014-2085-2078]Pann=14Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=6.053$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-14006	17227	4659	2399	-2645	-807	31.42	31.42	(4+5)-V-4	11
2	-28903	-4082	-6103	3864	381	720	31.42	31.42	1	12
3	-11213	19504	-4694	1625	-2267	917	31.42	31.42	(4+5)-V-4	12
4	-11223	22875	2263	1446	-3084	-182	31.42	31.42	(4+5)-V-4	11
5	-16690	19090	5757	1705	-2479	-636	31.42	31.42	(4+5)-V-3	12
6	-15027	14889	9490	1474	-1853	-1081	31.42	31.42	(4+5)-VII-3	13
7	-23249	-5819	11099	2581	722	-1645	31.42	31.42	1	12
8	-12019	5677	18144	845	-1253	-2886	31.42	31.42	3	10
9	-26437	-4511	12318	3074	445	-1758	31.42	31.42	1	11
10	-31929	-13300	10372	4401	1653	-1746	31.42	31.42	1	8.8
11	-36129	-12844	14584	5638	1753	-2006	31.42	31.42	1	7.2
12	-14222	-4341	16037	2835	897	-1779	31.42	31.42	2	10
13	-16860	4588	13586	2732	-790	-1987	31.42	31.42	3	10
14	-26277	-7167	12395	3276	1054	-1560	31.42	31.42	1	11
Massimi/minimi										
1							31.42			
1								31.42		
11										7.2

Muro [Platea]: 151 - Nodi: [2085-2084-2078]Pann=11Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=6.508$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	13280	-16977	-5455	-2202	1792	959	31.42	31.42	(4+5)-VII-3	12
2	-1590	-17397	-11915	-288	1908	2120	31.42	31.42	3	12
3	-16152	-22869	-10527	2086	3274	1425	31.42	31.42	1	11
4	-262	-16755	-9774	144	3044	911	31.42	31.42	3	12
5	2854	-18423	-5395	-142	4135	435	31.42	31.42	3	11
6	-17482	-29860	8878	2784	5108	-1687	31.42	31.42	1	7.8
7	-9706	-30301	7310	2179	4686	-1468	31.42	31.42	1	8.7
8	-8376	-25393	7279	1836	3578	-1585	31.42	31.42	1	10
9	17267	-8343	6191	-2075	67	-605	31.42	31.42	(4+5)-V-4	14
10	18071	-23116	4957	-3568	1084	319	31.42	31.42	(4+5)-V-3	9.6
11	16294	-20026	399	-2838	1692	701	31.42	31.42	(4+5)-V-3	11
Massimi/minimi										
1							31.42			
1								31.42		
6										7.8

Muro [Platea]: 152 - Nodi: [2078-2076-2014]Pann=13Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=4.124$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	13813	-5229	6318	-5679	1704	-2041	31.42	31.42	(4+5)-V-4	5.0
2	16333	-2621	27	-4936	4527	-3036	31.42	31.42	(4+5)-VII-3	4.7
3	13711	-1606	1577	-4293	6559	-1999	31.42	31.42	(4+5)-V-3	5.1
4	7343	-11818	-496	-4921	6565	558	31.42	31.42	3	6.6
5	7258	-20429	1241	-5524	4717	851	31.42	31.42	3	6.4
6	4330	-14361	-1275	-5349	6528	438	31.42	31.42	3	6.9
7	11637	-1629	2831	-4256	7116	-2211	31.42	31.42	(4+5)-VII-3	4.7
8	15943	2189	3221	-2857	6808	-4050	31.42	31.42	(4+5)-V-3	3.9

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
9	18328	1048	6808	-167	5325	-5107	31.42	31.42	(4+5)-V-3	4.1
10	15893	2642	8460	1376	571	-2987	31.42	31.42	(4+5)-I-3	8.7
11	11024	1697	7307	-1057	546	-1337	31.42	31.42	(4+5)-V-4	17
12	10477	-3893	5368	-3417	404	-970	31.42	31.42	(4+5)-V-4	9.1
13	15058	-4873	3279	-3220	3199	-3737	31.42	31.42	(4+5)-V-4	5.5
Massimi/minimi										
1							31.42			
1								31.42		
8										3.9

Muro [Platea]: 153 - Nodi: [2014-2076-2074]Pann=10Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_s=6.887$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-3082	-63	-5272	3161	-2275	5817	31.42	31.42	3	4.9
2	1170	8365	-5652	-1243	-2783	4049	31.42	31.42	(4+5)-V-4	5.9
3	466	9785	-4216	-1713	-3718	3281	31.42	31.42	(4+5)-V-4	5.7
4	-1061	12700	-4291	-1476	-5684	2810	31.42	31.42	(4+5)-V-4	4.6
5	-1183	13265	-3160	-556	-6515	2975	31.42	31.42	(4+5)-V-4	4.1
6	2869	8301	-6977	2281	-3258	5498	31.42	31.42	(4+5)-VII-3	4.6
7	-2064	-4512	-8651	4378	-3358	4890	31.42	31.42	3	4.8
8	-11822	-839	-9790	2919	-3923	3557	31.42	31.42	3	5.8
9	-5271	-2387	-8164	4276	-2348	4843	31.42	31.42	3	4.9
10	1938	9097	-3947	1161	-3877	4978	31.42	31.42	(4+5)-V-4	4.5
Massimi/minimi										
1							31.42			
1								31.42		
5										4.1

Muro [Platea]: 154 - Nodi: [2014-2074-2072-2069-2067-2011]Pann=68Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_s=3.774$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	3544	15150	4333	-1187	-7481	-313	31.42	31.42	(4+5)-V-4	4.9
2	4262	11343	6159	-2362	-7517	-1037	31.42	31.42	(4+5)-V-4	4.6
3	5667	10261	7323	-2352	-8066	-1618	31.42	31.42	(4+5)-V-4	4.1
4	12738	9141	10781	-3371	-8874	-3556	31.42	31.42	(4+5)-V-4	3.2
5	21952	-1580	7546	-6422	-7331	-4333	31.42	31.42	(4+5)-V-4	3.3
6	20980	-2577	2252	-6041	-6293	-3480	31.42	31.42	(4+5)-V-4	3.8
7	19710	-2196	-228	-6000	-5695	-4085	31.42	31.42	(4+5)-V-4	3.6
8	14879	-1384	-1376	-7351	-4235	-5468	31.42	31.42	3	3.0
9	9060	-4315	-2942	-10837	-2230	-4866	31.42	31.42	3	2.6
10	8565	682	-643	-9054	-664	-3200	31.42	31.42	3	3.3
11	5042	735	785	-7881	455	-2959	31.42	31.42	3	3.8
12	1319	1443	3220	-6862	2020	-2322	31.42	31.42	3	4.7
13	331	-3664	4894	-6989	4108	-3398	31.42	31.42	3	4.2
14	-2785	-8094	3745	-7618	4022	-2700	31.42	31.42	3	4.3
15	-4456	-15131	3640	-6250	1858	-1566	31.42	31.42	3	5.7
16	5834	57	-1258	-946	-4590	-1309	31.42	31.42	(4+5)-V-3	7.3
17	-12121	-14588	-12945	5768	-4183	1459	31.42	31.42	1	6.6
18	-13986	-5866	-11076	4701	-2567	2165	31.42	31.42	1	7.0
19	-9993	-12262	-9868	6171	-3888	2107	31.42	31.42	1	5.6
20	934	8368	-2733	4948	-8535	1599	31.42	31.42	(4+5)-V-3	4.0
21	2898	8022	27	2411	-6984	1207	31.42	31.42	(4+5)-V-3	5.0
22	4697	-1036	1818	-8248	1024	-3827	31.42	31.42	3	3.5
23	4282	-4513	2645	-7875	2380	-3635	31.42	31.42	3	3.6
24	5611	-2673	1223	-8275	997	-3849	31.42	31.42	3	3.4
25	9337	-2937	-825	-8924	-1246	-4314	31.42	31.42	3	3.0
26	7107	-2244	-278	-8731	-298	-4016	31.42	31.42	3	3.2
27	7579	-2887	25	-8454	-93	-4144	31.42	31.42	3	3.2
28	16681	-894	1491	-6430	-4708	-3702	31.42	31.42	(4+5)-V-4	3.7

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
29	15743	-774	-531	-6974	-3938	-3930	31.42	31.42	(4+5)-V-4	3.5
30	13613	-506	-35	-7305	-2834	-3506	31.42	31.42	(4+5)-V-4	3.6
31	10649	-2533	-584	-8009	-2439	-5029	31.42	31.42	3	3.0
32	8543	-2975	-575	-7598	-1269	-4449	31.42	31.42	3	3.4
33	6931	-3581	454	-8181	375	-4088	31.42	31.42	3	3.3
34	3137	6955	-271	2640	-8499	174	31.42	31.42	(4+5)-V-3	4.7
35	5926	8299	3789	558	-8858	-673	31.42	31.42	(4+5)-V-4	4.3
36	9253	6515	5889	-1591	-8557	-3519	31.42	31.42	(4+5)-V-3	3.4
37	5609	8605	3472	870	-8986	-1388	31.42	31.42	(4+5)-VII-3	3.9
38	8119	3586	2143	-899	-6541	-4795	31.42	31.42	(4+5)-V-3	3.7
39	9013	3954	3140	-1437	-6809	-4841	31.42	31.42	(4+5)-V-3	3.6
40	7358	-3252	-402	-275	-6640	-4908	31.42	31.42	3	3.8
41	6802	6192	1723	1372	-8424	-1627	31.42	31.42	(4+5)-V-3	4.1
42	7301	6120	3614	-290	-8510	-3034	31.42	31.42	(4+5)-V-3	3.6
43	6856	4946	3375	-66	-7802	-2681	31.42	31.42	(4+5)-V-3	4.0
44	8772	4206	3360	-817	-7972	-4009	31.42	31.42	(4+5)-V-3	3.5
45	7203	4682	2567	-271	-7587	-3618	31.42	31.42	(4+5)-V-3	3.7
46	7303	-4258	-1534	-575	-5586	-4818	31.42	31.42	3	4.3
47	5913	-4127	-1712	1006	-6159	-4866	31.42	31.42	3	4.1
48	5413	933	-340	335	-4945	-3557	31.42	31.42	(4+5)-I-3	5.1
49	6004	4290	-661	1232	-8218	-1483	31.42	31.42	(4+5)-V-3	4.3
50	5178	3750	1583	89	-7093	-3166	31.42	31.42	(4+5)-V-3	4.1
51	10299	3987	3957	-2172	-6738	-4906	31.42	31.42	(4+5)-V-3	3.6
52	10236	-4034	1981	-1876	-7486	-4644	31.42	31.42	3	3.7
53	9481	5159	5373	-1951	-7636	-4513	31.42	31.42	(4+5)-VII-3	3.4
54	9072	-3632	313	-1297	-6823	-4892	31.42	31.42	3	3.8
55	9104	-4194	-867	-1997	-5718	-4740	31.42	31.42	3	4.3
56	6006	-5286	-2082	-7379	-31	-2868	31.42	31.42	3	4.0
57	8897	778	-931	-5888	-2644	-2045	31.42	31.42	(4+5)-V-4	5.1
58	6148	-4344	-2208	-6385	-1347	-3329	31.42	31.42	3	4.2
59	9909	469	780	-4298	-3278	-3305	31.42	31.42	(4+5)-V-4	5.3
60	11709	593	908	-5285	-3497	-3747	31.42	31.42	(4+5)-V-4	4.4
61	10898	510	-223	-6632	-2802	-2443	31.42	31.42	(4+5)-V-4	4.4
62	16661	1226	4598	-5574	-6207	-4317	31.42	31.42	(4+5)-V-4	3.8
63	16560	-1283	1913	-6158	-4656	-3850	31.42	31.42	(4+5)-V-4	3.8
64	15027	539	2371	-5177	-4749	-4182	31.42	31.42	(4+5)-V-4	4.1
65	13171	319	1041	-5882	-3829	-3737	31.42	31.42	(4+5)-V-4	4.0
66	5659	-5242	452	-7832	1816	-3356	31.42	31.42	3	3.7
67	6807	-3777	-1020	-7092	-506	-3832	31.42	31.42	3	3.8
68	11941	-279	326	-7139	-2588	-2925	31.42	31.42	(4+5)-V-4	3.9
Massimi/minimi										
1							31.42			
1								31.42		
9										2.6

Muro [Platea]: 155 - Nodi: [1-15-13-11-53]Pann=27Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=6.550$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-150	-11620	10706	60	-232	688	20.11	20.11	3	21
2	423	-11358	9629	242	-317	806	20.11	20.11	2	16
3	-1095	-9401	9154	679	-316	953	20.11	20.11	1	10
4	1292	-7467	7060	1156	-631	798	20.11	20.11	1	8.3
5	3392	-5137	5864	1276	-1018	276	20.11	20.11	1	10
6	2969	-4988	5865	-517	-2192	-302	20.11	20.11	1	7.0
7	3043	-5856	5462	-411	-1192	678	20.11	20.11	1	9.5
8	2165	-4118	4872	-1130	-1265	786	20.11	20.11	1	8.4
9	180	-3328	4119	-1934	-1174	901	20.11	20.11	1	5.8
10	-1002	82	6419	-2767	-1044	941	20.11	20.11	1	4.5
11	-2727	1016	4956	-2098	-288	799	20.11	20.11	1	5.9
12	19505	-4385	3914	-1456	405	699	20.11	20.11	1	5.7
13	6412	-2447	4615	-258	149	265	20.11	20.11	3	29
14	736	-6316	10666	-117	-339	327	20.11	20.11	3	27
15	-1802	-276	8249	-970	-274	59	20.11	20.11	1	16
16	-2557	-1289	9350	-321	-149	30	20.11	20.11	1	49
17	-2298	-4421	9757	-340	-106	105	20.11	20.11	1	38
18	-110	-4523	7186	-1168	-569	239	20.11	20.11	1	12
19	-1154	-2607	6490	-1711	-711	342	20.11	20.11	1	8.2

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
20	2880	-5776	6531	-1310	-786	439	20.11	20.11	1	9.1
21	-1931	-2453	8208	-1222	-473	148	20.11	20.11	1	12
22	3265	-6500	7469	-151	-699	79	20.11	20.11	1	23
23	2197	-4871	5565	-971	-676	201	20.11	20.11	1	14
24	1456	-4972	7637	-695	-537	148	20.11	20.11	1	19
25	842	-6667	8133	191	-417	261	20.11	20.11	1	26
26	-142	-4819	8787	-532	-333	141	20.11	20.11	1	25
27	-1129	-5976	9205	-93	-276	214	20.11	20.11	1	36
Massimi/minimi										
1							20.11			
1								20.11		
10										4.5

Muro [Platea]: 156 - Nodi: [2010-2058-2070-2013]Pann=43Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=3.168$ [(4+5)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-5040	-23318	7668	7781	2639	503	31.42	31.42	1	3.2
2	-17808	-36672	-3028	9341	6739	110	31.42	31.42	1	3.1
3	-18334	-25767	-1981	7321	5673	970	31.42	31.42	1	3.5
4	-19040	-24658	350	4488	3476	18	31.42	31.42	1	6.5
5	-17520	-24149	1317	1941	2702	-362	31.42	31.42	1	9.9
6	-11163	-18244	2982	501	2005	-525	31.42	31.42	(4+5)-II-3	11
7	-9303	-18207	6155	-583	1647	-682	31.42	31.42	(4+5)-II-3	12
8	-9094	-4329	6260	-4084	-291	523	31.42	31.42	1	5.9
9	-13837	-15089	9838	-3575	1171	197	31.42	31.42	1	7.5
10	-16530	-22442	8307	-2445	2035	-189	31.42	31.42	1	11
11	-16504	-29374	6629	-2269	2383	-253	31.42	31.42	1	11
12	-17173	-33533	4360	-2611	2859	-414	31.42	31.42	1	9.5
13	-17613	-35487	1732	-2977	3012	-833	31.42	31.42	1	7.6
14	-17920	-34944	-664	-3399	2746	-1313	31.42	31.42	1	6.2
15	-18912	-31193	-1572	-4005	1988	-1673	31.42	31.42	1	5.1
16	-20347	-24617	764	-5132	610	-1595	31.42	31.42	1	4.4
17	-19247	-10128	5306	-7298	-1403	-1665	31.42	31.42	1	3.3
18	-5883	-1410	7424	-1565	-2246	-150	31.42	31.42	(4+5)-VII-1	11
19	-23713	-20922	11875	4265	831	-17	31.42	31.42	1	7.0
20	-30757	-26600	17273	8600	3286	206	31.42	31.42	1	3.6
21	-7024	-21862	9670	7545	1726	758	31.42	31.42	1	3.2
22	-17297	-25823	5676	1279	2156	-152	31.42	31.42	1	13
23	-10671	-105	4498	-2012	-510	-327	31.42	31.42	(4+5)-V-1	12
24	-14057	-13429	4025	1306	694	168	31.42	31.42	(4+5)-III-4	19
25	-18076	-28279	1543	-1476	2752	-675	31.42	31.42	1	9.0
26	-16472	-27795	2803	1281	3068	-399	31.42	31.42	1	8.9
27	-13844	-28296	3036	3786	3254	-367	31.42	31.42	1	6.8
28	-10975	-28278	2850	6119	3144	-408	31.42	31.42	1	4.2
29	-16809	-24193	11106	3834	1513	235	31.42	31.42	1	7.1
30	-10591	-27892	10671	5651	1994	167	31.42	31.42	1	4.7
31	-10604	-15896	4117	3270	1406	-228	31.42	31.42	(4+5)-VII-3	7.9
32	-18717	-26220	718	2235	3970	93	31.42	31.42	1	7.5
33	-18075	-26674	2328	395	3088	-223	31.42	31.42	1	9.3
34	-18388	-29229	1822	-242	3639	-223	31.42	31.42	1	8.1
35	-18345	-30535	449	-1001	3501	-663	31.42	31.42	1	7.5
36	-18839	-30349	930	-447	3833	-434	31.42	31.42	1	7.4
37	-19003	-26794	-824	3527	4912	-257	31.42	31.42	1	5.9
38	-20022	-25785	659	2882	4685	43	31.42	31.42	1	6.5
39	-20480	-26621	-878	4826	5398	-98	31.42	31.42	1	5.6
40	-18977	-27471	84	1760	4321	-216	31.42	31.42	1	6.8
41	-16127	-27344	-1131	6056	5018	-522	31.42	31.42	1	4.4
42	-17686	-28438	753	1439	3914	-467	31.42	31.42	1	7.1
43	-16894	-27601	-113	3818	4373	-469	31.42	31.42	1	6.4
Massimi/minimi										
1							31.42			
1								31.42		
2										3.1

Muro [Platea]: 157 - Nodi: [2070-2071-2073]Pann=8Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=9.850$ [(4+5)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-42100	-15222	12847	5222	3431	-131	31.42	31.42	1	6.3
2	-39045	-17238	16698	3724	684	419	31.42	31.42	1	8.0
3	-11883	-10119	5042	2314	1200	-1201	31.42	31.42	1	7.9
4	-10083	-10924	4825	2654	1921	-1908	31.42	31.42	1	6.0
5	-4330	-8100	-1523	2994	2592	-2446	31.42	31.42	1	4.8
6	-39724	-8682	2519	8865	2846	-2677	31.42	31.42	1	2.9
7	-42853	-16044	12508	7118	3709	-1885	31.42	31.42	1	3.7
8	-22745	-17181	7188	3857	2257	-1808	31.42	31.42	1	5.3
Massimi/minimi										
1							31.42			
1								31.42		
6										2.9

Muro [Platea]: 158 - Nodi: [2013-2070-2073]Pann=11Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=4.685$ [(4+5)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-16780	-13419	-1626	2476	1471	922	31.42	31.42	3	8.5
2	-19200	-7557	72	1714	384	-70	31.42	31.42	(4+5)-II-3	16
3	10059	5205	2286	-2473	-1821	-663	31.42	31.42	(4+5)-I-2	7.5
4	-19716	-7549	730	1695	-88	-399	31.42	31.42	(4+5)-II-3	14
5	-17719	-12874	-1061	2193	969	358	31.42	31.42	3	11
6	-19568	-19207	2840	3593	2657	800	31.42	31.42	1	6.7
7	-19392	-20303	3319	4699	4222	1782	31.42	31.42	1	4.5
8	-21402	-22373	-657	5902	5024	3736	31.42	31.42	1	3.1
9	-8240	-16714	4367	6373	1606	1918	31.42	31.42	1	3.3
10	-13833	-20615	3466	5327	2873	2239	31.42	31.42	1	3.7
11	-16805	-20361	1994	4084	2849	1392	31.42	31.42	1	5.3
Massimi/minimi										
1							31.42			
1								31.42		
8										3.1

Muro [Platea]: 159 - Nodi: [2073-2075-2082]Pann=9Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=12.823$ [(4+5)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-17724	-13027	13815	3792	5860	868	31.42	31.42	1	4.2
2	-14342	-16244	15547	3085	6041	-112	31.42	31.42	1	4.7
3	-9726	-32504	13862	2349	6025	-245	31.42	31.42	1	5.1
4	-13904	-19632	14574	2973	6005	-227	31.42	31.42	1	4.7
5	-16118	-9790	12080	3213	5754	441	31.42	31.42	1	4.4
6	-11584	-2255	5983	1681	5518	1340	31.42	31.42	1	3.8
7	-10511	-1462	7741	1966	5728	1169	31.42	31.42	1	3.7
8	-13635	-5298	7541	2814	5906	1366	31.42	31.42	1	3.6
9	-16299	-4780	10675	3181	5687	881	31.42	31.42	1	4.0
Massimi/minimi										
1							31.42			
1								31.42		
8										3.6

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
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Muro [Platea]: 160 - Nodi: [2013-2073-2082]Pann=15Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=5.522$ [(4+5)-I-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-32907	-11594	-6290	2341	2602	1155	31.42	31.42	1	7.4
2	-31918	-7771	-717	485	1681	976	31.42	31.42	1	10
3	-24823	-3719	7406	-662	1470	1279	31.42	31.42	1	9.5
4	5549	5141	3638	-3096	-561	876	31.42	31.42	(4+5)-II-2	6.1
5	-18168	-7596	3495	1580	608	-266	31.42	31.42	(4+5)-II-3	16
6	-19890	-11107	-1185	3257	974	683	31.42	31.42	3	7.5
7	-16221	-16268	-3760	5025	1559	773	31.42	31.42	2	4.9
8	-10194	-22030	-5007	6359	2027	113	31.42	31.42	1	4.2
9	-4114	-17730	-5404	6052	1796	-541	31.42	31.42	1	4.0
10	-10987	-19790	-10046	6002	2587	17	31.42	31.42	1	4.6
11	-20845	-17757	-13494	5620	2684	587	31.42	31.42	1	4.8
12	-30289	-16133	-15764	4956	2573	667	31.42	31.42	1	5.6
13	-28647	-10375	-12096	3788	2011	923	31.42	31.42	3	6.6
14	-24370	-9044	-3577	3321	1184	1002	31.42	31.42	3	7.0
15	-21626	-13547	-8287	4843	1799	828	31.42	31.42	2	5.2
Massimi/minimi										
1							31.42			
1								31.42		
9										4.0

Muro [Platea]: 161 - Nodi: [2007-2058-2010]Pann=29Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=3.154$ [(4+5)-VI-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-16388	-28682	769	-14	-4474	1688	31.42	31.42	1	5.0
2	-20107	-26176	501	459	-4269	1653	31.42	31.42	1	5.2
3	-22927	-24031	1379	664	-4164	1683	31.42	31.42	1	5.2
4	-24412	-22486	3064	693	-4168	1703	31.42	31.42	1	5.1
5	-24030	-21398	5306	580	-4338	1903	31.42	31.42	1	4.8
6	-22181	-20504	8248	-227	-40973	2376	31.42	31.42	1	4.0
7	-16706	-19563	10688	-1574	-6041	3084	31.42	31.42	1	3.2
8	-4631	-24533	9900	-3214	-7330	3379	31.42	31.42	2	2.8
9	-15458	-21743	9443	-770	-5862	2016	31.42	31.42	1	3.8
10	-19629	-21736	7103	648	-4226	1358	31.42	31.42	1	5.3
11	-21206	-22696	5159	1358	-2921	948	31.42	31.42	1	7.7
12	-8239	-16661	1981	1067	-1882	411	31.42	31.42	(4+5)-VII-1	13
13	-14524	-13397	3457	1638	535	-470	31.42	31.42	(4+5)-I-3	13
14	-14097	-14622	3287	1384	1222	-711	31.42	31.42	(4+5)-I-3	13
15	-12699	-17480	3234	563	2298	-960	31.42	31.42	(4+5)-VII-4	8.9
16	-20835	-30648	4500	-62	4053	-1533	31.42	31.42	1	5.6
17	-18892	-38017	-783	452	7597	-1815	31.42	31.42	1	3.5
18	-8410	-23503	2538	-246	3407	-847	31.42	31.42	(4+5)-V-3	7.1
19	11	-10026	2216	-2537	-1398	192	31.42	31.42	(4+5)-III-1	9.3
20	-7742	-21640	6224	-2555	-6715	2255	31.42	31.42	1	3.3
21	-11493	-29603	1742	-1043	-5058	2023	31.42	31.42	1	4.4
22	-21560	-24576	2263	1067	-2756	1205	31.42	31.42	1	7.6
23	-22030	-23905	3237	1366	-2544	1044	31.42	31.42	1	8.4
24	-6330	-17152	1105	736	-1808	419	31.42	31.42	(4+5)-III-1	13
25	-4448	-15868	2920	-379	-1234	182	31.42	31.42	(4+5)-V-2	20
26	525	-16080	4417	-1175	-2008	385	31.42	31.42	(4+5)-I-2	12
27	-17434	-27464	2647	174	-2298	1380	31.42	31.42	1	8.4
28	-4807	-17599	1261	357	-1456	278	31.42	31.42	(4+5)-I-2	17
29	-19615	-25988	2077	741	-2410	1210	31.42	31.42	1	8.4
Massimi/minimi										
1							31.42			
1								31.42		
8										2.8

Muro [Platea]: 162 - Nodi: [2007-2042-2047] Pann=28 Spess.=50 cm, Terreno=DefTerr_70882, , Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=4.082$ [(4+5)-I-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-26515	-10049	-1397	6650	2042	143	31.42	31.42		2 4.5
2	-25859	-11263	-849	6614	1892	432	31.42	31.42		2 4.3
3	-24632	-12301	-334	5904	1684	662	31.42	31.42		3 4.6
4	-23845	-13111	26	4239	1114	870	31.42	31.42		3 5.9
5	-16680	-10170	-1897	2332	560	853	31.42	31.42	(4+5)-VII-4	9.0
6	-8562	-9486	4147	-2412	-844	409	31.42	31.42	(4+5)-III-1	9.6
7	1476	-8742	487	-7898	-1848	964	31.42	31.42	(4+5)-I-2	2.8
8	-7544	-10341	2865	-2449	-960	329	31.42	31.42	(4+5)-III-1	9.7
9	-16570	-10145	-1713	2366	455	735	31.42	31.42	(4+5)-V-4	9.3
10	-23722	-13278	-428	4304	983	701	31.42	31.42		3 6.0
11	-24627	-12621	-918	6031	1502	575	31.42	31.42		3 4.6
12	-25247	-11697	-1524	6820	1735	365	31.42	31.42		3 4.2
13	-26273	-11125	-2230	7000	1735	181	31.42	31.42		2 4.3
14	-27089	-10845	-3014	6456	1500	84	31.42	31.42		1 4.7
15	-27739	-10203	-3929	5393	1311	-75	31.42	31.42		1 5.6
16	-28364	-9629	-4770	3586	953	-278	31.42	31.42		1 8.0
17	-28594	-9191	-4235	3413	1005	-370	31.42	31.42		1 8.2
18	-28409	-8751	-3856	3272	1119	-452	31.42	31.42		1 8.3
19	-27912	-8105	-3825	3235	1284	-539	31.42	31.42		1 8.2
20	-27982	-8471	-2707	5054	1663	-291	31.42	31.42		1 5.8
21	-26926	-8665	-2157	6096	1988	-154	31.42	31.42		2 4.9
22	-26427	-10232	-1710	6723	1899	110	31.42	31.42		2 4.5
23	-25968	-10995	-1421	6857	1826	299	31.42	31.42		2 4.3
24	-26471	-10455	-2107	6832	1801	139	31.42	31.42		2 4.4
25	-27946	-9600	-3523	5208	1349	-128	31.42	31.42		1 5.8
26	-28001	-9063	-3080	5106	1460	-203	31.42	31.42		1 5.8
27	-26979	-9669	-2884	6272	1687	-45	31.42	31.42		2 4.9
28	-26951	-9194	-2521	6153	1800	-108	31.42	31.42		2 4.9
Massimi/minimi										
1							31.42			
1								31.42		
7										2.8

Muro [Platea]: 163 - Nodi: [2056-2060-2059] Pann=9 Spess.=50 cm, Terreno=DefTerr_70882, , Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=7.274$ [(4+5)-III-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-7125	-18708	3191	1274	-1003	1575	31.42	31.42		2 9.4
2	-31575	-20329	-862	1419	-3848	2475	31.42	31.42		3 4.7
3	-20259	-13850	5792	-129	-3682	2675	31.42	31.42		3 4.4
4	-5267	-6360	4031	377	-4023	1008	31.42	31.42	(4+5)-VII-3	5.3
5	-964	5630	859	-682	-5067	1039	31.42	31.42	(4+5)-VII-3	4.0
6	-4173	-1006	1864	-910	-1481	1445	31.42	31.42		3 8.8
7	446	-1965	161	-798	-126	1198	31.42	31.42		3 13
8	872	5006	4539	-926	327	963	31.42	31.42		3 13
9	-1844	-13851	3933	596	349	1344	31.42	31.42		1 13
Massimi/minimi										
1							31.42			
1								31.42		
5										4.0

Muro [Platea]: 164 - Nodi: [2053-2056-2059] Pann=10 Spess.=50 cm, Terreno=DefTerr_70882, , Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=12.314$ [(4+5)-VII-2] : **Verificato**

Armatura a maglia doppia

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Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-22275	-5878	6974	-379	4992	1687	31.42	31.42		3 4.0
2	-27134	-17494	7337	-2191	3576	1549	31.42	31.42		3 5.6
3	-22131	-7067	5958	-243	2890	138	31.42	31.42		1 8.9
4	-14145	-988	6348	-293	2418	-495	31.42	31.42		2 8.8
5	-11853	1270	4783	-585	1161	-657	31.42	31.42		1 14
6	-16906	1024	8188	390	2733	-55	31.42	31.42		2 9.1
7	-21256	404	10892	1306	4098	301	31.42	31.42		3 5.8
8	-19851	-718	13419	1404	6267	878	31.42	31.42		3 3.6
9	-20283	-3301	10160	972	5931	1548	31.42	31.42		3 3.5
10	-22302	-2315	10322	446	4162	613	31.42	31.42		3 5.4
Massimi/minimi										
1							31.42			
1								31.42		
9										3.5

Muro [Platea]: 165 - Nodi: [2058-2053-2059]Pann=15Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=4.517$ [(4+5)-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-19146	-13660	-12212	1054	4044	931	31.42	31.42		1 5.7
2	-18016	-12411	-12567	1976	3882	413	31.42	31.42		1 6.5
3	-14521	-8793	-13309	2806	3347	-322	31.42	31.42		3 7.4
4	-13260	-10071	-14929	3670	3051	-748	31.42	31.42		3 6.4
5	-12357	-10693	-17535	5474	3072	-1424	31.42	31.42		3 4.0
6	-12970	-10166	-15854	3474	2510	-815	31.42	31.42		2 6.5
7	-10640	-10528	-12949	1867	1808	-348	31.42	31.42		1 12
8	2841	-3279	-4820	-852	-368	420	31.42	31.42	(4+5)-IV-1	20
9	-3573	-15268	-12185	-1073	202	1168	31.42	31.42		3 12
10	-9138	-21823	-17239	-1910	280	1709	31.42	31.42		3 7.5
11	-47942	-31875	-19860	2271	4037	3498	31.42	31.42		1 4.2
12	-27429	-19513	-14986	-690	4652	2464	31.42	31.42		1 4.1
13	-21540	-15836	-13369	-95	4366	1565	31.42	31.42		1 4.8
14	-14637	-12348	-12922	1793	3131	134	31.42	31.42		1 8.5
15	-14693	-13065	-13085	233	3104	849	31.42	31.42		1 7.1
Massimi/minimi										
1							31.42			
1								31.42		
5										4.0

Muro [Platea]: 166 - Nodi: [2007-2047-2053]Pann=24Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=4.338$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	-25668	-9825	4657	5936	2790	-948	31.42	31.42		2 4.4
2	-24811	-11777	4326	6183	2326	-693	31.42	31.42		2 4.4
3	-24165	-13323	3956	5653	1785	-345	31.42	31.42		2 5.0
4	-23081	-14296	3633	4372	1090	133	31.42	31.42		3 6.7
5	-17230	-9871	43	2663	392	391	31.42	31.42	(4+5)-VII-4	9.4
6	-7919	-10940	4466	-1803	-1086	1050	31.42	31.42	(4+5)-I-1	9.5
7	1114	-9430	2170	-6620	-2355	1847	31.42	31.42	(4+5)-III-1	3.0
8	-7298	-11555	4593	-1824	-909	722	31.42	31.42	(4+5)-III-1	11
9	-17149	-9774	208	2665	307	283	31.42	31.42	(4+5)-V-4	9.8
10	-22889	-14081	3416	4402	978	23	31.42	31.42		3 6.8
11	-24104	-13381	3682	5710	1667	-466	31.42	31.42		2 4.9
12	-24732	-12059	3976	6309	2196	-806	31.42	31.42		2 4.3
13	-25731	-10230	3983	6122	2541	-1101	31.42	31.42		2 4.2
14	-27042	-9441	3863	5483	2470	-1186	31.42	31.42		1 4.6
15	-27982	-7963	3519	4408	2365	-1187	31.42	31.42		1 5.5
16	-27812	-4860	1466	2298	2204	-1029	31.42	31.42		2 8.2
17	-28094	-3625	940	2317	2456	-1188	31.42	31.42		2 7.2

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
18	-28794	-3115	603	2433	2739	-1437	31.42	31.42	2	6.2
19	-30773	-1639	954	2529	3326	-1709	31.42	31.42	2	5.1
20	-27274	-3243	3558	3728	3574	-1133	31.42	31.42	3	5.5
21	-27164	-8576	4652	5163	2820	-1096	31.42	31.42	1	4.9
22	-28115	-6829	3982	3971	2936	-1203	31.42	31.42	1	6.0
23	-27417	-7757	4238	4991	2736	-1203	31.42	31.42	1	5.0
24	-28068	-7021	3371	4047	2573	-1159	31.42	31.42	1	5.9
Massimi/minimi										
1							31.42			
1								31.42		
7										3.0

Muro [Platea]: 167 - Nodi: [2007-2053-2058]Pann=51Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45,ζ_c=4.950 [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq			
1	-16761	-9280	1503	3680	975	-365	31.42	31.42	(4+5)-III-4	7.1
2	-22616	-15080	5704	5199	1945	-654	31.42	31.42	2	5.1
3	-22801	-13977	6442	5687	2631	-989	31.42	31.42	2	4.5
4	-23749	-13568	7186	5536	2890	-1116	31.42	31.42	1	4.5
5	-24424	-11084	8371	4899	3454	-1006	31.42	31.42	1	5.1
6	-25877	-5698	8815	3614	4040	-807	31.42	31.42	2	5.5
7	-28857	-1121	9737	2496	5408	-875	31.42	31.42	2	4.1
8	-23884	-4292	9459	3506	4460	-257	31.42	31.42	2	5.6
9	-23292	-8769	9918	4124	3301	5	31.42	31.42	1	7.3
10	-23056	-10517	10067	4538	2177	308	31.42	31.42	1	6.2
11	-23435	-13211	10342	5002	1035	441	31.42	31.42	1	5.5
12	-24866	-18407	9749	5921	-113	280	31.42	31.42	1	4.9
13	-28345	-26033	9475	7048	-1268	-354	31.42	31.42	1	4.2
14	-36669	-30052	10095	8464	-1272	-2903	31.42	31.42	1	2.9
15	-29219	-23242	5448	6017	-293	-1599	31.42	31.42	1	4.1
16	-26149	-20403	3854	4672	635	-809	31.42	31.42	1	5.6
17	-16503	-12086	1322	3009	864	-330	31.42	31.42	(4+5)-VII-4	8.6
18	-23602	-16681	4145	2237	887	808	31.42	31.42	3	9.9
19	-23884	-16974	4091	1496	755	1298	31.42	31.42	3	11
20	-17370	-9997	-218	1426	354	821	31.42	31.42	(4+5)-III-4	13
21	-12547	-12195	5331	-1294	-265	1590	31.42	31.42	(4+5)-III-1	9.7
22	-25566	-11800	4381	-2695	-1615	2453	31.42	31.42	1	5.9
23	157	-7705	10794	-5963	-2633	1622	31.42	31.42	(4+5)-V-1	3.4
24	-22000	-13402	4759	-968	-1821	1606	31.42	31.42	1	8.2
25	-17087	-10115	1003	2433	351	244	31.42	31.42	(4+5)-V-4	11
26	-22443	-15659	5251	3609	1102	407	31.42	31.42	3	7.4
27	-23083	-16082	4815	2499	830	979	31.42	31.42	3	8.6
28	-22625	-15939	4957	1707	201	1120	31.42	31.42	3	11
29	-23102	-16157	4825	3111	1179	671	31.42	31.42	3	7.9
30	-22771	-15566	5716	4714	1783	-201	31.42	31.42	2	6.1
31	-22755	-16265	4677	4064	1103	87	31.42	31.42	3	7.2
32	-23187	-16053	4771	3419	1193	439	31.42	31.42	3	7.8
33	-22706	-15839	5034	4395	1520	136	31.42	31.42	3	6.6
34	-22499	-15583	5316	4434	1689	106	31.42	31.42	3	6.6
35	-22991	-17125	6770	5486	1851	-262	31.42	31.42	1	5.2
36	-23530	-17707	5533	5030	1684	-241	31.42	31.42	1	5.7
37	-23387	-18498	6407	5544	1318	-191	31.42	31.42	1	5.2
38	-24273	-20195	5427	5353	605	-327	31.42	31.42	1	5.3
39	-24063	-18424	4896	5023	1337	-336	31.42	31.42	1	5.6
40	-22936	-17628	7647	5615	1365	-72	31.42	31.42	1	5.3
41	-23070	-16008	8906	5519	1235	167	31.42	31.42	1	5.3
42	-23657	-19215	7535	5854	552	-127	31.42	31.42	1	5.0
43	-22795	-13563	9319	5149	2135	72	31.42	31.42	1	5.7
44	-22803	-15894	8118	5509	1993	-147	31.42	31.42	1	5.3
45	-22591	-14635	6464	5449	2443	-596	31.42	31.42	2	4.9
46	-23353	-16765	5934	5185	1991	-377	31.42	31.42	1	5.4
47	-23345	-12832	8530	5053	3080	-544	31.42	31.42	1	5.4
48	-23031	-12093	9364	4961	3022	-280	31.42	31.42	1	5.7
49	-22934	-14332	8281	5403	2535	-328	31.42	31.42	1	5.2
50	-23351	-14611	7342	5516	2720	-744	31.42	31.42	1	4.8
51	-22993	-15845	7110	5489	2316	-433	31.42	31.42	1	5.1
Massimi/minimi										

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
1							31.42			
1								31.42		
14										2.9

Muro [Platea]: 168 - Nodi: [2067-2065-2060]Pann=8Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=4.911$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-2946	6441	-4289	-3840	473	3955	31.42	31.42	(4+5)-VII-3	5.7
2	8843	7719	-13981	-4871	-3115	5080	31.42	31.42	(4+5)-VII-3	4.1
3	10820	9100	-8279	389	5438	-4159	31.42	31.42	3	4.2
4	7392	-6608	-1681	-6415	412	292	31.42	31.42	(4+5)-V-4	6.1
5	-979	1217	-3560	-5459	316	1481	31.42	31.42	(4+5)-V-3	6.3
6	1088	1480	-6708	-3789	496	4105	31.42	31.42	(4+5)-VII-3	5.4
7	488	2694	-3975	-5752	-224	3441	31.42	31.42	(4+5)-VII-3	4.7
8	-10358	2953	-4400	-3591	-412	1901	31.42	31.42	(4+5)-V-3	8.5
Massimi/minimi										
1							31.42			
1								31.42		
2										4.1

Muro [Platea]: 169 - Nodi: [2011-2067-2060]Pann=6Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=5.817$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-9613	3539	-6555	5219	-6970	-3916	31.42	31.42	3	3.9
2	4980	5688	890	-343	-3731	-2701	31.42	31.42	(4+5)-VII-3	6.4
3	3408	-5081	-18462	6541	-5719	-5825	31.42	31.42	3	3.4
4	-16633	5604	-11188	5264	-5319	-6876	31.42	31.42	3	3.4
5	-27650	-5196	-13444	2451	-7860	-4172	31.42	31.42	3	3.7
6	-16135	-3568	-7213	4598	-6309	-4781	31.42	31.42	3	4.0
Massimi/minimi										
1							31.42			
1								31.42		
4										3.4

Muro [Platea]: 170 - Nodi: [2031-2037-2036]Pann=8Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=10.850$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-15152	-32759	747	3940	-1687	-867	31.42	31.42	3	10
2	-18909	-20037	-740	767	-2515	-264	31.42	31.42	(4+5)-III-4	18
3	-7360	-41487	-4712	7116	-2235	-3215	31.42	31.42	3	4.4
4	-12429	-35825	-5765	6271	-2073	-2207	31.42	31.42	3	5.6
5	-11727	-34153	-4245	5518	-1996	-1875	31.42	31.42	3	6.4
6	-12023	-36025	-3894	5783	-2468	-1929	31.42	31.42	3	6.1
7	-14542	-37375	-4376	6826	-1866	-2690	31.42	31.42	3	5.1
8	-8924	-36169	-6016	7118	-1431	-2994	31.42	31.42	3	4.6
Massimi/minimi										
1							31.42			
1								31.42		
3										4.4

Muro [Platea]: 171 - Nodi: [2028-2031-2036]Pann=7Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=8.887$ [(4+5)-III-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-43351	-21563	5345	2408	1823	1279	31.42	31.42		3 16
2	-48393	-22728	1178	5072	2295	1130	31.42	31.42		3 9.5
3	-45268	-19981	5886	3079	800	911	31.42	31.42		3 15
4	-33875	-10929	6043	-27	-820	1440	31.42	31.42	(4+5)-III-4	21
5	-37512	-16196	14172	-3804	-2308	3621	31.42	31.42	(4+5)-I-4	7.5
6	-32631	-24047	2326	2033	714	1686	31.42	31.42		3 15
7	-38914	-24075	7474	1202	1004	1734	31.42	31.42		3 19
Massimi/minimi										
1							31.42			
1								31.42		
5										7.5

Muro [Platea]: 172 - Nodi: [2087-2088-2092]Pann=19Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=10.067$ [(4+5)-VI-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-43282	-8920	3856	3531	-11	-66	31.42	31.42		1 9.4
2	-41929	-9120	4701	3374	117	-39	31.42	31.42		1 9.8
3	-38227	-9450	5607	3041	288	-65	31.42	31.42		2 11
4	-35158	-9388	5639	2726	405	38	31.42	31.42		1 12
5	-24696	-7679	8264	1937	461	-386	31.42	31.42	(4+5)-I-3	13
6	-20732	-7468	8519	1593	521	-408	31.42	31.42	(4+5)-III-3	15
7	-17438	-4282	7844	1330	305	-393	31.42	31.42	(4+5)-VII-3	17
8	-5775	-10934	8195	414	900	-661	31.42	31.42	(4+5)-II-3	18
9	-16972	-4678	6671	1421	425	-812	31.42	31.42	(4+5)-VII-3	13
10	-22293	-9062	4482	1884	881	-822	31.42	31.42		2 11
11	-28794	-9824	4231	2466	1049	-793	31.42	31.42		2 9.5
12	-34524	-9780	3551	2983	1180	-692	31.42	31.42		1 8.8
13	-38456	-9643	3538	3347	1312	-599	31.42	31.42		1 8.3
14	-41077	-9512	3495	3595	1442	-496	31.42	31.42		1 8.2
15	-42489	-9453	3366	3735	1556	-393	31.42	31.42		1 8.2
16	-42894	-9419	2895	3770	1635	-283	31.42	31.42		1 8.3
17	-42497	-11002	1275	3607	1329	-267	31.42	31.42		1 8.7
18	-43003	-6528	553	3553	125	-175	31.42	31.42		1 9.1
19	-43452	-8585	2662	3581	-115	-71	31.42	31.42		1 9.3
Massimi/minimi										
1							31.42			
1								31.42		
15										8.2

Muro [Platea]: 173 - Nodi: [2087-2092-2016]Pann=19Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=4.237$ [(4+5)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-13215	-7659	6851	1312	1570	-1122	31.42	31.42	(4+5)-II-3	10
2	-24067	-5682	5907	2239	1419	-1046	31.42	31.42		2 9.2
3	-30505	-5587	7271	2713	1248	-1016	31.42	31.42		1 8.4
4	-35043	-5357	8686	3049	1083	-1011	31.42	31.42		1 8.0
5	-38226	-4936	9589	3279	904	-976	31.42	31.42		1 7.7
6	-40143	-4420	9923	3405	718	-909	31.42	31.42		1 7.7
7	-40940	-3827	9553	3441	525	-814	31.42	31.42		1 7.9
8	-41049	-3211	8658	3418	268	-726	31.42	31.42		1 8.1
9	-41064	-3812	9614	3402	114	-821	31.42	31.42		1 7.9
10	-40138	-4536	10272	3346	35	-839	31.42	31.42		1 7.9

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
11	-37988	-5191	10528	3205	-45	-790	31.42	31.42		8.2
12	-34433	-5884	10505	2956	-121	-698	31.42	31.42		8.8
13	-29391	-6503	10291	2599	-202	-577	31.42	31.42		9.8
14	-22439	-7042	10332	2106	-303	-474	31.42	31.42		12
15	-18236	-4342	10121	1742	-189	-517	31.42	31.42	(4+5)-VII-3	13
16	-14826	-1793	10336	1361	-656	-538	31.42	31.42	(4+5)-VII-3	15
17	45	23892	-6870	-550	-2734	1063	31.42	31.42	(4+5)-II-2	5.4
18	-2327	-9196	5972	-405	1341	-557	31.42	31.42	(4+5)-II-3	14
19	-6126	-7215	5605	659	1780	-1081	31.42	31.42	(4+5)-II-3	9.4
Massimi/minimi										
1							31.42			
1								31.42		
17										5.4

Muro [Platea]: 174 - Nodi: [2089-2017-2088]Pann=14Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=2.635$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-3081	-27085	-8598	229	1913	1055	31.42	31.42	(4+5)-V-1	10
2	-8540	-24053	-7772	777	1758	884	31.42	31.42	(4+5)-V-1	11
3	-19622	-26528	-8069	1734	1774	1097	31.42	31.42		10
4	-24969	-27683	-10561	2108	2044	1131	31.42	31.42		9.4
5	-27910	-27506	-12135	2436	2293	1032	31.42	31.42		8.9
6	-24903	-25906	-11164	2084	2605	768	31.42	31.42		9.1
7	-21684	-24077	-8760	1754	2754	469	31.42	31.42		9.4
8	-17641	-20945	-5993	1416	2913	106	31.42	31.42		9.8
9	-8433	-15819	-1439	747	3106	-549	31.42	31.42		7.8
10	-3253	-10502	-2423	782	2977	-1261	31.42	31.42		6.5
11	1035	-11846	-3564	1636	2077	-1516	31.42	31.42		7.7
12	-11108	-14258	-2657	1841	1188	285	31.42	31.42		13
13	31871	-21752	757	-2856	600	534	31.42	31.42	(4+5)-VII-2	5.6
14	-1617	28815	14559	-825	-3622	-207	31.42	31.42	(4+5)-V-4	5.1
Massimi/minimi										
1							31.42			
1								31.42		
14										5.1

Muro [Platea]: 175 - Nodi: [2017-2092-2088]Pann=11Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45, $\zeta_e=1.517$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-26444	-3110	-6099	2130	597	680	31.42	31.42	(4+5)-V-1	11
2	-29186	467	-8954	2307	134	928	31.42	31.42	(4+5)-V-1	9.6
3	54426	949	6477	-4848	-124	-581	31.42	31.42	(4+5)-VII-3	2.6
4	-30388	2607	-6990	2496	-417	358	31.42	31.42	(4+5)-V-1	11
5	-27334	-2542	-6231	2265	-137	303	31.42	31.42	(4+5)-V-1	12
6	-32899	-5720	-4023	2764	-348	-128	31.42	31.42		11
7	-37106	-6902	-2550	3161	-296	-80	31.42	31.42		10
8	-40444	-5951	124	3575	93	35	31.42	31.42		9.2
9	-40115	-10460	1543	3601	1312	77	31.42	31.42		9.0
10	-37599	-7451	-413	3181	1507	211	31.42	31.42		9.7
11	-33480	-5658	-1274	2673	1284	444	31.42	31.42		10
Massimi/minimi										
1							31.42			
1								31.42		
3										2.6

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Muro [Platea]: 176 - Nodi: [17-1-15]Pann=7Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=9.395$ [(4+5)-III-4] : **Verificato**

Armatura a maglia doppia

Annotazioni a pagina doppia										
Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-4549	-6089	-5676	492	7	-415	20.11	20.11		3
2	1592	-2452	-2711	182	-375	-342	20.11	20.11	(4+5)-III-1	24
3	18446	-586	839	-511	29	-131	20.11	20.11		1
4	12058	-2682	1091	1234	-167	529	20.11	20.11		3
5	4702	1228	1812	496	-147	132	20.11	20.11	(4+5)-I-3	25
6	-5275	-6986	-6704	50	-1062	-605	20.11	20.11		2
7	6989	-5481	-2930	176	-500	-364	20.11	20.11		3
Massimi/minimi										
1							20.11			
1								20.11		
4										7.9

Muro [Platea]: 177 - Nodi: [2086-2085-2014]Pann=10Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND,
Materiale=C35/45, $\zeta_e=14.212$ [(4+5)-VIII-4] : **Verificato**

Armatura a maglia doppia

Armatura a maglia doppia										
Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-45354	-22470	-8890	3899	1728	423	31.42	31.42	2	7.9
2	-47992	-18729	-7868	4080	1591	543	31.42	31.42	2	7.5
3	-44239	-17357	-9844	3727	1632	1123	31.42	31.42	2	7.0
4	-31738	-21288	-9121	2810	2810	1249	31.42	31.42	1	7.3
5	-22853	-11754	-15498	1696	1507	2279	31.42	31.42	3	7.3
6	-27284	-12856	-13563	1076	1342	1245	31.42	31.42	1	11
7	-8658	-5081	-11396	-1366	105	688	31.42	31.42	(4+5)-II-3	13
8	-25560	-11936	-13175	1791	370	219	31.42	31.42	1	15
9	-29797	-21434	-15333	2780	803	780	31.42	31.42	2	8.8
10	-27975	-13960	-14414	2460	1404	1398	31.42	31.42	2	8.0
Massimi/minimi										
1							31.42			
1								31.42		
3										7.0

Muro : 178 - Nodi: [2029-3029-3028-2028], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=22.022$ [(4+5)-III-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs	
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq			
1	-505	-5873	-3628	425	79	-77	20.11	20.11		3	18
2	445	-4377	-47	48	6	43	20.11	20.11	(4+5)-III-1		98
3	444	-5058	1286	-48	-19	11	20.11	20.11	(4+5)-II-2		>100
4	-2633	-4941	3462	365	111	83	20.11	20.11		3	21
5	-640	-3060	-2877	116	93	-79	20.11	20.11		3	46
6	34	-2668	-134	44	30	25	20.11	20.11	(4+5)-III-1		>100
7	215	-5443	1209	43	3	52	20.11	20.11		3	94
8	-1111	-2139	1721	86	98	101	20.11	20.11		3	46
9	279	-1140	-2137	12	109	-61	20.11	20.11		3	54
10	-196	-1051	-66	27	47	19	20.11	20.11	(4+5)-III-1		>100
11	-215	-3943	692	35	24	65	20.11	20.11		3	89
12	-448	-1488	785	-16	62	72	20.11	20.11		3	68
13	227	1156	-1404	-4	155	-71	20.11	20.11		3	39
14	-142	131	83	10	57	17	20.11	20.11	(4+5)-III-1		>100
15	-336	-2860	263	9	37	62	20.11	20.11		3	95
16	-308	-1623	84	-20	39	46	20.11	20.11		3	>100
Massimi/minimi											
1							20.11				
1								20.11			
1											18

Muro : 179 - Nodi: [2036-3036-3028-2028], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=32.714$ [(4+5)-III-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-2955	-165	-2947	130	46	57	20.11	20.11	(4+5)-III-4	49
2	-3605	-10	-3926	178	83	76	20.11	20.11	(4+5)-III-4	37
3	-3050	1278	-4564	214	60	134	20.11	20.11	(4+5)-III-4	27
4	7549	8208	-9637	-147	-62	115	20.11	20.11	3	31
5	-2063	3875	-2822	74	59	94	20.11	20.11	(4+5)-III-4	55
6	-2390	3478	-4047	72	64	116	20.11	20.11	(4+5)-III-4	47
7	-1652	3526	-5704	16	49	125	20.11	20.11	(4+5)-III-4	49
8	5127	2166	-6586	-107	31	25	20.11	20.11	3	63
9	-980	7698	-2214	31	71	91	20.11	20.11	(4+5)-III-4	50
10	-1155	6246	-3362	13	66	96	20.11	20.11	(4+5)-III-4	51
11	-757	4017	-4262	-38	13	77	20.11	20.11	(4+5)-III-4	79
12	690	1088	-3480	-68	-131	-3	20.11	20.11	(4+5)-III-4	66
13	-148	11874	-882	6	77	76	20.11	20.11	(4+5)-III-4	49
14	-127	8995	-1341	-2	59	75	20.11	20.11	(4+5)-III-4	59
15	-252	4093	-1378	-3	54	-16	20.11	20.11	(4+5)-III-1	>100
16	-476	1140	-1393	-61	-163	-31	20.11	20.11	(4+5)-III-4	45
Massimi/minimi										
1							20.11			
1								20.11		
3										27

Muro : 180 - Nodi: [2037-2043-3043-3037], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=33.116$ [(4+5)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	2040	-7290	778	108	131	-51	20.11	20.11	2	54
2	3569	-5327	2285	136	40	-20	20.11	20.11	2	55
3	4467	-4158	2362	135	16	5	20.11	20.11	3	60
4	4921	-3295	1126	132	4	9	20.11	20.11	3	59
5	-1284	-6230	-583	56	107	40	20.11	20.11	3	66
6	1818	-4923	-2	87	89	34	20.11	20.11	3	72
7	4835	-3760	436	112	44	41	20.11	20.11	3	55
8	8314	-3187	180	127	8	38	20.11	20.11	3	48
9	-2750	-5169	-1684	87	208	165	20.11	20.11	2	26
10	350	-4212	-1076	145	63	102	20.11	20.11	3	36
11	4035	-3444	-676	136	22	75	20.11	20.11	3	40
12	8043	-3047	-141	130	6	62	20.11	20.11	3	42
13	-6176	-2632	-388	3	-47	129	20.11	20.11	3	53
14	-179	-2580	-715	-13	-21	40	20.11	20.11	(4+5)-I-2	>100
15	3227	-3330	-792	-24	-9	44	20.11	20.11	3	>100
16	6323	-3216	-328	-27	-2	42	20.11	20.11	3	>100
Massimi/minimi										
1							20.11			
1								20.11		
9										26

Muro : 181 - Nodi: [2029-2033-3033-3029], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=31.367$ [(4+5)-III-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	4697	5716	4724	153	-229	200	20.11	20.11	2	19

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
2	1004	1831	3835	154	25	76	20.11	20.11	(4+5)-II-4	38
3	735	128	3979	-33	-124	-2	20.11	20.11	2	71
4	27	-2007	3303	-189	-291	-78	20.11	20.11	2	25
5	900	-2618	3981	-143	-349	160	20.11	20.11	2	18
6	2756	-620	6463	-127	16	85	20.11	20.11	3	41
7	1775	-1289	5464	-94	-199	-54	20.11	20.11	2	36
8	1281	-997	3610	-85	-461	-2	20.11	20.11	2	20
9	-1480	-3885	3341	-163	-342	86	20.11	20.11	2	22
10	1813	-3289	5931	-156	-38	164	20.11	20.11	3	27
11	2705	-2226	5256	-103	-273	21	20.11	20.11	2	31
12	3343	-1361	3620	-75	-451	40	20.11	20.11	2	19
13	-3522	-3367	4190	12	-133	90	20.11	20.11	(4+5)-V-4	42
14	1033	-3958	4553	-44	-214	128	20.11	20.11	2	28
15	3399	-2757	4278	-58	-323	60	20.11	20.11	2	24
16	5093	-1468	3168	-66	-473	72	20.11	20.11	2	17
Massimi/minimi										
1							20.11			
1								20.11		
16										17

Muro : 182 - Nodi: [2036-2042-3042-3036], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45, $\zeta_e=21.460$ [(4+5)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	151	-2354	1844	38	80	-36	20.11	20.11	(4+5)-III-4	79
2	4588	-1465	1645	47	57	-61	20.11	20.11	(4+5)-III-4	77
3	9292	-656	1180	59	31	-65	20.11	20.11	(4+5)-III-4	63
4	14385	74	414	68	8	-59	20.11	20.11	(4+5)-III-4	57
5	401	-2279	969	57	71	13	20.11	20.11	3	>100
6	5257	-1161	499	49	41	-28	20.11	20.11	(4+5)-I-4	>100
7	10412	-508	303	56	22	-35	20.11	20.11	(4+5)-III-4	85
8	15786	195	99	61	5	-33	20.11	20.11	(4+5)-III-4	76
9	875	-1844	68	58	72	37	20.11	20.11	3	84
10	5611	-894	146	37	21	47	20.11	20.11	(4+5)-I-2	99
11	9808	-399	20	39	10	45	20.11	20.11	(4+5)-III-1	93
12	22814	136	-73	58	2	12	20.11	20.11	3	88
13	885	-1143	-253	14	4	71	20.11	20.11	(4+5)-I-2	>100
14	5177	-757	-298	19	2	55	20.11	20.11	(4+5)-III-1	>100
15	9639	-370	-207	20	-1	47	20.11	20.11	(4+5)-III-1	>100
16	14293	-39	-48	20	-0	41	20.11	20.11	(4+5)-III-1	>100
Massimi/minimi										
1							20.11			
1								20.11		
4										57

Muro : 183 - Nodi: [2032-2005-3005-3032], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45, $\zeta_e=1.017$ [(4+5)-III-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	2174	12025	2445	-479	-8072	-68	20.11	20.11	(4+5)-III-1	1.3
2	517	9893	346	61	-7355	265	20.11	20.11	(4+5)-III-1	1.5
3	-251	6880	1530	22	-5509	-97	20.11	20.11	(4+5)-III-1	2.1
4	282	1219	719	68	-1616	-328	20.11	20.11	(4+5)-III-1	6.4
5	1786	4570	64	-698	-8035	200	20.11	20.11	(4+5)-III-1	1.5
6	-165	8451	896	-134	-7413	420	20.11	20.11	(4+5)-III-1	1.4
7	-1793	8764	3642	108	-5993	-249	20.11	20.11	(4+5)-III-1	1.8
8	3339	2718	3374	551	-1972	-1046	20.11	20.11	(4+5)-III-1	4.1
9	207	2430	-2588	-898	-7953	336	20.11	20.11	(4+5)-III-1	1.5
10	-942	6758	-675	-420	-7425	615	20.11	20.11	(4+5)-III-1	1.4
11	-4264	11377	3328	116	-6941	-243	20.11	20.11	(4+5)-III-1	1.5
12	7022	8793	8538	1521	-3493	-2076	20.11	20.11	(4+5)-III-1	2.0

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
13	-2092	4845	-4983	-1014	-7846	346	20.11	20.11	(4+5)-III-1	1.5
14	-2040	5509	-1816	-932	-7417	734	20.11	20.11	(4+5)-III-1	1.5
15	-8596	11498	-1249	635	-8189	17	20.11	20.11	(4+5)-III-1	1.3
16	-1585	27334	13206	2396	-9155	-4835	20.11	30.00	(4+5)-III-1	1.0
Massimi/minimi										
1							20.11			
16								30.00		
16										1.0

Muro : 184 - Nodi: [2031-2037-3037-3031], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=21.355$ [(4+5)-VI-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	8662	15886	10713	-476	-507	-238	20.11	20.11		2 9.5
2	3527	3204	490	98	-24	68	20.11	20.11		3 51
3	743	564	222	-11	7	34	20.11	20.11		3 >100
4	-139	-15	-58	11	7	10	20.11	20.11		3 >100
5	7836	2150	4878	40	-178	-95	20.11	20.11	(4+5)-III-4	32
6	1756	4792	4636	81	-26	101	20.11	20.11		3 48
7	798	1121	1443	39	-1	39	20.11	20.11		3 >100
8	514	-25	319	33	5	19	20.11	20.11		3 >100
9	9171	-1800	4316	229	55	-92	20.11	20.11		2 24
10	3132	1601	5244	156	-47	56	20.11	20.11		3 41
11	1109	788	2621	78	-1	37	20.11	20.11		3 76
12	355	47	559	61	-1	17	20.11	20.11		3 >100
13	6882	-3743	2485	322	149	-106	20.11	20.11		2 19
14	3904	-1521	4426	182	-20	-5	20.11	20.11		2 45
15	2904	-900	3182	111	-8	26	20.11	20.11		3 63
16	1723	-1301	798	84	-4	14	20.11	20.11		3 89
Massimi/minimi										
1							20.11			
1								20.11		
1										9.5

Muro : 185 - Nodi: [2033-2038-3038-3033], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=34.298$ [(4+5)-IV-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-1066	-5140	5045	108	153	22	20.11	20.11		3 55
2	1896	-4764	3568	68	-232	99	20.11	20.11		2 29
3	3683	-2907	3467	-24	-351	59	20.11	20.11		2 23
4	5862	-1477	2702	-57	-489	92	20.11	20.11		2 16
5	-398	-4845	4280	77	146	40	20.11	20.11		3 51
6	1595	-4141	3258	56	-232	48	20.11	20.11		2 34
7	4005	-2814	2941	-3	-358	53	20.11	20.11		2 23
8	6570	-1517	2330	-45	-494	87	20.11	20.11		2 16
9	-97	-4716	3608	47	120	62	20.11	20.11		3 52
10	1730	-3847	2845	32	-218	35	20.11	20.11		2 37
11	4199	-2617	2481	2	-361	43	20.11	20.11		2 23
12	6938	-1475	2025	-34	-494	81	20.11	20.11		2 16
13	-82	-4365	2808	30	103	69	20.11	20.11		3 55
14	1901	-3645	2404	13	-214	30	20.11	20.11		2 38
15	4426	-2488	2066	1	-358	35	20.11	20.11		2 24
16	7189	-1432	1771	-27	-492	73	20.11	20.11		2 16
Massimi/minimi										
1							20.11			
1								20.11		
4										16

Muro : 186 - Nodi: [2005-2008-3008-3005], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=1.145$ [(4+5)-I-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	2631	-4480	4554	-770	-6379	400	20.11	20.11	(4+5)-I-2	2.0
2	1673	-355	3904	-556	-5811	1164	20.11	20.11	(4+5)-I-2	1.8
3	2529	2835	2221	-148	-5594	2302	20.11	20.11	(4+5)-I-2	1.6
4	6809	6477	-1834	154	-6316	3607	20.11	20.11	(4+5)-I-2	1.2
5	-1638	-5534	-1817	-506	-4366	351	20.11	20.11	(4+5)-I-2	2.9
6	964	-5481	2305	-741	-3590	877	20.11	20.11	(4+5)-III-1	3.0
7	1443	-2143	2647	-1220	-2129	1330	20.11	20.11	(4+5)-III-1	3.8
8	7690	-1309	404	-1629	-345	1050	20.11	20.11	(4+5)-I-2	4.3
9	-2335	-4712	64	-545	-4180	56	20.11	20.11	(4+5)-III-1	3.2
10	471	-4498	-121	-685	-3338	-261	20.11	20.11	(4+5)-III-1	3.7
11	3293	-2908	-184	-1134	-1975	-578	20.11	20.11	(4+5)-III-1	5.2
12	7627	-2671	279	1522	-420	627	20.11	20.11	(4+5)-III-4	5.3
13	-2629	-1126	-4870	-538	-5183	88	20.11	20.11	(4+5)-III-1	2.4
14	-2216	1682	-3922	-280	-4868	-302	20.11	20.11	(4+5)-III-1	2.4
15	-991	6694	-2287	199	-4940	-1198	20.11	20.11	(4+5)-III-1	1.9
16	6375	12549	3850	641	-5675	-2511	20.11	20.11	(4+5)-III-1	1.3
Massimi/minimi										
1							20.11			
1								20.11		
4										1.2

Muro : 187 - Nodi: [2008-2049-3049-3008], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=1.075$ [(4+5)-I-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-2954	32	5099	-701	-5632	201	20.11	20.11	(4+5)-I-2	2.2
2	-3022	2191	3541	-450	-5559	291	20.11	20.11	(4+5)-I-2	2.1
3	-4362	7821	1361	753	-6143	1367	20.11	20.11	(4+5)-I-2	1.5
4	5347	19928	-7313	2117	-6509	4259	20.11	24.00	(4+5)-I-2	1.1
5	-2585	-3561	1603	-355	-5391	295	20.11	20.11	(4+5)-I-2	2.3
6	-495	-151	131	-37	-4827	645	20.11	20.11	(4+5)-I-2	2.3
7	1254	2498	-2770	114	-3722	1753	20.11	20.11	(4+5)-I-2	2.2
8	-3137	-669	2191	306	-903	2078	20.11	20.11	(4+5)-III-1	4.3
9	-299	-3041	-566	-234	-5043	478	20.11	20.11	(4+5)-I-2	2.4
10	1222	-341	-2591	-40	-4169	817	20.11	20.11	(4+5)-I-2	2.6
11	1129	114	-1906	-120	-2659	1332	20.11	20.11	(4+5)-I-2	3.2
12	-926	-326	702	-365	-697	1258	20.11	20.11	(4+5)-III-1	6.5
13	3487	3986	-3216	-198	-4901	604	20.11	20.11	(4+5)-I-2	2.2
14	202	2306	-1609	16	-3840	603	20.11	20.11	(4+5)-I-2	2.8
15	113	851	-931	-73	-2315	691	20.11	20.11	(4+5)-I-2	4.2
16	-114	-218	65	-219	-593	474	20.11	20.11	(4+5)-III-1	12
Massimi/minimi										
1							20.11			
4								24.00		
4										1.1

Muro : 188 - Nodi: [2038-2044-3044-3038], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=18.886$ [(4+5)-II-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	522	-3747	1448	18	109	85	20.11	20.11	3	48
2	2286	-3170	1120	-9	-220	58	20.11	20.11	2	34
3	4543	-2167	1033	-9	-352	59	20.11	20.11	2	22
4	7179	-1365	1071	-18	-484	72	20.11	20.11	2	16

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
5	665	-2251	-65	27	175	102	20.11	20.11		3
6	2296	-2391	-105	-1	-206	109	20.11	20.11		2
7	4202	-1804	43	13	-325	122	20.11	20.11		2
8	6229	-1438	408	16	-458	128	20.11	20.11		2
9	651	-1583	-470	32	335	109	20.11	20.11		3
10	2445	-1356	-343	36	232	196	20.11	20.11		3
11	3473	-1550	-115	35	-259	234	20.11	20.11		2
12	5076	-1298	80	45	-454	222	20.11	20.11		2
13	-58	-2587	-919	245	878	319	20.11	20.11		3
14	1611	-1976	-13	293	386	265	20.11	20.11		3
15	4157	-1328	-83	207	84	259	20.11	20.11		3
16	5166	-1042	-414	98	-482	226	20.11	20.11		2
Massimi/minimi										
1							20.11			
1								20.11		
13										7.7

Muro : 189 - Nodi: [2044-2050-3050-3044], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45, $\zeta_e=12.469$ [(4+5)-VI-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-7267	-2574	-1956	474	935	201	20.11	20.11		8.1
2	997	-2029	-863	337	413	85	20.11	20.11		3
3	3607	-2139	-799	151	-202	167	20.11	20.11		2
4	6181	-1307	-1199	62	-487	132	20.11	20.11		2
5	-2470	-899	1671	-49	417	429	20.11	20.11		3
6	1095	-2096	-876	-46	374	121	20.11	20.11		3
7	3974	-2000	-1208	35	-188	169	20.11	20.11		2
8	6943	-1309	-1787	2	-468	108	20.11	20.11		2
9	-17	-2945	1513	-6	407	357	20.11	20.11		3
10	2910	-2239	-356	-55	294	272	20.11	20.11		3
11	4833	-2107	-1516	-41	-220	227	20.11	20.11		2
12	7643	-1309	-2279	-47	-474	110	20.11	20.11		2
13	1593	-4148	492	27	544	335	20.11	20.11		3
14	4484	-2663	-1070	-17	202	318	20.11	20.11		3
15	5998	-2044	-1845	-58	-310	268	20.11	20.11		2
16	8356	-1338	-2679	-83	-496	108	20.11	20.11		2
Massimi/minimi										
1							20.11			
1								20.11		
1										8.1

Muro : 190 - Nodi: [2050-2054-3054-3050], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45, $\zeta_e=12.161$ [(4+5)-VI-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	3174	-4185	-582	68	686	322	20.11	20.11		9.4
2	4564	-2673	-1556	-92	-35	347	20.11	20.11		2
3	6594	-1566	-2186	-138	-413	280	20.11	20.11		2
4	9105	-1251	-2839	-155	-526	78	20.11	20.11		2
5	4750	-3018	-1601	7	786	285	20.11	20.11		3
6	5025	-1534	-2384	-240	-75	314	20.11	20.11		2
7	6704	-741	-2208	-344	-497	284	20.11	20.11		2
8	9763	-1067	-2645	-330	-565	95	20.11	20.11		2
9	6602	-58	-2694	-195	823	209	20.11	20.11		3
10	4990	346	-3001	-547	-121	198	20.11	20.11		2
11	6409	228	-1654	-801	-529	272	20.11	20.11		2
12	10758	-943	-1942	-747	-636	178	20.11	20.11		2
13	8978	6763	-3183	-542	778	43	20.11	20.11		3
14	4981	2950	-2151	-1081	-116	-26	20.11	20.11		3
15	5468	-171	-1201	-1585	-559	73	20.11	20.11		2

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
16	13043	-470	-353	-1707	-666	312	20.11	20.11	2	3.7
Massimi/minimi										
1							20.11			
1								20.11		
16										3.7

Muro : 191 - Nodi: [2054-2057-3057-3054], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=2.871$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	6472	3201	650	-250	660	-354	20.11	20.11	(4+5)-II-4	8.5
2	5731	1241	1283	-899	-79	-412	20.11	20.11	3	6.3
3	6092	320	2	-1360	-299	-409	20.11	20.11	3	4.7
4	10746	683	-819	-1860	-203	-232	20.11	20.11	2	3.7
5	3253	-3078	-950	-24	353	-526	20.11	20.11	(4+5)-VI-4	11
6	6237	-2315	613	-355	-133	-786	20.11	20.11	1	7.2
7	6707	-724	-160	-507	-143	-764	20.11	20.11	1	6.4
8	10657	-389	-506	-617	-66	-608	20.11	20.11	2	6.3
9	4153	-4455	-1375	-144	-614	-692	20.11	20.11	1	7.2
10	6392	-2368	-1730	-28	-170	-770	20.11	20.11	1	9.8
11	6500	-212	1938	631	117	-448	20.11	20.11	(4+5)-V-4	7.6
12	12492	-61	1317	791	66	-388	20.11	20.11	(4+5)-V-4	6.3
13	7907	-980	-3611	265	-746	-387	20.11	20.11	1	8.0
14	4744	-2540	-3854	794	-48	-501	20.11	20.11	2	6.5
15	4675	-1519	713	1612	301	109	20.11	20.11	(4+5)-VII-3	4.9
16	14752	-100	1319	2454	182	69	20.11	20.11	(4+5)-V-4	2.9
Massimi/minimi										
1							20.11			
1								20.11		
16										2.9

Muro : 192 - Nodi: [2011-2014-3014-3011], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=1.403$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-7643	1663	3025	-364	-3485	165	20.11	20.11	(4+5)-VII-2	2.4
2	-7926	1384	2853	-117	-3188	357	20.11	20.11	(4+5)-VII-2	2.5
3	-8702	5077	2441	264	-3155	987	20.11	20.11	(4+5)-VII-2	2.0
4	-4645	9107	-1847	615	-3497	1828	20.11	20.11	(4+5)-VII-2	1.5
5	-4315	-672	2995	-475	-2627	186	20.11	20.11	(4+5)-VII-2	3.2
6	-4503	-863	2280	-618	-1869	513	20.11	20.11	(4+5)-VII-2	3.8
7	-3987	-538	1435	-848	-945	759	20.11	20.11	(4+5)-VII-2	5.3
8	-1880	-606	612	-1104	12	700	20.11	20.11	(4+5)-V-1	5.1
9	-3327	-2759	3852	-271	-1899	-192	20.11	20.11	(4+5)-V-1	4.4
10	-844	-2287	3316	-347	-1442	-232	20.11	20.11	(4+5)-V-1	5.5
11	1832	-960	2416	-533	-721	-334	20.11	20.11	(4+5)-V-1	8.6
12	4620	567	537	-776	181	-285	20.11	20.11	(4+5)-V-1	7.9
13	-2790	-4979	-55	151	1095	-488	20.11	20.11	(4+5)-VII-3	6.0
14	-2582	-1885	-217	-4	1730	-533	20.11	20.11	(4+5)-VII-3	4.0
15	1439	2183	-1735	572	-2821	-333	20.11	20.11	(4+5)-V-1	2.8
16	7894	5929	998	832	-4112	-1546	20.11	20.11	(4+5)-V-1	1.5
Massimi/minimi										
1							20.11			
1								20.11		
16										1.5

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Muro : 193 - Nodi: [2057-3057-3011-2011], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=1.201$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	3518	-876	-5931	1420	-75	281	20.11	20.11	(4+5)-V-1	5.0
2	-3126	-1416	-6003	2317	221	269	20.11	20.11	(4+5)-V-1	3.6
3	-4420	-2118	-6769	2996	331	97	20.11	20.11	(4+5)-V-1	3.1
4	-3933	-2660	-7963	3423	439	-121	20.11	20.11	(4+5)-VII-1	2.7
5	5043	3559	-2864	915	-23	908	20.11	20.11	(4+5)-V-1	4.6
6	-2041	400	-3970	1712	70	915	20.11	20.11	(4+5)-V-1	3.5
7	-3130	-4214	-10593	-2273	-1	-1130	20.11	20.11	(4+5)-VII-3	2.7
8	-2862	-4689	-6694	3604	189	169	20.11	20.11	(4+5)-V-1	2.5
9	-4460	3113	-2889	-705	-1631	-1206	20.11	20.11	(4+5)-VII-3	3.0
10	-2289	818	-6085	-1130	-632	-1839	20.11	20.11	(4+5)-VII-3	3.1
11	-1255	-2965	-8056	-1954	197	-2026	20.11	20.11	(4+5)-VII-3	2.3
12	-1303	-7739	-4665	4032	-866	1043	20.11	20.11	(4+5)-V-1	1.8
13	-1009	10608	-659	-261	-2162	-1286	20.11	20.11	(4+5)-VII-3	2.2
14	-76	6722	-2426	-368	-917	-1847	20.11	20.11	(4+5)-VII-3	3.0
15	-679	1288	-2879	-490	231	-2430	20.11	20.11	(4+5)-VII-3	3.1
16	2457	-8126	-606	4067	-2563	2995	20.11	20.11	(4+5)-V-1	1.2
Massimi/minimi										
1							20.11			
1								20.11		
16										1.2

Muro : 194 - Nodi: [2014-3014-3085-2085], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=1.032$ [(4+5)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-2359	-1158	6746	-520	-420	586	20.11	20.11	(4+5)-V-4	8.3
2	-6434	-444	3415	-172	-250	423	20.11	20.11	(4+5)-VII-3	13
3	-6581	-312	2658	9	-52	290	20.11	20.11	(4+5)-VII-3	26
4	-7429	210	757	77	-355	-18	20.11	20.11	(4+5)-VII-2	24
5	-1413	-3200	4850	-2008	-1086	1047	20.11	20.11	(4+5)-V-4	3.0
6	-524	-2284	4573	-1600	-614	931	20.11	20.11	(4+5)-V-4	3.6
7	733	-2094	3875	-1231	-258	782	20.11	20.11	(4+5)-V-4	4.4
8	2144	-1253	3504	-974	290	294	20.11	20.11	(4+5)-V-4	6.9
9	-165	-5053	1455	4534	-781	-2022	20.11	20.11	(4+5)-VII-2	1.4
10	1143	-2024	-375	3650	-96	-2164	20.11	20.11	(4+5)-VII-2	1.5
11	1896	-887	-1330	2831	387	-2171	20.11	20.11	(4+5)-VII-2	1.7
12	4151	-353	-1417	2075	769	-1118	20.11	20.11	(4+5)-VII-2	2.6
13	5059	-1320	-4152	6520	-4449	-5559	30.00	24.00	(4+5)-VII-2	1.0
14	3359	955	-4651	3052	-1757	-4120	20.11	20.11	(4+5)-VII-2	1.2
15	875	1041	-3465	1827	1331	-3311	20.11	20.11	(4+5)-VII-2	1.7
16	-2256	3731	-2540	1428	4985	-1714	20.11	20.11	(4+5)-VII-2	1.3
Massimi/minimi										
13							30.00			
13								24.00		
13										1.0

Muro : 195 - Nodi: [2084-2085-3085-3084], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=1.766$ [(4+5)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	1562	-317	-58	-75	-639	99	20.11	20.11	1	12
2	-1613	-4352	-5146	-140	-24	292	20.11	20.11	(4+5)-VII-3	21
3	-2738	-1960	-3177	-249	1	251	20.11	20.11	(4+5)-V-4	19
4	-4900	682	-1140	-284	-5	172	20.11	20.11	(4+5)-V-4	21
5	911	1137	4662	-40	-331	82	20.11	20.11	(4+5)-V-1	21
6	848	-1326	2	-76	-185	98	20.11	20.11	1	32

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
7	-6360	-1352	-4573	-103	-10	200	20.11	20.11	(4+5)-V-3	32
8	-9914	720	-1813	-150	-10	166	20.11	20.11	(4+5)-V-3	32
9	284	-2172	-2392	-6	374	60	20.11	20.11	(4+5)-VII-3	21
10	47	2646	5514	103	-127	127	20.11	20.11	(4+5)-VII-2	34
11	6987	2413	7786	147	0	173	20.11	20.11	(4+5)-V-1	25
12	17717	-172	3802	220	28	163	20.11	20.11	(4+5)-V-1	18
13	723	-1843	-462	-100	-538	-65	20.11	20.11	1	15
14	5863	177	-1087	-570	6	-377	20.11	20.11	(4+5)-VII-3	8.7
15	-817	-664	-5314	-1110	-232	-437	20.11	20.11	(4+5)-V-4	5.8
16	33286	3943	7483	912	-84	92	20.11	20.11	(4+5)-VII-2	4.9
Massimi/minimi										
1							20.11			
1								20.11		
16										4.9

Muro : 196 - Nodi: [2078-3078-3084-2084], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=9.310$ [(4+5)-VI-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-4488	-120	2079	813	-12	-250	20.11	20.11	(4+5)-VII-3	8.9
2	-5208	192	844	632	94	-379	20.11	20.11	(4+5)-VII-3	9.4
3	-4924	741	-781	166	42	-318	20.11	20.11	(4+5)-III-3	20
4	-3787	1566	-1348	-352	16	-305	20.11	20.11	(4+5)-V-4	14
5	-2071	30	2951	121	-417	-155	20.11	20.11	(4+5)-V-4	16
6	-3202	296	1493	91	-52	-518	20.11	20.11	(4+5)-V-4	15
7	-3395	520	-170	92	63	-548	20.11	20.11	(4+5)-V-4	15
8	-2827	11	-1183	51	200	-449	20.11	20.11	(4+5)-V-4	14
9	-943	-482	2194	-68	-741	-238	20.11	20.11	(4+5)-V-4	9.2
10	-1391	165	1258	-44	-199	-483	20.11	20.11	(4+5)-V-4	13
11	-1651	217	0	61	101	-513	20.11	20.11	(4+5)-V-4	15
12	-1875	-164	-959	163	390	-432	20.11	20.11	(4+5)-V-4	11
13	-307	-552	895	-74	-854	-254	20.11	20.11	(4+5)-V-4	8.1
14	-223	684	578	-36	-281	-380	20.11	20.11	(4+5)-V-4	13
15	-238	1179	117	21	123	-398	20.11	20.11	(4+5)-V-4	17
16	-893	788	-738	97	566	-297	20.11	20.11	(4+5)-V-4	10
Massimi/minimi										
1							20.11			
1								20.11		
13										8.1

Muro : 197 - Nodi: [3030-3034-3033-3029], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=125.706$ [(4+5)-IV-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	181	9	-122	-9	1	6	20.11	20.11		>100
2	382	635	-648	-6	60	5	20.11	20.11		80
3	544	1436	-1307	-2	166	3	20.11	20.11		31
4	587	2423	-2122	-35	353	-37	20.11	20.11		13
5	1125	-59	-340	-20	1	9	20.11	20.11		>100
6	1657	-24	-1134	-17	55	-5	20.11	20.11		89
7	1815	-78	-1706	-11	143	-12	20.11	20.11		34
8	1565	-75	-2065	0	261	-62	20.11	20.11		16
9	2323	3	-313	-9	1	13	20.11	20.11		>100
10	2761	-54	-1028	-5	49	-6	20.11	20.11		96
11	2673	-91	-1572	10	135	-9	20.11	20.11		37
12	2607	-184	-2114	32	267	-53	20.11	20.11		17
13	3407	41	-287	7	1	18	20.11	20.11		>100
14	3837	-19	-928	10	49	0	20.11	20.11		>100
15	3661	-71	-1478	26	138	0	20.11	20.11		38
16	3542	-130	-1994	52	274	-42	20.11	20.11		17
Massimi/minimi										

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
1							20.11			
1								20.11		
4										13

Muro : 198 - Nodi: [3034-3039-3038-3033], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45,ζ_e=75.387 [(4+5)-II-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	4183	30	-301	17	2	20	20.11	20.11	3	>100
2	4612	-2	-874	19	50	5	20.11	20.11	2	96
3	4378	-75	-1371	35	141	6	20.11	20.11	2	36
4	4236	-191	-1814	62	280	-38	20.11	20.11	2	17
5	4763	3	-294	22	2	22	20.11	20.11	3	>100
6	4693	-9	-800	26	20	29	20.11	20.11	3	89
7	4828	-96	-1289	39	143	10	20.11	20.11	2	34
8	4647	-195	-1698	64	284	-32	20.11	20.11	2	17
9	5330	13	-292	26	3	23	20.11	20.11	3	100
10	5147	-68	-740	29	22	31	20.11	20.11	3	81
11	5239	-140	-1216	41	145	12	20.11	20.11	2	33
12	5008	-237	-1586	67	286	-27	20.11	20.11	2	17
13	5969	-409	-204	28	4	23	20.11	20.11	3	94
14	5549	-74	-717	31	22	32	20.11	20.11	3	77
15	5601	-101	-1136	42	146	12	20.11	20.11	2	33
16	5362	-363	-1489	66	287	-22	20.11	20.11	2	17
Massimi/minimi										
1							20.11			
1								20.11		
4										17

Muro : 199 - Nodi: [3039-3045-3044-3038], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45,ζ_e=27.872 [(4+5)-II-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	7393	138	-216	17	3	31	20.11	20.11	3	99
2	7379	54	-641	19	49	23	20.11	20.11	2	73
3	6632	-1	-955	33	140	22	20.11	20.11	2	33
4	5976	42	-1169	54	278	-4	20.11	20.11	2	19
5	9759	370	-166	1	2	41	20.11	20.11	3	>100
6	9018	68	-458	3	46	42	20.11	20.11	2	60
7	7589	-6	-624	18	131	41	20.11	20.11	2	31
8	6196	178	-667	42	262	22	20.11	20.11	2	19
9	11398	537	-107	3	2	51	20.11	20.11	3	82
10	9976	97	-248	4	48	61	20.11	20.11	2	48
11	7985	2	-324	18	136	63	20.11	20.11	2	26
12	6026	222	-353	41	268	55	20.11	20.11	2	16
13	11308	528	153	27	4	50	20.11	20.11	3	58
14	9809	7	401	26	57	67	20.11	20.11	2	43
15	7857	-239	575	38	154	69	20.11	20.11	2	24
16	6019	-345	701	58	299	70	20.11	20.11	2	14
Massimi/minimi										
1							20.11			
1								20.11		
16										14

Muro : 200 - Nodi: [3045-3051-3050-3044], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45,ζ_e=27.618 [(4+5)-II-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	9277	324	348	46	5	43	20.11	20.11	3	52
2	8454	-42	1044	43	61	64	20.11	20.11	2	42
3	7014	-332	1474	54	163	65	20.11	20.11	2	23
4	5568	-746	1706	84	312	75	20.11	20.11	2	14
5	8077	125	494	32	9	46	20.11	20.11	2	60
6	7096	-7	1367	37	60	60	20.11	20.11	2	44
7	6226	-194	1919	47	160	60	20.11	20.11	2	24
8	5511	-479	2124	69	301	84	20.11	20.11	2	14
9	5734	18	586	26	9	43	20.11	20.11	2	70
10	5471	-35	1607	31	60	55	20.11	20.11	2	46
11	5329	-174	2249	42	157	56	20.11	20.11	2	25
12	5228	-344	2547	64	296	90	20.11	20.11	2	14
13	3087	-109	630	22	9	39	20.11	20.11	2	83
14	3626	4	1717	27	61	50	20.11	20.11	2	47
15	4195	19	2468	38	160	53	20.11	20.11	2	25
16	4842	-80	2908	59	301	97	20.11	20.11	2	13
Massimi/minimi										
1							20.11			
1								20.11		
16										13

Muro : 201 - Nodi: [3051-3055-3054-3050], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=27.999$ [(4+5)-II-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	1059	-137	534	20	10	33	20.11	20.11	2	98
2	2037	210	1509	24	65	46	20.11	20.11	2	48
3	3010	510	2379	33	166	51	20.11	20.11	2	24
4	4182	540	3032	54	309	106	20.11	20.11	2	13
5	-95	-15	279	18	12	28	20.11	20.11	2	>100
6	831	516	899	20	71	39	20.11	20.11	2	48
7	1719	1193	1880	28	176	46	20.11	20.11	2	23
8	3198	1649	2989	44	323	109	20.11	20.11	2	12
9	-448	37	-66	14	14	20	20.11	20.11	2	>100
10	80	576	50	16	80	30	20.11	20.11	2	48
11	-39	1529	489	21	194	40	20.11	20.11	2	22
12	1156	2758	2305	26	359	107	20.11	20.11	2	11
13	-122	-80	-117	6	15	8	20.11	20.11	2	>100
14	-39	-304	-253	6	87	15	20.11	20.11	2	52
15	27	-369	-269	16	216	27	20.11	20.11	2	22
16	-3887	1374	-890	-39	434	62	20.11	20.11	2	10
Massimi/minimi										
1							20.11			
1								20.11		
16										10

Muro : 202 - Nodi: [2073-2075-3075-3073], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=10.415$ [(4+5)-IV-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx kg	Ny kg	Nxy kg	Mx kg*m	My kg*m	Mxy kg*m	Ax cmq	Ay cmq	C	Cs
1	8511	-5458	1226	-83	-1554	-72	20.11	20.11	1	4.7
2	10031	-3471	-239	7	-593	-383	20.11	20.11	1	7.6
3	8178	-1486	-1173	109	-142	-348	20.11	20.11	1	14
4	7206	-209	-935	175	-9	-241	20.11	20.11	1	15
5	9206	-5506	496	-200	-1838	-118	20.11	20.11	1	3.9
6	10792	-2733	-1469	-62	-615	-365	20.11	20.11	1	7.5
7	8247	-684	-1878	123	-90	-307	20.11	20.11	1	15
8	6433	-107	-1002	249	15	-219	20.11	20.11	1	14
9	11172	-3323	-361	-273	-2102	-161	20.11	20.11	1	3.3

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
10	11219	-141	-2769	5	-581	-302	20.11	20.11	1	8.0
11	8101	210	-1993	261	-36	-224	20.11	20.11	1	13
12	5712	-63	-862	398	42	-171	20.11	20.11	1	12
13	15257	5166	-2442	-293	-2251	-89	20.11	20.11	1	2.8
14	10820	3719	-2022	309	-513	-121	20.11	20.11	1	11
15	7042	1297	-1318	556	16	-96	20.11	20.11	1	9.8
16	4945	48	-596	650	57	-90	20.11	20.11	1	9.0
Massimi/minimi										
1							20.11			
1								20.11		
13										2.8

Muro : 203 - Nodi: [2068-2071-3071-3068], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=8.864$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	3877	16072	6224	29	175	188	20.11	20.11	1	15
2	317	5451	2222	22	12	126	20.11	20.11	3	48
3	-375	47	496	18	-97	58	20.11	20.11	1	46
4	-407	-60	141	13	-42	0	20.11	20.11	1	>100
5	1277	4059	7699	129	163	237	20.11	20.11	1	17
6	2542	1681	6460	91	-9	165	20.11	20.11	3	27
7	2120	-2300	1240	57	-137	79	20.11	20.11	1	34
8	-364	-823	-372	62	-73	-23	20.11	20.11	1	75
9	-348	-1677	10154	255	164	225	20.11	20.11	1	15
10	5345	-3821	7703	153	-59	121	20.11	20.11	3	24
11	4761	-5220	2295	41	-169	87	20.11	20.11	1	30
12	-1343	-5133	-2650	129	-226	-63	20.11	20.11	1	26
13	492	-9083	12599	471	-107	161	20.11	20.11	3	11
14	8159	-6328	7361	176	-89	-65	20.11	20.11	3	26
15	5816	-6699	4414	84	-115	-57	20.11	20.11	3	45
16	11515	-19229	-3221	35	-1106	-578	20.11	20.11	3	5.2
Massimi/minimi										
1							20.11			
1								20.11		
16										5.2

Muro : 204 - Nodi: [2071-2073-3073-3071], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=13.170$ [(4+5)-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	5660	-13842	3626	205	-587	70	20.11	20.11	1	13
2	7759	-10045	3273	142	-287	-42	20.11	20.11	1	24
3	10337	-9582	2106	-245	-222	-82	20.11	20.11	1	19
4	2497	-18143	6731	-759	-1625	786	20.11	20.11	3	3.6
5	6325	-11035	3190	171	-666	12	20.11	20.11	1	12
6	8763	-9422	2008	26	-364	-175	20.11	20.11	1	15
7	8338	-8076	3301	-284	-291	-294	20.11	20.11	1	11
8	3377	-1897	2486	-444	-358	-75	20.11	20.11	1	13
9	6865	-8761	2453	54	-903	-53	20.11	20.11	1	8.3
10	9046	-7424	1437	-2	-462	-317	20.11	20.11	1	10.0
11	7790	-4715	1375	-126	-263	-355	20.11	20.11	1	12
12	6900	-924	285	-182	-116	-212	20.11	20.11	1	16
13	8123	-6243	2389	-34	-1216	-70	20.11	20.11	1	6.0
14	9823	-4673	452	32	-525	-373	20.11	20.11	1	8.4
15	7913	-2449	-226	46	-190	-361	20.11	20.11	1	13
16	7080	-428	-590	53	-46	-249	20.11	20.11	1	21
Massimi/minimi										
1							20.11			
1								20.11		
4										3.6

Muro : 205 - Nodi: [2075-2077-3077-3075], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=9.525$ [(4+5)-IV-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	11331	5096	-1866	-196	-2234	91	20.11	20.11	1	2.8
2	10974	3810	36	294	-499	-37	20.11	20.11	1	13
3	7380	1518	-60	568	31	-50	20.11	20.11	1	10
4	5292	309	-265	674	58	-55	20.11	20.11	1	9.0
5	7487	-3128	-3669	-239	-2031	80	20.11	20.11	1	3.5
6	10111	-46	273	11	-573	55	20.11	20.11	1	11
7	7665	519	576	291	-27	-25	20.11	20.11	1	20
8	5392	44	217	459	38	-27	20.11	20.11	1	14
9	6023	-4859	-4120	-249	-1787	64	20.11	20.11	1	4.1
10	9647	-2517	-1004	-29	-629	116	20.11	20.11	1	9.8
11	7629	-598	493	160	-70	64	20.11	20.11	1	28
12	5575	-113	429	312	32	33	20.11	20.11	1	19
13	4434	-4193	-5297	-142	-1545	86	20.11	20.11	1	4.6
14	7760	-2214	-1776	23	-632	148	20.11	20.11	1	9.3
15	6903	-893	47	158	-101	138	20.11	20.11	1	22
16	5740	-139	392	265	24	88	20.11	20.11	1	19
Massimi/minimi										
1							20.11			
1								20.11		
1										2.8

Muro : 206 - Nodi: [2077-2079-3079-3077], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=9.655$ [(4+5)-VI-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	331	-2801	-5962	-29	-1312	104	20.11	20.11	1	5.2
2	6704	-2074	-2139	29	-590	158	20.11	20.11	1	9.7
3	6662	-1066	-288	140	-112	178	20.11	20.11	1	20
4	5839	-278	233	231	15	135	20.11	20.11	1	18
5	-1029	-3352	-5345	-41	-1127	74	20.11	20.11	1	6.2
6	5001	-2866	-2924	1	-552	148	20.11	20.11	1	11
7	5772	-1275	-790	80	-129	201	20.11	20.11	1	22
8	5857	-267	56	160	6	171	20.11	20.11	1	20
9	-1002	-3363	-4885	-103	-977	69	20.11	20.11	1	7.1
10	3850	-2409	-3544	-4	-483	140	20.11	20.11	1	12
11	4903	-1336	-1354	87	-118	236	20.11	20.11	1	20
12	5666	-283	-159	173	-0	204	20.11	20.11	1	17
13	-277	-1180	-5803	-244	-835	115	20.11	20.11	1	7.6
14	1727	-567	-3207	13	-411	190	20.11	20.11	1	12
15	3376	-717	-1676	176	-108	281	20.11	20.11	1	15
16	4912	-223	-433	262	-13	219	20.11	20.11	1	14
Massimi/minimi										
1							20.11			
1								20.11		
1										5.2

Muro : 207 - Nodi: [2074-2072-3072-3074], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=4.233$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-11947	2430	-931	273	1574	-147	20.11	20.11	(4+5)-V-4	4.0

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
2	-10159	1008	629	173	498	-47	20.11	20.11	(4+5)-V-4	13
3	-428	-810	-2190	143	-208	-221	20.11	20.11	1	17
4	160	-308	-1202	158	-90	-304	20.11	20.11	1	15
5	-12456	3823	582	320	1663	-116	20.11	20.11	(4+5)-V-4	3.8
6	-10574	527	2055	221	523	-54	20.11	20.11	(4+5)-V-4	12
7	-438	-1902	-1993	159	-317	-222	20.11	20.11	1	13
8	-1410	-793	-1748	223	-171	-383	20.11	20.11	1	12
9	-14453	1347	2073	328	1735	-79	20.11	20.11	(4+5)-V-4	3.8
10	-10473	-2050	3932	126	504	-85	20.11	20.11	(4+5)-V-4	12
11	-185	-2462	-1147	59	-404	-134	20.11	20.11	1	14
12	-2654	-2692	-3387	336	-474	-448	20.11	20.11	1	8.0
13	-18839	-8146	4381	207	1740	-123	20.11	20.11	(4+5)-V-4	4.2
14	-9141	-6666	3390	-181	448	-129	20.11	20.11	(4+5)-V-4	13
15	2395	-2344	391	-21	-377	-73	20.11	20.11	1	16
16	3972	-7020	-2767	174	-2275	-980	20.11	20.11	3	2.4
Massimi/minimi										
1							20.11			
1								20.11		
16										2.4

Muro : 208 - Nodi: [2059-2064-3064-3059], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=10.888$ [(4+5)-IV-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	1698	14425	-160	1001	836	311	20.11	40.21	3	5.3
2	-5105	7078	503	1238	529	-14	20.11	40.21	3	6.0
3	-7617	2908	484	959	230	-20	20.11	20.11	3	8.0
4	-10131	876	247	731	74	-57	20.11	20.11	2	10
5	4095	12033	4534	621	239	350	20.11	20.11	3	6.9
6	-4386	6925	3411	734	409	22	20.11	20.11	3	9.9
7	-6739	2512	2256	700	189	-59	20.11	20.11	2	10
8	-9507	304	1042	626	39	-55	20.11	20.11	2	12
9	2765	6906	5466	410	18	325	20.11	20.11	3	9.3
10	-3608	5127	5913	419	248	68	20.11	20.11	3	15
11	-4847	988	3430	425	135	-97	20.11	20.11	1	14
12	-6410	51	1478	432	24	-77	20.11	20.11	1	15
13	527	2938	5767	244	-137	223	20.11	20.11	3	15
14	-2774	568	5484	190	131	-45	20.11	20.11	1	31
15	-3613	-69	4136	212	105	-111	20.11	20.11	1	23
16	-4485	-190	1806	252	29	-76	20.11	20.11	1	23
Massimi/minimi										
1							20.11			
1								40.21		
1										5.3

Muro : 209 - Nodi: [2079-2078-3078-3079], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=5.961$ [(4+5)-V-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-7321	5	-6554	-164	-679	250	20.11	20.11	1	7.6
2	2712	1050	-2648	-30	-248	296	20.11	20.11	1	13
3	3940	560	-1223	148	-16	345	20.11	20.11	1	14
4	4067	21	-358	248	43	275	20.11	20.11	1	13
5	-8863	-995	-6809	-52	-434	206	20.11	20.11	1	11
6	258	-1166	-3120	-99	-223	321	20.11	20.11	1	13
7	2798	-480	-916	-93	-65	370	20.11	20.11	1	15
8	3396	-181	-74	-90	-1	315	20.11	20.11	1	17
9	-10105	-9	-5365	-20	-230	149	20.11	20.11	1	19
10	-1324	-2022	-3093	-176	-171	268	20.11	20.11	1	16
11	1926	-1354	-1184	-314	-91	339	20.11	20.11	1	11
12	2975	-330	-243	-403	-31	298	20.11	20.11	1	9.7

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
13	-13711	10407	-3796	394	143	-41	20.11	20.11	(4+5)-V-4	19
14	-8625	3394	-1265	542	79	-13	20.11	20.11	(4+5)-V-4	14
15	1354	-1815	-1599	-542	-106	249	20.11	20.11	1	8.8
16	3038	-761	-657	-755	-61	249	20.11	20.11	1	6.8
Massimi/minimi										
1							20.11			
1								20.11		
16										6.8

Muro : 210 - Nodi: [2072-2069-3069-3072], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=7.296$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-13466	-6802	3978	183	1960	-294	20.11	20.11	(4+5)-V-4	3.4
2	-8386	-6555	1245	-177	489	-83	20.11	20.11	(4+5)-VII-3	13
3	1676	-1231	314	34	-329	-55	20.11	20.11	1	19
4	5381	-7092	3339	-730	-2346	1280	20.11	20.11	3	2.1
5	-11075	107	5970	342	1930	-344	20.11	20.11	(4+5)-VII-3	3.1
6	-6374	-3642	1798	94	606	-190	20.11	20.11	(4+5)-VII-3	9.3
7	1319	-3648	1384	-45	-358	-47	20.11	20.11	1	18
8	-703	-3880	2648	-231	-531	354	20.11	20.11	3	8.4
9	-9610	-470	8279	299	1782	-339	20.11	20.11	(4+5)-VII-3	3.4
10	-3658	-2609	2860	117	736	-248	20.11	20.11	(4+5)-VII-3	7.4
11	563	-3668	1496	19	-261	-34	20.11	20.11	1	25
12	-1349	-1069	1435	-35	-183	144	20.11	20.11	1	22
13	-8120	-9994	9746	219	1676	-351	20.11	20.11	(4+5)-VII-3	3.9
14	-807	1446	411	14	801	-171	20.11	20.11	(4+5)-VII-3	7.1
15	240	-3170	537	18	-180	-22	20.11	20.11	1	37
16	-83	-771	328	-7	-115	46	20.11	20.11	1	44
Massimi/minimi										
1							20.11			
1								20.11		
4										2.1

Muro : 211 - Nodi: [2064-2066-3066-3064], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=24.192$ [(4+5)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-440	-620	6370	123	-191	153	20.11	20.11	3	21
2	-2927	-1405	5840	68	60	-49	20.11	20.11	1	63
3	-3516	-985	4205	92	68	-95	20.11	20.11	1	40
4	-3738	-208	1751	98	14	-67	20.11	20.11	1	45
5	-2641	-5504	6981	-28	-310	164	20.11	20.11	3	16
6	-1443	-2902	4784	-0	-77	46	20.11	20.11	(4+5)-III-1	60
7	-2010	-2147	3719	37	55	-41	20.11	20.11	1	75
8	-1949	-458	1308	54	22	-41	20.11	20.11	1	77
9	-3890	-11943	7128	-182	-444	186	20.11	20.11	3	13
10	-728	-5506	3899	-19	-108	47	20.11	20.11	(4+5)-III-1	49
11	-802	-2826	2555	9	41	-26	20.11	20.11	1	>100
12	-860	-558	746	26	20	-28	20.11	20.11	1	>100
13	-1306	-23693	6209	-368	-453	206	20.11	20.11	3	13
14	238	-7330	1385	33	-130	29	20.11	20.11	(4+5)-III-1	49
15	282	-2969	976	-13	34	-14	20.11	20.11	1	>100
16	206	-476	244	8	20	-14	20.11	20.11	1	>100
Massimi/minimi										
1							20.11			
1								20.11		
13										13

Muro : 212 - Nodi: [2076-2074-3074-3076], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=7.791$ [(4+5)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-10351	-3287	-3363	1	1215	-156	20.11	20.11	(4+5)-V-4	5.4
2	-6640	260	-746	-346	39	107	20.11	20.11	(4+5)-II-2	17
3	-5067	358	-188	-456	-99	126	20.11	20.11	(4+5)-VI-4	13
4	-4405	27	87	-509	-49	77	20.11	20.11	(4+5)-VI-4	13
5	-9661	1995	-2865	194	1366	-221	20.11	20.11	(4+5)-V-4	4.3
6	-6669	349	-2394	58	277	-112	20.11	20.11	(4+5)-VII-3	18
7	864	-480	-2324	-19	-96	-247	20.11	20.11	1	21
8	-4659	-55	157	-364	-52	23	20.11	20.11	(4+5)-II-2	19
9	-9517	3403	-2038	243	1417	-187	20.11	20.11	(4+5)-V-4	4.2
10	-7612	1068	-1591	170	373	-129	20.11	20.11	(4+5)-VII-3	14
11	356	-689	-2440	53	-117	-257	20.11	20.11	1	19
12	1799	-216	-1002	30	-39	-252	20.11	20.11	1	24
13	-10430	1927	-1253	261	1478	-145	20.11	20.11	(4+5)-V-4	4.3
14	-9663	968	34	144	452	-79	20.11	20.11	(4+5)-V-4	13
15	-207	-471	-2333	106	-148	-227	20.11	20.11	1	19
16	683	-210	-1113	80	-57	-259	20.11	20.11	1	21
Massimi/minimi										
1							20.11			
1								20.11		
9										4.2

Muro : 213 - Nodi: [2078-2076-3076-3078], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=6.303$ [(4+5)-VI-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-4203	7344	-393	-389	229	33	20.11	20.11	(4+5)-VII-3	18
2	-1067	-1927	-2326	-679	-129	-9	20.11	20.11	1	10
3	1994	-1289	-1184	-1083	-166	-9	20.11	20.11	1	6.3
4	4197	46	-379	-1531	-144	-2	20.11	20.11	1	4.4
5	-6904	2994	-1475	-147	500	-16	20.11	20.11	(4+5)-V-4	13
6	-1313	-1799	-1832	-510	-112	-129	20.11	20.11	1	11
7	1839	-1356	-1545	-789	-143	-153	20.11	20.11	1	7.3
8	4187	-362	-641	-1023	-76	-144	20.11	20.11	1	5.7
9	-8680	590	-1865	-55	688	-40	20.11	20.11	(4+5)-V-4	9.7
10	-1224	-2082	-1987	-347	-108	-219	20.11	20.11	1	13
11	1511	-1291	-1807	-503	-118	-247	20.11	20.11	1	9.3
12	3451	-373	-899	-633	-35	-218	20.11	20.11	1	7.9
13	-10824	-5076	-703	-52	893	-43	20.11	20.11	(4+5)-V-4	8.1
14	-8245	-1306	-199	-355	25	132	20.11	20.11	(4+5)-VI-4	16
15	-5079	-240	-230	-454	-122	146	20.11	20.11	(4+5)-VI-4	13
16	-3846	-80	-137	-502	-54	114	20.11	20.11	(4+5)-VI-4	12
Massimi/minimi										
1							20.11			
1								20.11		
4										4.4

Muro : 214 - Nodi: [2060-3060-3059-2059], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=6.900$ [(4+5)-I-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-7926	-22737	-10737	5	-339	208	20.11	20.11	(4+5)-III-3	21
2	-1544	-3377	-2127	-667	-289	271	20.11	20.11	3	9.7
3	-2013	3906	-2709	-1152	-385	166	20.11	20.11	3	7.0
4	7116	15733	-10562	-1829	-829	-87	20.11	20.11	3	4.2

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
5	-3006	-114	-1714	49	417	-124	20.11	20.11	(4+5)-I-2	17
6	-1909	-5711	-7882	-333	-279	-69	20.11	20.11	3	23
7	8	-797	-8161	-663	-457	-152	20.11	20.11	3	11
8	5356	-2587	-6741	-810	-679	-248	20.11	20.11	3	7.9
9	-1201	30	-1465	58	518	-178	20.11	20.11	(4+5)-I-2	13
10	-607	-6834	-7266	-117	-328	-196	20.11	20.11	(4+5)-I-3	19
11	-121	-7930	-7375	-251	-510	-243	20.11	20.11	3	13
12	2000	-10960	-4329	-287	-558	-236	20.11	20.11	3	13
13	386	1158	-1053	63	638	-173	20.11	20.11	(4+5)-I-2	11
14	-12	-8202	-2953	-28	-355	-196	20.11	20.11	(4+5)-I-3	18
15	-362	-13599	-2987	-33	-508	-219	20.11	20.11	3	14
16	-911	-19832	-1930	-51	-470	-220	20.11	20.11	3	16
Massimi/minimi										
1							20.11			
1								20.11		
4										4.2

Muro : 215 - Nodi: [2058-2059-3059-3058], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45, $\zeta_e=10.987$ [(4+5)-III-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-269	-2731	-2203	182	-753	471	20.11	20.11	(4+5)-III-1	7.6
2	6073	2298	-1577	418	-175	341	20.11	20.11	3	11
3	3705	2286	-972	374	-31	246	20.11	20.11	3	14
4	2334	1425	-1019	385	20	173	20.11	20.11	3	16
5	-2015	-4591	-6730	-463	-1471	555	20.11	20.11	3	4.7
6	1448	-4620	-5145	-506	-636	414	20.11	20.11	3	9.0
7	1862	-2539	-2658	-437	-227	277	20.11	20.11	3	12
8	843	56	-630	-406	-29	224	20.11	20.11	3	14
9	-451	-1848	-4447	-439	-1678	178	20.11	20.11	3	4.9
10	-127	-2348	-5607	-535	-915	228	20.11	20.11	3	8.1
11	-2063	-1241	-4720	-587	-347	211	20.11	20.11	3	12
12	-4398	-307	-1923	-595	-60	181	20.11	20.11	3	12
13	1783	9215	-3076	-338	-1942	-10	20.11	20.11	3	4.0
14	-859	5101	-2932	-85	-805	134	20.11	20.11	3	8.9
15	-4861	2095	-2225	22	-246	173	20.11	20.11	3	21
16	-12437	-738	-965	159	4	130	20.11	20.11	(4+5)-I-3	36
Massimi/minimi										
1							20.11			
1								20.11		
13										4.0

Muro : 216 - Nodi: [2070-2058-3058-3070], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45, $\zeta_e=10.440$ [(4+5)-III-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	15889	-6942	2379	587	3513	-670	20.11	20.11	1	2.3
2	5316	1121	1500	-19	926	-135	20.11	20.11	1	8.3
3	3662	1256	547	-218	191	92	20.11	20.11	1	28
4	2980	109	7	-213	-3	93	20.11	20.11	1	28
5	3175	-7285	-5456	458	2974	-257	20.11	20.11	1	3.0
6	5842	-5126	-1605	642	1459	-191	20.11	20.11	1	5.8
7	3952	-2010	-262	723	466	44	20.11	20.11	1	11
8	3427	-209	123	695	64	83	20.11	20.11	1	11
9	602	-3967	-5955	489	2997	242	20.11	20.11	1	2.9
10	2155	-3834	-4355	741	1523	389	20.11	20.11	1	4.9
11	2082	-1871	-2585	883	484	187	20.11	20.11	1	8.1
12	1038	-111	-661	916	57	97	20.11	20.11	3	8.7
13	3016	-5704	-5246	923	3514	828	20.11	20.11	1	2.2
14	-233	-871	-5138	532	1046	447	20.11	20.11	1	6.1
15	-1887	-2091	-3500	585	293	180	20.11	20.11	3	12

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
16	-2064	-1357	-2008	574	26	80	20.11	20.11	3	14
Massimi/minimi										
1							20.11			
1								20.11		
13										2.2

Muro : 217 - Nodi: [2070-3070-3071-2071], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=8.072$ [(4+5)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	20680	32851	8041	2310	770	10	20.11	40.21	1	2.8
2	-9706	20226	-4941	1757	508	-109	20.11	40.21	1	5.4
3	-11126	11941	-11167	1101	231	-41	20.11	20.11	1	9.0
4	-7996	4944	-11332	609	214	-168	20.11	20.11	1	13
5	11729	9093	259	198	-371	35	20.11	20.11	1	19
6	5029	9869	3695	310	182	-188	20.11	20.11	1	17
7	-4172	8723	-257	386	396	-229	20.11	20.11	1	13
8	-11197	6837	-2427	478	574	-429	20.11	20.11	1	8.1
9	6337	3203	2073	-59	-623	4	20.11	20.11	1	14
10	2323	1288	1708	95	-24	94	20.11	20.11	(4+5)-V-1	46
11	2060	2963	2935	170	407	-198	20.11	20.11	1	14
12	-4674	2414	-1736	200	656	-407	20.11	20.11	1	8.1
13	1088	2823	1544	-47	-665	45	20.11	20.11	1	12
14	1091	4653	2729	42	-134	61	20.11	20.11	3	43
15	6581	5071	5615	224	115	64	20.11	20.11	3	28
16	15439	-7261	3977	1248	655	178	20.11	20.11	1	5.0
Massimi/minimi										
1							20.11			
1								40.21		
1										2.8

Muro : 218 - Nodi: [2042-2047-3047-3042], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=22.327$ [(4+5)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	2192	-2424	-911	-6	-110	65	20.11	20.11	3	53
2	8051	-1556	-1033	-21	-79	21	20.11	20.11	3	91
3	10893	-577	-622	-39	-41	-26	20.11	20.11	(4+5)-IV-4	>100
4	16127	-197	-214	-45	-9	-25	20.11	20.11	(4+5)-IV-4	100
5	2453	-3628	-1523	-9	-204	50	20.11	20.11	3	37
6	6131	-1770	-1242	-44	-118	-18	20.11	20.11	(4+5)-IV-4	67
7	10552	-871	-1019	-46	-52	-37	20.11	20.11	(4+5)-IV-4	93
8	15478	-154	-415	-49	-9	-34	20.11	20.11	(4+5)-IV-4	86
9	2826	-5275	-2686	-2	-319	24	20.11	20.11	3	28
10	6127	-2530	-2130	-42	-153	-26	20.11	20.11	(4+5)-IV-4	52
11	9993	-1207	-1787	-29	-58	-43	20.11	20.11	(4+5)-IV-4	90
12	14354	-174	-746	-23	-8	-39	20.11	20.11	(4+5)-IV-4	>100
13	3281	-6600	-4534	29	-425	-7	20.11	20.11	3	22
14	7891	-4181	-4786	15	-199	21	20.11	20.11	3	43
15	6443	-1225	-2273	57	-25	46	20.11	20.11	(4+5)-IV-1	79
16	11105	-239	-977	81	-2	-29	20.11	20.11	(4+5)-III-4	70
Massimi/minimi										
1							20.11			
1								20.11		
13										22

Muro : 219 - Nodi: [2043-2048-3048-3043], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=29.065$ [(4+5)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-409	-4345	475	-202	-345	213	20.11	20.11		2
2	451	-3085	-1002	-267	-91	107	20.11	20.11		2
3	2470	-1939	-1233	-170	-18	69	20.11	20.11		3
4	5058	-790	-596	-137	-2	49	20.11	20.11		3
5	352	-4129	-1083	-63	-196	89	20.11	20.11		3
6	1321	-2366	-1943	-118	-116	122	20.11	20.11		3
7	2275	-1092	-2163	-136	-42	94	20.11	20.11		3
8	3593	-73	-1066	-131	-6	63	20.11	20.11		3
9	1045	-2275	-2611	-22	-108	56	20.11	20.11		3
10	1804	-540	-3227	-45	-107	81	20.11	20.11		3
11	1460	-102	-2376	-68	-62	76	20.11	20.11		3
12	1820	-189	-990	-83	-15	53	20.11	20.11		3
13	2784	5797	-3883	-4	-68	48	20.11	20.11		3
14	232	3451	-2050	-7	-95	56	20.11	20.11		3
15	134	1328	-1169	-16	-70	49	20.11	20.11		3
16	316	104	-378	-24	-22	27	20.11	20.11		3
Massimi/minimi										>100
1							20.11			
1								20.11		
1										17

Muro : 220 - Nodi: [2053-3053-3047-2047], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=17.978$ [(4+5)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	10502	5424	12918	-723	229	59	20.11	20.11		3
2	-1461	5268	10485	-481	213	12	20.11	20.11		3
3	-5407	4443	8241	-498	149	57	20.11	20.11		3
4	-6871	3730	6511	-484	112	53	20.11	20.11		3
5	4105	3656	7653	-193	488	-23	20.11	20.11		3
6	1258	5562	9552	-252	345	-166	20.11	20.11		3
7	-2207	6852	8366	-235	211	-109	20.11	20.11		3
8	-3764	7465	6718	-220	96	-58	20.11	20.11		3
9	1047	4142	4693	63	756	-94	20.11	20.11		3
10	636	6429	5754	-26	543	-143	20.11	20.11		3
11	-493	8477	5978	-52	341	-62	20.11	20.11		3
12	-1470	10151	5276	-61	190	-21	20.11	20.11		3
13	-16	6326	1237	65	1111	-136	20.11	20.11		3
14	37	8210	1926	10	728	-99	20.11	20.11		3
15	-129	10816	2259	12	431	-41	20.11	20.11		3
16	-295	13462	2175	2	238	-9	20.11	20.11		3
Massimi/minimi										30
1							20.11			
1								20.11		
13										6.6

Muro : 221 - Nodi: [2053-2056-3056-3053], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=9.437$ [(4+5)-VI-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-3179	1838	-9235	-52	-470	277	20.11	20.11		3
2	-312	2993	-4720	185	-37	393	20.11	20.11		3
3	927	1116	-1673	404	107	406	20.11	20.11		1
4	1373	-11	-258	438	56	374	20.11	20.11		1
5	-7993	2314	-6858	-82	-251	352	20.11	20.11		3
6	-4568	1038	-3301	8	-2	640	20.11	20.11		3

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
7	-666	-215	-377	111	79	576	20.11	20.11	1	13
8	913	-178	110	164	37	473	20.11	20.11	1	14
9	-11158	2122	-2569	37	341	409	20.11	20.11	1	12
10	-5919	-175	42	56	97	587	20.11	20.11	1	13
11	-2508	-505	251	-33	3	621	20.11	20.11	3	14
12	404	-142	160	-54	-15	518	20.11	20.11	3	16
13	-18537	-41	3596	-99	470	387	20.11	20.11	1	10
14	-3682	-1840	725	-83	150	460	20.11	20.11	1	15
15	-494	-1136	-169	-215	-15	462	20.11	20.11	1	13
16	550	-663	-419	-361	-48	394	20.11	20.11	3	12
Massimi/minimi										
1							20.11			
1								20.11		
13										10

Muro : 222 - Nodi: [2056-2060-3060-3056], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=7.274$ [(4+5)-V-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-4110	620	3637	-340	-1346	738	20.11	20.11	3	4.3
2	-981	970	1425	-251	-19	299	20.11	20.11	1	16
3	786	424	472	-345	23	239	20.11	20.11	1	15
4	3629	238	-299	-427	5	177	20.11	20.11	1	14
5	-2434	-4886	2701	-500	-1289	487	20.11	20.11	3	5.4
6	164	-3019	1091	-600	-381	419	20.11	20.11	3	8.8
7	1550	-1029	-171	-613	-52	242	20.11	20.11	3	10
8	3415	-205	-269	-579	11	186	20.11	20.11	3	11
9	-450	-5633	650	-513	-1554	-23	20.11	20.11	(4+5)-V-3	6.1
10	1593	-3077	-1331	-635	-491	233	20.11	20.11	3	10
11	1789	-1541	-1294	-665	-107	275	20.11	20.11	3	9.3
12	2844	-284	-531	-612	-7	222	20.11	20.11	3	10
13	3976	-688	-3320	-766	-1946	-321	20.11	20.11	(4+5)-V-3	4.0
14	1593	-1931	-2270	-698	-376	171	20.11	20.11	3	10
15	1442	-1489	-1778	-566	-63	277	20.11	20.11	2	10
16	1611	-899	-1064	-475	-14	251	20.11	20.11	2	12
Massimi/minimi										
1							20.11			
1								20.11		
13										4.0

Verifica delle travi (Stati limite esercizio)

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Simbologia

Terreno Nome della stratigrafia per travi Winkler
L [cm] Lunghezza teorica elemento (distanza tra i nodi)
Ln [cm] Lunghezza netta elemento (tiene conto dei conci rigidi)
L2,L3 [cm] Lunghezze libere di inflessione
Sez. R: Sezione Rettangolare
By[cm]: Larghezza (asse locale y)
Bz[cm]: Larghezza (asse locale z)
Sez. T: Sezione a T (rovescia e non)
Ba[cm]: Larghezza base inferiore
Ha[cm]: Altezza inferiore
Bs[cm]: Larghezza superiore
Hs[cm]: Altezza superiore
Sez. L: Sezione ad L (rovescia e non)
Ba[cm]: Larghezza base inferiore
Ha[cm]: Altezza inferiore
Bs[cm]: Larghezza superiore
Hs[cm]: Altezza superiore
Sez. C: Sezione circolare
R[cm]: Raggio
Sez. G: Sezione generica

B[cm]	Larghezza
H[cm]	Altezza
X [cm]	Punto di verifica
σ_{ca} [kg/cmq]	Tensione ammissibile nel cls
σ_{fa} [kg/cmq]	Tensione ammissibile nell'acciaio
σ_{cta} [kg/cmq]	Tensione ammissibile a trazione (quando richiesto dalla verifica)
M- [kg*m]	Momento negativo massimo di calcolo
M+ [kg*m]	Momento positivo massimo di calcolo
M [kg*m]	Momento di calcolo (travi a flessione, pilastri circolari)
My [kg*m]	Momento calcolo per verifiche a pressoflessione
Mz [kg*m]	Momento calcolo per verifiche a pressoflessione (Sez. L, Pilastri)
N [kg]	Sforzo normale corrispondente ad My (e Mz per Sez. L, Pilastri)
Afsup [cmq]	Area di ferro superiore
Afinf [cmq]	Area di ferro inferiore
Afsin [cmq]	Area di ferro sinistra (Sez. L)
Afdes [cmq]	Area di ferro destra (Sez. L)
σ_{c-} [kg/cmq]	Tensione nel cls compresso per effetto di M-
σ_{cy} [kg/cmq]	Tensione nel cls compresso per effetto di (N,My) in caso di pressoflessione retta
σ_{cz} [kg/cmq]	Tensione nel cls compresso per effetto di (N,Mz) in caso di pressoflessione retta
σ_{c+} [kg/cmq]	Tensione nel cls compresso per effetto di M+
σ_{ct-} [kg/cmq]	Tensione nel cls teso per effetto di M-
σ_{ct+} [kg/cmq]	Tensione nel cls teso per effetto di M+
σ_{f-} [kg/cmq]	Tensione nell'acciaio per effetto di M-
σ_{f+} [kg/cmq]	Tensione nell'acciaio per effetto di M+
σ_{fy} [kg/cmq]	Tensione nel acciaio per effetto di (N,My) in caso di pressoflessione retta
σ_{fz} [kg/cmq]	Tensione nel acciaio per effetto di (N,Mz) in caso di pressoflessione retta
Cb-	Combinazione di carico generatore di M-
Cb+	Combinazione di carico generatore di M+
σ_c [kg/cmq]	Tensione nel cls per effetto di N My
σ_f [kg/cmq]	Tensione nell'acciaio per effetto di N My
Cb	Combinazione di carico generatore di N My
Act [mq]	Area di calcestruzzo teso
Aft [cmq]	Area di acciaio teso
pAft [cm]	Perimetro area di acciaio teso
$S_{r,max}$ [cm]	Distanza massima delle fessure
σ_{fmed} [kg/cmq]	Tensione media dell'acciaio
Wd [mm]	Apertura delle fessure
Wk [mm]	Apertura caratteristica delle fessure
Wamm_Freq [mm]	Apertura ammissibile delle fessure per combinazione Frequente
Wamm_Qp [mm]	Apertura ammissibile delle fessure per combinazione Quasi Permanente
Wamm_Rara [mm]	Apertura ammissibile delle fessure per combinazione Rara
Cs	Coefficiente di sicurezza definito come minimo di σ_{Amm}/σ tra acciaio e calcestruzzo oppure Wamm/Wk

Trave: 301 [3071,3072], Pilastrate [--,--] Sez. R: By=70.00 cm Bz=25.00 cm L=410.00 cm Ln=410.00 cm I2=410.00 cm
I3=410.00 cm Criterio: CLS TraviAlte
Verifica snellezza: $f_{cd}=212$ [kg/cmq] - **Verificato**

Cb	N	$f_{cd} \cdot A_c$	v	λ_{max}	λ_{lim}
	kg	kg			
8	1031	370387	0.003	56.811	473.857

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	2051	6.03	6.03	--	--	-60	1998	6	6	Si	1.8
41.00	--	904	6.03	6.03	--	--	-26	880	6	6	Si	4.1
205.00	1269	--	6.03	6.03	-37	1236	--	--	6	6	Si	2.9
369.00	--	425	6.03	6.03	--	--	-12	413	6	6	Si	8.7
410.00	--	1452	6.03	6.03	--	--	-42	1414	6	6	Si	2.5

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	2041	6.03	6.03	--	--	-60	1987	8	8	Si	1.8
41.00	--	895	6.03	6.03	--	--	-26	872	8	8	Si	4.1
205.00	1269	--	6.03	6.03	-37	1236	--	--	8	8	Si	2.9
369.00	--	433	6.03	6.03	--	--	-13	422	8	8	Si	8.5
410.00	--	1462	6.03	6.03	--	--	-43	1424	8	8	Si	2.5

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	2043	4.47E-02	12.06	30.16	27.07	1013	0.078	0.078	7 (Fr)	Si	3.8
0.00	2041	4.47E-02	12.06	30.16	27.07	1012	0.078	0.078	8 (Qp)	Si	2.6
41.00	895	4.47E-02	12.06	30.16	27.07	444	0.034	0.034	8 (Qp)	Si	5.8
41.00	898	4.47E-02	12.06	30.16	27.07	445	0.034	0.034	7 (Fr)	Si	8.7
205.00	-1269	4.47E-02	12.06	30.16	27.07	629	0.049	0.049	8 (Qp)	Si	4.1
205.00	-1269	4.47E-02	12.06	30.16	27.07	629	0.049	0.049	7 (Fr)	Si	6.2
369.00	433	4.47E-02	12.06	30.16	27.07	215	0.017	0.017	8 (Qp)	Si	12
369.00	430	4.47E-02	12.06	30.16	27.07	213	0.017	0.017	7 (Fr)	Si	18
410.00	1462	4.47E-02	12.06	30.16	27.07	725	0.056	0.056	8 (Qp)	Si	3.6
410.00	1459	4.47E-02	12.06	30.16	27.07	724	0.056	0.056	7 (Fr)	Si	5.4

Trave: 401 [4001,4002], Pilastrate [2001,2002] Sez. R: By=30.00 cm Bz=50.00 cm L=782.00 cm Ln=782.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	4388	8.04	6.03	--	--	-43	1400	6	6	Si	2.6
78.20	--	998	8.04	6.03	--	--	-10	318	6	6	Si	11
391.00	4154	--	6.03	6.03	-46	1748	--	--	6	6	Si	2.1
703.80	--	4148	14.07	6.03	--	--	-34	775	6	6	Si	4.6
782.00	--	8326	14.07	6.03	--	--	-68	1555	6	6	Si	2.3

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	4406	8.04	6.03	--	--	-44	1406	8	8	Si	2.6
78.20	--	1013	8.04	6.03	--	--	-10	323	8	8	Si	11
391.00	4153	--	6.03	6.03	-46	1748	--	--	8	8	Si	2.1
703.80	--	4136	14.07	6.03	--	--	-34	773	8	8	Si	4.7
782.00	--	8310	14.07	6.03	--	--	-68	1552	8	8	Si	2.3

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	4403	3.61E-02	8.04	20.11	29.20	1405	0.117	0.117	7 (Fr)	Si	2.6
0.00	4406	3.61E-02	8.04	20.11	29.20	1406	0.117	0.117	8 (Qp)	Si	1.7
78.20	1013	3.61E-02	8.04	20.11	29.20	323	0.027	0.027	8 (Qp)	Si	7.4
78.20	1010	3.61E-02	8.04	20.11	29.20	322	0.027	0.027	7 (Fr)	Si	11
391.00	-4153	3.76E-02	6.03	15.08	33.98	1748	0.170	0.170	8 (Qp)	Si	1.2
391.00	-4153	3.76E-02	6.03	15.08	33.98	1748	0.170	0.170	7 (Fr)	Si	1.8
703.80	4136	3.26E-02	14.07	35.19	23.29	773	0.051	0.051	8 (Qp)	Si	3.9

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
703.80	4137	3.26E-02	14.07	35.19	23.29	773	0.051	0.051	7 (Fr)	Si	5.8
782.00	8310	3.26E-02	14.07	35.19	23.29	1552	0.115	0.115	8 (Qp)	Si	1.7
782.00	8312	3.26E-02	14.07	35.19	23.29	1553	0.116	0.116	7 (Fr)	Si	2.6

Trave: 401 [4002,4003], Pilastrate [2002,2003] Sez. R: By=30.00 cm Bz=50.00 cm L=678.00 cm Ln=678.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	7579	14.07	6.03	--	--	-62	1416	6	6	Si	2.5
67.80	--	4299	14.07	6.03	--	--	-35	803	6	6	Si	4.5
339.00	2500	--	8.04	6.03	-26	1053	--	--	6	6	Si	3.4
610.20	--	813	8.04	6.03	--	--	-8	259	6	6	Si	14
678.00	--	3222	8.04	6.03	--	--	-32	1028	6	6	Si	3.5

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	7592	14.07	6.03	--	--	-62	1418	8	8	Si	2.5
67.80	--	4310	14.07	6.03	--	--	-35	805	8	8	Si	4.5
339.00	2500	--	8.04	6.03	-26	1053	--	--	8	8	Si	3.4
610.20	--	804	8.04	6.03	--	--	-8	256	8	8	Si	14
678.00	--	3210	8.04	6.03	--	--	-32	1024	8	8	Si	3.5

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	7582	3.26E-02	14.07	35.19	23.29	1416	0.100	0.100	7 (Fr)	Si	3.0
0.00	7592	3.26E-02	14.07	35.19	23.29	1418	0.101	0.101	8 (Qp)	Si	2.0
67.80	4310	3.26E-02	14.07	35.19	23.29	805	0.054	0.054	8 (Qp)	Si	3.7
67.80	4302	3.26E-02	14.07	35.19	23.29	804	0.053	0.053	7 (Fr)	Si	5.6
339.00	-2500	3.80E-02	6.03	15.08	34.12	1053	0.103	0.103	8 (Qp)	Si	1.9
339.00	-2501	3.80E-02	6.03	15.08	34.12	1053	0.103	0.103	7 (Fr)	Si	2.9
610.20	804	3.61E-02	8.04	20.11	29.20	256	0.021	0.021	8 (Qp)	Si	9.4
610.20	810	3.61E-02	8.04	20.11	29.20	258	0.022	0.022	7 (Fr)	Si	14
678.00	3210	3.61E-02	8.04	20.11	29.20	1024	0.085	0.085	8 (Qp)	Si	2.3
678.00	3218	3.61E-02	8.04	20.11	29.20	1027	0.086	0.086	7 (Fr)	Si	3.5

Trave: 402 [4003,4006], Pilastrate [2003,2006] Sez. R: By=30.00 cm Bz=50.00 cm L=465.00 cm Ln=465.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	4730	8.04	6.03	--	--	-47	1509	6	6	Si	2.4
46.50	--	1610	8.04	6.03	--	--	-16	514	6	6	Si	7.0
232.50	3532	--	6.03	6.03	-39	1487	--	--	6	6	Si	2.4
418.50	--	3216	8.04	6.03	--	--	-32	1026	6	6	Si	3.5
465.00	--	6761	8.04	6.03	--	--	-67	2157	6	6	Si	1.7

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	4486	8.04	6.03	--	--	-44	1431	8	8	Si	2.5
46.50	--	1552	8.04	6.03	--	--	-15	495	8	8	Si	7.3
232.50	3280	--	6.03	6.03	-36	1380	--	--	8	8	Si	2.6
418.50	--	3068	8.04	6.03	--	--	-30	979	8	8	Si	3.7
465.00	--	6401	8.04	6.03	--	--	-63	2042	8	8	Si	1.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	4486	3.61E-02	8.04	20.11	29.20	1431	0.119	0.119	7 (Fr)	Si	2.5
0.00	4486	3.61E-02	8.04	20.11	29.20	1431	0.119	0.119	8 (Qp)	Si	1.7
46.50	1552	3.61E-02	8.04	20.11	29.20	495	0.041	0.041	8 (Qp)	Si	4.8
46.50	1552	3.61E-02	8.04	20.11	29.20	495	0.041	0.041	7 (Fr)	Si	7.3
232.50	-3280	3.76E-02	6.03	15.08	33.98	1380	0.134	0.134	8 (Qp)	Si	1.5

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
232.50	-3280	3.76E-02	6.03	15.08	33.98	1381	0.134	0.134	7 (Fr)	Si	2.2
418.50	3068	3.61E-02	8.04	20.11	29.20	979	0.082	0.082	8 (Qp)	Si	2.4
418.50	3067	3.61E-02	8.04	20.11	29.20	979	0.082	0.082	7 (Fr)	Si	3.7
465.00	6401	3.61E-02	8.04	20.11	29.20	2042	0.172	0.172	8 (Qp)	Si	1.2
465.00	6401	3.61E-02	8.04	20.11	29.20	2042	0.172	0.172	7 (Fr)	Si	1.7

Trave: 402 [4006,4009], Pilastrate [2006,2009] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	4541	6.03	6.03	--	--	-50	1911	6	6	Si	1.9
40.00	--	2239	6.03	6.03	--	--	-25	942	6	6	Si	3.8
200.00	1470	--	6.03	6.03	-16	619	--	--	6	6	Si	5.8
360.00	--	3620	10.05	6.03	--	--	-33	932	6	6	Si	3.9
400.00	--	6267	10.05	6.03	--	--	-57	1614	6	6	Si	2.2

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	4236	6.03	6.03	--	--	-47	1783	8	8	Si	2.0
40.00	--	2079	6.03	6.03	--	--	-23	875	8	8	Si	4.1
200.00	1380	--	6.03	6.03	-15	581	--	--	8	8	Si	6.2
360.00	--	3434	10.05	6.03	--	--	-31	884	8	8	Si	4.1
400.00	--	5930	10.05	6.03	--	--	-54	1527	8	8	Si	2.4

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	4235	3.76E-02	6.03	15.08	33.98	1783	0.173	0.173	7 (Fr)	Si	1.7
0.00	4236	3.76E-02	6.03	15.08	33.98	1783	0.173	0.173	8 (Qp)	Si	1.2
40.00	2079	3.76E-02	6.03	15.08	33.98	875	0.085	0.085	8 (Qp)	Si	2.4
40.00	2078	3.76E-02	6.03	15.08	33.98	875	0.085	0.085	7 (Fr)	Si	3.5
200.00	-1380	3.76E-02	6.03	15.08	33.98	581	0.056	0.056	8 (Qp)	Si	3.5
200.00	-1379	3.76E-02	6.03	15.08	33.98	581	0.056	0.056	7 (Fr)	Si	5.3
360.00	3434	3.47E-02	10.05	25.13	26.40	884	0.067	0.067	8 (Qp)	Si	3.0
360.00	3436	3.47E-02	10.05	25.13	26.40	885	0.067	0.067	7 (Fr)	Si	4.5
400.00	5930	3.47E-02	10.05	25.13	26.40	1527	0.115	0.115	8 (Qp)	Si	1.7
400.00	5932	3.47E-02	10.05	25.13	26.40	1528	0.115	0.115	7 (Fr)	Si	2.6

Trave: 402 [4009,4012], Pilastrate [2009,2012] Sez. R: By=30.00 cm Bz=50.00 cm L=500.00 cm Ln=525.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	6602	12.06	6.03	--	--	-57	1428	6	6	Si	2.5
52.50	--	2569	6.03	6.03	--	--	-28	1081	6	6	Si	3.3
262.50	4088	--	6.03	6.03	-45	1720	--	--	6	6	Si	2.1
472.50	--	4413	8.04	6.03	--	--	-44	1408	6	6	Si	2.6
525.00	--	8842	10.05	6.03	--	--	-81	2277	6	6	Si	1.6

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	6199	12.06	6.03	--	--	-53	1341	8	8	Si	2.7
52.50	--	2411	6.03	6.03	--	--	-26	1015	8	8	Si	3.5
262.50	3832	--	6.03	6.03	-42	1613	--	--	8	8	Si	2.2
472.50	--	4176	8.04	6.03	--	--	-41	1332	8	8	Si	2.7
525.00	--	8346	10.05	6.03	--	--	-76	2150	8	8	Si	1.7

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	6203	3.36E-02	12.06	30.16	24.57	1342	0.094	0.094	7 (Fr)	Si	3.2
0.00	6199	3.36E-02	12.06	30.16	24.57	1341	0.094	0.094	8 (Qp)	Si	2.1
52.50	2411	3.76E-02	6.03	15.08	33.98	1015	0.099	0.099	8 (Qp)	Si	2.0

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
52.50	2416	3.76E-02	6.03	15.08	33.98	1017	0.099	0.099	7 (Fr)	Si	3.0
262.50	-3832	3.76E-02	6.03	15.08	33.98	1613	0.157	0.157	8 (Qp)	Si	1.3
262.50	-3829	3.76E-02	6.03	15.08	33.98	1611	0.156	0.156	7 (Fr)	Si	1.9
472.50	4176	3.61E-02	8.04	20.11	29.20	1332	0.111	0.111	8 (Qp)	Si	1.8
472.50	4178	3.61E-02	8.04	20.11	29.20	1333	0.111	0.111	7 (Fr)	Si	2.7
525.00	8346	3.47E-02	10.05	25.13	26.40	2150	0.187	0.187	8 (Qp)	Si	1.1
525.00	8348	3.47E-02	10.05	25.13	26.40	2150	0.187	0.187	7 (Fr)	Si	1.6

Trave: 402 [4012,4015], Pilastrate [2012,2015] Sez. R: By=30.00 cm Bz=50.00 cm L=460.00 cm Ln=485.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	6898	8.04	8.04	--	--	-66	2200	6	6	Si	1.6
48.50	--	3294	8.04	8.04	--	--	-31	1050	6	6	Si	3.4
242.50	3131	--	6.03	6.03	-34	1318	--	--	6	6	Si	2.7
436.50	--	3230	10.05	6.03	--	--	-30	832	6	6	Si	4.3
485.00	--	6754	10.05	6.03	--	--	-62	1740	6	6	Si	2.1

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	6517	8.04	8.04	--	--	-62	2078	8	8	Si	1.7
48.50	--	3096	8.04	8.04	--	--	-29	987	8	8	Si	3.6
242.50	2986	--	6.03	6.03	-33	1257	--	--	8	8	Si	2.9
436.50	--	3093	10.05	6.03	--	--	-28	797	8	8	Si	4.5
485.00	--	6455	10.05	6.03	--	--	-59	1663	8	8	Si	2.2

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	6540	3.64E-02	8.04	20.11	29.32	2086	0.178	0.178	7 (Fr)	Si	1.7
0.00	6517	3.64E-02	8.04	20.11	29.32	2078	0.177	0.177	8 (Qp)	Si	1.1
48.50	3096	3.64E-02	8.04	20.11	29.32	987	0.083	0.083	8 (Qp)	Si	2.4
48.50	3115	3.64E-02	8.04	20.11	29.32	993	0.083	0.083	7 (Fr)	Si	3.6
242.50	-2986	3.76E-02	6.03	15.08	33.98	1257	0.122	0.122	8 (Qp)	Si	1.6
242.50	-2985	3.76E-02	6.03	15.08	33.98	1256	0.122	0.122	7 (Fr)	Si	2.5
436.50	3093	3.47E-02	10.05	25.13	26.40	797	0.060	0.060	8 (Qp)	Si	3.3
436.50	3078	3.47E-02	10.05	25.13	26.40	793	0.060	0.060	7 (Fr)	Si	5.0
485.00	6455	3.47E-02	10.05	25.13	26.40	1663	0.125	0.125	8 (Qp)	Si	1.6
485.00	6435	3.47E-02	10.05	25.13	26.40	1658	0.125	0.125	7 (Fr)	Si	2.4

Trave: 402 [4015,4018], Pilastrate [2015,2018] Sez. R: By=30.00 cm Bz=50.00 cm L=435.00 cm Ln=435.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	6222	10.05	6.03	--	--	-57	1603	6	6	Si	2.2
43.50	--	3136	10.05	6.03	--	--	-29	808	6	6	Si	4.5
217.50	2778	--	6.03	6.03	-31	1169	--	--	6	6	Si	3.1
391.50	--	1592	8.04	6.03	--	--	-16	508	6	6	Si	7.1
435.00	--	4269	8.04	6.03	--	--	-42	1362	6	6	Si	2.6

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	5924	10.05	6.03	--	--	-54	1526	8	8	Si	2.4
43.50	--	2996	10.05	6.03	--	--	-27	772	8	8	Si	4.7
217.50	2601	--	6.03	6.03	-29	1095	--	--	8	8	Si	3.3
391.50	--	1585	8.04	6.03	--	--	-16	506	8	8	Si	7.1
435.00	--	4139	8.04	6.03	--	--	-41	1320	8	8	Si	2.7

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	5940	3.47E-02	10.05	25.13	26.40	1530	0.115	0.115	7 (Fr)	Si	2.6

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale- Edificio Grigliatura fine**

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X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
0.00	5924	3.47E-02	10.05	25.13	26.40	1526	0.115	0.115	8 (Qp)	Si	1.7
43.50	2996	3.47E-02	10.05	25.13	26.40	772	0.058	0.058	8 (Qp)	Si	3.4
43.50	3009	3.47E-02	10.05	25.13	26.40	775	0.058	0.058	7 (Fr)	Si	5.1
217.50	-2601	3.76E-02	6.03	15.08	33.98	1095	0.106	0.106	8 (Qp)	Si	1.9
217.50	-2604	3.76E-02	6.03	15.08	33.98	1096	0.106	0.106	7 (Fr)	Si	2.8
391.50	1585	3.61E-02	8.04	20.11	29.20	506	0.042	0.042	8 (Qp)	Si	4.7
391.50	1567	3.61E-02	8.04	20.11	29.20	500	0.042	0.042	7 (Fr)	Si	7.2
435.00	4139	3.61E-02	8.04	20.11	29.20	1320	0.110	0.110	8 (Qp)	Si	1.8
435.00	4118	3.61E-02	8.04	20.11	29.20	1314	0.110	0.110	7 (Fr)	Si	2.7

Trave: 403 [4011,4010], Pilastrate [2011,2010] Sez. R: By=50.00 cm Bz=30.00 cm L=797.00 cm Ln=767.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	1373	6.03	6.03	--	--	-32	1077	6	6	Si	3.3
76.70	--	534	6.03	6.03	--	--	-13	419	6	6	Si	8.6
383.50	617	--	6.03	6.03	-14	484	--	--	6	6	Si	7.4
690.30	--	1762	10.05	6.03	--	--	-34	853	6	6	Si	4.2
767.00	--	2909	10.05	6.03	--	--	-56	1407	6	6	Si	2.6

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	1361	6.03	6.03	--	--	-32	1067	8	8	Si	3.4
76.70	--	524	6.03	6.03	--	--	-12	411	8	8	Si	8.8
383.50	615	--	6.03	6.03	-14	482	--	--	8	8	Si	7.5
690.30	--	1776	10.05	6.03	--	--	-34	859	8	8	Si	4.2
767.00	--	2925	10.05	6.03	--	--	-56	1415	8	8	Si	2.5

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	1363	3.76E-02	6.03	15.08	33.98	1069	0.104	0.104	7 (Fr)	Si	2.9
0.00	1361	3.76E-02	6.03	15.08	33.98	1067	0.104	0.104	8 (Qp)	Si	1.9
76.70	524	3.76E-02	6.03	15.08	33.98	411	0.040	0.040	8 (Qp)	Si	5.0
76.70	526	3.76E-02	6.03	15.08	33.98	413	0.040	0.040	7 (Fr)	Si	7.5
383.50	-615	3.76E-02	6.03	15.08	33.98	482	0.047	0.047	8 (Qp)	Si	4.3
383.50	-615	3.76E-02	6.03	15.08	33.98	483	0.047	0.047	7 (Fr)	Si	6.4
690.30	1776	3.51E-02	10.05	25.13	26.50	859	0.065	0.065	8 (Qp)	Si	3.1
690.30	1773	3.51E-02	10.05	25.13	26.50	858	0.065	0.065	7 (Fr)	Si	4.6
767.00	2925	3.51E-02	10.05	25.13	26.50	1415	0.107	0.107	8 (Qp)	Si	1.9
767.00	2921	3.51E-02	10.05	25.13	26.50	1413	0.107	0.107	7 (Fr)	Si	2.8

Trave: 403 [4012,4011], Pilastrate [2012,2011] Sez. R: By=50.00 cm Bz=30.00 cm L=663.00 cm Ln=678.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	2667	8.04	6.03	--	--	-56	1593	6	6	Si	2.3
67.80	--	1736	8.04	6.03	--	--	-36	1037	6	6	Si	3.5
339.00	261	--	6.03	6.03	-6	205	--	--	6	6	Si	18
610.20	--	500	6.03	6.03	--	--	-12	392	6	6	Si	9.2
678.00	--	1121	6.03	6.03	--	--	-26	879	6	6	Si	4.1

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	2687	8.04	6.03	--	--	-56	1605	8	8	Si	2.2
67.80	--	1752	8.04	6.03	--	--	-37	1047	8	8	Si	3.4
339.00	264	--	6.03	6.03	-6	207	--	--	8	8	Si	17
610.20	--	478	6.03	6.03	--	--	-11	375	8	8	Si	9.6
678.00	--	1095	6.03	6.03	--	--	-26	858	8	8	Si	4.2

Verifica aperture fessure:Wamm_Freq[mm]=0.300 Wamm_Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	2682	3.63E-02	8.04	20.11	29.27	1602	0.134	0.134	7 (Fr)	Si	2.2
0.00	2687	3.63E-02	8.04	20.11	29.27	1605	0.134	0.134	8 (Qp)	Si	1.5
67.80	1752	3.63E-02	8.04	20.11	29.27	1047	0.088	0.088	8 (Qp)	Si	2.3
67.80	1748	3.63E-02	8.04	20.11	29.27	1044	0.087	0.087	7 (Fr)	Si	3.4
339.00	-264	3.76E-02	6.03	15.08	33.98	207	0.020	0.020	8 (Qp)	Si	10.0
339.00	-263	3.76E-02	6.03	15.08	33.98	206	0.020	0.020	7 (Fr)	Si	15
610.20	478	3.76E-02	6.03	15.08	33.98	375	0.036	0.036	8 (Qp)	Si	5.5
610.20	484	3.76E-02	6.03	15.08	33.98	380	0.037	0.037	7 (Fr)	Si	8.1
678.00	1095	3.76E-02	6.03	15.08	33.98	858	0.083	0.083	8 (Qp)	Si	2.4
678.00	1102	3.76E-02	6.03	15.08	33.98	864	0.084	0.084	7 (Fr)	Si	3.6

Trave: 404 [4004,4001], Pilastrate [2004,2001] Sez. R: By=30.00 cm Bz=50.00 cm L=465.00 cm Ln=465.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	7094	10.18	7.63	--	--	-63	1804	6	6	Si	2.0
46.50	--	3321	10.18	7.63	--	--	-29	844	6	6	Si	4.3
232.50	3741	--	7.63	7.63	-37	1254	--	--	6	6	Si	2.9
418.50	--	2048	10.18	7.63	--	--	-18	521	6	6	Si	6.9
465.00	--	5477	10.18	7.63	--	--	-48	1393	6	6	Si	2.6

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	6746	10.18	7.63	--	--	-60	1715	8	8	Si	2.1
46.50	--	3173	10.18	7.63	--	--	-28	807	8	8	Si	4.5
232.50	3502	--	7.63	7.63	-34	1174	--	--	8	8	Si	3.1
418.50	--	2011	10.18	7.63	--	--	-18	511	8	8	Si	7.0
465.00	--	5269	10.18	7.63	--	--	-46	1340	8	8	Si	2.7

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	6751	3.50E-02	10.18	22.62	27.51	1717	0.138	0.138	7 (Fr)	Si	2.2
0.00	6746	3.50E-02	10.18	22.62	27.51	1715	0.138	0.138	8 (Qp)	Si	1.4
46.50	3173	3.50E-02	10.18	22.62	27.51	807	0.063	0.063	8 (Qp)	Si	3.2
46.50	3177	3.50E-02	10.18	22.62	27.51	808	0.064	0.064	7 (Fr)	Si	4.7
232.50	-3502	3.67E-02	7.63	16.96	31.69	1174	0.106	0.106	8 (Qp)	Si	1.9
232.50	-3503	3.67E-02	7.63	16.96	31.69	1175	0.106	0.106	7 (Fr)	Si	2.8
418.50	2011	3.50E-02	10.18	22.62	27.51	511	0.040	0.040	8 (Qp)	Si	5.0
418.50	2003	3.50E-02	10.18	22.62	27.51	509	0.040	0.040	7 (Fr)	Si	7.5
465.00	5269	3.50E-02	10.18	22.62	27.51	1340	0.105	0.105	8 (Qp)	Si	1.9
465.00	5260	3.50E-02	10.18	22.62	27.51	1337	0.105	0.105	7 (Fr)	Si	2.9

Trave: 404 [4007,4004], Pilastrate [2007,2004] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	6571	12.72	15.27	--	--	-47	1343	6	6	Si	2.7
40.00	--	3746	12.72	7.63	--	--	-31	769	6	6	Si	4.7
200.00	1613	--	7.63	7.63	-16	541	--	--	6	6	Si	6.7
360.00	--	2537	7.63	7.63	--	--	-25	851	6	6	Si	4.2
400.00	--	5060	7.63	7.63	--	--	-49	1697	6	6	Si	2.1

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	6243	12.72	15.27	--	--	-45	1276	8	8	Si	2.8
40.00	--	3562	12.72	7.63	--	--	-29	731	8	8	Si	4.9
200.00	1523	--	7.63	7.63	-15	511	--	--	8	8	Si	7.0
360.00	--	2410	7.63	7.63	--	--	-24	808	8	8	Si	4.5
400.00	--	4802	7.63	7.63	--	--	-47	1610	8	8	Si	2.2

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	S _{r,max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	6251	3.49E-02	12.72	28.27	25.39	1277	0.093	0.093	7 (Fr)	Si	3.2
0.00	6243	3.49E-02	12.72	28.27	25.39	1276	0.093	0.093	8 (Qp)	Si	2.2
40.00	3562	3.36E-02	12.72	28.27	25.07	731	0.052	0.052	8 (Qp)	Si	3.8
40.00	3569	3.36E-02	12.72	28.27	25.07	733	0.052	0.052	7 (Fr)	Si	5.7
200.00	-1523	3.67E-02	7.63	16.96	31.69	511	0.046	0.046	8 (Qp)	Si	4.3
200.00	-1524	3.67E-02	7.63	16.96	31.69	511	0.046	0.046	7 (Fr)	Si	6.5
360.00	2410	3.67E-02	7.63	16.96	31.69	808	0.073	0.073	8 (Qp)	Si	2.7
360.00	2400	3.67E-02	7.63	16.96	31.69	805	0.073	0.073	7 (Fr)	Si	4.1
400.00	4802	3.67E-02	7.63	16.96	31.69	1610	0.146	0.146	8 (Qp)	Si	1.4
400.00	4790	3.67E-02	7.63	16.96	31.69	1606	0.145	0.145	7 (Fr)	Si	2.1

Trave: 404 [4010,4007], Pilastrate [2010,2007] Sez. R: By=30.00 cm Bz=50.00 cm L=500.00 cm Ln=525.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σca[kg/cmq]=224 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	9378	10.18	7.63	--	--	-83	2385	6	6	Si	1.5
52.50	--	4626	10.18	7.63	--	--	-41	1176	6	6	Si	3.1
262.50	4436	--	7.63	7.63	-43	1488	--	--	6	6	Si	2.4
472.50	--	2881	15.27	7.63	--	--	-22	497	6	6	Si	7.2
525.00	--	7270	15.27	7.63	--	--	-56	1254	6	6	Si	2.9

Combinazione QP: σca[kg/cmq]=168 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	8848	10.18	7.63	--	--	-78	2250	8	8	Si	1.6
52.50	--	4349	10.18	7.63	--	--	-38	1106	8	8	Si	3.3
262.50	4205	--	7.63	7.63	-41	1410	--	--	8	8	Si	2.6
472.50	--	2775	15.27	7.63	--	--	-21	479	8	8	Si	7.5
525.00	--	6947	15.27	7.63	--	--	-54	1198	8	8	Si	3.0

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	S _{r,max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	8867	3.50E-02	10.18	22.62	27.51	2255	0.209	0.209	7 (Fr)	Si	1.4
52.50	4349	3.50E-02	10.18	22.62	27.51	1106	0.087	0.087	8 (Qp)	Si	2.3
52.50	4365	3.50E-02	10.18	22.62	27.51	1110	0.087	0.087	7 (Fr)	Si	3.4
262.50	-4205	3.67E-02	7.63	16.96	31.69	1410	0.128	0.128	8 (Qp)	Si	1.6
262.50	-4203	3.67E-02	7.63	16.96	31.69	1409	0.128	0.128	7 (Fr)	Si	2.4
472.50	2775	3.23E-02	15.27	33.93	23.48	479	0.032	0.032	8 (Qp)	Si	6.2
472.50	2764	3.23E-02	15.27	33.93	23.48	477	0.032	0.032	7 (Fr)	Si	9.4
525.00	6947	3.23E-02	15.27	33.93	23.48	1198	0.080	0.080	8 (Qp)	Si	2.5
525.00	6933	3.23E-02	15.27	33.93	23.48	1196	0.080	0.080	7 (Fr)	Si	3.7

Trave: 404 [4013,4010], Pilastrate [2013,2010] Sez. R: By=30.00 cm Bz=50.00 cm L=460.00 cm Ln=485.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σca[kg/cmq]=224 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	7455	12.72	7.63	--	--	-61	1531	6	6	Si	2.4
48.50	--	3577	12.72	7.63	--	--	-29	735	6	6	Si	4.9
242.50	3488	--	7.63	7.63	-34	1170	--	--	6	6	Si	3.1
436.50	--	3425	10.18	10.18	--	--	-29	870	6	6	Si	4.1
485.00	--	7338	10.18	10.18	--	--	-62	1863	6	6	Si	1.9

Combinazione QP: σca[kg/cmq]=168 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	7055	12.72	7.63	--	--	-58	1448	8	8	Si	2.5
48.50	--	3377	12.72	7.63	--	--	-28	693	8	8	Si	5.2
242.50	3318	--	7.63	7.63	-32	1113	--	--	8	8	Si	3.2
436.50	--	3246	10.18	10.18	--	--	-27	824	8	8	Si	4.4
485.00	--	6958	10.18	10.18	--	--	-59	1767	8	8	Si	2.0

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	S _{r,max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	7055	3.36E-02	12.72	28.27	25.07	1449	0.107	0.107	7 (Fr)	Si	2.8
0.00	7055	3.36E-02	12.72	28.27	25.07	1448	0.107	0.107	8 (Qp)	Si	1.9
48.50	3377	3.36E-02	12.72	28.27	25.07	693	0.050	0.050	8 (Qp)	Si	4.0
48.50	3378	3.36E-02	12.72	28.27	25.07	694	0.050	0.050	7 (Fr)	Si	6.0
242.50	-3318	3.67E-02	7.63	16.96	31.69	1113	0.101	0.101	8 (Qp)	Si	2.0
242.50	-3313	3.67E-02	7.63	16.96	31.69	1111	0.101	0.101	7 (Fr)	Si	3.0
436.50	3246	3.54E-02	10.18	22.62	27.65	824	0.065	0.065	8 (Qp)	Si	3.1
436.50	3253	3.54E-02	10.18	22.62	27.65	826	0.065	0.065	7 (Fr)	Si	4.6
485.00	6958	3.54E-02	10.18	22.62	27.65	1767	0.145	0.145	8 (Qp)	Si	1.4
485.00	6966	3.54E-02	10.18	22.62	27.65	1769	0.145	0.145	7 (Fr)	Si	2.1

Trave: 404 [4016,4013], Pilastrate [2016,2013] Sez. R: By=30.00 cm Bz=50.00 cm L=435.00 cm Ln=435.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σca[kg/cmq]=224 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	4961	10.18	7.63	--	--	-44	1261	6	6	Si	2.9
43.50	--	1990	10.18	7.63	--	--	-18	506	6	6	Si	7.1
217.50	2969	--	7.63	7.63	-29	996	--	--	6	6	Si	3.6
391.50	--	3317	12.72	7.63	--	--	-27	681	6	6	Si	5.3
435.00	--	6645	12.72	7.63	--	--	-54	1364	6	6	Si	2.6

Combinazione QP: σca[kg/cmq]=168 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	4806	10.18	7.63	--	--	-42	1222	8	8	Si	2.9
43.50	--	1977	10.18	7.63	--	--	-17	503	8	8	Si	7.2
217.50	2771	--	7.63	7.63	-27	929	--	--	8	8	Si	3.9
391.50	--	3146	12.72	7.63	--	--	-26	646	8	8	Si	5.6
435.00	--	6292	12.72	7.63	--	--	-52	1292	8	8	Si	2.8

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	S _{r,max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	4787	3.50E-02	10.18	22.62	27.51	1217	0.096	0.096	7 (Fr)	Si	3.1
0.00	4806	3.50E-02	10.18	22.62	27.51	1222	0.096	0.096	8 (Qp)	Si	2.1
43.50	1977	3.50E-02	10.18	22.62	27.51	503	0.040	0.040	8 (Qp)	Si	5.1
43.50	1961	3.50E-02	10.18	22.62	27.51	499	0.039	0.039	7 (Fr)	Si	7.7
217.50	-2771	3.67E-02	7.63	16.96	31.69	929	0.084	0.084	8 (Qp)	Si	2.4
217.50	-2772	3.67E-02	7.63	16.96	31.69	929	0.084	0.084	7 (Fr)	Si	3.6
391.50	3146	3.36E-02	12.72	28.27	25.07	646	0.046	0.046	8 (Qp)	Si	4.3
391.50	3161	3.36E-02	12.72	28.27	25.07	649	0.046	0.046	7 (Fr)	Si	6.5
435.00	6292	3.36E-02	12.72	28.27	25.07	1292	0.093	0.093	8 (Qp)	Si	2.2
435.00	6310	3.36E-02	12.72	28.27	25.07	1296	0.093	0.093	7 (Fr)	Si	3.2

Trave: 405 [4005,4004], Pilastrate [2005,2004] Sez. R: By=50.00 cm Bz=30.00 cm L=797.00 cm Ln=767.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σca[kg/cmq]=224 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	1578	12.06	6.03	--	--	-29	643	6	6	Si	5.6
76.70	--	670	6.03	6.03	--	--	-16	526	6	6	Si	6.8
383.50	756	--	6.03	6.03	-18	593	--	--	6	6	Si	6.1
690.30	--	1347	6.03	6.03	--	--	-32	1057	6	6	Si	3.4
767.00	--	2425	8.04	6.03	--	--	-51	1449	6	6	Si	2.5

Combinazione QP: σca[kg/cmq]=168 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	1570	12.06	6.03	--	--	-28	639	8	8	Si	5.6
76.70	--	664	6.03	6.03	--	--	-16	521	8	8	Si	6.9
383.50	755	--	6.03	6.03	-18	592	--	--	8	8	Si	6.1
690.30	--	1356	6.03	6.03	--	--	-32	1064	8	8	Si	3.4
767.00	--	2436	8.04	6.03	--	--	-51	1455	8	8	Si	2.5

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	S _{r,max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	1571	3.41E-02	12.06	30.16	24.68	640	0.045	0.045	7 (Fr)	Si	6.7
0.00	1570	3.41E-02	12.06	30.16	24.68	639	0.045	0.045	8 (Qp)	Si	4.4
76.70	664	3.76E-02	6.03	15.08	33.98	521	0.051	0.051	8 (Qp)	Si	4.0
76.70	665	3.76E-02	6.03	15.08	33.98	521	0.051	0.051	7 (Fr)	Si	5.9
383.50	-755	3.76E-02	6.03	15.08	33.98	592	0.057	0.057	8 (Qp)	Si	3.5
383.50	-755	3.76E-02	6.03	15.08	33.98	592	0.057	0.057	7 (Fr)	Si	5.2
690.30	1356	3.76E-02	6.03	15.08	33.98	1064	0.103	0.103	8 (Qp)	Si	1.9
690.30	1355	3.76E-02	6.03	15.08	33.98	1063	0.103	0.103	7 (Fr)	Si	2.9
767.00	2436	3.63E-02	8.04	20.11	29.27	1455	0.122	0.122	8 (Qp)	Si	1.6
767.00	2434	3.63E-02	8.04	20.11	29.27	1454	0.122	0.122	7 (Fr)	Si	2.5

Trave: 405 [4005,4006], Pilastrate [2005,2006] Sez. R: By=50.00 cm Bz=30.00 cm L=663.00 cm Ln=678.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σca[kg/cmq]=224 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	1530	12.06	6.03	--	--	-28	623	6	6	Si	5.8
67.80	--	812	6.03	6.03	--	--	-19	637	6	6	Si	5.7
339.00	336	--	6.03	6.03	-8	264	--	--	6	6	Si	14
610.20	--	1274	6.03	6.03	--	--	-30	999	6	6	Si	3.6
678.00	--	2107	8.04	6.03	--	--	-44	1259	6	6	Si	2.9

Combinazione QP: σca[kg/cmq]=168 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	1529	12.06	6.03	--	--	-28	623	8	8	Si	5.8
67.80	--	811	6.03	6.03	--	--	-19	636	8	8	Si	5.7
339.00	337	--	6.03	6.03	-8	264	--	--	8	8	Si	14
610.20	--	1272	6.03	6.03	--	--	-30	998	8	8	Si	3.6
678.00	--	2106	8.04	6.03	--	--	-44	1258	8	8	Si	2.9

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	S _{r,max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	1526	3.41E-02	12.06	30.16	24.68	621	0.044	0.044	7 (Fr)	Si	6.8
0.00	1529	3.41E-02	12.06	30.16	24.68	623	0.044	0.044	8 (Qp)	Si	4.6
67.80	811	3.76E-02	6.03	15.08	33.98	636	0.062	0.062	8 (Qp)	Si	3.2
67.80	809	3.76E-02	6.03	15.08	33.98	634	0.062	0.062	7 (Fr)	Si	4.9
339.00	-337	3.76E-02	6.03	15.08	33.98	264	0.026	0.026	8 (Qp)	Si	7.8
339.00	-337	3.76E-02	6.03	15.08	33.98	264	0.026	0.026	7 (Fr)	Si	12
610.20	1272	3.76E-02	6.03	15.08	33.98	998	0.097	0.097	8 (Qp)	Si	2.1
610.20	1275	3.76E-02	6.03	15.08	33.98	1000	0.097	0.097	7 (Fr)	Si	3.1
678.00	2106	3.63E-02	8.04	20.11	29.27	1258	0.105	0.105	8 (Qp)	Si	1.9
678.00	2109	3.63E-02	8.04	20.11	29.27	1260	0.105	0.105	7 (Fr)	Si	2.8

Trave: 406 [4008,4007], Pilastrate [2008,2007] Sez. R: By=50.00 cm Bz=30.00 cm L=797.00 cm Ln=767.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σca[kg/cmq]=224 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	1410	6.03	6.03	--	--	-33	1106	6	6	Si	3.3
76.70	--	553	6.03	6.03	--	--	-13	434	6	6	Si	8.3
383.50	667	--	6.03	6.03	-16	523	--	--	6	6	Si	6.9
690.30	--	1642	8.04	6.03	--	--	-34	981	6	6	Si	3.7
767.00	--	2771	8.04	6.03	--	--	-58	1655	6	6	Si	2.2

Combinazione QP: σca[kg/cmq]=168 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	1400	6.03	6.03	--	--	-33	1098	8	8	Si	3.3
76.70	--	546	6.03	6.03	--	--	-13	428	8	8	Si	8.4
383.50	666	--	6.03	6.03	-16	522	--	--	8	8	Si	6.9
690.30	--	1653	8.04	6.03	--	--	-35	987	8	8	Si	3.6

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
767.00	--	2784	8.04	6.03	--	--	-58	1663	8	8	Si	2.2

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{x,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	1402	3.76E-02	6.03	15.08	33.98	1099	0.107	0.107	7 (Fr)	Si	2.8
0.00	1400	3.76E-02	6.03	15.08	33.98	1098	0.107	0.107	8 (Qp)	Si	1.9
76.70	546	3.76E-02	6.03	15.08	33.98	428	0.042	0.042	8 (Qp)	Si	4.8
76.70	547	3.76E-02	6.03	15.08	33.98	429	0.042	0.042	7 (Fr)	Si	7.2
383.50	-666	3.76E-02	6.03	15.08	33.98	522	0.051	0.051	8 (Qp)	Si	3.9
383.50	-666	3.76E-02	6.03	15.08	33.98	522	0.051	0.051	7 (Fr)	Si	5.9
690.30	1653	3.63E-02	8.04	20.11	29.27	987	0.083	0.083	8 (Qp)	Si	2.4
690.30	1651	3.63E-02	8.04	20.11	29.27	986	0.082	0.082	7 (Fr)	Si	3.6
767.00	2784	3.63E-02	8.04	20.11	29.27	1663	0.139	0.139	8 (Qp)	Si	1.4
767.00	2781	3.63E-02	8.04	20.11	29.27	1662	0.139	0.139	7 (Fr)	Si	2.2

Trave: 406 [4008,4009], Pilastrate [2008,2009] Sez. R: By=50.00 cm Bz=30.00 cm L=663.00 cm Ln=678.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	1288	6.03	6.03	--	--	-30	1010	6	6	Si	3.6
67.80	--	630	6.03	6.03	--	--	-15	494	6	6	Si	7.3
339.00	277	--	6.03	6.03	-7	217	--	--	6	6	Si	17
610.20	--	1575	8.04	6.03	--	--	-33	941	6	6	Si	3.8
678.00	--	2468	8.04	6.03	--	--	-52	1475	6	6	Si	2.4

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	1278	6.03	6.03	--	--	-30	1003	8	8	Si	3.6
67.80	--	622	6.03	6.03	--	--	-15	488	8	8	Si	7.4
339.00	279	--	6.03	6.03	-7	219	--	--	8	8	Si	16
610.20	--	1578	8.04	6.03	--	--	-33	943	8	8	Si	3.8
678.00	--	2474	8.04	6.03	--	--	-52	1478	8	8	Si	2.4

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{x,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	1278	3.76E-02	6.03	15.08	33.98	1003	0.097	0.097	7 (Fr)	Si	3.1
0.00	1278	3.76E-02	6.03	15.08	33.98	1003	0.097	0.097	8 (Qp)	Si	2.1
67.80	622	3.76E-02	6.03	15.08	33.98	488	0.047	0.047	8 (Qp)	Si	4.2
67.80	622	3.76E-02	6.03	15.08	33.98	488	0.047	0.047	7 (Fr)	Si	6.3
339.00	-279	3.76E-02	6.03	15.08	33.98	219	0.021	0.021	8 (Qp)	Si	9.4
339.00	-278	3.76E-02	6.03	15.08	33.98	218	0.021	0.021	7 (Fr)	Si	14
610.20	1578	3.63E-02	8.04	20.11	29.27	943	0.079	0.079	8 (Qp)	Si	2.5
610.20	1580	3.63E-02	8.04	20.11	29.27	944	0.079	0.079	7 (Fr)	Si	3.8
678.00	2474	3.63E-02	8.04	20.11	29.27	1478	0.124	0.124	8 (Qp)	Si	1.6
678.00	2475	3.63E-02	8.04	20.11	29.27	1479	0.124	0.124	7 (Fr)	Si	2.4

Trave: 407 [4002,4005], Pilastrate [2002,2005] Sez. R: By=30.00 cm Bz=50.00 cm L=465.24 cm Ln=465.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	8189	10.18	7.63	--	--	-72	2082	6	6	Si	1.7
46.50	--	3636	10.18	7.63	--	--	-32	924	6	6	Si	3.9
232.50	4448	--	7.63	7.63	-43	1492	--	--	6	6	Si	2.4
418.50	--	3991	10.18	7.63	--	--	-35	1015	6	6	Si	3.5
465.00	--	8683	10.18	7.63	--	--	-77	2208	6	6	Si	1.6

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	7888	10.18	7.63	--	--	-70	2006	8	8	Si	1.8
46.50	--	3667	10.18	7.63	--	--	-32	932	8	8	Si	3.9

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
232.50	3927	--	7.63	7.63	-38	1317	--	--	8	8	Si	2.7
418.50	--	3629	10.18	7.63	--	--	-32	923	8	8	Si	3.9
465.00	--	7885	10.18	7.63	--	--	-70	2005	8	8	Si	1.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	7884	3.50E-02	10.18	22.62	27.51	2004	0.176	0.176	7 (Fr)	Si	1.7
0.00	7888	3.50E-02	10.18	22.62	27.51	2006	0.176	0.176	8 (Qp)	Si	1.1
46.50	3667	3.50E-02	10.18	22.62	27.51	932	0.073	0.073	8 (Qp)	Si	2.7
46.50	3664	3.50E-02	10.18	22.62	27.51	932	0.073	0.073	7 (Fr)	Si	4.1
232.50	-3927	3.67E-02	7.63	16.96	31.69	1317	0.119	0.119	8 (Qp)	Si	1.7
232.50	-3927	3.67E-02	7.63	16.96	31.69	1317	0.119	0.119	7 (Fr)	Si	2.5
418.50	3629	3.50E-02	10.18	22.62	27.51	923	0.073	0.073	8 (Qp)	Si	2.8
418.50	3633	3.50E-02	10.18	22.62	27.51	924	0.073	0.073	7 (Fr)	Si	4.1
465.00	7885	3.50E-02	10.18	22.62	27.51	2005	0.176	0.176	8 (Qp)	Si	1.1
465.00	7889	3.50E-02	10.18	22.62	27.51	2006	0.176	0.176	7 (Fr)	Si	1.7

Trave: 407 [4005,4008], Pilastrate [2005,2008] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	6303	10.18	7.63	--	--	-56	1603	6	6	Si	2.2
40.00	--	3060	10.18	7.63	--	--	-27	778	6	6	Si	4.6
200.00	2272	--	7.63	7.63	-22	762	--	--	6	6	Si	4.7
360.00	--	4623	12.72	7.63	--	--	-38	949	6	6	Si	3.8
400.00	--	8257	12.72	12.72	--	--	-62	1689	6	6	Si	2.1

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	5742	10.18	7.63	--	--	-51	1460	8	8	Si	2.5
40.00	--	2774	10.18	7.63	--	--	-24	705	8	8	Si	5.1
200.00	2088	--	7.63	7.63	-20	700	--	--	8	8	Si	5.1
360.00	--	4259	12.72	7.63	--	--	-35	875	8	8	Si	4.1
400.00	--	7598	12.72	12.72	--	--	-57	1554	8	8	Si	2.3

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	5722	3.50E-02	10.18	22.62	27.51	1455	0.114	0.114	7 (Fr)	Si	2.6
0.00	5742	3.50E-02	10.18	22.62	27.51	1460	0.115	0.115	8 (Qp)	Si	1.7
40.00	2774	3.50E-02	10.18	22.62	27.51	705	0.055	0.055	8 (Qp)	Si	3.6
40.00	2759	3.50E-02	10.18	22.62	27.51	701	0.055	0.055	7 (Fr)	Si	5.4
200.00	-2088	3.67E-02	7.63	16.96	31.69	700	0.063	0.063	8 (Qp)	Si	3.2
200.00	-2090	3.67E-02	7.63	16.96	31.69	701	0.063	0.063	7 (Fr)	Si	4.7
360.00	4259	3.36E-02	12.72	28.27	25.07	875	0.063	0.063	8 (Qp)	Si	3.2
360.00	4272	3.36E-02	12.72	28.27	25.07	877	0.063	0.063	7 (Fr)	Si	4.8
400.00	7598	3.45E-02	12.72	28.27	25.29	1554	0.119	0.119	8 (Qp)	Si	1.7
400.00	7614	3.45E-02	12.72	28.27	25.29	1558	0.120	0.120	7 (Fr)	Si	2.5

Trave: 407 [4008,4011], Pilastrate [2008,2011] Sez. R: By=30.00 cm Bz=50.00 cm L=500.00 cm Ln=525.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	9439	15.27	7.63	--	--	-73	1628	6	6	Si	2.2
52.50	--	3760	15.27	7.63	--	--	-29	649	6	6	Si	5.6
262.50	5793	--	7.63	7.63	-57	1943	--	--	6	6	Si	1.9
472.50	--	5718	12.72	7.63	--	--	-47	1174	6	6	Si	3.1
525.00	--	11750	12.72	7.63	--	--	-96	2412	6	6	Si	1.5

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
0.00	--	8710	15.27	7.63	--	--	-67	1503	8	8	Si	2.4
52.50	--	3493	15.27	7.63	--	--	-27	603	8	8	Si	6.0
262.50	5305	--	7.63	7.63	-52	1779	--	--	8	8	Si	2.0
472.50	--	5207	12.72	7.63	--	--	-43	1069	8	8	Si	3.4
525.00	--	10728	12.72	7.63	--	--	-88	2203	8	8	Si	1.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	8690	3.23E-02	15.27	33.93	23.48	1499	0.113	0.113	7 (Fr)	Si	2.6
0.00	8710	3.23E-02	15.27	33.93	23.48	1503	0.114	0.114	8 (Qp)	Si	1.8
52.50	3493	3.23E-02	15.27	33.93	23.48	603	0.040	0.040	8 (Qp)	Si	4.9
52.50	3477	3.23E-02	15.27	33.93	23.48	600	0.040	0.040	7 (Fr)	Si	7.5
262.50	-5305	3.67E-02	7.63	16.96	31.69	1779	0.161	0.161	8 (Qp)	Si	1.2
262.50	-5303	3.67E-02	7.63	16.96	31.69	1778	0.161	0.161	7 (Fr)	Si	1.9
472.50	5207	3.36E-02	12.72	28.27	25.07	1069	0.077	0.077	8 (Qp)	Si	2.6
472.50	5228	3.36E-02	12.72	28.27	25.07	1073	0.077	0.077	7 (Fr)	Si	3.9
525.00	10728	3.36E-02	12.72	28.27	25.07	2203	0.197	0.197	8 (Qp)	Si	1.0
525.00	10753	3.36E-02	12.72	28.27	25.07	2208	0.197	0.197	7 (Fr)	Si	1.5

Trave: 407 [4011,4014], Pilastrate [2011,2014] Sez. R: By=30.00 cm Bz=50.00 cm L=460.00 cm Ln=485.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	9218	10.18	10.18	--	--	-78	2341	6	6	Si	1.5
48.50	--	4239	10.18	10.18	--	--	-36	1077	6	6	Si	3.3
242.50	4534	--	7.63	7.63	-44	1521	--	--	6	6	Si	2.4
436.50	--	4519	12.72	7.63	--	--	-37	928	6	6	Si	3.9
485.00	--	9431	12.72	7.63	--	--	-77	1936	6	6	Si	1.9

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	8529	10.18	10.18	--	--	-72	2166	8	8	Si	1.7
48.50	--	3921	10.18	10.18	--	--	-33	996	8	8	Si	3.6
242.50	4213	--	7.63	7.63	-41	1413	--	--	8	8	Si	2.5
436.50	--	4135	12.72	7.63	--	--	-34	849	8	8	Si	4.2
485.00	--	8672	12.72	7.63	--	--	-71	1780	8	8	Si	2.0

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	8536	3.54E-02	10.18	22.62	27.65	2168	0.198	0.198	7 (Fr)	Si	1.5
0.00	8529	3.54E-02	10.18	22.62	27.65	2166	0.197	0.197	8 (Qp)	Si	1.0
48.50	3921	3.54E-02	10.18	22.62	27.65	996	0.079	0.079	8 (Qp)	Si	2.5
48.50	3927	3.54E-02	10.18	22.62	27.65	997	0.079	0.079	7 (Fr)	Si	3.8
242.50	-4213	3.67E-02	7.63	16.96	31.69	1413	0.128	0.128	8 (Qp)	Si	1.6
242.50	-4210	3.67E-02	7.63	16.96	31.69	1412	0.128	0.128	7 (Fr)	Si	2.3
436.50	4135	3.36E-02	12.72	28.27	25.07	849	0.061	0.061	8 (Qp)	Si	3.3
436.50	4134	3.36E-02	12.72	28.27	25.07	849	0.061	0.061	7 (Fr)	Si	4.9
485.00	8672	3.36E-02	12.72	28.27	25.07	1780	0.146	0.146	8 (Qp)	Si	1.4
485.00	8670	3.36E-02	12.72	28.27	25.07	1780	0.146	0.146	7 (Fr)	Si	2.1

Trave: 407 [4014,4017], Pilastrate [2014,2017] Sez. R: By=30.00 cm Bz=50.00 cm L=435.26 cm Ln=435.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	7737	12.72	7.63	--	--	-63	1588	6	6	Si	2.3
43.50	--	3716	12.72	7.63	--	--	-30	763	6	6	Si	4.7
217.50	3403	--	7.63	7.63	-33	1141	--	--	6	6	Si	3.2
391.50	--	3818	10.18	7.63	--	--	-34	971	6	6	Si	3.7
435.00	--	7815	10.18	7.63	--	--	-69	1987	6	6	Si	1.8

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	7038	12.72	7.63	--	--	-58	1445	8	8	Si	2.5
43.50	--	3371	12.72	7.63	--	--	-28	692	8	8	Si	5.2
217.50	3011	--	7.63	7.63	-29	1010	--	--	8	8	Si	3.6
391.50	--	3864	10.18	7.63	--	--	-34	983	8	8	Si	3.7
435.00	--	7610	10.18	7.63	--	--	-67	1935	8	8	Si	1.9

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	7065	3.36E-02	12.72	28.27	25.07	1451	0.107	0.107	7 (Fr)	Si	2.8
0.00	7038	3.36E-02	12.72	28.27	25.07	1445	0.106	0.106	8 (Qp)	Si	1.9
43.50	3371	3.36E-02	12.72	28.27	25.07	692	0.050	0.050	8 (Qp)	Si	4.0
43.50	3394	3.36E-02	12.72	28.27	25.07	697	0.050	0.050	7 (Fr)	Si	6.0
217.50	-3011	3.67E-02	7.63	16.96	31.69	1010	0.091	0.091	8 (Qp)	Si	2.2
217.50	-3006	3.67E-02	7.63	16.96	31.69	1008	0.091	0.091	7 (Fr)	Si	3.3
391.50	3864	3.50E-02	10.18	22.62	27.51	983	0.077	0.077	8 (Qp)	Si	2.6
391.50	3852	3.50E-02	10.18	22.62	27.51	979	0.077	0.077	7 (Fr)	Si	3.9
435.00	7610	3.50E-02	10.18	22.62	27.51	1935	0.167	0.167	8 (Qp)	Si	1.2
435.00	7593	3.50E-02	10.18	22.62	27.51	1931	0.166	0.166	7 (Fr)	Si	1.8

Trave: 408 [4014,4013], Pilastrate [2014,2013] Sez. R: By=50.00 cm Bz=30.00 cm L=797.00 cm Ln=767.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	1593	12.06	6.03	--	--	-29	648	6	6	Si	5.6
76.70	--	689	6.03	6.03	--	--	-16	540	6	6	Si	6.7
383.50	721	--	6.03	6.03	-17	565	--	--	6	6	Si	6.4
690.30	--	1399	6.03	6.03	--	--	-33	1097	6	6	Si	3.3
767.00	--	2481	8.04	6.03	--	--	-52	1482	6	6	Si	2.4

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	1575	12.06	6.03	--	--	-28	641	8	8	Si	5.6
76.70	--	674	6.03	6.03	--	--	-16	529	8	8	Si	6.8
383.50	720	--	6.03	6.03	-17	565	--	--	8	8	Si	6.4
690.30	--	1415	6.03	6.03	--	--	-33	1109	8	8	Si	3.2
767.00	--	2500	8.04	6.03	--	--	-52	1494	8	8	Si	2.4

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	1579	3.41E-02	12.06	30.16	24.68	643	0.045	0.045	7 (Fr)	Si	6.6
0.00	1575	3.41E-02	12.06	30.16	24.68	641	0.045	0.045	8 (Qp)	Si	4.4
76.70	674	3.76E-02	6.03	15.08	33.98	529	0.051	0.051	8 (Qp)	Si	3.9
76.70	678	3.76E-02	6.03	15.08	33.98	532	0.052	0.052	7 (Fr)	Si	5.8
383.50	-720	3.76E-02	6.03	15.08	33.98	565	0.055	0.055	8 (Qp)	Si	3.6
383.50	-720	3.76E-02	6.03	15.08	33.98	565	0.055	0.055	7 (Fr)	Si	5.5
690.30	1415	3.76E-02	6.03	15.08	33.98	1109	0.108	0.108	8 (Qp)	Si	1.9
690.30	1411	3.76E-02	6.03	15.08	33.98	1106	0.107	0.107	7 (Fr)	Si	2.8
767.00	2500	3.63E-02	8.04	20.11	29.27	1494	0.125	0.125	8 (Qp)	Si	1.6
767.00	2495	3.63E-02	8.04	20.11	29.27	1491	0.125	0.125	7 (Fr)	Si	2.4

Trave: 408 [4015,4014], Pilastrate [2015,2014] Sez. R: By=50.00 cm Bz=30.00 cm L=663.00 cm Ln=678.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	2225	8.04	6.03	--	--	-47	1329	6	6	Si	2.7
67.80	--	1368	8.04	6.03	--	--	-29	817	6	6	Si	4.4
339.00	336	--	6.03	6.03	-8	263	--	--	6	6	Si	14
610.20	--	719	6.03	6.03	--	--	-17	564	6	6	Si	6.4
678.00	--	1414	12.06	6.03	--	--	-26	575	6	6	Si	6.3

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c	σ_f	σ_c	σ_f	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	2253	8.04	6.03	--	--	-47	1346	8	8	Si	2.7
67.80	--	1390	8.04	6.03	--	--	-29	830	8	8	Si	4.3
339.00	338	--	6.03	6.03	-8	265	--	--	8	8	Si	14
610.20	--	691	6.03	6.03	--	--	-16	542	8	8	Si	6.6
678.00	--	1380	12.06	6.03	--	--	-25	562	8	8	Si	6.4

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	2244	3.63E-02	8.04	20.11	29.27	1341	0.112	0.112	7 (Fr)	Si	2.7
0.00	2253	3.63E-02	8.04	20.11	29.27	1346	0.113	0.113	8 (Qp)	Si	1.8
67.80	1390	3.63E-02	8.04	20.11	29.27	830	0.069	0.069	8 (Qp)	Si	2.9
67.80	1383	3.63E-02	8.04	20.11	29.27	826	0.069	0.069	7 (Fr)	Si	4.3
339.00	-338	3.76E-02	6.03	15.08	33.98	265	0.026	0.026	8 (Qp)	Si	7.8
339.00	-337	3.76E-02	6.03	15.08	33.98	265	0.026	0.026	7 (Fr)	Si	12
610.20	691	3.76E-02	6.03	15.08	33.98	542	0.053	0.053	8 (Qp)	Si	3.8
610.20	701	3.76E-02	6.03	15.08	33.98	549	0.053	0.053	7 (Fr)	Si	5.6
678.00	1380	3.41E-02	12.06	30.16	24.68	562	0.040	0.040	8 (Qp)	Si	5.0
678.00	1391	3.41E-02	12.06	30.16	24.68	566	0.040	0.040	7 (Fr)	Si	7.5

Trave: 409 [4017,4016], Pilastrate [2017,2016] Sez. R: By=30.00 cm Bz=50.00 cm L=782.00 cm Ln=782.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c	σ_f	σ_c	σ_f	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	8380	14.07	6.03	--	--	-69	1565	6	6	Si	2.3
78.20	--	4193	14.07	6.03	--	--	-34	783	6	6	Si	4.6
391.00	4147	--	6.03	6.03	-46	1745	--	--	6	6	Si	2.1
703.80	--	967	8.04	6.03	--	--	-10	308	6	6	Si	12
782.00	--	4347	8.04	6.03	--	--	-43	1387	6	6	Si	2.6

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c	σ_f	σ_c	σ_f	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	8342	14.07	6.03	--	--	-68	1558	8	8	Si	2.3
78.20	--	4161	14.07	6.03	--	--	-34	777	8	8	Si	4.6
391.00	4151	--	6.03	6.03	-46	1747	--	--	8	8	Si	2.1
703.80	--	990	8.04	6.03	--	--	-10	316	8	8	Si	11
782.00	--	4377	8.04	6.03	--	--	-43	1397	8	8	Si	2.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	8351	3.26E-02	14.07	35.19	23.29	1560	0.116	0.116	7 (Fr)	Si	2.6
0.00	8342	3.26E-02	14.07	35.19	23.29	1558	0.116	0.116	8 (Qp)	Si	1.7
78.20	4161	3.26E-02	14.07	35.19	23.29	777	0.052	0.052	8 (Qp)	Si	3.9
78.20	4169	3.26E-02	14.07	35.19	23.29	779	0.052	0.052	7 (Fr)	Si	5.8
391.00	-4151	3.76E-02	6.03	15.08	33.98	1747	0.170	0.170	8 (Qp)	Si	1.2
391.00	-4150	3.76E-02	6.03	15.08	33.98	1747	0.170	0.170	7 (Fr)	Si	1.8
703.80	990	3.61E-02	8.04	20.11	29.20	316	0.026	0.026	8 (Qp)	Si	7.6
703.80	985	3.61E-02	8.04	20.11	29.20	314	0.026	0.026	7 (Fr)	Si	11
782.00	4377	3.61E-02	8.04	20.11	29.20	1397	0.117	0.117	8 (Qp)	Si	1.7
782.00	4371	3.61E-02	8.04	20.11	29.20	1394	0.116	0.116	7 (Fr)	Si	2.6

Trave: 409 [4018,4017], Pilastrate [2018,2017] Sez. R: By=30.00 cm Bz=50.00 cm L=678.00 cm Ln=678.00 cm Criterio: CLS_TraviAlte

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_c	σ_f	σ_c	σ_f	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	3180	8.04	6.03	--	--	-31	1014	6	6	Si	3.5
67.80	--	773	8.04	6.03	--	--	-8	247	6	6	Si	15
339.00	2533	--	8.04	6.03	-27	1066	--	--	6	6	Si	3.4
610.20	--	4274	14.07	6.03	--	--	-35	798	6	6	Si	4.5
678.00	--	7556	14.07	6.03	--	--	-62	1412	6	6	Si	2.6

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.00	--	3222	8.04	6.03	--	--	-32	1028	8	8	Si	3.5
67.80	--	805	8.04	6.03	--	--	-8	257	8	8	Si	14
339.00	2543	--	8.04	6.03	-27	1071	--	--	8	8	Si	3.4
610.20	--	4222	14.07	6.03	--	--	-35	789	8	8	Si	4.6
678.00	--	7493	14.07	6.03	--	--	-61	1400	8	8	Si	2.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	3208	3.61E-02	8.04	20.11	29.20	1023	0.085	0.085	7 (Fr)	Si	3.5
0.00	3222	3.61E-02	8.04	20.11	29.20	1028	0.086	0.086	8 (Qp)	Si	2.3
67.80	805	3.61E-02	8.04	20.11	29.20	257	0.021	0.021	8 (Qp)	Si	9.3
67.80	794	3.61E-02	8.04	20.11	29.20	253	0.021	0.021	7 (Fr)	Si	14
339.00	-2543	3.80E-02	6.03	15.08	34.12	1071	0.104	0.104	8 (Qp)	Si	1.9
339.00	-2540	3.80E-02	6.03	15.08	34.12	1069	0.104	0.104	7 (Fr)	Si	2.9
610.20	4222	3.26E-02	14.07	35.19	23.29	789	0.052	0.052	8 (Qp)	Si	3.8
610.20	4239	3.26E-02	14.07	35.19	23.29	792	0.053	0.053	7 (Fr)	Si	5.7
678.00	7493	3.26E-02	14.07	35.19	23.29	1400	0.099	0.099	8 (Qp)	Si	2.0
678.00	7514	3.26E-02	14.07	35.19	23.29	1404	0.099	0.099	7 (Fr)	Si	3.0

Verifica dei Muri (Stati limite esercizio)

Scenario di calcolo: ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO

Simbologia

P.	Numero pannello
Nx [daN/cm ²]	Sforzo normale in direzione x
Ny [daN/cm ²]	Sforzo normale in direzione y
Nxy [daN/cm ²]	Sforzo tagliante in direzione xy
Mx [kg]	Momento flettente in direzione x
My [kg]	Momento flettente in direzione y
Mxy [kg]	Momento torcente
Afx [cmq/m]	Area acciaio in direzione x per metro lineare
Afy [cmq/m]	Area acciaio in direzione y per metro lineare
σ_c [kg/cm ²]	Tensione nel calcestruzzo compresso
σ_f [kg/cm ²]	Tensione nell'acciaio
σ_{ct} [kg/cm ²]	Tensione nel calcestruzzo teso
σ_{sct} [kg/cm ²]	Tensione nel calcestruzzo teso (quando richiesto dalla verifica)
σ_{sca} [kg/cm ²]	Tensione ammissibile nel calcestruzzo
σ_{sfa} [kg/cm ²]	Tensione ammissibile nell'acciaio
σ_{scta} [kg/cm ²]	Tensione ammissibile nel calcestruzzo teso
Cbc	Combinazione generatore della tensione nel cls compresso
Cbct	Combinazione generatore della tensione nel cls teso
Cbf	Combinazione generatore della tensione nell'acciaio
Cb	Combinazione
σ_{fmed} [kg/cm ²]	Tensione media dell'acciaio
Wd [mm]	Apertura delle fessure
Wk [mm]	Apertura caratteristica delle fessure
Wamm_Freq [mm]	Apertura ammissibile delle fessure per combinazione Frequente
Wamm_Qp [mm]	Apertura ammissibile delle fessure per combinazione Quasi Permanente
Wamm_Rara [mm]	Apertura ammissibile delle fessure per combinazione Rara
Cs	Coefficiente di sicurezza definito come minimo di σ_{Amm}/σ tra acciaio e calcestruzzo oppure Wamm/Wk

Muro [Platea]: 1 - Nodi: [2024-2027-2003-2023]Pann=4Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	31.42	31.42	-0	71	6	6	Si	51
3	31.42	31.42	0	334	6	6	Si	11

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	31.42	31.42	-0	69	8	8	Si	52
3	31.42	31.42	0	330	8	8	Si	11

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
3	1.40	0.09	-0.67	-674	53	293	330	0.050	0.050	8 (Qp)	Si	4.0
3	1.39	0.09	-0.66	-674	53	292	329	0.050	0.050	7 (Fr)	Si	6.0

Muro [Platea]: 2 - Nodi: [2023-2003-2002-2022]Pann=28Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-10	5	6	6	Si	23
15	31.42	31.42	-0	426	6	6	Si	8.4

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-10	5	8	8	Si	18
15	31.42	31.42	-0	421	8	8	Si	8.5

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
15	-0.10	1.53	0.25	-89	-1117	311	421	0.056	0.056	8 (Qp)	Si	3.5
15	-0.10	1.52	0.26	-89	-1113	308	419	0.056	0.056	7 (Fr)	Si	5.3

Muro [Platea]: 3 - Nodi: [2022-2002-2026-2021]Pann=12Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
6	31.42	31.42	-11	18	6	6	Si	20
1	31.42	31.42	-1	316	6	6	Si	11

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
6	31.42	31.42	-11	17	8	8	Si	15
1	31.42	31.42	-1	278	8	8	Si	13

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
7	0.18	0.46	0.75	-176	-748	162	190	0.025	0.025	8 (Qp)	Si	8.1
7	0.19	0.48	0.76	-176	-752	158	193	0.025	0.025	7 (Fr)	Si	12

Muro [Platea]: 4 - Nodi: [2021-2026-2001-2020]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
3	31.42	31.42	-13	10	6	6	Si	18
20	31.42	31.42	-0	428	6	6	Si	8.4

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
3	31.42	31.42	-12	10	8	8	Si	14
20	31.42	31.42	-0	417	8	8	Si	8.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
20	-0.14	1.49	-0.37	-65	-1129	-288	417	0.055	0.055	8 (Qp)	Si	3.6
20	-0.14	1.50	-0.37	-64	-1129	-287	418	0.055	0.055	7 (Fr)	Si	5.4

Muro [Platea]: 5 - Nodi: [2020-2001-2025-2019]Pann=4Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
3	31.42	31.42	-0	101	6	6	Si	36
4	31.42	31.42	0	344	6	6	Si	10

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
3	31.42	31.42	-0	99	8	8	Si	36
4	31.42	31.42	0	338	8	8	Si	11

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
4	1.44	0.11	0.70	-689	64	-303	338	0.051	0.051	8 (Qp)	Si	3.9
4	1.44	0.11	0.70	-690	64	-303	339	0.051	0.051	7 (Fr)	Si	5.9

Muro [Platea]: 6 - Nodi: [2001-2004-2035-2025]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
14	31.42	31.42	-6	-0	6	6	Si	36
1	31.42	31.42	-1	769	6	6	Si	4.7

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
14	31.42	31.42	-6	0	8	8	Si	27
1	31.42	31.42	-1	762	8	8	Si	4.7

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
1	2.97	0.19	0.72	-1822	-310	-798	762	0.108	0.108	8 (Qp)	Si	1.9
1	2.97	0.19	0.72	-1824	-309	-798	763	0.108	0.108	7 (Fr)	Si	2.8

Muro [Platea]: 7 - Nodi: [2004-2007-2041-2035]Pann=16Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-5	1	6	6	Si	42
16	31.42	31.42	-0	256	6	6	Si	14

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-5	1	8	8	Si	31
16	31.42	31.42	-0	215	8	8	Si	17

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
16	0.79	-0.12	0.50	-559	29	-475	215	0.029	0.029	8 (Qp)	Si	6.9
16	0.81	-0.12	0.50	-564	29	-474	218	0.030	0.030	7 (Fr)	Si	10

Muro [Platea]: 8 - Nodi: [2007-2010-2061-2041]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
10	31.42	31.42	-5	-0	6	6	Si	43
20	31.42	31.42	-0	475	6	6	Si	7.6

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
10	31.42	31.42	-5	-0	8	8	Si	33
20	31.42	31.42	-0	501	8	8	Si	7.2

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
20	1.95	-0.09	0.06	-1202	18	-385	501	0.071	0.071	8 (Qp)	Si	2.8
20	1.86	-0.09	0.06	-1167	18	-382	482	0.068	0.068	7 (Fr)	Si	4.4

Muro [Platea]: 9 - Nodi: [2010-2013-2080-2061]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
10	31.42	31.42	-7	2	6	6	Si	31
2	31.42	31.42	-0	401	6	6	Si	9.0

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
10	31.42	31.42	-7	2	8	8	Si	24
2	31.42	31.42	-0	425	8	8	Si	8.5

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
2	1.63	-0.21	-0.61	-1044	19	628	425	0.059	0.059	8 (Qp)	Si	3.4
2	1.55	-0.22	-0.62	-1010	19	630	407	0.056	0.056	7 (Fr)	Si	5.3

Muro [Platea]: 10 - Nodi: [2013-2016-2091-2080]Pann=16Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-5	-0	6	6	Si	50
15	31.42	31.42	-1	626	6	6	Si	5.8

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-4	-0	8	8	Si	38
15	31.42	31.42	-1	620	8	8	Si	5.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
15	2.45	0.16	-0.17	-1444	-243	485	620	0.089	0.089	8 (Qp)	Si	2.3
15	2.46	0.16	-0.17	-1447	-241	484	621	0.089	0.089	7 (Fr)	Si	3.4

Muro [Platea]: 11 - Nodi: [2016-2095-2094-2091]Pann=4Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	31.42	31.42	-0	46	6	6	Si	78
2	31.42	31.42	-0	291	6	6	Si	12

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	31.42	31.42	-0	48	8	8	Si	76
2	31.42	31.42	-0	286	8	8	Si	13

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
2	1.20	0.06	-0.53	-602	60	237	286	0.043	0.043	8 (Qp)	Si	4.7
2	1.20	0.06	-0.53	-603	60	237	287	0.043	0.043	7 (Fr)	Si	7.0

Muro [Platea]: 12 - Nodi: [2092-2096-2095-2016]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-10	-0	6	6	Si	23
10	31.42	31.42	-1	260	6	6	Si	14

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
3	31.42	31.42	-9	-0	8	8	Si	18
10	31.42	31.42	-1	254	8	8	Si	14

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
10	-0.05	0.82	0.62	-105	-777	123	135	0.014	0.014	8 (Qp)	Si	15
10	-0.06	0.82	0.63	-103	-776	120	134	0.013	0.013	7 (Fr)	Si	22

Muro [Platea]: 13 - Nodi: [2017-2097-2096-2092]Pann=12Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
6	31.42	31.42	-9	3	6	6	Si	24
1	31.42	31.42	-1	80	6	6	Si	45

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
6	31.42	31.42	-9	3	8	8	Si	19
2	31.42	31.42	-3	77	8	8	Si	46

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
2	0.28	-1.62	-0.01	-203	776	-700	77	0.010	0.010	8 (Qp)	Si	19
2	0.28	-1.70	-0.01	-203	810	-696	78	0.010	0.010	7 (Fr)	Si	29

Muro [Platea]: 14 - Nodi: [2093-2099-2098-2018]Pann=4Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-0	73	6	6	Si	49
1	31.42	31.42	0	183	6	6	Si	20

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-0	72	8	8	Si	50
1	31.42	31.42	0	180	8	8	Si	20

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
1	0.74	0.08	0.32	-392	35	-148	180	0.026	0.026	8 (Qp)	Si	7.6
1	0.74	0.08	0.32	-393	35	-149	181	0.027	0.027	7 (Fr)	Si	11

Muro [Platea]: 15 - Nodi: [2018-2098-2097-2017]Pann=28Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-9	3	6	6	Si	24
14	31.42	31.42	-1	105	6	6	Si	34

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-9	4	8	8	Si	18
14	31.42	31.42	-1	102	8	8	Si	35

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
14	0.36	-0.08	1.33	-278	-282	-276	102	0.013	0.013	8 (Qp)	Si	15
14	0.36	-0.16	1.33	-276	-249	-275	101	0.013	0.013	7 (Fr)	Si	23

Muro [Platea]: 16 - Nodi: [2027-2040-2006-2003]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	31.42	31.42	-5	-0	6	6	Si	46
2	31.42	31.42	-1	741	6	6	Si	4.9

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	31.42	31.42	-5	-0	8	8	Si	35
2	31.42	31.42	-1	739	8	8	Si	4.9

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
2	2.92	0.13	-0.61	-1722	-245	685	739	0.106	0.106	8 (Qp)	Si	1.9
2	2.92	0.13	-0.61	-1721	-245	684	738	0.105	0.105	7 (Fr)	Si	2.8

Muro [Platea]: 17 - Nodi: [2040-2046-2009-2006]Pann=16Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-4	1	6	6	Si	57
15	31.42	31.42	-0	184	6	6	Si	20

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-4	1	8	8	Si	42
15	31.42	31.42	-0	160	8	8	Si	23

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
2	-0.59	0.35	0.34	-91	-265	162	98	0.013	0.013	8 (Qp)	Si	15
2	-0.58	0.35	0.35	-92	-264	157	98	0.013	0.013	7 (Fr)	Si	23

Muro [Platea]: 18 - Nodi: [2046-2063-2012-2009]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
11	31.42	31.42	-6	-0	6	6	Si	40
1	31.42	31.42	-1	118	6	6	Si	31

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
11	31.42	31.42	-5	-0	8	8	Si	31
1	31.42	31.42	-1	98	8	8	Si	37

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
1	0.20	-0.04	0.18	-428	1	-410	98	0.013	0.013	8 (Qp)	Si	16
1	0.19	-0.04	0.19	-420	2	-412	95	0.012	0.012	7 (Fr)	Si	24

Muro [Platea]: 19 - Nodi: [2063-2081-2015-2012]Pann=20Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
11	31.42	31.42	-6	-0	6	6	Si	39
20	31.42	31.42	-1	75	6	6	Si	48

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
11	31.42	31.42	-6	-0	8	8	Si	30
1	31.42	31.42	-1	73	8	8	Si	49

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
1	0.08	0.01	0.01	-391	22	-298	73	0.010	0.010	8 (Qp)	Si	21
1	0.02	0.01	0.03	-362	22	-301	59	0.008	0.008	7 (Fr)	Si	39

Muro [Platea]: 20 - Nodi: [2081-2093-2018-2015]Pann=16Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-5	7	6	6	Si	49
16	31.42	31.42	-1	404	6	6	Si	8.9

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-5	6	8	8	Si	36
16	31.42	31.42	-1	398	8	8	Si	9.0

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
16	1.55	0.22	0.32	-954	-261	-437	398	0.056	0.056	8 (Qp)	Si	3.6
16	1.56	0.22	0.31	-957	-261	-435	401	0.057	0.057	7 (Fr)	Si	5.3

Muro [Platea]: 21 - Nodi: [2018-2017-2089-2090]Pann=28Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
14	31.42	31.42	-9	46	6	6	Si	24
27	31.42	31.42	-1	179	6	6	Si	20

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
12	31.42	31.42	-9	50	8	8	Si	18
27	31.42	31.42	-1	174	8	8	Si	21

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
27	-1.10	0.73	-0.44	-29	-368	392	174	0.026	0.026	8 (Qp)	Si	7.7
27	-1.17	0.73	-0.43	5	-369	388	175	0.026	0.026	7 (Fr)	Si	12

Muro [Platea]: 22 - Nodi: [2090-2015-2018]Pann=13Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
7	31.42	31.42	-7	96	6	6	Si	33

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
7	31.42	31.42	-7	98	8	8	Si	24

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cmq	mm	mm			
7	-2.27	-1.56	-0.04	1306	1952	20	98	0.010	0.010	8 (Qp)	Si	19
7	-2.23	-1.54	-0.04	1286	1935	20	97	0.010	0.010	7 (Fr)	Si	29

Muro [Platea]: 23 - Nodi: [2012-2062-2054]Pann=31Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-15	216	6	6	Si	14
17	31.42	31.42	-2	329	6	6	Si	11

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-15	220	8	8	Si	11
17	31.42	31.42	-2	313	8	8	Si	11

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cmq	mm	mm			
17	1.12	-1.21	-0.40	-850	-451	-1044	313	0.042	0.042	8 (Qp)	Si	4.8
17	1.12	-1.27	-0.44	-852	-430	-1029	314	0.042	0.042	7 (Fr)	Si	7.2

Muro [Platea]: 24 - Nodi: [2062-2014-2011]Pann=15Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
6	31.42	31.42	-17	558	6	6	Si	6.5
7	31.42	31.42	-15	635	6	6	Si	5.7

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
6	31.42	31.42	-16	558	8	8	Si	6.4
7	31.42	31.42	-15	646	8	8	Si	5.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cmq	mm	mm			
7	-1.60	-0.12	1.51	1088	4279	1012	646	0.084	0.084	8 (Qp)	Si	2.4
7	-1.63	-0.19	1.48	1098	4300	994	639	0.083	0.083	7 (Fr)	Si	3.6

Muro [Platea]: 25 - Nodi: [2015-2062-2012]Pann=35Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-11	59	6	6	Si	21
8	31.42	31.42	-7	159	6	6	Si	23

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-11	57	8	8	Si	16
8	31.42	31.42	-6	141	8	8	Si	26

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	0.33	-0.89	-0.82	-304	-1720	337	141	0.017	0.017	8 (Qp)	Si	12
8	0.26	-0.88	-0.84	-272	-1722	347	143	0.017	0.017	7 (Fr)	Si	18

Muro [Platea]: 26 - Nodi: [2013-2087-2016]Pann=14Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-4	22	6	6	Si	53
12	31.42	31.42	0	777	6	6	Si	4.6

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-4	22	8	8	Si	41
12	31.42	31.42	0	769	8	8	Si	4.7

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
12	3.35	0.75	0.74	-1481	-361	-356	769	0.118	0.118	8 (Qp)	Si	1.7
12	3.36	0.74	0.75	-1485	-360	-361	771	0.119	0.119	7 (Fr)	Si	2.5

Muro [Platea]: 27 - Nodi: [2004-2036-2007]Pann=51Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	31.42	31.42	-21	432	6	6	Si	8.3

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	31.42	31.42	-20	415	8	8	Si	8.3

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
16	-3.29	-0.74	0.46	-5628	-1022	-96	415	0.048	0.048	8 (Qp)	Si	4.2
16	-3.29	-0.72	0.46	-5640	-1032	-100	416	0.048	0.048	7 (Fr)	Si	6.2

Muro [Platea]: 28 - Nodi: [2001-2026-2028]Pann=44Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[\text{kg/cm}^2]=224$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	31.42	31.42	-18	384	6	6	Si	9.4

Combinazione QP: $\sigma_{ca}[\text{kg/cm}^2]=168$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	31.42	31.42	-18	400	8	8	Si	9.0

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
15	1.19	-0.32	-1.08	-1172	-2731	-1403	376	0.049	0.049	8 (Qp)	Si	4.1
15	1.19	-0.32	-1.08	-1173	-2732	-1405	376	0.049	0.049	7 (Fr)	Si	6.1

Muro [Platea]: 29 - Nodi: [2009-2044-2006]Pann=56Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[\text{kg/cm}^2]=224$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
28	31.42	31.42	-12	-1	6	6	Si	18
16	31.42	31.42	-5	264	6	6	Si	14

Combinazione QP: $\sigma_{ca}[\text{kg/cm}^2]=168$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
28	31.42	31.42	-12	-1	8	8	Si	14
16	31.42	31.42	-5	253	8	8	Si	14

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
16	0.14	-0.23	-0.78	-1491	-571	-510	253	0.033	0.033	8 (Qp)	Si	6.1
16	0.14	-0.24	-0.80	-1488	-565	-500	252	0.033	0.033	7 (Fr)	Si	9.1

Muro [Platea]: 30 - Nodi: [2003-2029-2002]Pann=56Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[\text{kg/cm}^2]=224$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
14	31.42	31.42	-16	396	6	6	Si	9.1
27	31.42	31.42	-9	410	6	6	Si	8.8

Combinazione QP: $\sigma_{ca}[\text{kg/cm}^2]=168$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
14	31.42	31.42	-16	388	8	8	Si	9.3
27	31.42	31.42	-9	408	8	8	Si	8.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
27	0.12	0.94	1.18	-2503	-1203	1318	408	0.053	0.053	8 (Qp)	Si	3.8
27	0.12	0.93	1.18	-2499	-1200	1319	407	0.053	0.053	7 (Fr)	Si	5.7

Muro [Platea]: 31 - Nodi: [2084-2085-2088]Pann=21Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[\text{kg/cm}^2]=224$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
19	31.42	31.42	-9	-6	6	6	Si	24
9	31.42	31.42	-8	5	6	6	Si	27

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
19	31.42	31.42	-9	-5	8	8	Si	19
9	31.42	31.42	-8	5	8	8	Si	20

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
9	-1.88	-4.70	0.44	1147	1937	-424	5	0.000	0.000	8 (Qp)	Si	>100
9	-2.00	-4.73	0.46	1202	1958	-426	5	0.000	0.000	7 (Fr)	Si	>100

Muro [Platea]: 32 - Nodi: [2002-2028-2026]Pann=25Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
15	31.42	31.42	-20	254	6	6	Si	11
8	31.42	31.42	-13	275	6	6	Si	13

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
15	31.42	31.42	-20	260	8	8	Si	8.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
8	-2.07	-1.31	1.12	-3516	-2254	2067	257	0.030	0.030	8 (Qp)	Si	6.7
8	-2.05	-1.30	1.11	-3516	-2243	2060	259	0.030	0.030	7 (Fr)	Si	10.0

Muro [Platea]: 33 - Nodi: [2037-2043-2042-2036]Pann=8Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
7	31.42	31.42	-6	26	6	6	Si	40

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
7	31.42	31.42	-6	32	8	8	Si	30

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
7	-2.17	-2.02	1.03	152	-3975	2146	32	0.003	0.003	8 (Qp)	Si	59
7	-2.14	-2.03	1.03	154	-3935	2120	30	0.003	0.003	7 (Fr)	Si	97

Muro [Platea]: 34 - Nodi: [2032-2031-2028-2029]Pann=16Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	31.42	31.42	-5	-16	6	6	Si	47

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
1	31.42	31.42	-3	-9	6	6	Si	78

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	31.42	31.42	-5	-18	8	8	Si	36
1	31.42	31.42	-3	-12	8	8	Si	60

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	-0.95	-2.91	0.32	-147	66	-1327	0	0.000	0.000	8 (Qp)	Si	>100
1	-0.94	-2.89	0.30	-163	28	-1324	0	0.000	0.000	7 (Fr)	Si	>100

Muro [Platea]: 35 - Nodi: [2033-2038-2005-2032]Pann=16Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
3	31.42	31.42	-4	16	6	6	Si	53

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
3	31.42	31.42	-4	14	8	8	Si	39

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	-1.76	-0.85	-0.91	2994	945	1601	14	0.001	0.001	8 (Qp)	Si	>100
3	-1.73	-0.83	-0.89	2967	927	1571	14	0.001	0.001	7 (Fr)	Si	>100

Muro [Platea]: 36 - Nodi: [2033-2032-2029]Pann=9Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-5	-10	6	6	Si	44
1	31.42	31.42	-3	-13	6	6	Si	84

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-5	-9	8	8	Si	31
1	31.42	31.42	-3	-12	8	8	Si	58

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	-1.27	-2.68	1.14	526	445	-902	0	0.000	0.000	8 (Qp)	Si	>100
1	-1.25	-2.66	1.12	498	405	-896	0	0.000	0.000	7 (Fr)	Si	>100

Muro [Platea]: 37 - Nodi: [2032-2005-2037-2031]Pann=16Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	31.42	31.42	-10	387	6	6	Si	9.3

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	31.42	31.42	-10	415	8	8	Si	8.7

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
4	-0.73	-1.50	-1.40	6432	1745	-3556	415	0.054	0.054	8 (Qp)	Si	3.7
4	-0.74	-1.50	-1.39	6329	1737	-3588	405	0.053	0.053	7 (Fr)	Si	5.7

Muro [Platea]: 38 - Nodi: [2038-2044-2008-2005]Pann=16Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	31.42	31.42	-8	491	6	6	Si	7.3

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	31.42	31.42	-8	505	8	8	Si	7.1

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
13	-0.84	0.07	-0.43	1291	5356	579	505	0.066	0.066	8 (Qp)	Si	3.0
13	-0.84	0.06	-0.43	1269	5263	540	495	0.065	0.065	7 (Fr)	Si	4.7

Muro [Platea]: 39 - Nodi: [2044-2050-2049-2008]Pann=16Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	31.42	31.42	-5	473	6	6	Si	7.6

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	31.42	31.42	-5	489	8	8	Si	7.4

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	-1.57	0.50	1.12	448	4016	3058	489	0.064	0.064	8 (Qp)	Si	3.1
1	-1.58	0.48	1.11	389	3945	2989	479	0.062	0.062	7 (Fr)	Si	4.8

Muro [Platea]: 40 - Nodi: [2005-2008-2043-2037]Pann=16Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	31.42	31.42	-8	254	6	6	Si	14

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	31.42	31.42	-7	243	8	8	Si	15

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
13	-1.33	-0.76	0.25	-2	-4550	1265	243	0.032	0.032	8 (Qp)	Si	6.3
13	-1.32	-0.76	0.27	-18	-4523	1234	239	0.031	0.031	7 (Fr)	Si	9.6

Muro [Platea]: 41 - Nodi: [2029-2028-2002]Pann=25Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
10	31.42	31.42	-16	281	6	6	Si	13
5	31.42	31.42	-15	382	6	6	Si	9.4

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
10	31.42	31.42	-17	292	8	8	Si	10
5	31.42	31.42	-15	373	8	8	Si	9.7

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
5	-1.42	-1.75	0.43	-1875	-4021	2	373	0.045	0.045	8 (Qp)	Si	4.4
5	-1.40	-1.73	0.42	-1880	-4009	7	373	0.045	0.045	7 (Fr)	Si	6.6

Muro [Platea]: 42 - Nodi: [2001-2028-2036-2004]Pann=100Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
33	31.42	31.42	-22	274	6	6	Si	10
22	31.42	31.42	-11	637	6	6	Si	5.7

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
33	31.42	31.42	-22	276	8	8	Si	7.6
22	31.42	31.42	-11	630	8	8	Si	5.7

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
22	-0.52	2.51	0.92	-2997	-1447	-244	630	0.091	0.091	8 (Qp)	Si	2.2
22	-0.51	2.51	0.92	-3000	-1449	-245	631	0.091	0.091	7 (Fr)	Si	3.3

Muro [Platea]: 43 - Nodi: [2003-2006-2029]Pann=69Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	31.42	31.42	-11	52	6	6	Si	20
18	31.42	31.42	-8	708	6	6	Si	5.1

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	31.42	31.42	-11	55	8	8	Si	15
18	31.42	31.42	-8	707	8	8	Si	5.1

Verifica aperture fessure:Wamm_Freq[mm]=0.300 Wamm_Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
18	2.52	-0.44	-0.66	-1926	-2226	-734	707	0.094	0.094	8 (Qp)	Si	2.1
18	2.52	-0.44	-0.65	-1923	-2222	-735	706	0.093	0.093	7 (Fr)	Si	3.2

Muro [Platea]: 44 - Nodi: [2006-2033-2029] Pann=23Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
3	31.42	31.42	-11	12	6	6	Si	20
19	31.42	31.42	-2	436	6	6	Si	8.3

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
3	31.42	31.42	-11	16	8	8	Si	15
19	31.42	31.42	-1	424	8	8	Si	8.5

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
19	1.71	-1.59	-1.88	-951	15	-1323	424	0.061	0.061	8 (Qp)	Si	3.3
19	1.70	-1.58	-1.89	-948	6	-1317	421	0.061	0.061	7 (Fr)	Si	4.9

Muro [Platea]: 45 - Nodi: [2006-2038-2033] Pann=22Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
14	31.42	31.42	-12	-7	6	6	Si	19
8	31.42	31.42	-2	375	6	6	Si	9.6

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
14	31.42	31.42	-12	-7	8	8	Si	14
8	31.42	31.42	-2	363	8	8	Si	9.9

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	1.61	-1.33	-0.31	-666	555	61	363	0.057	0.057	8 (Qp)	Si	3.5
8	1.61	-1.33	-0.33	-664	552	66	361	0.057	0.057	7 (Fr)	Si	5.3

Muro [Platea]: 46 - Nodi: [2006-2044-2038] Pann=42Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
31	31.42	31.42	-10	-1	6	6	Si	23
8	31.42	31.42	-2	114	6	6	Si	32

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
31	31.42	31.42	-10	-1	8	8	Si	17
8	31.42	31.42	-2	87	8	8	Si	41

Verifica aperture fessure:Wamm_Freq[mm]=0.300 Wamm_Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	-0.03	-0.44	0.87	-591	-36	-618	87	0.011	0.011	8 (Qp)	Si	18
8	-0.02	-0.45	0.86	-595	-31	-614	90	0.012	0.012	7 (Fr)	Si	26

Muro [Platea]: 47 - Nodi: [2009-2050-2044] Pann=27 Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	31.42	31.42	-11	78	6	6	Si	20
19	31.42	31.42	-4	509	6	6	Si	7.1

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	31.42	31.42	-11	79	8	8	Si	15
19	31.42	31.42	-4	484	8	8	Si	7.4

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
19	1.36	-0.13	0.93	-1713	-102	978	244	0.024	0.024	8 (Qp)	Si	8.3
19	1.37	-0.16	0.91	-1715	-92	984	245	0.024	0.024	7 (Fr)	Si	12

Muro : 48 - Nodi: [4-3-2-5], Pann.X=4, Pann.Y=4 Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
16	20.11	20.11	-5	83	6	6	Si	42
2	20.11	20.11	-4	253	6	6	Si	14

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
16	20.11	20.11	-5	97	8	8	Si	32
2	20.11	20.11	-4	290	8	8	Si	12

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
16	-2.99	0.61	3.00	-312	32	-109	97	0.018	0.018	8 (Qp)	Si	11
16	-2.98	0.57	2.91	-312	30	-104	90	0.017	0.017	7 (Fr)	Si	18

Muro : 49 - Nodi: [6-4-5-7], Pann.X=4, Pann.Y=4 Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	20.11	20.11	-5	-3	6	6	Si	43
10	20.11	20.11	-4	258	6	6	Si	14

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	20.11	20.11	-5	-2	8	8	Si	32
10	20.11	20.11	-4	296	8	8	Si	12

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
1	0.47	0.94	1.88	-6	288	-132	62	0.014	0.014	8 (Qp)	Si	14
1	0.45	0.89	1.83	-9	271	-128	61	0.014	0.014	7 (Fr)	Si	22

Muro : 50 - Nodi: [8-6-7-9], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-5	4	6	6	Si	42
2	20.11	20.11	-4	177	6	6	Si	20

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-5	8	8	8	Si	31
2	20.11	20.11	-4	217	8	8	Si	17

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
1	0.71	0.75	1.22	21	-7	24	98	0.023	0.023	8 (Qp)	Si	8.6
1	0.68	0.68	1.19	19	-21	25	97	0.021	0.021	7 (Fr)	Si	15

Muro : 51 - Nodi: [10-8-9-11], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-9	7	6	6	Si	24
1	20.11	20.11	-2	163	6	6	Si	22

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-9	8	8	8	Si	19
14	20.11	20.11	-5	199	8	8	Si	18

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
5	0.71	0.03	0.44	52	-18	-45	123	0.021	0.021	8 (Qp)	Si	9.4
5	0.69	-0.04	0.43	50	-33	-43	119	0.021	0.021	7 (Fr)	Si	15

Muro : 52 - Nodi: [12-10-11-13], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-12	13	6	6	Si	19
13	20.11	20.11	-1	242	6	6	Si	15

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-11	11	8	8	Si	15
13	20.11	20.11	-2	247	8	8	Si	15

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
9	0.93	0.11	-1.59	86	56	29	173	0.028	0.028	8 (Qp)	Si	7.2
9	0.91	0.05	-1.59	85	40	29	169	0.027	0.027	7 (Fr)	Si	11

Muro : 53 - Nodi: [14-12-13-15], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=---,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
15	20.11	20.11	-6	174	6	6	Si	21
4	20.11	20.11	-5	286	6	6	Si	13

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
15	20.11	20.11	-6	193	8	8	Si	19
4	20.11	20.11	-5	287	8	8	Si	13

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
10	-2.23	0.39	-3.26	9	327	-155	236	0.024	0.024	7 (Fr)	Si	12
14	-1.95	0.14	-2.97	30	362	-144	221	0.022	0.022	8 (Qp)	Si	9.0

Muro : 54 - Nodi: [16-14-15-17], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=---,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-7	3	6	6	Si	30
2	20.11	20.11	-4	318	6	6	Si	11

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-7	8	8	8	Si	22
5	20.11	20.11	-5	368	8	8	Si	9.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
4	-1.63	1.36	-3.31	-63	64	63	212	0.041	0.041	8 (Qp)	Si	4.9
4	-1.66	1.32	-3.22	-65	60	63	205	0.040	0.040	7 (Fr)	Si	7.6

Muro : 55 - Nodi: [18-16-17-19], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=---,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-4	2	6	6	Si	53
4	20.11	20.11	-2	356	6	6	Si	10

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-4	24	8	8	Si	38
4	20.11	20.11	-2	393	8	8	Si	9.2

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
4	-1.60	2.95	-3.13	-110	39	110	393	0.091	0.091	8 (Qp)	Si	2.2
4	-1.59	2.85	-3.05	-106	37	105	380	0.088	0.088	7 (Fr)	Si	3.4

Muro : 56 - Nodi: [20-18-19-21], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=---,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-5	245	6	6	Si	15
13	20.11	20.11	-4	330	6	6	Si	11

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-5	382	8	8	Si	9.4

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
16	-3.39	1.90	-2.63	-183	-52	48	271	0.058	0.058	8 (Qp)	Si	3.5
16	-3.38	1.81	-2.58	-183	-53	44	261	0.055	0.055	7 (Fr)	Si	5.5

Muro : 57 - Nodi: [22-20-21-23], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
3	20.11	20.11	-5	143	6	6	Si	25
14	20.11	20.11	-4	260	6	6	Si	14

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	20.11	20.11	-6	95	8	8	Si	31
14	20.11	20.11	-4	299	8	8	Si	12

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
4	-2.83	1.57	-1.63	-277	44	83	225	0.048	0.048	8 (Qp)	Si	4.2
4	-2.82	1.52	-1.56	-278	42	80	217	0.046	0.046	7 (Fr)	Si	6.5

Muro : 58 - Nodi: [24-22-23-25], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
15	20.11	20.11	-5	199	6	6	Si	18
4	20.11	20.11	-4	306	6	6	Si	12

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
15	20.11	20.11	-5	225	8	8	Si	16
4	20.11	20.11	-4	344	8	8	Si	10

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
4	-2.64	2.09	-0.79	144	126	7	344	0.063	0.063	8 (Qp)	Si	3.2
4	-2.63	2.01	-0.72	143	124	7	332	0.060	0.060	7 (Fr)	Si	5.0

Muro : 59 - Nodi: [26-24-25-27], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	20.11	20.11	-5	185	6	6	Si	19
12	20.11	20.11	-4	321	6	6	Si	11

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	20.11	20.11	-5	221	8	8	Si	16
12	20.11	20.11	-4	363	8	8	Si	9.9

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
8	-2.69	2.32	-0.15	44	85	50	345	0.070	0.070	8 (Qp)	Si	2.9
8	-2.68	2.21	-0.10	45	85	49	331	0.067	0.067	7 (Fr)	Si	4.5

Muro : 60 - Nodi: [28-26-27-29], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
14	20.11	20.11	-5	159	6	6	Si	23
8	20.11	20.11	-4	329	6	6	Si	11

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
14	20.11	20.11	-5	200	8	8	Si	18
8	20.11	20.11	-4	376	8	8	Si	9.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
12	-2.76	2.45	1.02	55	86	-46	362	0.074	0.074	8 (Qp)	Si	2.7
12	-2.74	2.33	1.02	56	86	-44	346	0.070	0.070	7 (Fr)	Si	4.3

Muro : 61 - Nodi: [30-28-29-31], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
3	20.11	20.11	-5	203	6	6	Si	18
16	20.11	20.11	-4	312	6	6	Si	12

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-6	362	8	8	Si	9.9
10	20.11	20.11	-5	364	8	8	Si	9.9

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
16	-2.80	2.25	1.78	158	119	-20	359	0.067	0.067	8 (Qp)	Si	3.0
16	-2.78	2.12	1.75	158	119	-20	343	0.063	0.063	7 (Fr)	Si	4.7

Muro : 62 - Nodi: [32-30-31-33], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
15	20.11	20.11	-5	129	6	6	Si	28

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
2	20.11	20.11	-4	273	6	6	Si	13

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
15	20.11	20.11	-6	159	8	8	Si	23
2	20.11	20.11	-4	318	8	8	Si	11

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
16	-2.97	1.68	2.50	-294	29	-138	228	0.052	0.052	8 (Qp)	Si	3.9
16	-2.95	1.56	2.43	-292	30	-134	214	0.048	0.048	7 (Fr)	Si	6.3

Muro : 63 - Nodi: [3-32-33-2], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-5	333	6	6	Si	11

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-6	388	8	8	Si	9.3

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
16	-2.93	1.39	3.16	140	117	-26	250	0.041	0.041	8 (Qp)	Si	4.8
16	-2.91	1.30	3.06	139	115	-26	237	0.039	0.039	7 (Fr)	Si	7.8

Muro : 64 - Nodi: [5-2-2079-2077], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-11	423	6	6	Si	8.5
12	20.11	20.11	-9	574	6	6	Si	6.3

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-10	388	8	8	Si	9.3
16	20.11	20.11	-7	551	8	8	Si	6.5

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
15	-2.25	1.85	1.96	-226	39	-39	255	0.056	0.056	8 (Qp)	Si	3.5
15	-2.33	1.76	1.88	-233	40	-36	246	0.054	0.054	7 (Fr)	Si	5.6

Muro : 65 - Nodi: [7-5-2077-2075], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	20.11	20.11	-16	369	6	6	Si	9.8
16	20.11	20.11	-13	480	6	6	Si	7.5

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	20.11	20.11	-15	330	8	8	Si	11
16	20.11	20.11	-12	447	8	8	Si	8.1

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
16	-1.77	0.33	2.17	117	718	-169	447	0.045	0.045	8 (Qp)	Si	4.4
16	-1.83	0.34	2.12	121	735	-166	458	0.046	0.046	7 (Fr)	Si	6.5

Muro : 66 - Nodi: [9-7-2075-2073], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--, Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
16	20.11	20.11	-22	464	6	6	Si	7.8
12	20.11	20.11	-22	594	6	6	Si	6.1

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
16	20.11	20.11	-21	447	8	8	Si	7.9
12	20.11	20.11	-21	569	8	8	Si	6.3

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
12	-0.94	-1.05	1.89	232	1250	-152	569	0.055	0.055	8 (Qp)	Si	3.6
12	-0.99	-1.04	1.86	232	1259	-152	575	0.056	0.056	7 (Fr)	Si	5.3

Muro : 67 - Nodi: [11-9-2073-2071], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--, Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
16	20.11	20.11	-18	476	6	6	Si	7.6
4	20.11	20.11	-13	803	6	6	Si	4.5

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
16	20.11	20.11	-18	463	8	8	Si	7.8
4	20.11	20.11	-13	795	8	8	Si	4.5

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	0.29	1.02	0.51	308	997	123	695	0.071	0.071	8 (Qp)	Si	2.8
8	0.29	1.02	0.50	309	999	124	695	0.071	0.071	7 (Fr)	Si	4.2

Muro : 68 - Nodi: [13-11-2071-2068], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--, Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
16	20.11	20.11	-11	291	6	6	Si	12
4	20.11	20.11	-2	377	6	6	Si	9.5

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
16	20.11	20.11	-11	296	8	8	Si	12

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
4	20.11	20.11	-2	376	8	8	Si	9.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
4	-2.14	2.75	0.35	-43	51	17	376	0.084	0.084	8 (Qp)	Si	2.4
4	-2.11	2.73	0.35	-42	52	18	374	0.084	0.084	7 (Fr)	Si	3.6

Muro : 69 - Nodi: [15-13-2068-2066], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	20.11	20.11	-17	452	6	6	Si	8.0

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	20.11	20.11	-17	464	8	8	Si	7.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
16	-2.53	2.14	1.52	-202	-13	-85	274	0.067	0.067	8 (Qp)	Si	3.0
16	-2.50	2.13	1.51	-200	-12	-82	273	0.067	0.067	7 (Fr)	Si	4.5

Muro : 70 - Nodi: [17-15-2066-2064], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
15	20.11	20.11	-10	158	6	6	Si	23
1	20.11	20.11	-3	174	6	6	Si	21

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
16	20.11	20.11	-10	20	8	8	Si	17
1	20.11	20.11	-3	209	8	8	Si	17

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
2	-0.27	0.52	-2.25	33	-51	107	99	0.016	0.016	8 (Qp)	Si	13
15	-1.55	-3.22	-0.01	-616	-157	73	160	0.014	0.014	7 (Fr)	Si	21

Muro : 71 - Nodi: [19-17-2064-2059], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
16	20.11	20.11	-4	256	6	6	Si	14
7	20.11	20.11	-3	775	6	6	Si	4.6

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
16	20.11	20.11	-4	280	8	8	Si	13
7	20.11	20.11	-2	841	8	8	Si	4.3

Verifica aperture fessure:Wamm_Freq[mm]=0.300 Wamm_Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
4	5.62	9.40	-2.32	174	-761	287	814	0.170	0.170	8 (Qp)	Si	1.2
4	5.36	9.11	-2.22	184	-736	282	789	0.162	0.162	7 (Fr)	Si	1.9

Muro : 72 - Nodi: [21-19-2059-2065], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	20.11	20.11	-9	48	6	6	Si	25
16	20.11	20.11	-7	1199	6	6	Si	3.0

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	20.11	20.11	-10	36	8	8	Si	18
16	20.11	20.11	-8	1316	8	8	Si	2.7

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
15	-0.95	4.00	0.52	176	-442	-122	791	0.120	0.120	8 (Qp)	Si	1.7
15	-1.03	3.88	0.51	168	-435	-119	771	0.116	0.116	7 (Fr)	Si	2.6

Muro : 73 - Nodi: [23-21-2065-2067], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
12	20.11	20.11	-19	733	6	6	Si	4.9
4	20.11	20.11	-12	1578	6	6	Si	2.3

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
12	20.11	20.11	-21	790	8	8	Si	4.6
4	20.11	20.11	-14	1758	8	8	Si	2.0

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	0.56	5.70	-1.78	-166	-532	83	1062	0.170	0.170	8 (Qp)	Si	1.2
3	0.46	5.55	-1.69	-172	-520	80	1035	0.166	0.166	7 (Fr)	Si	1.8

Muro : 74 - Nodi: [25-23-2067-2069], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	20.11	20.11	-20	942	6	6	Si	3.8
16	20.11	20.11	-18	1538	6	6	Si	2.3

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	20.11	20.11	-23	1083	8	8	Si	3.3
16	20.11	20.11	-21	1716	8	8	Si	2.1

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
14	-0.48	3.23	-1.00	-178	-199	35	534	0.096	0.096	8 (Qp)	Si	2.1

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
14	-0.54	3.17	-0.94	-182	-197	33	525	0.095	0.095	7 (Fr)	Si	3.2

Muro : 75 - Nodi: [27-25-2069-2072], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-20	944	6	6	Si	3.8
4	20.11	20.11	-14	1429	6	6	Si	2.5

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-23	1095	8	8	Si	3.3
4	20.11	20.11	-16	1657	8	8	Si	2.2

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
3	0.93	5.54	-0.46	-2	-517	-9	1032	0.166	0.166	8 (Qp)	Si	1.2
3	0.82	5.29	-0.42	-6	-496	-9	986	0.158	0.158	7 (Fr)	Si	1.9

Muro : 76 - Nodi: [29-27-2072-2074], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
12	20.11	20.11	-13	1069	6	6	Si	3.4
16	20.11	20.11	-10	1414	6	6	Si	2.5

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
12	20.11	20.11	-15	1244	8	8	Si	2.9
16	20.11	20.11	-12	1637	8	8	Si	2.2

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
15	1.13	6.07	0.50	4	-455	-36	1056	0.181	0.181	8 (Qp)	Si	1.1
15	1.02	5.82	0.50	1	-433	-36	1011	0.174	0.174	7 (Fr)	Si	1.7

Muro : 77 - Nodi: [31-29-2074-2076], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-9	825	6	6	Si	4.4

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-11	986	8	8	Si	3.7

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
14	-0.54	2.96	1.48	45	-108	4	440	0.089	0.089	8 (Qp)	Si	2.2
14	-0.61	2.80	1.46	50	-102	4	416	0.085	0.085	7 (Fr)	Si	3.5

Muro : 78 - Nodi: [33-31-2076-2078], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-4	267	6	6	Si	13
16	20.11	20.11	-2	687	6	6	Si	5.2

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-4	315	8	8	Si	11
16	20.11	20.11	-2	881	8	8	Si	4.1

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
16	-0.07	5.78	1.11	-112	-244	-161	881	0.174	0.174	8 (Qp)	Si	1.2
16	-0.20	5.45	1.04	-110	-197	-158	808	0.164	0.164	7 (Fr)	Si	1.8

Muro : 79 - Nodi: [2-33-2078-2079], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-6	59	6	6	Si	40
16	20.11	20.11	-2	243	6	6	Si	15

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-5	15	8	8	Si	31
15	20.11	20.11	-1	250	8	8	Si	14

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
15	-1.45	1.58	2.54	-4	-81	28	250	0.047	0.047	8 (Qp)	Si	4.2
15	-1.56	1.51	2.45	-0	-68	29	232	0.045	0.045	7 (Fr)	Si	6.6

Muro : 80 - Nodi: [53-1-2058-2070], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
12	20.11	20.11	-36	1160	6	6	Si	3.1
16	20.11	20.11	-35	1393	6	6	Si	2.6

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
12	20.11	20.11	-35	1132	8	8	Si	3.2
16	20.11	20.11	-34	1385	8	8	Si	2.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
16	-0.80	0.42	0.49	72	-2975	446	1385	0.155	0.155	8 (Qp)	Si	1.3
16	-0.86	0.36	0.46	72	-2979	443	1379	0.154	0.154	7 (Fr)	Si	1.9

Muro [Platea]: 81 - Nodi: [10-12-34-35]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cmq]=224$ $\sigma_{fa}[kg/cmq]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-11	701	6	6	Si	5.1
4	20.11	20.11	-7	838	6	6	Si	4.3

Combinazione QP: $\sigma_{ca}[kg/cmq]=168$ $\sigma_{fa}[kg/cmq]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-13	779	8	8	Si	4.6
4	20.11	20.11	-6	911	8	8	Si	4.0

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
6	3.44	-1.13	-1.00	-613	-906	-460	888	0.173	0.173	8 (Qp)	Si	1.2
6	3.33	-1.13	-0.99	-593	-917	-454	860	0.168	0.168	7 (Fr)	Si	1.8

Muro [Platea]: 82 - Nodi: [6-8-36-37]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cmq]=224$ $\sigma_{fa}[kg/cmq]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-12	620	6	6	Si	5.8
6	20.11	20.11	-7	855	6	6	Si	4.2

Combinazione QP: $\sigma_{ca}[kg/cmq]=168$ $\sigma_{fa}[kg/cmq]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-14	705	8	8	Si	5.1
6	20.11	20.11	-6	933	8	8	Si	3.9

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
6	3.26	-0.92	0.73	-857	-992	225	933	0.166	0.166	8 (Qp)	Si	1.2
6	3.16	-0.92	0.71	-833	-999	223	905	0.161	0.161	7 (Fr)	Si	1.9

Muro [Platea]: 83 - Nodi: [18-20-38-39]Pann=9Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cmq]=224$ $\sigma_{fa}[kg/cmq]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	20.11	20.11	-3	64	6	6	Si	56
4	20.11	20.11	-3	241	6	6	Si	15

Combinazione QP: $\sigma_{ca}[kg/cmq]=168$ $\sigma_{fa}[kg/cmq]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	20.11	20.11	-3	90	8	8	Si	40
4	20.11	20.11	-3	284	8	8	Si	13

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
4	-1.53	0.89	-1.63	-434	-322	-386	284	0.046	0.046	8 (Qp)	Si	4.4
4	-1.54	0.87	-1.58	-401	-287	-373	268	0.045	0.045	7 (Fr)	Si	6.7

Muro [Platea]: 84 - Nodi: [4-6-37-40]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	20.11	20.11	-10	437	6	6	Si	8.2
7	20.11	20.11	-3	533	6	6	Si	6.8

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	20.11	20.11	-12	508	8	8	Si	7.1
7	20.11	20.11	-3	595	8	8	Si	6.1

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
5	1.88	-0.55	1.55	-655	-501	342	591	0.097	0.097	8 (Qp)	Si	2.1
5	1.81	-0.55	1.51	-634	-509	336	570	0.093	0.093	7 (Fr)	Si	3.2

Muro [Platea]: 85 - Nodi: [3-4-40-41] Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	20.11	20.11	-8	341	6	6	Si	11
7	20.11	20.11	-3	444	6	6	Si	8.1

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	20.11	20.11	-9	410	8	8	Si	8.8
7	20.11	20.11	-3	504	8	8	Si	7.1

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
7	1.54	-0.49	1.55	-596	-437	500	504	0.080	0.080	8 (Qp)	Si	2.5
7	1.48	-0.49	1.50	-576	-448	487	486	0.077	0.077	7 (Fr)	Si	3.9

Muro [Platea]: 86 - Nodi: [12-42-34] Pann=3Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-11	506	6	6	Si	7.1
2	20.11	20.11	-7	763	6	6	Si	4.7

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-12	580	8	8	Si	6.2
2	20.11	20.11	-7	840	8	8	Si	4.3

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
2	-1.28	2.87	0.96	-1080	-814	405	840	0.146	0.146	8 (Qp)	Si	1.4
2	-1.26	2.77	0.95	-1072	-785	400	811	0.141	0.141	7 (Fr)	Si	2.1

Muro [Platea]: 87 - Nodi: [14-16-43-44] Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cmq]=224$ $\sigma_{fa}[kg/cmq]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	20.11	20.11	-6	286	6	6	Si	13
1	20.11	20.11	-4	303	6	6	Si	12

Combinazione QP: $\sigma_{ca}[kg/cmq]=168$ $\sigma_{fa}[kg/cmq]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	20.11	20.11	-8	330	8	8	Si	11
1	20.11	20.11	-4	357	8	8	Si	10

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
2	0.05	-0.13	-2.27	-811	-1143	-372	330	0.044	0.044	8 (Qp)	Si	4.6
2	0.00	-0.12	-2.22	-774	-1085	-364	314	0.042	0.042	7 (Fr)	Si	7.2

Muro [Platea]: 88 - Nodi: [8-10-35-36]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cmq]=224$ $\sigma_{fa}[kg/cmq]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	20.11	20.11	-13	772	6	6	Si	4.7
3	20.11	20.11	-8	864	6	6	Si	4.2

Combinazione QP: $\sigma_{ca}[kg/cmq]=168$ $\sigma_{fa}[kg/cmq]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	20.11	20.11	-14	852	8	8	Si	4.2
3	20.11	20.11	-8	940	8	8	Si	3.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
1	3.38	-1.12	0.20	-774	-1148	149	929	0.171	0.171	8 (Qp)	Si	1.2
1	3.28	-1.11	0.20	-752	-1152	145	901	0.166	0.166	7 (Fr)	Si	1.8

Muro [Platea]: 89 - Nodi: [16-18-39-43]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cmq]=224$ $\sigma_{fa}[kg/cmq]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	20.11	20.11	-5	164	6	6	Si	22

Combinazione QP: $\sigma_{ca}[kg/cmq]=168$ $\sigma_{fa}[kg/cmq]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	20.11	20.11	-6	202	8	8	Si	18
8	20.11	20.11	-5	206	8	8	Si	18

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
8	0.71	-1.20	-1.87	-196	-824	-255	206	0.036	0.036	8 (Qp)	Si	5.6
8	0.64	-1.17	-1.85	-171	-773	-249	184	0.033	0.033	7 (Fr)	Si	9.2

Muro [Platea]: 90 - Nodi: [12-14-44-42]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cmq]=224$ $\sigma_{fa}[kg/cmq]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	20.11	20.11	-10	620	6	6	Si	5.8
1	20.11	20.11	-5	728	6	6	Si	4.9

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	20.11	20.11	-11	700	8	8	Si	5.1
1	20.11	20.11	-4	799	8	8	Si	4.5

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
1	2.65	-0.68	-1.50	-822	-699	-518	799	0.136	0.136	8 (Qp)	Si	1.5
1	2.55	-0.68	-1.48	-799	-708	-513	772	0.131	0.131	7 (Fr)	Si	2.3

Muro [Platea]: 91 - Nodi: [30-32-45-46]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	20.11	20.11	-3	138	6	6	Si	26

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	20.11	20.11	-3	175	8	8	Si	21

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
8	-0.48	0.12	1.93	-351	-484	397	175	0.024	0.024	8 (Qp)	Si	8.3
8	-0.48	0.10	1.88	-331	-458	387	163	0.022	0.022	7 (Fr)	Si	13

Muro [Platea]: 92 - Nodi: [20-22-47-38]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-2	31	6	6	Si	>100
2	20.11	20.11	-1	114	6	6	Si	31

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-2	57	8	8	Si	64
2	20.11	20.11	-2	150	8	8	Si	24

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
2	-1.16	0.50	-1.68	-175	-152	-363	150	0.026	0.026	8 (Qp)	Si	7.8
2	-1.18	0.49	-1.63	-151	-120	-352	138	0.025	0.025	7 (Fr)	Si	12

Muro [Platea]: 93 - Nodi: [22-24-48-49]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
1	20.11	20.11	-3	202	6	6	Si	18

Combinazione QP: $\sigma_{ca}[\text{kg/cm}^2]=168$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-3	247	8	8	Si	15

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
2	-1.61	0.71	-0.37	-145	160	-105	194	0.036	0.036	8 (Qp)	Si	5.6
2	-1.61	0.69	-0.34	-123	179	-100	196	0.035	0.035	7 (Fr)	Si	8.6

Muro [Platea]: 94 - Nodi: [22-49-47]Pann=3Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[\text{kg/cm}^2]=224$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	20.11	20.11	-2	129	6	6	Si	28

Combinazione QP: $\sigma_{ca}[\text{kg/cm}^2]=168$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	20.11	20.11	-2	148	8	8	Si	24

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	0.19	-0.39	1.46	14	100	216	43	0.010	0.010	8 (Qp)	Si	21
1	0.19	-0.43	1.42	39	114	213	51	0.010	0.010	7 (Fr)	Si	31

Muro [Platea]: 95 - Nodi: [24-26-50-48]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[\text{kg/cm}^2]=224$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
7	20.11	20.11	-3	218	6	6	Si	17
8	20.11	20.11	-2	245	6	6	Si	15

Combinazione QP: $\sigma_{ca}[\text{kg/cm}^2]=168$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
7	20.11	20.11	-3	270	8	8	Si	13

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	-1.68	0.90	-0.37	-111	226	4	254	0.046	0.046	8 (Qp)	Si	4.4
8	-1.66	0.87	-0.35	-95	236	6	252	0.044	0.044	7 (Fr)	Si	6.8

Muro [Platea]: 96 - Nodi: [26-28-51-50]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[\text{kg/cm}^2]=224$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
7	20.11	20.11	-2	66	6	6	Si	55
8	20.11	20.11	-1	177	6	6	Si	20

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
7	20.11	20.11	-3	115	8	8	Si	31
8	20.11	20.11	-2	183	8	8	Si	20

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	-1.36	0.75	0.93	-88	99	188	183	0.038	0.038	8 (Qp)	Si	5.3
8	-1.35	0.72	0.91	-75	111	183	180	0.036	0.036	7 (Fr)	Si	8.3

Muro [Platea]: 97 - Nodi: [28-30-46-51]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
7	20.11	20.11	-3	242	6	6	Si	15

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	20.11	20.11	-3	240	8	8	Si	15
7	20.11	20.11	-3	300	8	8	Si	12

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	-1.76	1.19	0.92	-393	-12	226	240	0.060	0.060	8 (Qp)	Si	3.3
8	-1.73	1.14	0.90	-372	1	222	227	0.057	0.057	7 (Fr)	Si	5.2

Muro [Platea]: 98 - Nodi: [52-41-40]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	0	218	6	6	Si	17
2	20.11	20.11	0	256	6	6	Si	14

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	0	272	8	8	Si	13
2	20.11	20.11	0	314	8	8	Si	11

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
2	1.09	0.83	-0.16	-291	-139	47	314	0.056	0.056	8 (Qp)	Si	3.6
2	1.03	0.76	-0.15	-272	-123	43	294	0.052	0.052	7 (Fr)	Si	5.8

Muro [Platea]: 99 - Nodi: [32-3-41-45]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	20.11	20.11	-4	266	6	6	Si	14

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	20.11	20.11	-5	313	8	8	Si	11

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	-0.62	0.40	1.86	-725	-748	439	313	0.044	0.044	8 (Qp)	Si	4.5
8	-0.63	0.37	1.80	-694	-715	429	297	0.042	0.042	7 (Fr)	Si	7.2

Muro [Platea]: 100 - Nodi: [52-40-37]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	0	252	6	6	Si	14
2	20.11	20.11	0	287	6	6	Si	13

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	0	307	8	8	Si	12
2	20.11	20.11	0	346	8	8	Si	10

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
2	1.20	0.98	-0.21	-324	-199	65	346	0.061	0.061	8 (Qp)	Si	3.3
2	1.13	0.90	-0.20	-305	-182	62	326	0.058	0.058	7 (Fr)	Si	5.2

Muro [Platea]: 101 - Nodi: [52-43-39]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	0	150	6	6	Si	24
2	20.11	20.11	0	201	6	6	Si	18

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	0	211	8	8	Si	17
2	20.11	20.11	0	265	8	8	Si	14

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	0.83	0.78	0.20	-246	-216	-36	247	0.043	0.043	8 (Qp)	Si	4.7
3	0.76	0.71	0.20	-224	-196	-36	225	0.039	0.039	7 (Fr)	Si	7.7

Muro [Platea]: 102 - Nodi: [52-44-43]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	0	212	6	6	Si	17
2	20.11	20.11	0	268	6	6	Si	13

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	0	275	8	8	Si	13
2	20.11	20.11	0	334	8	8	Si	11

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
2	0.58	1.07	0.36	-174	-365	-69	334	0.055	0.055	8 (Qp)	Si	3.6
2	0.51	0.99	0.36	-156	-342	-70	311	0.051	0.051	7 (Fr)	Si	5.9

Muro [Platea]: 103 - Nodi: [52-39-38] Pann=3Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm] = 224 σ_{fa} [kg/cm] = 3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				
1	20.11	20.11	-0	114	6	6	Si	32
2	20.11	20.11	0	183	6	6	Si	20

Combinazione QP: σ_{ca} [kg/cm] = 168 σ_{fa} [kg/cm] = 3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				
1	20.11	20.11	0	176	8	8	Si	20
2	20.11	20.11	0	243	8	8	Si	15

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
2	0.82	0.69	0.12	-242	-181	-18	243	0.042	0.042	8 (Qp)	Si	4.8
2	0.74	0.61	0.12	-222	-161	-18	221	0.038	0.038	7 (Fr)	Si	7.9

Muro [Platea]: 104 - Nodi: [52-42-44] Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm] = 224 σ_{fa} [kg/cm] = 3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				
1	20.11	20.11	0	297	6	6	Si	12
2	20.11	20.11	0	342	6	6	Si	11

Combinazione QP: σ_{ca} [kg/cm] = 168 σ_{fa} [kg/cm] = 3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				
1	20.11	20.11	0	364	8	8	Si	9.9
2	20.11	20.11	0	411	8	8	Si	8.8

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
2	0.60	1.34	0.31	-181	-438	-54	411	0.069	0.069	8 (Qp)	Si	2.9
2	0.53	1.25	0.31	-162	-415	-55	387	0.064	0.064	7 (Fr)	Si	4.7

Muro [Platea]: 105 - Nodi: [52-37-36] Pann=3Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm] = 224 σ_{fa} [kg/cm] = 3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				
1	20.11	20.11	0	324	6	6	Si	11

Combinazione QP: σ_{ca} [kg/cm] = 168 σ_{fa} [kg/cm] = 3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	0	397	8	8	Si	9.1

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	1.11	1.35	-0.28	-289	-386	63	397	0.069	0.069	8 (Qp)	Si	2.9
1	1.04	1.27	-0.27	-271	-361	62	372	0.065	0.065	7 (Fr)	Si	4.6

Muro [Platea]: 106 - Nodi: [52-36-35]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	0	357	6	6	Si	10
7	20.11	20.11	0	359	6	6	Si	10

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	0	430	8	8	Si	8.4
7	20.11	20.11	0	432	8	8	Si	8.3

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
7	1.06	1.50	-0.25	-271	-403	56	432	0.076	0.076	8 (Qp)	Si	2.6
7	0.99	1.42	-0.24	-254	-379	56	407	0.072	0.072	7 (Fr)	Si	4.2

Muro [Platea]: 107 - Nodi: [52-35-34]Pann=3Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	0	425	6	6	Si	8.5

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	0	497	8	8	Si	7.2

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	0.93	1.72	-0.16	-251	-469	53	497	0.087	0.087	8 (Qp)	Si	2.3
1	0.85	1.63	-0.16	-232	-446	51	472	0.083	0.083	7 (Fr)	Si	3.6

Muro [Platea]: 108 - Nodi: [52-34-42]Pann=3Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	0	418	6	6	Si	8.6
2	20.11	20.11	0	469	6	6	Si	7.7

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	0	489	8	8	Si	7.4

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
2	20.11	20.11	0	542	8	8	Si	6.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
2	0.66	1.91	0.04	-178	-487	-16	542	0.097	0.097	8 (Qp)	Si	2.1
2	0.60	1.82	0.04	-161	-463	-18	516	0.092	0.092	7 (Fr)	Si	3.2

Muro [Platea]: 109 - Nodi: [52-38-47]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
6	20.11	20.11	-0	107	6	6	Si	34
3	20.11	20.11	0	169	6	6	Si	21

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
6	20.11	20.11	-0	154	8	8	Si	23
3	20.11	20.11	0	226	8	8	Si	16

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	0.76	0.60	0.04	-227	-171	7	226	0.039	0.039	8 (Qp)	Si	5.2
3	0.69	0.53	0.04	-208	-151	7	206	0.035	0.035	7 (Fr)	Si	8.5

Muro [Platea]: 110 - Nodi: [52-47-49]Pann=3Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	-0	85	6	6	Si	42
3	20.11	20.11	0	141	6	6	Si	26

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	-0	129	8	8	Si	28
3	20.11	20.11	0	197	8	8	Si	18

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	0.65	0.69	-0.02	-205	-182	23	197	0.035	0.035	8 (Qp)	Si	5.7
3	0.58	0.61	-0.02	-186	-162	23	175	0.031	0.031	7 (Fr)	Si	9.7

Muro [Platea]: 111 - Nodi: [52-51-46]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
7	20.11	20.11	-0	99	6	6	Si	36
3	20.11	20.11	0	169	6	6	Si	21

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
1	20.11	20.11	0	152	8	8	Si	24
3	20.11	20.11	0	227	8	8	Si	16

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	0.64	0.79	-0.03	-180	-210	-10	227	0.040	0.040	8 (Qp)	Si	5.0
3	0.56	0.72	-0.03	-160	-192	-10	207	0.037	0.037	7 (Fr)	Si	8.2

Muro [Platea]: 112 - Nodi: [52-50-51]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
7	20.11	20.11	-0	70	6	6	Si	51
3	20.11	20.11	0	160	6	6	Si	23

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
7	20.11	20.11	-0	119	8	8	Si	30
3	20.11	20.11	0	217	8	8	Si	17

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	0.56	0.75	-0.06	-166	-203	5	217	0.038	0.038	8 (Qp)	Si	5.2
3	0.50	0.68	-0.06	-146	-184	6	197	0.035	0.035	7 (Fr)	Si	8.6

Muro [Platea]: 113 - Nodi: [52-48-50]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
6	20.11	20.11	-0	57	6	6	Si	64
3	20.11	20.11	0	147	6	6	Si	24

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
7	20.11	20.11	-0	100	8	8	Si	36
3	20.11	20.11	0	206	8	8	Si	17

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	0.54	0.71	-0.09	-165	-194	18	206	0.036	0.036	8 (Qp)	Si	5.5
3	0.48	0.64	-0.09	-146	-175	19	185	0.033	0.033	7 (Fr)	Si	9.2

Muro [Platea]: 114 - Nodi: [52-46-45]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	20.11	20.11	-0	160	6	6	Si	23
3	20.11	20.11	0	168	6	6	Si	21

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	0	186	8	8	Si	19
3	20.11	20.11	0	227	8	8	Si	16

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
3	0.75	0.80	-0.00	-206	-208	-20	227	0.040	0.040	8 (Qp)	Si	4.9
3	0.67	0.73	0.00	-185	-190	-20	207	0.037	0.037	7 (Fr)	Si	8.1

Muro [Platea]: 115 - Nodi: [52-49-48]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				
7	20.11	20.11	-0	45	6	6	Si	80
3	20.11	20.11	0	137	6	6	Si	26

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				
7	20.11	20.11	-0	87	8	8	Si	41
3	20.11	20.11	0	198	8	8	Si	18

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
3	0.58	0.68	-0.08	-181	-189	26	198	0.035	0.035	8 (Qp)	Si	5.7
3	0.51	0.61	-0.09	-162	-169	27	177	0.031	0.031	7 (Fr)	Si	9.7

Muro [Platea]: 116 - Nodi: [52-45-41]Pann=8Spess.=40 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				
1	20.11	20.11	0	176	6	6	Si	20
2	20.11	20.11	0	212	6	6	Si	17

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				
1	20.11	20.11	0	230	8	8	Si	16
2	20.11	20.11	0	270	8	8	Si	13

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
2	0.94	0.68	-0.12	-250	-100	41	270	0.048	0.048	8 (Qp)	Si	4.2
2	0.87	0.61	-0.12	-231	-86	37	250	0.044	0.044	7 (Fr)	Si	6.8

Muro : 117 - Nodi: [1-19-2059-2058], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				
16	20.11	20.11	-17	1379	6	6	Si	2.6

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
16	20.11	20.11	-19	1473	8	8	Si	2.4

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	9.54	1.86	3.89	69	72	-47	729	0.107	0.107	8 (Qp)	Si	1.9
1	9.42	1.82	3.84	76	75	-46	722	0.106	0.106	7 (Fr)	Si	2.8

Muro [Platea]: 118 - Nodi: [2062-2011-2057]Pann=19Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
5	31.42	31.42	-17	321	6	6	Si	11

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
5	31.42	31.42	-17	326	8	8	Si	9.9

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
5	-2.90	-2.68	0.94	4687	1465	391	326	0.037	0.037	8 (Qp)	Si	5.3
5	-2.93	-2.71	0.91	4676	1503	412	321	0.037	0.037	7 (Fr)	Si	8.2

Muro [Platea]: 119 - Nodi: [2062-2057-2054]Pann=17Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	31.42	31.42	-16	326	6	6	Si	11

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	31.42	31.42	-15	328	8	8	Si	11

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
4	-2.39	-3.44	0.86	4274	1708	-1010	328	0.038	0.038	8 (Qp)	Si	5.2
4	-2.45	-3.43	0.84	4291	1723	-977	324	0.038	0.038	7 (Fr)	Si	8.0

Muro [Platea]: 120 - Nodi: [2086-2014-2062]Pann=16Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
7	31.42	31.42	-13	27	6	6	Si	17

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
7	31.42	31.42	-13	31	8	8	Si	13

Verifica aperture fessure:Wamm_Freq[mm]=0.300 Wamm_Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
7	-5.44	-2.25	0.04	3647	1122	-115	31	0.002	0.002	8 (Qp)	Si	89
7	-5.48	-2.27	0.01	3631	1125	-95	29	0.002	0.002	7 (Fr)	Si	>100

Muro : 121 - Nodi: [53-2070-2071-11], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
13	20.11	20.11	-21	-70	6	6	Si	11
16	20.11	20.11	-10	806	6	6	Si	4.5

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
13	20.11	20.11	-21	-69	8	8	Si	8.0
16	20.11	20.11	-10	798	8	8	Si	4.5

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
15	-0.74	-1.18	0.86	-1029	-220	229	347	0.037	0.037	8 (Qp)	Si	5.4
15	-0.73	-1.16	0.85	-1036	-223	228	352	0.038	0.038	7 (Fr)	Si	7.9

Muro [Platea]: 122 - Nodi: [2007-2036-2042]Pann=42Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
21	31.42	31.42	-14	358	6	6	Si	10

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
21	31.42	31.42	-13	333	8	8	Si	11

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
21	-1.68	-1.70	-0.53	-3700	-2417	-1431	333	0.040	0.040	8 (Qp)	Si	5.0
21	-1.68	-1.71	-0.55	-3705	-2438	-1437	335	0.040	0.040	7 (Fr)	Si	7.4

Muro [Platea]: 123 - Nodi: [2043-2008-2049-2048]Pann=16Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
13	31.42	31.42	-8	271	6	6	Si	13

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
13	31.42	31.42	-8	257	8	8	Si	14

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
13	-0.83	-1.07	-0.28	-4902	-268	-888	257	0.034	0.034	8 (Qp)	Si	6.0
13	-0.84	-1.07	-0.29	-4874	-292	-857	253	0.033	0.033	7 (Fr)	Si	9.1

Muro [Platea]: 124 - Nodi: [2042-2043-2048-2047]Pann=8Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-8	30	6	6	Si	30

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-7	35	8	8	Si	23

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
5	-2.80	-1.64	-0.54	-5205	768	-1836	35	0.003	0.003	8 (Qp)	Si	59
5	-2.82	-1.62	-0.52	-5180	745	-1793	33	0.003	0.003	7 (Fr)	Si	95

Muro [Platea]: 125 - Nodi: [2015-2086-2062]Pann=15Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	31.42	31.42	-12	8	6	6	Si	19
12	31.42	31.42	-11	12	6	6	Si	20

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	31.42	31.42	-11	7	8	8	Si	15
12	31.42	31.42	-11	10	8	8	Si	15

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
12	-5.17	-2.97	-1.18	3067	1448	686	10	0.001	0.001	8 (Qp)	Si	>100
12	-5.14	-3.00	-1.19	3065	1471	703	11	0.001	0.001	7 (Fr)	Si	>100

Muro [Platea]: 126 - Nodi: [2015-2090-2086]Pann=9Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-10	-5	6	6	Si	22
6	31.42	31.42	-8	3	6	6	Si	28

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-10	-7	8	8	Si	17
6	31.42	31.42	-8	2	8	8	Si	20

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
6	-2.89	-4.21	-0.72	1621	2137	510	2	0.000	0.000	8 (Qp)	Si	>100
6	-2.85	-4.17	-0.71	1606	2112	515	2	0.000	0.000	7 (Fr)	Si	>100

Muro [Platea]: 127 - Nodi: [2090-2089-2086]Pann=42Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
14	31.42	31.42	-11	-3	6	6	Si	21
12	31.42	31.42	-8	10	6	6	Si	28

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
14	31.42	31.42	-10	-3	8	8	Si	16
12	31.42	31.42	-8	11	8	8	Si	21

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
12	-4.67	-2.57	-0.46	1762	1647	292	11	0.001	0.001	8 (Qp)	Si	>100
12	-4.70	-2.58	-0.44	1792	1650	290	11	0.001	0.001	7 (Fr)	Si	>100

Muro [Platea]: 128 - Nodi: [2089-2085-2086]Pann=12Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
5	31.42	31.42	-9	-11	6	6	Si	24
1	31.42	31.42	-9	-15	6	6	Si	25

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
5	31.42	31.42	-9	-10	8	8	Si	18
1	31.42	31.42	-9	-14	8	8	Si	19

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	-4.90	-2.62	1.20	2163	462	-398	0	0.000	0.000	8 (Qp)	Si	>100
1	-4.92	-2.69	1.19	2176	515	-404	0	0.000	0.000	7 (Fr)	Si	>100

Muro [Platea]: 129 - Nodi: [2050-2054-2049]Pann=10Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
5	31.42	31.42	-5	65	6	6	Si	50

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
5	31.42	31.42	-5	85	8	8	Si	34

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
5	-1.03	-1.59	0.41	3245	-2323	1793	85	0.011	0.011	8 (Qp)	Si	18
5	-1.04	-1.61	0.43	3171	-2297	1754	77	0.010	0.010	7 (Fr)	Si	30

Muro [Platea]: 130 - Nodi: [2049-2054-2057]Pann=12Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
8	31.42	31.42	-10	324	6	6	Si	11

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
8	31.42	31.42	-10	334	8	8	Si	11

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	-1.32	-1.16	0.22	-2727	6544	1283	334	0.044	0.044	8 (Qp)	Si	4.6
8	-1.38	-1.18	0.22	-2630	6573	1313	333	0.043	0.043	7 (Fr)	Si	6.9

Muro [Platea]: 131 - Nodi: [2048-2049-2057]Pann=12Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
9	31.42	31.42	-11	421	6	6	Si	8.6
10	31.42	31.42	-9	432	6	6	Si	8.3

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
9	31.42	31.42	-10	418	8	8	Si	8.6
3	31.42	31.42	-9	443	8	8	Si	8.1

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	-1.68	-0.34	0.47	-1693	5736	-292	443	0.058	0.058	8 (Qp)	Si	3.5
10	-1.74	-0.29	-0.23	-1775	5502	-2691	432	0.056	0.056	7 (Fr)	Si	5.3

Muro [Platea]: 132 - Nodi: [2048-2057-2056]Pann=10Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
3	31.42	31.42	-8	395	6	6	Si	9.1

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
3	31.42	31.42	-8	413	8	8	Si	8.7

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	-0.79	-0.29	0.43	-395	5285	3231	413	0.054	0.054	8 (Qp)	Si	3.7
3	-0.82	-0.31	0.47	-258	5287	3241	409	0.053	0.053	7 (Fr)	Si	5.6

Muro [Platea]: 133 - Nodi: [2048-2056-2053]Pann=9Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-9	520	6	6	Si	6.9

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-10	600	8	8	Si	6.0

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
2	0.03	-1.48	1.19	6516	-633	3354	600	0.078	0.078	8 (Qp)	Si	2.6
2	-0.03	-1.51	1.15	6337	-640	3269	570	0.074	0.074	7 (Fr)	Si	4.0

Muro [Platea]: 134 - Nodi: [2047-2048-2053]Pann=7Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
3	31.42	31.42	-8	197	6	6	Si	18

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
3	31.42	31.42	-8	234	8	8	Si	15

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
3	-1.83	-1.07	-0.51	-1542	5187	-1995	234	0.031	0.031	8 (Qp)	Si	6.6
3	-1.86	-1.09	-0.48	-1549	5061	-1944	220	0.029	0.029	7 (Fr)	Si	10

Muro [Platea]: 135 - Nodi: [2056-2057-2011-2060]Pann=8Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-8	471	6	6	Si	7.6

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-8	446	8	8	Si	8.1

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
5	-0.84	0.00	-0.98	294	4892	-1770	446	0.058	0.058	8 (Qp)	Si	3.4
5	-0.84	0.02	-0.97	351	4972	-1684	458	0.060	0.060	7 (Fr)	Si	5.0

Muro [Platea]: 136 - Nodi: [2088-2085-2089]Pann=27Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
14	31.42	31.42	-9	-3	6	6	Si	24
9	31.42	31.42	-8	22	6	6	Si	26

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
14	31.42	31.42	-9	-2	8	8	Si	18
9	31.42	31.42	-8	21	8	8	Si	21

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
9	-2.96	-3.42	0.91	1366	2317	-462	21	0.002	0.002	8 (Qp)	Si	>100
9	-3.02	-3.46	0.86	1394	2348	-449	21	0.002	0.002	7 (Fr)	Si	>100

Muro [Platea]: 137 - Nodi: [2009-2052-2050]Pann=28Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
6	31.42	31.42	-10	88	6	6	Si	22
18	31.42	31.42	-3	229	6	6	Si	16

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
6	31.42	31.42	-10	92	8	8	Si	17
18	31.42	31.42	-3	203	8	8	Si	18

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
9	-1.46	-3.15	-0.65	2311	1426	988	157	0.018	0.018	8 (Qp)	Si	11
9	-1.47	-3.19	-0.63	2271	1414	975	151	0.017	0.017	7 (Fr)	Si	17

Muro [Platea]: 138 - Nodi: [2052-2054-2050]Pann=14Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-14	184	6	6	Si	16
6	31.42	31.42	-14	197	6	6	Si	16

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-14	188	8	8	Si	12
6	31.42	31.42	-14	207	8	8	Si	12

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
6	-3.00	-2.25	-0.42	3902	1574	41	207	0.022	0.022	8 (Qp)	Si	8.9
6	-3.02	-2.28	-0.45	3884	1574	62	202	0.022	0.022	7 (Fr)	Si	14

Muro [Platea]: 139 - Nodi: [2012-2054-2052]Pann=31Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
6	31.42	31.42	-13	176	6	6	Si	17
20	31.42	31.42	-5	286	6	6	Si	13

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
6	31.42	31.42	-13	180	8	8	Si	13
20	31.42	31.42	-5	291	8	8	Si	12

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
20	0.31	-0.89	0.44	-1564	-154	1079	291	0.038	0.038	8 (Qp)	Si	5.3
20	0.27	-0.90	0.40	-1550	-148	1097	283	0.037	0.037	7 (Fr)	Si	8.1

Muro [Platea]: 140 - Nodi: [2009-2012-2052]Pann=29Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-8	75	6	6	Si	29
17	31.42	31.42	-1	225	6	6	Si	16

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-8	75	8	8	Si	22
8	31.42	31.42	-1	216	8	8	Si	17

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
17	-0.86	0.88	-0.44	-36	-476	374	215	0.031	0.031	8 (Qp)	Si	6.4
17	-0.91	0.88	-0.41	-17	-477	360	215	0.031	0.031	7 (Fr)	Si	9.5

Muro [Platea]: 141 - Nodi: [2079-2078-2084]Pann=8Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
3	31.42	31.42	-8	-5	6	6	Si	27
2	31.42	31.42	-7	6	6	6	Si	34

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
3	31.42	31.42	-9	23	8	8	Si	18
2	31.42	31.42	-7	45	8	8	Si	24

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
2	-3.25	0.05	1.01	-1908	-241	-213	45	0.006	0.006	8 (Qp)	Si	34
2	-3.45	0.00	0.98	-1777	-195	-178	31	0.004	0.004	7 (Fr)	Si	75

Muro [Platea]: 142 - Nodi: [2083-2079-2084]Pann=8Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-16	238	6	6	Si	14
8	31.42	31.42	-15	263	6	6	Si	14

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-16	272	8	8	Si	11
8	31.42	31.42	-15	307	8	8	Si	12

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	-2.25	-1.44	-0.21	4009	24	-201	307	0.036	0.036	8 (Qp)	Si	5.6
8	-2.40	-1.53	-0.28	4021	90	-180	290	0.033	0.033	7 (Fr)	Si	9.0

Muro [Platea]: 143 - Nodi: [2083-2077-2079]Pann=8Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
3	31.42	31.42	-10	319	6	6	Si	11
8	31.42	31.42	-6	387	6	6	Si	9.3

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
3	31.42	31.42	-9	315	8	8	Si	11
8	31.42	31.42	-6	385	8	8	Si	9.3

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	0.66	-4.36	-0.73	1813	390	-524	385	0.050	0.050	8 (Qp)	Si	4.0
8	0.62	-4.47	-0.66	1860	454	-505	386	0.050	0.050	7 (Fr)	Si	6.0

Muro [Platea]: 144 - Nodi: [2088-2083-2084]Pann=13Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
9	31.42	31.42	-11	-6	6	6	Si	21
8	31.42	31.42	-10	3	6	6	Si	21

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
9	31.42	31.42	-10	-6	8	8	Si	17
8	31.42	31.42	-10	7	8	8	Si	17

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	-2.07	-4.67	-1.07	860	2724	585	7	0.000	0.000	8 (Qp)	Si	>100
8	-2.12	-4.79	-1.03	884	2741	566	5	0.000	0.000	7 (Fr)	Si	>100

Muro [Platea]: 145 - Nodi: [2082-2075-2077]Pann=8Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	31.42	31.42	-10	437	6	6	Si	8.2
8	31.42	31.42	-8	484	6	6	Si	7.4

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	31.42	31.42	-10	427	8	8	Si	8.4
8	31.42	31.42	-8	472	8	8	Si	7.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	0.65	-3.56	-0.91	2386	1451	248	472	0.061	0.061	8 (Qp)	Si	3.3
8	0.62	-3.63	-0.86	2435	1503	265	475	0.062	0.062	7 (Fr)	Si	4.8

Muro [Platea]: 146 - Nodi: [2082-2077-2083]Pann=3Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	31.42	31.42	-14	227	6	6	Si	16

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	31.42	31.42	-14	231	8	8	Si	12

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	-2.67	-2.29	-2.56	3829	689	85	231	0.026	0.026	8 (Qp)	Si	7.8
1	-2.73	-2.35	-2.59	3852	746	87	229	0.025	0.025	7 (Fr)	Si	12

Muro [Platea]: 147 - Nodi: [2013-2082-2087]Pann=31Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
17	31.42	31.42	-10	88	6	6	Si	21
10	31.42	31.42	-5	301	6	6	Si	12

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
17	31.42	31.42	-10	82	8	8	Si	17
10	31.42	31.42	-5	288	8	8	Si	12

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
10	0.36	-1.13	-0.06	-1494	-26	-590	288	0.038	0.038	8 (Qp)	Si	5.3
10	0.36	-1.17	-0.07	-1498	-9	-583	289	0.038	0.038	7 (Fr)	Si	8.0

Muro [Platea]: 148 - Nodi: [2082-2083-2088]Pann=14Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
11	31.42	31.42	-10	-5	6	6	Si	21
9	31.42	31.42	-10	0	6	6	Si	23

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
11	31.42	31.42	-10	-5	8	8	Si	17
9	31.42	31.42	-9	1	8	8	Si	18

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
9	-5.24	-2.42	1.41	2287	1348	-818	1	0.000	0.000	8 (Qp)	Si	>100
9	-5.33	-2.46	1.39	2306	1353	-798	1	0.000	0.000	7 (Fr)	Si	>100

Muro [Platea]: 149 - Nodi: [2082-2088-2087]Pann=43Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
16	31.42	31.42	-11	-4	6	6	Si	21
26	31.42	31.42	-10	2	6	6	Si	22

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
16	31.42	31.42	-11	-6	8	8	Si	16
26	31.42	31.42	-10	2	8	8	Si	17

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
26	-2.32	-4.97	0.56	1311	2640	-204	2	0.000	0.000	8 (Qp)	Si	>100
26	-2.37	-4.99	0.58	1333	2651	-216	2	0.000	0.000	7 (Fr)	Si	>100

Muro [Platea]: 150 - Nodi: [2014-2085-2078]Pann=14Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
11	31.42	31.42	-4	-0	6	6	Si	54
4	31.42	31.42	-2	251	6	6	Si	14

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
11	31.42	31.42	-4	0	8	8	Si	44
4	31.42	31.42	-2	385	8	8	Si	9.4

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
4	-1.28	1.10	0.37	1262	-1141	-263	385	0.063	0.063	8 (Qp)	Si	3.2
4	-1.32	0.97	0.33	1302	-1002	-222	339	0.056	0.056	7 (Fr)	Si	5.4

Muro [Platea]: 151 - Nodi: [2085-2084-2078]Pann=11Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
6	31.42	31.42	-4	8	6	6	Si	54
10	31.42	31.42	-3	191	6	6	Si	19

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
6	31.42	31.42	-4	37	8	8	Si	41
10	31.42	31.42	-3	324	8	8	Si	11

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
10	0.78	-2.30	0.12	-1394	522	623	324	0.046	0.046	8 (Qp)	Si	4.3
10	0.65	-2.31	0.14	-1242	565	587	279	0.039	0.039	7 (Fr)	Si	7.6

Muro [Platea]: 152 - Nodi: [2078-2076-2014]Pann=13Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
7	31.42	31.42	-9	328	6	6	Si	11
5	31.42	31.42	-4	470	6	6	Si	7.7

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
7	31.42	31.42	-9	428	8	8	Si	8.4
5	31.42	31.42	-5	533	8	8	Si	6.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
5	0.72	-1.67	0.07	-3893	3198	602	533	0.069	0.069	8 (Qp)	Si	2.9
5	0.64	-1.70	0.07	-3730	3243	566	499	0.065	0.065	7 (Fr)	Si	4.6

Muro [Platea]: 153 - Nodi: [2014-2076-2074]Pann=10Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
5	31.42	31.42	-5	366	6	6	Si	9.8

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
5	31.42	31.42	-6	526	8	8	Si	6.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
5	-0.26	0.52	-0.31	157	-4355	2594	526	0.069	0.069	8 (Qp)	Si	2.9
5	-0.27	0.39	-0.31	221	-4088	2565	468	0.061	0.061	7 (Fr)	Si	4.9

Muro [Platea]: 154 - Nodi: [2014-2074-2072-2069-2067-2011]Pann=68Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
9	31.42	31.42	-10	753	6	6	Si	4.8

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
9	31.42	31.42	-10	873	8	8	Si	4.1

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
9	0.80	-0.39	-0.27	-7421	-1603	-3326	873	0.114	0.114	8 (Qp)	Si	1.8
9	0.72	-0.37	-0.26	-7130	-1496	-3166	826	0.108	0.108	7 (Fr)	Si	2.8

Muro [Platea]: 155 - Nodi: [1-15-13-11-53]Pann=27Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
10	20.11	20.11	-6	362	6	6	Si	9.9
12	20.11	20.11	-1	891	6	6	Si	4.0

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
10	20.11	20.11	-6	353	8	8	Si	10
12	20.11	20.11	-1	916	8	8	Si	3.9

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
12	2.99	-0.69	0.49	-699	290	383	916	0.190	0.190	8 (Qp)	Si	1.1
12	2.93	-0.68	0.48	-693	286	382	902	0.186	0.186	7 (Fr)	Si	1.6

Muro [Platea]: 156 - Nodi: [2010-2058-2070-2013]Pann=43Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
2	31.42	31.42	-20	540	6	6	Si	6.7
1	31.42	31.42	-17	610	6	6	Si	5.9

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
2	31.42	31.42	-20	502	8	8	Si	7.2
1	31.42	31.42	-16	574	8	8	Si	6.3

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	-0.79	-1.86	1.20	4457	1265	479	574	0.074	0.074	8 (Qp)	Si	2.7
1	-0.78	-1.92	1.19	4494	1291	472	581	0.075	0.075	7 (Fr)	Si	4.0

Muro [Platea]: 157 - Nodi: [2070-2071-2073]Pann=8Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
6	31.42	31.42	-19	223	6	6	Si	12

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
6	31.42	31.42	-18	214	8	8	Si	9.1

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
6	-4.72	-0.98	0.57	5253	1357	-1486	214	0.022	0.022	8 (Qp)	Si	9.1
6	-4.74	-0.99	0.55	5279	1379	-1500	216	0.022	0.022	7 (Fr)	Si	14

Muro [Platea]: 158 - Nodi: [2013-2070-2073]Pann=11Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
9	31.42	31.42	-13	412	6	6	Si	8.7

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
9	31.42	31.42	-12	389	8	8	Si	9.3

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
9	-0.92	-1.64	0.22	3377	909	1281	389	0.049	0.049	8 (Qp)	Si	4.1
9	-0.93	-1.68	0.24	3415	919	1282	393	0.050	0.050	7 (Fr)	Si	6.0

Muro [Platea]: 159 - Nodi: [2073-2075-2082]Pann=9Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
3	31.42	31.42	-13	116	6	6	Si	17
7	31.42	31.42	-11	436	6	6	Si	8.3

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
3	31.42	31.42	-13	115	8	8	Si	13
7	31.42	31.42	-10	410	8	8	Si	8.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
7	-0.35	-0.22	1.22	669	2851	837	410	0.053	0.053	8 (Qp)	Si	3.7
7	-0.42	-0.21	1.20	701	2893	827	417	0.054	0.054	7 (Fr)	Si	5.5

Muro [Platea]: 160 - Nodi: [2013-2073-2082]Pann=15Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
8	31.42	31.42	-14	420	6	6	Si	8.6
9	31.42	31.42	-12	468	6	6	Si	7.7

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
8	31.42	31.42	-14	402	8	8	Si	9.0
9	31.42	31.42	-12	446	8	8	Si	8.1

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
9	-0.43	-1.48	-0.88	3285	798	-72	446	0.058	0.058	8 (Qp)	Si	3.5
9	-0.43	-1.54	-0.87	3321	817	-83	451	0.059	0.059	7 (Fr)	Si	5.1

Muro [Platea]: 161 - Nodi: [2007-2058-2010]Pann=29Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-17	312	6	6	Si	12
20	31.42	31.42	-17	359	6	6	Si	10

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-17	299	8	8	Si	10
20	31.42	31.42	-16	379	8	8	Si	9.5

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
20	0.36	-2.62	0.98	-2076	-4480	984	379	0.049	0.049	8 (Qp)	Si	4.0
20	0.29	-2.64	0.97	-2055	-4482	1013	364	0.048	0.048	7 (Fr)	Si	6.3

Muro [Platea]: 162 - Nodi: [2007-2042-2047]Pann=28Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
7	31.42	31.42	-22	589	6	6	Si	6.1

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
7	31.42	31.42	-21	566	8	8	Si	6.4

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
7	-2.19	-1.05	0.15	-5693	-1860	453	566	0.070	0.070	8 (Qp)	Si	2.9
7	-2.20	-1.04	0.13	-5710	-1872	442	567	0.070	0.070	7 (Fr)	Si	4.3

Muro [Platea]: 163 - Nodi: [2056-2060-2059]Pann=9Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-9	75	6	6	Si	25
5	31.42	31.42	-8	281	6	6	Si	13

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-10	96	8	8	Si	18
5	31.42	31.42	-9	435	8	8	Si	8.3

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
5	-0.76	0.10	0.63	-483	-2702	1199	435	0.057	0.057	8 (Qp)	Si	3.5

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
5	-0.92	-0.11	0.76	-431	-2558	1167	380	0.050	0.050	7 (Fr)	Si	6.1

Muro [Platea]: 164 - Nodi: [2053-2056-2059]Pann=10Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
8	31.42	31.42	-14	584	6	6	Si	6.2

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
8	31.42	31.42	-14	613	8	8	Si	5.9

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	-2.56	-0.02	1.72	823	3968	655	613	0.080	0.080	8 (Qp)	Si	2.5
8	-2.57	-0.09	1.71	827	3962	630	602	0.079	0.079	7 (Fr)	Si	3.8

Muro [Platea]: 165 - Nodi: [2058-2053-2059]Pann=15Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
5	31.42	31.42	-13	291	6	6	Si	12

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
5	31.42	31.42	-12	305	8	8	Si	12

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
5	-1.53	-1.37	-2.28	3381	1896	-1017	305	0.037	0.037	8 (Qp)	Si	5.4
5	-1.59	-1.39	-2.26	3399	1892	-995	300	0.036	0.036	7 (Fr)	Si	8.3

Muro [Platea]: 166 - Nodi: [2007-2047-2053]Pann=24Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
7	31.42	31.42	-17	420	6	6	Si	8.6

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
7	31.42	31.42	-16	400	8	8	Si	9.0

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
7	-2.12	-1.33	0.59	-4532	-2141	1427	400	0.048	0.048	8 (Qp)	Si	4.2
7	-2.13	-1.31	0.59	-4555	-2149	1420	402	0.048	0.048	7 (Fr)	Si	6.2

Muro [Platea]: 167 - Nodi: [2007-2053-2058]Pann=51Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
14	31.42	31.42	-17	182	6	6	Si	13
7	31.42	31.42	-12	524	6	6	Si	6.9

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
14	31.42	31.42	-16	153	8	8	Si	10
7	31.42	31.42	-12	548	8	8	Si	6.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
7	-3.70	0.11	1.19	1286	3420	-430	548	0.071	0.071	8 (Qp)	Si	2.8
7	-3.71	0.05	1.20	1316	3418	-450	539	0.070	0.070	7 (Fr)	Si	4.3

Muro [Platea]: 168 - Nodi: [2067-2065-2060]Pann=8Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
7	31.42	31.42	-5	184	6	6	Si	20
3	31.42	31.42	-4	461	6	6	Si	7.8

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
7	31.42	31.42	-5	243	8	8	Si	15
3	31.42	31.42	-4	482	8	8	Si	7.5

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	0.93	0.70	-0.70	-120	3390	-2490	482	0.063	0.063	8 (Qp)	Si	3.2
3	0.90	0.68	-0.67	-9	3375	-2494	476	0.062	0.062	7 (Fr)	Si	4.8

Muro [Platea]: 169 - Nodi: [2011-2067-2060]Pann=6Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-8	345	6	6	Si	10
1	31.42	31.42	-6	421	6	6	Si	8.5

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	31.42	31.42	-8	381	8	8	Si	9.4
1	31.42	31.42	-7	532	8	8	Si	6.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	-0.74	0.43	-0.51	3190	-4689	-2735	532	0.069	0.069	8 (Qp)	Si	2.9
1	-0.75	0.32	-0.53	3171	-4503	-2639	488	0.064	0.064	7 (Fr)	Si	4.7

Muro [Platea]: 170 - Nodi: [2031-2037-2036]Pann=8Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-7	248	6	6	Si	15
3	31.42	31.42	-7	277	6	6	Si	13

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-7	269	8	8	Si	13
3	31.42	31.42	-7	297	8	8	Si	12

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	-0.53	-3.38	-0.43	4614	-1840	-2202	297	0.039	0.039	8 (Qp)	Si	5.2
3	-0.53	-3.38	-0.43	4527	-1844	-2231	289	0.038	0.038	7 (Fr)	Si	7.9

Muro [Platea]: 171 - Nodi: [2028-2031-2036]Pann=7Spess.=80 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-6	-14	6	6	Si	35
1	31.42	31.42	-5	-15	6	6	Si	49

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-6	-12	8	8	Si	27
1	31.42	31.42	-5	-14	8	8	Si	37

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	-3.52	-1.72	0.43	1476	971	892	0	0.000	0.000	8 (Qp)	Si	>100
1	-3.52	-1.72	0.44	1490	943	876	0	0.000	0.000	7 (Fr)	Si	>100

Muro [Platea]: 172 - Nodi: [2087-2088-2092]Pann=19Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
15	31.42	31.42	-10	17	6	6	Si	23
16	31.42	31.42	-10	21	6	6	Si	23

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
15	31.42	31.42	-9	17	8	8	Si	18
16	31.42	31.42	-9	20	8	8	Si	18

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
16	-5.06	-1.37	0.41	2220	1109	-170	20	0.002	0.002	8 (Qp)	Si	>100
16	-5.13	-1.37	0.40	2253	1109	-167	21	0.002	0.002	7 (Fr)	Si	>100

Muro [Platea]: 173 - Nodi: [2087-2092-2016]Pann=19Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
7	31.42	31.42	-9	3	6	6	Si	24
17	31.42	31.42	-2	514	6	6	Si	7.0

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
7	31.42	31.42	-9	3	8	8	Si	19
17	31.42	31.42	-2	507	8	8	Si	7.1

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
17	0.37	1.73	0.05	-711	-1458	473	276	0.028	0.028	8 (Qp)	Si	7.1
17	0.36	1.74	0.05	-709	-1462	478	278	0.028	0.028	7 (Fr)	Si	11

Muro [Platea]: 174 - Nodi: [2089-2017-2088]Pann=14Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
9	31.42	31.42	-7	66	6	6	Si	30
13	31.42	31.42	-3	247	6	6	Si	15

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
9	31.42	31.42	-7	65	8	8	Si	23
13	31.42	31.42	-3	267	8	8	Si	13

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
13	1.00	-1.50	-0.37	-680	-864	534	267	0.037	0.037	8 (Qp)	Si	5.5
13	0.95	-1.53	-0.41	-660	-857	551	256	0.035	0.035	7 (Fr)	Si	8.6

Muro [Platea]: 175 - Nodi: [2017-2092-2088]Pann=11Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-9	-9	6	6	Si	25
3	31.42	31.42	-0	184	6	6	Si	20

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
8	31.42	31.42	-9	-9	8	8	Si	20
3	31.42	31.42	-1	179	8	8	Si	20

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	-0.03	0.77	0.10	-173	-350	-89	179	0.027	0.027	8 (Qp)	Si	7.3
3	-0.10	0.77	0.11	-143	-351	-93	179	0.027	0.027	7 (Fr)	Si	11

Muro [Platea]: 176 - Nodi: [17-1-15]Pann=7Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
6	20.11	20.11	-3	13	6	6	Si	85
3	20.11	20.11	-1	605	6	6	Si	5.9

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
6	20.11	20.11	-3	11	8	8	Si	65
4	20.11	20.11	-1	624	8	8	Si	5.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	2.39	-0.27	-0.01	46	-187	-224	606	0.151	0.151	8 (Qp)	Si	1.3
3	2.39	-0.26	-0.01	23	-185	-219	600	0.150	0.150	7 (Fr)	Si	2.0

Muro [Platea]: 177 - Nodi: [2086-2085-2014]Pann=10Spess.=50 cm, Terreno=DefTerr_70882, ,Criterio=CLS_Platee_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-11	-8	6	6	Si	19
4	31.42	31.42	-7	22	6	6	Si	31

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	31.42	31.42	-11	-8	8	8	Si	15
4	31.42	31.42	-7	23	8	8	Si	24

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
4	-3.73	-2.04	-1.36	1697	1557	1034	23	0.002	0.002	8 (Qp)	Si	>100
4	-3.82	-2.09	-1.38	1732	1575	1026	23	0.002	0.002	7 (Fr)	Si	>100

Muro : 178 - Nodi: [2029-3029-3028-2028], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-3	95	6	6	Si	38
13	20.11	20.11	0	108	6	6	Si	33

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-3	102	8	8	Si	35

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
2	0.32	-1.56	-0.41	15	-6	22	55	0.012	0.012	8 (Qp)	Si	17
2	0.33	-1.56	-0.41	16	-6	21	57	0.012	0.012	7 (Fr)	Si	25

Muro : 179 - Nodi: [2036-3036-3028-2028], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	20.11	20.11	-1	29	6	6	Si	>100
13	20.11	20.11	-0	540	6	6	Si	6.7

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
2	20.11	20.11	-1	35	8	8	Si	>100
13	20.11	20.11	-0	565	8	8	Si	6.4

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
13	-0.05	3.64	-0.29	3	46	28	565	0.136	0.136	8 (Qp)	Si	1.5
13	-0.05	3.58	-0.28	3	46	29	557	0.134	0.134	7 (Fr)	Si	2.2

Muro : 180 - Nodi: [2037-2043-3043-3037], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-2	105	6	6	Si	34
8	20.11	20.11	-1	283	6	6	Si	13

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-2	112	8	8	Si	32
8	20.11	20.11	-1	303	8	8	Si	12

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	1.74	-0.71	0.04	87	5	26	303	0.064	0.064	8 (Qp)	Si	3.1
8	1.70	-0.71	0.04	88	5	26	297	0.063	0.063	7 (Fr)	Si	4.8

Muro : 181 - Nodi: [2029-2033-3033-3029], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-4	185	6	6	Si	19
1	20.11	20.11	-0	249	6	6	Si	14

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	20.11	20.11	-2	71	8	8	Si	51
1	20.11	20.11	0	274	8	8	Si	13

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	1.04	1.28	1.08	108	-167	147	274	0.047	0.047	8 (Qp)	Si	4.2
1	1.00	1.21	1.06	109	-175	145	267	0.045	0.045	7 (Fr)	Si	6.7

Muro : 182 - Nodi: [2036-2042-3042-3036], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-1	17	6	6	Si	>100
12	20.11	20.11	0	720	6	6	Si	5.0

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-1	24	8	8	Si	>100
12	20.11	20.11	0	757	8	8	Si	4.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
12	4.93	0.02	-0.02	41	2	9	757	0.185	0.185	8 (Qp)	Si	1.1
12	4.85	0.02	-0.02	41	2	9	744	0.182	0.182	7 (Fr)	Si	1.6

Muro : 183 - Nodi: [2032-2005-3005-3032], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-3	10	6	6	Si	87
3	20.11	20.11	-1	69	6	6	Si	52

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-2	8	8	8	Si	72
3	20.11	20.11	-1	73	8	8	Si	49

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	0.25	0.14	0.33	5	-86	54	51	0.013	0.013	8 (Qp)	Si	16
1	0.23	0.07	0.31	4	-97	51	48	0.012	0.012	7 (Fr)	Si	26

Muro : 184 - Nodi: [2031-2037-3037-3031], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-1	340	6	6	Si	11
1	20.11	20.11	0	675	6	6	Si	5.3

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-1	353	8	8	Si	10
1	20.11	20.11	0	711	8	8	Si	5.1

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	2.03	3.64	2.51	-323	-338	-159	711	0.134	0.134	8 (Qp)	Si	1.5
1	1.99	3.55	2.45	-324	-341	-160	699	0.131	0.131	7 (Fr)	Si	2.3

Muro : 185 - Nodi: [2033-2038-3038-3033], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
12	20.11	20.11	-4	230	6	6	Si	16
16	20.11	20.11	-4	234	6	6	Si	15

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
12	20.11	20.11	-2	257	8	8	Si	14
16	20.11	20.11	-2	265	8	8	Si	14

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
16	1.73	-0.23	0.38	-13	-194	78	265	0.065	0.065	8 (Qp)	Si	3.1
16	1.67	-0.27	0.38	-16	-253	67	257	0.063	0.063	7 (Fr)	Si	4.8

Muro : 186 - Nodi: [2005-2008-3008-3005], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	-4	190	6	6	Si	19
8	20.11	20.11	-2	303	6	6	Si	12

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	-3	209	8	8	Si	17
8	20.11	20.11	-2	336	8	8	Si	11

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
8	1.63	-0.50	-0.00	37	-394	92	336	0.082	0.082	8 (Qp)	Si	2.4
8	1.57	-0.51	-0.01	37	-393	89	325	0.079	0.079	7 (Fr)	Si	3.8

Muro : 187 - Nodi: [2008-2049-3049-3008], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
13	20.11	20.11	-4	151	6	6	Si	24

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
13	20.11	20.11	-3	203	8	8	Si	18

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
13	0.72	0.18	-0.51	36	-539	118	154	0.036	0.036	8 (Qp)	Si	5.6
13	0.67	0.11	-0.47	32	-533	120	144	0.034	0.034	7 (Fr)	Si	8.9

Muro : 188 - Nodi: [2038-2044-3044-3038], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-4	183	6	6	Si	20
4	20.11	20.11	-4	227	6	6	Si	16

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-6	133	8	8	Si	27
4	20.11	20.11	-2	260	8	8	Si	14

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
4	1.72	-0.21	0.23	-5	-188	75	260	0.065	0.065	8 (Qp)	Si	3.1
4	1.66	-0.25	0.23	-9	-247	65	252	0.062	0.062	7 (Fr)	Si	4.8

Muro : 189 - Nodi: [2044-2050-3050-3044], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-5	89	6	6	Si	40
16	20.11	20.11	-4	291	6	6	Si	12

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-6	156	8	8	Si	23
16	20.11	20.11	-2	309	8	8	Si	12

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
16	1.93	-0.21	-0.61	-43	-197	51	309	0.072	0.072	8 (Qp)	Si	2.8
16	1.88	-0.25	-0.60	-48	-255	62	304	0.070	0.070	7 (Fr)	Si	4.3

Muro : 190 - Nodi: [2050-2054-3054-3050], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
15	20.11	20.11	-11	645	6	6	Si	5.6
16	20.11	20.11	-10	953	6	6	Si	3.8

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
15	20.11	20.11	-11	661	8	8	Si	5.4
16	20.11	20.11	-10	921	8	8	Si	3.9

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
8	2.15	-0.15	-0.60	-202	-245	37	422	0.079	0.079	8 (Qp)	Si	2.5
8	2.14	-0.19	-0.59	-209	-302	50	423	0.079	0.079	7 (Fr)	Si	3.8

Muro : 191 - Nodi: [2054-2057-3057-3054], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-12	917	6	6	Si	3.9

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-12	884	8	8	Si	4.1

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
8	2.22	-0.08	-0.05	-391	-42	-392	525	0.083	0.083	8 (Qp)	Si	2.4
8	2.27	-0.09	-0.08	-397	-42	-391	536	0.085	0.085	7 (Fr)	Si	3.5

Muro : 192 - Nodi: [2011-2014-3014-3011], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	20.11	20.11	-7	227	6	6	Si	16
1	20.11	20.11	-6	262	6	6	Si	14

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	20.11	20.11	-7	275	8	8	Si	13
1	20.11	20.11	-6	310	8	8	Si	12

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
1	-2.60	0.50	0.56	-117	-524	148	310	0.036	0.036	8 (Qp)	Si	5.6
1	-2.49	0.42	0.63	-118	-521	145	297	0.034	0.034	7 (Fr)	Si	8.8

Muro : 193 - Nodi: [2057-3057-3011-2011], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-10	607	6	6	Si	5.9

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-10	581	8	8	Si	6.2

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
9	-0.29	0.51	-0.91	-63	-705	102	392	0.045	0.045	8 (Qp)	Si	4.4
9	-0.26	0.56	-0.84	-63	-713	100	403	0.046	0.046	7 (Fr)	Si	6.5

Muro : 194 - Nodi: [2014-3014-3085-2085], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-3	103	6	6	Si	35

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-4	115	8	8	Si	31

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
16	-0.00	-0.20	0.30	5	-324	-61	115	0.012	0.012	8 (Qp)	Si	16
16	0.00	-0.19	0.28	5	-309	-58	109	0.012	0.012	7 (Fr)	Si	25

Muro : 195 - Nodi: [2084-2085-3085-3084], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-3	75	6	6	Si	48
16	20.11	20.11	-2	87	6	6	Si	41

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-3	60	8	8	Si	56
16	20.11	20.11	-3	90	8	8	Si	40

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
16	-0.07	-0.07	-0.06	-227	-26	19	90	0.010	0.010	8 (Qp)	Si	20
16	-0.06	-0.06	-0.06	-218	-24	18	89	0.010	0.010	7 (Fr)	Si	31

Muro : 196 - Nodi: [2078-3078-3084-2084], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-3	48	6	6	Si	68
4	20.11	20.11	-1	117	6	6	Si	31

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-4	69	8	8	Si	42
4	20.11	20.11	-1	109	8	8	Si	33

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
4	-0.07	0.72	-0.28	79	4	-89	109	0.027	0.027	8 (Qp)	Si	7.4
4	0.01	0.75	-0.31	92	4	-82	113	0.028	0.028	7 (Fr)	Si	11

Muro : 197 - Nodi: [3030-3034-3033-3029], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=224$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-7	278	6	6	Si	13

Combinazione QP: $\sigma_{ca}[kg/cm^2]=168$ $\sigma_{fa}[kg/cm^2]=3600$

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-3	166	8	8	Si	22

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cmq	daN/cmq	daN/cmq	kg	kg	kg	kg/cmq	mm	mm			
13	1.17	0.01	-0.09	3	2	9	119	0.024	0.024	8 (Qp)	Si	8.2
13	1.23	0.02	-0.10	2	3	6	125	0.026	0.026	7 (Fr)	Si	12

Muro : 198 - Nodi: [3034-3039-3038-3033], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-6	213	6	6	Si	17
13	20.11	20.11	-0	230	6	6	Si	16

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-3	213	8	8	Si	17
13	20.11	20.11	-0	217	8	8	Si	17

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cmq	daN/cmq	daN/cmq	kg	kg	kg	kg/cmq	mm	mm			
13	2.01	-0.14	-0.07	17	3	14	217	0.041	0.041	8 (Qp)	Si	4.9
13	2.09	-0.13	-0.07	16	4	11	223	0.043	0.043	7 (Fr)	Si	7.0

Muro : 199 - Nodi: [3039-3045-3044-3038], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-6	227	6	6	Si	16
13	20.11	20.11	0	401	6	6	Si	9.0

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
16	20.11	20.11	-3	233	8	8	Si	15
13	20.11	20.11	0	393	8	8	Si	9.2

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cmq	daN/cmq	daN/cmq	kg	kg	kg	kg/cmq	mm	mm			
9	3.80	0.18	-0.04	1	2	35	379	0.080	0.080	8 (Qp)	Si	2.5
9	3.86	0.18	-0.04	-1	3	34	385	0.082	0.082	7 (Fr)	Si	3.7

Muro : 200 - Nodi: [3045-3051-3050-3044], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-6	230	6	6	Si	16
1	20.11	20.11	-0	348	6	6	Si	10

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-4	235	8	8	Si	15
1	20.11	20.11	0	339	8	8	Si	11

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
1	3.12	0.11	0.11	29	4	31	339	0.063	0.063	8 (Qp)	Si	3.2
1	3.19	0.11	0.11	27	5	32	344	0.065	0.065	7 (Fr)	Si	4.6

Muro : 201 - Nodi: [3051-3055-3054-3050], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				
16	20.11	20.11	-9	283	6	6	Si	13
12	20.11	20.11	-7	292	6	6	Si	12

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				
16	20.11	20.11	-5	179	8	8	Si	20
12	20.11	20.11	-4	219	8	8	Si	16

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
4	1.37	0.20	0.98	26	128	63	163	0.027	0.027	8 (Qp)	Si	7.4
4	1.37	0.19	0.99	30	162	66	166	0.027	0.027	7 (Fr)	Si	11

Muro : 202 - Nodi: [2073-2075-3075-3073], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				
13	20.11	20.11	-18	682	6	6	Si	5.3

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				
13	20.11	20.11	-17	618	8	8	Si	5.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
13	2.84	0.36	-0.78	-166	-1016	-17	463	0.085	0.085	8 (Qp)	Si	2.4
13	2.88	0.42	-0.76	-166	-1040	-21	468	0.086	0.086	7 (Fr)	Si	3.5

Muro : 203 - Nodi: [2068-2071-3071-3068], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				
16	20.11	20.11	-12	392	6	6	Si	9.2
1	20.11	20.11	0	565	6	6	Si	6.4

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm	kg/cm				

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
16	20.11	20.11	-12	404	8	8	Si	8.9
1	20.11	20.11	0	571	8	8	Si	6.3

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	0.94	4.16	1.42	18	82	114	571	0.127	0.127	8 (Qp)	Si	1.6
1	0.94	4.12	1.42	18	82	113	567	0.126	0.126	7 (Fr)	Si	2.4

Muro : 204 - Nodi: [2071-2073-3073-3071], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	20.11	20.11	-17	366	6	6	Si	9.8

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	20.11	20.11	-17	350	8	8	Si	10

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	2.32	-2.47	0.35	-27	-114	-27	306	0.072	0.072	8 (Qp)	Si	2.8
3	2.33	-2.48	0.36	-34	-116	-29	312	0.072	0.072	7 (Fr)	Si	4.2

Muro : 205 - Nodi: [2075-2077-3077-3075], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	-17	651	6	6	Si	5.5

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	-16	583	8	8	Si	6.2

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
1	1.64	0.26	-0.84	-74	-977	64	583	0.059	0.059	8 (Qp)	Si	3.4
1	1.71	0.34	-0.81	-77	-1002	62	607	0.061	0.061	7 (Fr)	Si	4.9

Muro : 206 - Nodi: [2077-2079-3079-3077], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	-7	161	6	6	Si	22

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
1	20.11	20.11	-6	126	8	8	Si	26

Verifica aperture fessure:Wamm_Freq[mm]=0.300 Wamm_Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
3	0.78	-0.30	-0.51	14	-68	82	106	0.024	0.024	8 (Qp)	Si	8.4
3	0.84	-0.30	-0.47	22	-68	84	119	0.026	0.026	7 (Fr)	Si	12

Muro : 207 - Nodi: [2074-2072-3072-3074], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
16	20.11	20.11	-26	639	6	6	Si	5.6

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
16	20.11	20.11	-26	648	8	8	Si	5.6
5	20.11	20.11	-16	659	8	8	Si	5.5

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
5	-3.57	0.96	0.10	186	948	-124	659	0.068	0.068	8 (Qp)	Si	3.0
5	-3.40	0.91	0.05	176	885	-123	617	0.063	0.063	7 (Fr)	Si	4.7

Muro : 208 - Nodi: [2059-2064-3064-3059], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
2	20.11	40.21	-13	284	6	6	Si	13
5	20.11	20.11	-7	462	6	6	Si	7.8

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
2	20.11	40.21	-13	292	8	8	Si	12
5	20.11	20.11	-6	499	8	8	Si	7.2

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
5	1.15	3.18	1.23	408	156	234	499	0.095	0.095	8 (Qp)	Si	2.1
5	1.06	3.07	1.21	407	157	226	486	0.092	0.092	7 (Fr)	Si	3.3

Muro : 209 - Nodi: [2079-2078-3078-3079], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
13	20.11	20.11	-4	167	6	6	Si	22

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
13	20.11	20.11	-4	235	8	8	Si	15

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
13	-3.50	1.69	-0.95	97	39	2	235	0.051	0.051	8 (Qp)	Si	3.9

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
13	-3.45	1.52	-0.91	83	30	6	209	0.047	0.047	7 (Fr)	Si	6.4

Muro : 210 - Nodi: [2072-2069-3069-3072], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-27	660	6	6	Si	5.5

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-27	671	8	8	Si	5.4

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
4	1.51	-1.98	0.92	-494	-1633	882	668	0.064	0.064	7 (Fr)	Si	4.7
5	-3.07	-0.33	1.75	230	1259	-262	666	0.066	0.066	8 (Qp)	Si	3.0

Muro : 211 - Nodi: [2064-2066-3066-3064], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-8	92	6	6	Si	29

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-8	91	8	8	Si	20

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
13	-0.35	-6.41	1.66	-241	-297	135	91	0.009	0.009	8 (Qp)	Si	23
13	-0.34	-6.25	1.63	-239	-293	132	91	0.009	0.009	7 (Fr)	Si	35

Muro : 212 - Nodi: [2076-2074-3074-3076], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-11	410	6	6	Si	8.8
9	20.11	20.11	-10	418	6	6	Si	8.6

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-13	514	8	8	Si	7.0
9	20.11	20.11	-12	529	8	8	Si	6.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
9	-2.80	0.78	-0.68	124	757	-155	529	0.054	0.054	8 (Qp)	Si	3.7
9	-2.67	0.71	-0.70	116	702	-154	488	0.050	0.050	7 (Fr)	Si	6.0

Muro : 213 - Nodi: [2078-2076-3076-3078], Pann.X=4, Pann.Y=4Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-7	242	6	6	Si	15

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-7	97	8	8	Si	25
1	20.11	20.11	-4	210	8	8	Si	17

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
1	-2.33	1.20	-0.50	-215	91	32	210	0.036	0.036	8 (Qp)	Si	5.6
1	-2.25	1.05	-0.47	-215	79	30	183	0.031	0.031	7 (Fr)	Si	9.6

Muro : 214 - Nodi: [2060-3060-3059-2059], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-12	735	6	6	Si	4.9

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	20.11	20.11	-13	793	8	8	Si	4.5

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
4	1.60	3.50	-2.34	-1204	-545	-58	793	0.130	0.130	8 (Qp)	Si	1.5
4	1.53	3.40	-2.26	-1184	-536	-52	774	0.126	0.126	7 (Fr)	Si	2.4

Muro : 215 - Nodi: [2058-2059-3059-3058], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-13	830	6	6	Si	4.3

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-13	893	8	8	Si	4.0

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
9	-0.12	-0.42	-1.02	-289	-1121	111	434	0.048	0.048	8 (Qp)	Si	4.2
9	-0.11	-0.43	-0.98	-289	-1105	108	426	0.047	0.047	7 (Fr)	Si	6.4

Muro : 216 - Nodi: [2070-2058-3058-3070], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-24	670	6	6	Si	5.4
9	20.11	20.11	-21	701	6	6	Si	5.1

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-23	622	8	8	Si	5.8
9	20.11	20.11	-19	661	8	8	Si	5.4

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
1	2.72	-1.90	0.27	357	2029	-431	583	0.100	0.100	8 (Qp)	Si	2.0
1	2.75	-1.87	0.28	357	2044	-432	587	0.101	0.101	7 (Fr)	Si	3.0

Muro : 217 - Nodi: [2070-3070-3071-2071], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	40.21	-11	1133	6	6	Si	3.2

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	40.21	-11	1050	8	8	Si	3.4

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
3	-2.28	2.09	-2.65	555	130	20	376	0.077	0.077	8 (Qp)	Si	2.6
3	-2.28	2.12	-2.64	562	130	18	381	0.078	0.078	7 (Fr)	Si	3.8

Muro : 218 - Nodi: [2042-2047-3047-3042], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-3	104	6	6	Si	35
4	20.11	20.11	-0	649	6	6	Si	5.5

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-3	113	8	8	Si	32
4	20.11	20.11	-0	690	8	8	Si	5.2

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cm	mm	mm			
4	4.57	-0.06	-0.06	-17	-5	1	690	0.172	0.172	8 (Qp)	Si	1.2
4	4.49	-0.06	-0.06	-16	-4	1	678	0.169	0.169	7 (Fr)	Si	1.8

Muro : 219 - Nodi: [2043-2048-3048-3043], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
1	20.11	20.11	-3	47	6	6	Si	77
4	20.11	20.11	-0	193	6	6	Si	19

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-2	44	8	8	Si	69
4	20.11	20.11	-0	204	8	8	Si	18

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
13	0.58	1.15	-0.81	-2	-46	33	194	0.043	0.043	8 (Qp)	Si	4.7
13	0.57	1.12	-0.79	-2	-45	33	190	0.041	0.041	7 (Fr)	Si	7.2

Muro : 220 - Nodi: [2053-3053-3047-2047], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-7	502	6	6	Si	7.2
1	20.11	20.11	-1	504	6	6	Si	7.1

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-7	531	8	8	Si	6.8
1	20.11	20.11	-1	534	8	8	Si	6.7

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
16	-0.07	2.91	0.47	1	158	-12	512	0.107	0.107	8 (Qp)	Si	1.9
16	-0.07	2.85	0.46	1	156	-13	503	0.105	0.105	7 (Fr)	Si	2.8

Muro : 221 - Nodi: [2053-2056-3056-3053], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-6	95	6	6	Si	38
9	20.11	20.11	-3	215	6	6	Si	17

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-6	87	8	8	Si	28
9	20.11	20.11	-3	219	8	8	Si	16

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm ²	daN/cm ²	daN/cm ²	kg	kg	kg	kg/cm ²	mm	mm			
9	-3.18	0.94	-0.86	-7	159	269	219	0.035	0.035	8 (Qp)	Si	5.7
9	-3.13	0.90	-0.83	-4	165	267	217	0.034	0.034	7 (Fr)	Si	8.9

Muro : 222 - Nodi: [2056-2060-3060-3056], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	20.11	20.11	-10	412	6	6	Si	8.7

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

P.	Afx	Afy	σ_c	σ_f	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	kg/cmq	kg/cmq				
13	20.11	20.11	-12	416	8	8	Si	8.7
1	20.11	20.11	-11	440	8	8	Si	8.2

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	daN/cm	daN/cm	daN/cm	kg	kg	kg	kg/cmq	mm	mm			
1	-0.93	0.07	0.85	-226	-965	499	440	0.049	0.049	8 (Qp)	Si	4.1
1	-0.93	0.08	0.83	-223	-937	492	428	0.048	0.048	7 (Fr)	Si	6.3

Verifica dei pilastri (Stati limite esercizio)

Scenario di calcolo: ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO

Simbologia

Terreno	Nome della stratigrafia per travi Winkler
L [cm]	Lunghezza teorica elemento (distanza tra i nodi)
Ln [cm]	Lunghezza netta elemento (tiene conto dei concetti rigidi)
L2,L3 [cm]	Lunghezze libere di inflessione
Sez. R: Sezione	Rettangolare
	By[cm]: Larghezza (asse locale y)
	Bz[cm]: Larghezza (asse locale z)
Sez. T: Sezione	a T (rovescia e non)
	Ba[cm]: Larghezza base inferiore
	Ha[cm]: Altezza inferiore
	Bs[cm]: Larghezza superiore
	Hs[cm]: Altezza superiore
Sez. L: Sezione	ad L (rovescia e non)
	Ba[cm]: Larghezza base inferiore
	Ha[cm]: Altezza inferiore
	Bs[cm]: Larghezza superiore
	Hs[cm]: Altezza superiore
Sez. C: Sezione	circolare
	R[cm]: Raggio
Sez. G: Sezione	generica
	B[cm]: Larghezza
	H[cm]: Altezza
X [cm]	Punto di verifica
σ_{ca} [kg/cmq]	Tensione ammissibile nel cls
σ_{fa} [kg/cmq]	Tensione ammissibile nell'acciaio
σ_{cta} [kg/cmq]	Tensione ammissibile a trazione (quando richiesto dalla verifica)
M- [kg*m]	Momento negativo massimo di calcolo
M+ [kg*m]	Momento positivo massimo di calcolo
M [kg*m]	Momento di calcolo (travi a flessione, pilastri circolari)
My [kg*m]	Momento calcolo per verifiche a pressoflessione
Mz [kg*m]	Momento calcolo per verifiche a pressoflessione (Sez. L, Pilastri)
N [kg]	Sforzo normale corrispondente ad My (e Mz per Sez. L, Pilastri)
Afsup [cmq]	Area di ferro superiore
Afinf [cmq]	Area di ferro inferiore
Afsin [cmq]	Area di ferro sinistra (Sez. L)
Afdes [cmq]	Area di ferro destra (Sez. L)
σ_{c-} [kg/cmq]	Tensione nel cls compresso per effetto di M-
σ_{cy} [kg/cmq]	Tensione nel cls compresso per effetto di (N,My) in caso di pressoflessione retta
σ_{cz} [kg/cmq]	Tensione nel cls compresso per effetto di (N,Mz) in caso di pressoflessione retta
σ_{c+} [kg/cmq]	Tensione nel cls compresso per effetto di M+
σ_{ct-} [kg/cmq]	Tensione nel cls teso per effetto di M-
σ_{ct+} [kg/cmq]	Tensione nel cls teso per effetto di M+
σ_{f-} [kg/cmq]	Tensione nell'acciaio per effetto di M-
σ_{f+} [kg/cmq]	Tensione nell'acciaio per effetto di M+
σ_{fy} [kg/cmq]	Tensione nel acciaio per effetto di (N,My) in caso di pressoflessione retta
σ_{fz} [kg/cmq]	Tensione nel acciaio per effetto di (N,Mz) in caso di pressoflessione retta
Cb-	Combinazione di carico generatore di M-
Cb+	Combinazione di carico generatore di M+
σ_c [kg/cmq]	Tensione nel cls per effetto di N My
σ_f [kg/cmq]	Tensione nell'acciaio per effetto di N My
Cb	Combinazione di carico generatore di N My
Act [mq]	Area di calcestruzzo teso
Aft [cmq]	Area di acciaio teso
pAft [cm]	Perimetro area di acciaio teso

$S_{r,max}$ [cm] Distanza massima delle fessure
 σ_{sfmed} [kg/cmq] Tensione media dell'acciaio
 W_d [mm] Apertura delle fessure
 W_k [mm] Apertura caratteristica delle fessure
 W_{amm_Freq} [mm] Apertura ammissibile delle fessure per combinazione Frequente
 W_{amm_Qp} [mm] Apertura ammissibile delle fessure per combinazione Quasi Permanente
 W_{amm_Rara} [mm] Apertura ammissibile delle fessure per combinazione Rara
 C_s Coefficiente di sicurezza definito come minimo di σ_{Amm}/σ tra acciaio e calcestruzzo oppure W_{amm}/W_k

Pilastro: 2001 [2001,4001] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm L2=545.00 cm L3=545.00 cm
Criterio: CLS_Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
545.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

Verifica snellezza: fcd=212 [kg/cm²] - **Verificato**

Cb	N	fcd*Ac	v	λ _{max}	λ _{lim}
	kg	kg			
6	14859	317475	0.047	62.931	115.557

Combinazione Rara: σ_{ca}[kg/cm²]=224 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-14859	-1587	348	-24	46	6	Si	9.5
545.00	-12816	950	585	-21	35	6	Si	11

Combinazione QP: σ_{ca}[kg/cm²]=168 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-14476	-1634	322	-24	54	8	Si	7.1
545.00	-12433	1081	601	-22	60	8	Si	7.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{r,max}	σ _{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cm ²	mm	mm			
0.00	-14472	-1646	326	8.68E-03	3.80	7.60	23.53	56	0.004	0.004	7 (Fr)	Si	80
0.00	-14476	-1634	322	8.47E-03	3.78	7.56	23.37	54	0.004	0.004	8 (Qp)	Si	56
545.00	-12433	1081	601	8.41E-03	4.18	8.36	22.54	60	0.004	0.004	8 (Qp)	Si	52
545.00	-12429	1089	598	8.45E-03	4.18	8.36	22.58	61	0.004	0.004	7 (Fr)	Si	77

Pilastro: 2002 [2002,4002] Sez. R: By=50.00 cm Bz=30.00 cm L=545.00 cm Ln=545.00 cm L2=545.00 cm L3=545.00 cm
Criterio: CLS_Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 3.14	Afz = 3.14
545.00	AfSpigolo = 3.14	Afy = 3.14	Afz = 3.14

Verifica snellezza: fcd=212 [kg/cm²] - **Verificato**

Cb	N	fcd*Ac	v	λ _{max}	λ _{lim}
	kg	kg			
6	23577	317475	0.074	62.931	91.739

Combinazione Rara: σ_{ca}[kg/cm²]=224 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-23577	-664	96	-21	-116	6	Si	11
545.00	-21533	563	-734	-22	-66	6	Si	10

Combinazione QP: σ_{ca}[kg/cm²]=168 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-22818	-734	65	-21	-105	8	Si	8.1
545.00	-20774	710	-705	-23	-47	8	Si	7.2

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{r,max}	σ _{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cm ²	mm	mm			
0.00	-22814	-737	79	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100
0.00	-22818	-734	65	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100

X	N	My	Mz	Act	Aft	pAft	S _{F,max}	σ _{fmed}	Wd	Wk	Cb	Ver.	Cs
545.00	-20774	710	-705	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
545.00	-20770	713	-717	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100

Pilastro: 2003 [2003,4003] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm L2=545.00 cm L3=545.00 cm
Criterio: CLS_Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
545.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

Verifica snellezza: fcd=212 [kg/cm²] - **Verificato**

Cb	N	fcd*Ac	v	λ _{max}	λ _{lim}
	kg	kg			
6	13312	317475	0.042	62.931	122.088

Combinazione Rara: σ_{ca}[kg/cm²]=224 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-13312	-1618	-699	-28	143	6	Si	7.9
545.00	-11268	931	278	-15	8	6	Si	15

Combinazione QP: σ_{ca}[kg/cm²]=168 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-12886	-1694	-706	-29	168	8	Si	5.7
545.00	-10842	1091	287	-16	32	8	Si	10

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{F,max}	σ _{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cm ²	mm	mm			
0.00	-12888	-1695	-698	1.56E-02	6.41	12.83	24.03	113	0.008	0.008	7 (Fr)	Si	39
0.00	-12886	-1694	-706	1.56E-02	6.44	12.88	24.02	114	0.008	0.008	8 (Qp)	Si	25
545.00	-10842	1091	287	6.99E-03	4.31	8.63	21.14	32	0.002	0.002	8 (Qp)	Si	>100
545.00	-10845	1091	280	6.91E-03	4.28	8.56	21.11	31	0.002	0.002	7 (Fr)	Si	>100

Pilastro: 2004 [2004,4004] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm L2=545.00 cm L3=545.00 cm
Criterio: CLS_Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
545.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

Verifica snellezza: fcd=212 [kg/cm²] - **Verificato**

Cb	N	fcd*Ac	v	λ _{max}	λ _{lim}
	kg	kg			
6	19621	317475	0.062	62.931	100.561

Combinazione Rara: σ_{ca}[kg/cm²]=224 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-19621	-1715	1338	-42	184	6	Si	5.4
545.00	-17577	2017	-1569	-50	362	6	Si	4.5

Combinazione QP: σ_{ca}[kg/cm²]=168 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-18782	-1650	1315	-41	186	8	Si	4.1
545.00	-16739	1923	-1558	-49	368	8	Si	3.4

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{F,max}	σ _{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	-18780	-1667	1318	1.35E-02	5.02	10.04	24.98	111	0.008	0.008	7 (Fr)	Si	38
0.00	-18782	-1650	1315	1.34E-02	5.01	10.02	24.91	108	0.008	0.008	8 (Qp)	Si	26
545.00	-16739	1923	-1558	2.02E-02	5.83	11.66	27.76	261	0.021	0.021	8 (Qp)	Si	9.7
545.00	-16736	1940	-1560	2.03E-02	5.83	11.67	27.80	264	0.021	0.021	7 (Fr)	Si	14

Pilastro: 2005 [2005,3005] Sez. R: By=30.00 cm Bz=50.00 cm L=145.00 cm Ln=145.00 cm L2=145.00 cm L3=145.00 cm
Criterio: CLS_Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
145.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

Verifica snellezza: fcd=212 [kg/cmq] - **Verificato**

Cb	N	fcd*Ac	v	λ _{max}	λ _{lim}
	kg	kg			
6	19469	317475	0.061	16.743	100.953

Combinazione Rara: σ_{ca}[kg/cmq]=224 σ_{fa}[kg/cmq]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cmq	kg/cmq			
0.00	-15419	-546	121	-13	-72	6	Si	17
145.00	-19469	-528	105	-15	-107	6	Si	15

Combinazione QP: σ_{ca}[kg/cmq]=168 σ_{fa}[kg/cmq]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cmq	kg/cmq			
0.00	-14454	-598	107	-13	-62	8	Si	13
145.00	-18141	-482	99	-14	-100	8	Si	12

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{F,max}	σ _{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	-14451	-583	110	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100
0.00	-14454	-598	107	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
145.00	-18141	-482	99	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
145.00	-18094	-493	100	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100

Pilastro: 2005 [3005,4005] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm L2=400.00 cm L3=400.00 cm
Criterio: CLS_Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
400.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

Verifica snellezza: fcd=212 [kg/cmq] - **Verificato**

Cb	N	fcd*Ac	v	λ _{max}	λ _{lim}
	kg	kg			
6	24278	317475	0.076	46.188	90.403

Combinazione Rara: σ_{ca}[kg/cmq]=224 σ_{fa}[kg/cmq]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cmq	kg/cmq			
0.00	-24278	-1759	-37	-25	-62	6	Si	9.1
400.00	-22778	2420	-247	-31	34	6	Si	7.2

Combinazione QP: σ_{ca}[kg/cmq]=168 σ_{fa}[kg/cmq]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cmq	kg/cmq			
0.00	-22476	-1608	-36	-23	-59	8	Si	7.4

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
400.00	-20976	2194	-239	-29	29	8	Si	5.9

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	$S_{x,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	m ²	cm ²	cm	cm	kg/cm ²	mm	mm			
0.00	-22469	-1637	-34	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100
0.00	-22476	-1608	-36	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
400.00	-20976	2194	-239	6.51E-03	3.68	7.36	21.67	29	0.002	0.002	8 (Qp)	Si	>100
400.00	-20969	2218	-243	6.83E-03	3.74	7.47	21.88	32	0.002	0.002	7 (Fr)	Si	>100

Pilastro: 2006 [2006,4006] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm L2=545.00 cm L3=545.00 cm
Criterio: CLS_Pilastrri

Zona	Armature		
cm	cm ²	cm ²	cm ²
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
545.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

Verifica snellezza: fcd=212 [kg/cm²] - **Verificato**

Cb	N	fcd*Ac	v	λ_{max}	λ_{lim}
	kg	kg			
6	18265	317475	0.058	62.931	104.228

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-18265	-1936	-1555	-49	321	6	Si	4.6
545.00	-16221	2196	1979	-62	612	6	Si	3.6

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-17360	-1911	-1557	-49	345	8	Si	3.4
545.00	-15316	2136	1981	-62	639	8	Si	2.7

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	$S_{x,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	m ²	cm ²	cm	cm	kg/cm ²	mm	mm			
0.00	-17360	-1911	-1551	1.92E-02	5.72	11.45	27.39	239	0.019	0.019	7 (Fr)	Si	16
0.00	-17360	-1911	-1557	1.93E-02	5.74	11.47	27.41	241	0.019	0.019	8 (Qp)	Si	11
545.00	-15316	2136	1981	2.57E-02	9.42	18.85	25.13	363	0.026	0.026	8 (Qp)	Si	7.7
545.00	-15316	2136	1977	2.57E-02	9.42	18.85	25.12	361	0.026	0.026	7 (Fr)	Si	12

Pilastro: 2007 [2007,4007] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm L2=545.00 cm L3=545.00 cm
Criterio: CLS_Pilastrri

Zona	Armature		
cm	cm ²	cm ²	cm ²
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
545.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

Verifica snellezza: fcd=212 [kg/cm²] - **Verificato**

Cb	N	fcd*Ac	v	λ_{max}	λ_{lim}
	kg	kg			
6	20800	317475	0.066	62.931	97.670

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-20800	21	1463	-29	-10	6	Si	7.8

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
545.00	-18757	-726	-1978	-45	268	6	Si	5.0

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cmq	kg/cmq			
0.00	-19940	65	1438	-29	2	8	Si	5.9
545.00	-17896	-726	-1966	-45	291	8	Si	3.8

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	-19938	39	1442	9.85E-03	3.23	6.46	26.28	0	0.000	0.000	7 (Fr)	Si	>100
0.00	-19940	65	1438	9.77E-03	3.58	7.16	25.12	2	0.000	0.000	8 (Qp)	Si	>100
545.00	-17896	-726	-1966	2.10E-02	9.42	18.85	23.31	208	0.014	0.014	8 (Qp)	Si	14
545.00	-17894	-704	-1968	2.10E-02	9.42	18.85	23.31	209	0.014	0.014	7 (Fr)	Si	22

Pilastro: 2008 [2008,3008] Sez. R: By=30.00 cm Bz=50.00 cm L=145.00 cm Ln=145.00 cm L2=145.00 cm L3=145.00 cm
Criterio: CLS_Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
145.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

Verifica snellezza: fcd=212 [kg/cmq] - **Verificato**

Cb	N	fcd*Ac	v	λ_{max}	λ_{lim}
	kg	kg			
6	23271	317475	0.073	16.743	92.339

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cmq	kg/cmq			
0.00	-16650	-2	154	-11	-119	6	Si	21
145.00	-23271	-102	107	-14	-168	6	Si	16

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cmq	kg/cmq			
0.00	-15836	-2	150	-10	-112	8	Si	17
145.00	-21794	-81	104	-13	-158	8	Si	13

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	-15807	-2	150	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100
0.00	-15836	-2	150	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
145.00	-21794	-81	104	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
145.00	-21820	-94	104	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100

Pilastro: 2008 [3008,4008] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm L2=400.00 cm L3=400.00 cm
Criterio: CLS_Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
400.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

Verifica snellezza: fcd=212 [kg/cmq] - **Verificato**

Cb	N	fcd*Ac	v	λ_{max}	λ_{lim}
	kg	kg			
6	25970	317475	0.082	46.188	87.409

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-25970	-94	93	-15	-192	6	Si	15
400.00	-24470	-1109	-307	-23	-86	6	Si	9.6

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-24162	-57	102	-14	-179	8	Si	12
400.00	-22662	-1047	-306	-22	-76	8	Si	7.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cm ²	mm	mm			
0.00	-24162	-96	101	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100
0.00	-24162	-57	102	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
400.00	-22662	-1047	-306	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
400.00	-22662	-1011	-307	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100

Pilastro: 2009 [2009,4009] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm L2=545.00 cm L3=545.00 cm
Criterio: CLS_Pilastri

Zona	Armature
cm	cmq
0.00	AfSpigolo = 3.14
545.00	AfSpigolo = 3.14

Verifica snellezza: fcd=212 [kg/cm²] - **Verificato**

Cb	N	fcd*Ac	v	λ_{max}	λ_{lim}
	kg	kg			
6	19378	317475	0.061	62.931	101.192

Combinazione Rara: σ_{ca} [kg/cm²]=224 σ_{fa} [kg/cm²]=3600

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-19378	-354	-1672	-35	100	6	Si	6.4
545.00	-17334	-380	2285	-48	399	6	Si	4.7

Combinazione QP: σ_{ca} [kg/cm²]=168 σ_{fa} [kg/cm²]=3600

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-18440	-379	-1664	-35	122	8	Si	4.8
545.00	-16396	-312	2280	-47	424	8	Si	3.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cm ²	mm	mm			
0.00	-18441	-378	-1661	1.61E-02	9.42	18.85	21.44	82	0.005	0.005	7 (Fr)	Si	59
0.00	-18440	-379	-1664	1.61E-02	9.42	18.85	21.46	83	0.005	0.005	8 (Qp)	Si	39
545.00	-16396	-312	2280	2.50E-02	9.42	18.85	24.83	385	0.027	0.027	8 (Qp)	Si	7.3
545.00	-16398	-314	2279	2.49E-02	9.42	18.85	24.83	384	0.027	0.027	7 (Fr)	Si	11

Pilastro: 2010 [2010,4010] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm L2=545.00 cm L3=545.00 cm
Criterio: CLS_Pilastri

Zona	Armature
cm	cmq
0.00	AfSpigolo = 3.14
545.00	AfSpigolo = 3.14

Verifica snellezza: fcd=212 [kg/cm²] - **Verificato**

Cb	N	fcd*Ac	v	λ_{max}	λ_{lim}
	kg	kg			
6	22231	317475	0.070	62.931	94.475

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cmq	kg/cmq			
0.00	-22231	246	1469	-31	-8	6	Si	7.2
545.00	-20187	-343	-2145	-44	238	6	Si	5.1

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cmq	kg/cmq			
0.00	-21279	283	1428	-31	1	8	Si	5.5
545.00	-19236	-371	-2127	-44	264	8	Si	3.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	-21286	272	1437	7.99E-03	3.22	6.44	24.24	1	0.000	0.000	7 (Fr)	Si	>100
0.00	-21279	283	1428	7.82E-03	3.18	6.35	24.16	1	0.000	0.000	8 (Qp)	Si	>100
545.00	-19236	-371	-2127	2.09E-02	9.42	18.85	23.27	222	0.015	0.015	8 (Qp)	Si	14
545.00	-19243	-362	-2131	2.09E-02	9.42	18.85	23.29	223	0.015	0.015	7 (Fr)	Si	20

Pilastro: 2011 [2011,3011] Sez. R: By=30.00 cm Bz=50.00 cm L=145.00 cm Ln=145.00 cm L2=145.00 cm L3=145.00 cm
Criterio: CLS_Pilastri

Zona	Armature
cm	cmq
0.00	AfSpigolo = 3.14
145.00	AfSpigolo = 3.14

Verifica snellezza: fcd=212 [kg/cmq] - **Verificato**

Cb	N	fcd*Ac	v	λ_{max}	λ_{lim}
	kg	kg			
6	22998	317475	0.072	16.743	92.886

Combinazione Rara: σ_{ca} [kg/cmq]=224 σ_{fa} [kg/cmq]=3600

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cmq	kg/cmq			
0.00	-14322	677	85	-13	-62	6	Si	17
145.00	-22998	290	199	-17	-152	6	Si	13

Combinazione QP: σ_{ca} [kg/cmq]=168 σ_{fa} [kg/cmq]=3600

X	N	My	Mz	σ_c	σ_f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cmq	kg/cmq			
0.00	-13161	770	74	-13	-46	8	Si	13
145.00	-21341	305	214	-16	-136	8	Si	10

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	-13250	733	80	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100
0.00	-13161	770	74	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
145.00	-21341	305	214	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
145.00	-21409	299	209	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100

Pilastro: 2011 [3011,4011] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm L2=400.00 cm L3=400.00 cm
Criterio: CLS_Pilastri

Zona	Armature
cm	cmq
0.00	AfSpigolo = 3.14

Zona	Armature		
400.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

Verifica snellezza: fcd=212 [kg/cm²] - **Verificato**

Cb	N	fcd*Ac	v	λmax	λlim
	kg	kg			
6	27099	317475	0.085	46.188	85.569

Combinazione Rara: σca[kg/cm²]=224 σfa[kg/cm²]=3600

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-27099	474	392	-23	-154	6	Si	9.9
400.00	-25599	-463	-467	-23	-135	6	Si	9.9

Combinazione QP: σca[kg/cm²]=168 σfa[kg/cm²]=3600

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-25236	562	422	-23	-129	8	Si	7.5
400.00	-23736	-543	-483	-22	-111	8	Si	7.6

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{r,max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cm ²	mm	mm			
0.00	-25250	542	411	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100
0.00	-25236	562	422	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
400.00	-23736	-543	-483	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
400.00	-23750	-528	-477	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100

Pilastro: 2012 [2012,4012] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm L2=545.00 cm L3=545.00 cm
Criterio: CLS_Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
545.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

Verifica snellezza: fcd=212 [kg/cm²] - **Verificato**

Cb	N	fcd*Ac	v	λmax	λlim
	kg	kg			
6	20743	317475	0.065	62.931	97.804

Combinazione Rara: σca[kg/cm²]=224 σfa[kg/cm²]=3600

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-20743	281	-1756	-36	86	6	Si	6.2
545.00	-18699	-286	2436	-49	401	6	Si	4.5

Combinazione QP: σca[kg/cm²]=168 σfa[kg/cm²]=3600

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-19825	254	-1729	-35	96	8	Si	4.8
545.00	-17781	-274	2416	-49	426	8	Si	3.4

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{r,max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cm ²	mm	mm			
0.00	-19832	277	-1735	1.52E-02	9.42	18.85	21.12	72	0.004	0.004	7 (Fr)	Si	69
0.00	-19825	254	-1729	1.51E-02	9.42	18.85	21.09	70	0.004	0.004	8 (Qp)	Si	47
545.00	-17781	-274	2416	2.46E-02	9.42	18.85	24.69	392	0.028	0.028	8 (Qp)	Si	7.2
545.00	-17788	-295	2421	2.46E-02	9.42	18.85	24.70	394	0.028	0.028	7 (Fr)	Si	11

Pilastro: 2013 [2013,4013] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm L2=545.00 cm L3=545.00 cm
Criterio: CLS_Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
545.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

Verifica snellezza: fcd=212 [kg/cm²] - **Verificato**

Cb	N	fcd*Ac	v	λ _{max}	λ _{lim}
	kg	kg			
6	20519	317475	0.065	62.931	98.336

Combinazione Rara: σ_{ca}[kg/cm²]=224 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-20519	1343	1373	-39	121	6	Si	5.8
545.00	-18476	-1283	-1684	-44	248	6	Si	5.1

Combinazione QP: σ_{ca}[kg/cm²]=168 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-19639	1292	1332	-37	120	8	Si	4.5
545.00	-17595	-1222	-1664	-43	258	8	Si	3.9

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{z,max}	σ _{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	m ²	cmq	cm	cm	kg/cm ²	mm	mm			
0.00	-19645	1312	1342	1.11E-02	4.79	9.59	23.61	66	0.004	0.004	7 (Fr)	Si	68
0.00	-19639	1292	1332	1.09E-02	4.76	9.52	23.50	62	0.004	0.004	8 (Qp)	Si	48
545.00	-17595	-1222	-1664	1.85E-02	6.23	12.46	25.99	192	0.014	0.014	8 (Qp)	Si	14
545.00	-17601	-1240	-1668	1.86E-02	6.23	12.46	26.04	195	0.015	0.015	7 (Fr)	Si	21

Pilastro: 2014 [2014,3014] Sez. R: By=30.00 cm Bz=50.00 cm L=145.00 cm Ln=145.00 cm L2=145.00 cm L3=145.00 cm
Criterio: CLS_Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
145.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

Verifica snellezza: fcd=212 [kg/cm²] - **Verificato**

Cb	N	fcd*Ac	v	λ _{max}	λ _{lim}
	kg	kg			
6	20766	317475	0.065	16.743	97.749

Combinazione Rara: σ_{ca}[kg/cm²]=224 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-15582	102	-47	-9	-113	6	Si	24
145.00	-20766	99	168	-13	-143	6	Si	17

Combinazione QP: σ_{ca}[kg/cm²]=168 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-14987	3	-35	-8	-116	8	Si	20
145.00	-19414	87	180	-13	-132	8	Si	13

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{z,max}	σ _{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	m ²	cmq	cm	cm	kg/cm ²	mm	mm			
0.00	-14860	47	-42	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100
0.00	-14987	3	-35	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
145.00	-19414	87	180	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
145.00	-19382	94	175	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100

Pilastro: 2014 [3014,4014] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm L2=400.00 cm L3=400.00 cm
Criterio: CLS_Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
400.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

Verifica snellezza: fcd=212 [kg/cmq] - **Verificato**

Cb	N	fcd*Ac	v	λmax	λlim
	kg	kg			
6	24714	317475	0.078	46.188	89.603

Combinazione Rara: σca[kg/cmq]=224 σfa[kg/cmq]=3600

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cmq	kg/cmq			
0.00	-24714	789	287	-21	-113	6	Si	11
400.00	-23214	-979	-403	-23	-76	6	Si	9.8

Combinazione QP: σca[kg/cmq]=168 σfa[kg/cmq]=3600

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cmq	kg/cmq			
0.00	-23016	697	308	-20	-104	8	Si	8.4
400.00	-21516	-846	-417	-21	-71	8	Si	7.9

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{r,max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	-23028	728	300	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100
0.00	-23016	697	308	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
400.00	-21516	-846	-417	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
400.00	-21528	-874	-411	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100

Pilastro: 2015 [2015,4015] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm L2=545.00 cm L3=545.00 cm
Criterio: CLS_Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
545.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

Verifica snellezza: fcd=212 [kg/cmq] - **Verificato**

Cb	N	fcd*Ac	v	λmax	λlim
	kg	kg			
6	18983	317475	0.060	62.931	102.238

Combinazione Rara: σca[kg/cmq]=224 σfa[kg/cmq]=3600

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cmq	kg/cmq			
0.00	-18983	1405	-1600	-44	225	6	Si	5.1
545.00	-16939	-1363	2055	-54	461	6	Si	4.2

Combinazione QP: σca[kg/cmq]=168 σfa[kg/cmq]=3600

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cmq	kg/cmq			
0.00	-18249	1319	-1562	-42	220	8	Si	4.0
545.00	-16205	-1276	2027	-52	463	8	Si	3.2

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{r,max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	-18246	1360	-1573	1.67E-02	5.72	11.43	25.80	159	0.012	0.012	7 (Fr)	Si	26
0.00	-18249	1319	-1562	1.64E-02	5.70	11.40	25.67	152	0.011	0.011	8 (Qp)	Si	18

X	N	My	Mz	Act	Aft	pAft	S _{F,max}	σ _{fmed}	Wd	Wk	Cb	Ver.	Cs
545.00	-16205	-1276	2027	2.39E-02	9.42	18.85	24.44	306	0.021	0.021	8 (Qp)	Si	9.4
545.00	-16202	-1309	2036	2.40E-02	9.42	18.85	24.48	311	0.022	0.022	7 (Fr)	Si	14

Pilastro: 2016 [2016,4016] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm L2=545.00 cm L3=545.00 cm
Criterio: CLS_Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14
545.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 3.14

Verifica snellezza: fcd=212 [kg/cm²] - **Verificato**

Cb	N	fcd*Ac	v	λ _{max}	λ _{lim}
	kg	kg			
6	14251	317475	0.045	62.931	117.997

Combinazione Rara: σ_{ca}[kg/cm²]=224 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-14251	1646	314	-24	58	6	Si	9.5
545.00	-12207	-1333	598	-25	101	6	Si	9.1

Combinazione QP: σ_{ca}[kg/cm²]=168 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-13917	1655	273	-23	58	8	Si	7.3
545.00	-11873	-1415	624	-26	128	8	Si	6.5

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{F,max}	σ _{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cm ²	mm	mm			
0.00	-13906	1680	281	1.01E-02	3.86	7.71	24.77	63	0.004	0.004	7 (Fr)	Si	67
0.00	-13917	1655	273	9.67E-03	3.81	7.62	24.44	58	0.004	0.004	8 (Qp)	Si	49
545.00	-11873	-1415	624	1.36E-02	4.67	9.34	25.76	128	0.009	0.009	8 (Qp)	Si	21
545.00	-11862	-1433	619	1.37E-02	4.67	9.34	25.88	130	0.010	0.010	7 (Fr)	Si	31

Pilastro: 2017 [2017,4017] Sez. R: By=50.00 cm Bz=30.00 cm L=545.00 cm Ln=545.00 cm L2=545.00 cm L3=545.00 cm
Criterio: CLS_Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 3.14	Afz = 3.14
545.00	AfSpigolo = 3.14	Afy = 3.14	Afz = 3.14

Verifica snellezza: fcd=212 [kg/cm²] - **Verificato**

Cb	N	fcd*Ac	v	λ _{max}	λ _{lim}
	kg	kg			
6	22919	317475	0.072	62.931	93.045

Combinazione Rara: σ_{ca}[kg/cm²]=224 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-22919	758	247	-22	-91	6	Si	10
545.00	-20876	-796	-787	-25	-33	6	Si	9.0

Combinazione QP: σ_{ca}[kg/cm²]=168 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-22284	788	287	-22	-80	8	Si	7.5
545.00	-20240	-884	-810	-26	-15	8	Si	6.5

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{r,max}	σ _{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	-22281	801	269	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100
0.00	-22284	788	287	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
545.00	-20240	-884	-810	0.00E00	0.00	0.00	0.00	0	0.000	0.000	8 (Qp)	Si	>100
545.00	-20237	-897	-798	0.00E00	0.00	0.00	0.00	0	0.000	0.000	7 (Fr)	Si	>100

Pilastro: 2018 [2018,4018] Sez. R: By=30.00 cm Bz=50.00 cm L=545.00 cm Ln=545.00 cm L2=545.00 cm L3=545.00 cm
Criterio: CLS_Pilastr

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28
545.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 6.28

Verifica snellezza: fcd=212 [kg/cm²] - **Verificato**

Cb	N	fcd*Ac	v	λ _{max}	λ _{lim}
	kg	kg			
6	12701	317475	0.040	62.931	124.988

Combinazione Rara: σ_{ca}[kg/cm²]=224 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-12701	1685	-729	-30	176	6	Si	7.6
545.00	-10658	-1261	257	-18	53	6	Si	13

Combinazione QP: σ_{ca}[kg/cm²]=168 σ_{fa}[kg/cm²]=3600

X	N	My	Mz	σ _c	σ _f	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	kg/cm ²	kg/cm ²			
0.00	-12419	1697	-686	-29	175	8	Si	5.8
545.00	-10375	-1333	220	-18	64	8	Si	9.4

Verifica aperture fessure: Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{r,max}	σ _{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kg	kg*m	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.00	-12405	1721	-699	1.67E-02	9.82	19.64	21.44	86	0.005	0.005	7 (Fr)	Si	57
0.00	-12419	1697	-686	1.64E-02	9.69	19.38	21.38	81	0.005	0.005	8 (Qp)	Si	40
545.00	-10375	-1333	220	1.25E-02	8.41	16.82	20.65	38	0.002	0.002	8 (Qp)	Si	89
545.00	-10362	-1353	233	1.30E-02	8.56	17.13	20.75	42	0.002	0.002	7 (Fr)	Si	>100

PROGETTO DEL SOLAIO MONOTRAVE A TRAVETTI IN CALCESTRUZZO PRECOMPRESSO H = 25+5 CM, INTERASSE 50 CM

I solai saranno del tipo latero cementizio con travetti in calcestruzzo precompresso della larghezza di 12 cm. L'altezza sarà pari a 30 cm di cui 5 cm di soletta collaborante. L'interasse dei travetti sarà pari a 50 cm.

Luce netta massima 7,25 m con luce di calcolo 7.80 m

ANALISI DEI CARICHI SOLAIO:

Peso proprio = 420 daN/m²
Sovraccarichi permanenti = 200 daN/m²
Sovraccarico di esercizio = 50 daN/m²
Carico neve = 60 daN/m²

Si utilizzeranno i valori relativi allo stato limite di esercizio per le verifiche relative ai travetti ed alle armature aggiuntive per i momenti negativi, mentre si farà ricorso agli stati limite ultimi per le verifiche relative alle fasce piene e semipiene e per il calcolo dell'armatura inferiore sugli appoggi.

SLE: COMBINAZIONE RARA

Il carico totale massimo in combinazione rara è pari a (420 x 1+200 x 1+50 x 1 + 60 x 1) daN/m² =730 daN/m².

I vincoli vengono considerati come semi appoggi, per cui il momento flettente positivo di servizio sollecitante una fascia di solaio larga 1,00 m è il seguente:

$$M_{dmax+} = q \times l^2 / 12 = 730 \times 7,8^2 / 12 = 3700 \text{ daNm}$$

Si utilizzerà un solaio con travetti in c.a.p. tipo T5 della ITA avente momento di servizio positivo minimo in combinazione rara maggiore di 3700 daNm/m.

$$\text{Il momento negativo è pari a } M_{dmax-} = q \times l^2 / 12 = 730 \times 7,8^2 / 12 = 3700 \text{ daNm}$$

$$M_{dmax-} / \text{travetto} = 3700 \text{ daNm} / 2 = 1850 \text{ daNm}$$

$$\text{Armatura a momento negativo: } A_a = M_{dmax-} / (0,88 \times s_f \times h) = 1850 / (0,88 \times 26 \times 24) = 3,36 \text{ cm}^2$$

$$\text{Si utilizzano } 2\Phi 16 \text{ a travetto} = 4,02 \text{ cm}^2$$

SLU

Il carico totale è:

$$(420 \times 1,30 + 200 \times 1,50 + 50 \times 0 + 60 \times 1,50) \text{ daN/m}^2 = 936 \text{ daN/m}^2$$

Verifica a flessione

I vincoli vengono considerati come semi appoggi, per cui il momento flettente positivo di servizio sollecitante una fascia di solaio larga 1,00 m è il seguente:

$$M_{dmax+} = q \times l^2 / 12 = 936 \times 7,8^2 / 12 = 4745 \text{ daNm}$$

Si utilizzerà un solaio con travetti in c.a.p. tipo T5 della ITA avente momento allo SLU positivo minimo pari a 4814 daNm.

$$\text{Il momento negativo è pari a } M_{dmax-} = q \times l^2 / 12 = 936 \times 7,8^2 / 12 = 4745 \text{ daNm}$$

$$M_{dmax-} / \text{travetto} = 4745 \text{ daNm} / 2 = 2380 \text{ daNm}$$

$$\text{Armatura a momento negativo: } A_a = M_{dmax-} / (0,88 \times s_f \times h) = 2380 / (0,88 \times 26 \times 39) = 2,66 \text{ cm}^2$$

$$\text{Si utilizzano } 2\Phi 16 \text{ a travetto} = 4,01 \text{ cm}^2$$

Verifica a taglio

Il taglio massimo sollecitante una fascia di solaio della larghezza di 1 m è pari a

$$T_{max} = 936 \text{ daN/m} \times 7,8 \text{ m} / 2 = 3650 \text{ daN}$$

Per cui:

$$T_{max} \text{ travetto} = 3650 / 2 = 1830 \text{ daN}$$

Determinazione armatura inferiore appoggi

$$T_{max} \text{ travetto} / f_{yd} = 18300 \text{ N} / 391,3 \text{ N/mm}^2 = 46 \text{ mm}^2 = 0,46 \text{ cm}^2$$

$$\text{Si adottano } 2 \Phi 10 \text{ a travetto per complessivi } 1,57 \text{ cm}^2$$

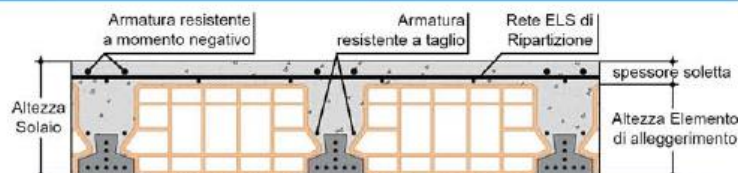
L'armatura della soletta collaborante sarà costituita da una rete elettrosaldata $\Phi 8$ passo 20x20 cm corrispondente ad un'area di armatura pari a 2,00 cm² in entrambe le direzioni (tale area risulta > del 20% dell'area dell'armatura longitudinale)

Si considera comunque, a vantaggio di sicurezza, la realizzazione di una fascia piena in corrispondenza degli appoggi avente larghezza pari a 25 cm.

SOLAIO MONOTRAVE

interasse nervature: 50 cm
interasse di calcolo: 100 cm
numero di travetti per interasse di calcolo: 2

MOMENTI RESISTENTI (RIFERITI AD UNA STRISCIA DI SOLAIO LARGA UN METRO)



	ALTEZZA PIGNATTE	SPESSORE SOLETTA	ALTEZZA SOLAIO	$M_{Rd,SLU}/(M_{SLE,CR})$ [kNm]								PESO TRAVETTI E BLOCCHI	PESO SOLAIO IN OPERA	c.l.s.	CARATTERISTICHE SEZIONE PARZIALIZZATA (con travetto reagente a trazione)				
				T1	T3	T4	T5	T6	T7	T8	Y _{GR} cm				Y _{GR} cm	I ₀ cm ⁴	W _x cm ³	W _y cm ³	
																			cm
H ₁₂₊₄	12,00	4,00	16	9,20 (8,01)	13,61 (11,83)	18,33 (15,94)	22,32 (18,03)	26,13 (19,18)	29,79 (20,72)	33,35 (22,19)	90	230	54	5,64	10,36	8'892	1'576	572	
H ₁₂₊₅	12,00	5,00	17	9,98 (8,68)	14,81 (12,88)	19,99 (17,39)	24,46 (19,85)	28,78 (21,12)	32,96 (22,82)	37,08 (24,44)	90	230	64	5,82	11,18	10'571	1'817	630	
H ₁₆₊₄	16,00	4,00	20	12,12 (10,54)	17,98 (15,63)	24,16 (21,01)	29,60 (25,74)	34,88 (27,54)	39,99 (29,76)	45,01 (31,89)	96	260	63	6,93	13,07	16'167	2'333	825	
H ₁₆₊₅	16,00	5,00	21	12,90 (11,22)	19,19 (16,68)	25,82 (22,46)	31,74 (27,6)	37,52 (29,54)	43,16 (31,93)	48,74 (34,21)	96	280	74	6,97	14,03	18'643	2'674	886	
H ₂₀₊₄	20,00	4,00	24	15,03 (13,07)	22,35 (19,44)	29,99 (26,08)	36,89 (32,08)	43,62 (36,26)	50,19 (39,2)	56,67 (42,02)	113	300	73	8,16	15,84	25'865	3'168	1'089	
H ₂₀₊₅	20,00	5,00	25	15,81 (13,75)	23,56 (20,49)	31,85 (27,53)	39,03 (33,94)	46,27 (38,31)	53,37 (41,42)	60,40 (44,41)	113	320	83	8,08	16,92	29'250	3'618	1'153	
H ₂₅₊₄	25,00	4,00	29	18,68 (16,24)	27,81 (24,19)	37,28 (32,42)	46,00 (40)	54,55 (47,43)	62,94 (51,28)	71,25 (54,98)	126	345	85	9,64	19,36	41'463	4'303	1'427	
H ₂₅₊₅	25,00	5,00	30	19,46 (16,92)	29,02 (25,24)	38,94 (33,86)	48,14 (41,86)	57,20 (49,54)	66,12 (53,57)	74,97 (57,43)	126	365	95	9,42	20,58	46'127	4'895	1'495	
H ₃₀₊₄	30,00	4,00	34	22,32 (19,41)	33,28 (28,94)	44,57 (38,75)	55,11 (47,92)	65,48 (56,94)	75,70 (63,53)	85,82 (68,11)	143	390	97	11,04	22,96	61'000	5'525	1'771	
H ₃₀₊₅	30,00	5,00	35	23,10 (20,09)	34,49 (29,99)	46,23 (39,19)	57,25 (49,19)	68,13 (59,24)	78,87 (65,88)	89,55 (70,65)	143	410	107	10,71	24,29	67'082	6'261	1'841	
H ₃₅₊₄	35,00	4,00	39	25,97 (22,58)	38,74 (33,69)	51,85 (42,99)	64,22 (53,96)	76,41 (65,09)	88,45 (75,87)	100,39 (81,36)	154	430	110	12,39	26,61	84'545	6'824	2'118	
H ₃₅₊₅	35,00	5,00	40	26,75 (23,26)	39,95 (34,74)	53,51 (43,43)	66,35 (54,51)	79,06 (65,75)	91,62 (78,31)	104,12 (83,97)	154	450	120	11,96	28,04	92'168	7'708	2'191	
H ₄₀₊₄	40,00	4,00	44	29,61 (25,75)	44,21 (38,44)	59,14 (47,33)	73,32 (59,39)	87,34 (71,63)	101,20 (85,71)	114,97 (94,66)	168	480	121	13,69	30,31	112'162	8'195	2'467	
H ₄₀₊₅	40,00	5,00	45	30,39 (26,43)	45,42 (39,49)	60,80 (47,86)	75,46 (60,07)	89,99 (72,44)	104,37 (86,68)	118,69 (97,35)	168	500	131	13,16	31,84	121'435	9'227	2'543	